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ASX Announcement

June 2021 Quarterly Report

29 July 2021

Highlights

Paterson Project

Final diamond drill hole locations for the Apollo, Atlas, Juno and Voyager targets were determined, and sufficient funds allocated to budget in the quarter to drill these targets and more upon receipt of final heritage clearances from the Traditional Owners.

As detailed and extensive planning in advance of the Q3/Q4 2021 Paterson drill campaign is now largely complete with the Paterson Central exploration team currently in the pre-mobilisation phase with respect to rig booking and logistical planning in advance of receiving final heritage clearances. Once complete, the Company will then move to immediately commence drilling and intends to drill continuously for the remainder of the calendar year.

The Company intends to provide a more detailed update on the proposed final drill program hole locations and site mobilisation start dates in the near future.

Carlow Castle Au-Cu-Co Project

The commencement of the newly planned campaign of drilling for circa 11,000 metres, signals a new phase of exploration and evaluation at the Carlow Castle Project. This drilling is also designed to test the long-awaited Good Luck and Little Fortune Projects, located approximately one kilometre to the south of Carlow Castle.

As at 30 of June, a total of 16 holes have been drilled for a total of 3,506 metres of which 2,020 metres was RC and 1,486 metres was diamond.

Results for RC holes ARC310 to 313 and ARC315 have been received which focussed on the Carlow Castle Western Zone. These holes returned significant results of:

- **6m @ 14.97g/t Au, 7.09% Cu, 0.06% Co from 53 metres Hole ARC310**
  - **Including; 3m @ 13.92g/t Au, 5.11% Cu 0.03% Co from 54 metres**
- **6m @ 2.61g/t Au, 0.54% Cu, 0.14% Co from 186 metres Hole ARC311**
  - **Including; 1m @ 6.27g/t Au, 1.07% Cu, 0.05% Co from 187 metres**
- **4m @ 2.09g/t Au, 0.50% Cu, 0.06% Co from 121 metres Hole ARC313**
  - **Including; 1m @ 5.76g/t Au, 1.74% Cu, 0.07% Co from 124 metres**
- **1m @ 9.29g/t Au, 0.67% Cu, 0.17% Co from 114 metres Hole ARC312**

Diamond drilling results are pending review and RC drilling at Carlow Castle is currently in progress, testing the new interpretation designed to add significant ounces to the project.

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Carlow Castle Mineral Resource Estimate

The Mineral Resource report was completed by CSA and submitted in May. The updated Mineral Resource is 14.3 million tonnes at 0.7 g/t Au, 0.4% Cu, and 0.05% Co for 320,000 ounces gold, 53,000 tonnes contained copper, and 7,000 tonnes contained cobalt. The difference in resource numbers occurred due to additional drilling, redefinition and increase in the confidence of the model.

The Company is currently reviewing the recent Mineral Resource estimate with a view to approaching the Carlow Castle Project via a new strategy, aiming to increase tonnages and grade by targeting the higher-grade mineralised features, thus allowing for more effective geological control to drive project development. The current Q3 2021 RC drill program has been designed to achieve this objective and combined with the Mineral Resource review should, with success, allow the Company to clearly demonstrate the potential of the project to host a robust and significant gold, copper and cobalt resource.

Munni Munni Project

Drilling at Munni Munni comprised of 15 RC drill holes for 2,740 metres, completed between April and May, with drill holes spread through the entire upper portion of the mineralisation, to a maximum depth of 250 metres.

Significant intersections include:

- **7m @ 2.20g/t 2PGE + Au (1.46g/t Pd, 0.67 g/t Pt, 0.07g/t Au) from 124 metres, 21MMRC005;**
- **7m @ 2.35g/t 2PGE + Au (1.33g/t Pd, 0.84 g/t Pt, 0.18g/t Au), from 96 metres , 21MMRC006;**
- **4m @ 2.45g/t 2PGE + Au (1.31g/t Pd, 0.85g/t Pt, 0.29g/t Au) from 60 metres , 21MMRC007;**
- **5m @ 2.35g/t 2PGE + Au (1.36g/t Pd, 0.68g/t Pt, 0.31g/t Au) from 75 metres , 21MMRC008;**
- **4m @ 2.87g/t 2PGE + Au (1.76g/t Pd, 0.89g/t Pt, 0.22g/t Au) from 115 metres, 2MMRC010.**

Artemis is pleased to have now executed a full Joint Venture Agreement and associated documents that will proceed to a Joint Venture Agreement for 100% of the Munni Munni Project with Platina Resources Limited in the ratio of beneficial interests, 70% ARV and 30% PGM.

Artemis and Platina continue to explore ways to monetise Munni Munni for the benefit of shareholders.

Radio Hill FLEM Survey

A Fixed-Loop Electromagnetic (FLEM) survey was completed in May which detected deep and untested conductor anomaly zones of interest identified from historic deep drilling and follow-up DHEM survey data. From this survey, the Radio Hill Project is still considered prospective for additional Ni-Cu-Co-PGE discoveries. Recommendations for further work at Radio Hill are pending.

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Whundo GAIP Survey

A Gradient-Array Induced Polarisation (GAIP) survey was conducted at the Whundo VMS project to identify VMS-style mineralisation along target trends located to the northeast of the main Whundo deposit. Additional work has been recommended post-survey that has identified anomalous trends that will require another GAIP survey and drilling.

SUMMARY OF DRILLING AT CARLOW CASTLE

Artemis Resources (ASX: ARV) is pleased to release this June Quarterly, highlighting the achievements gained during the reporting period.

The June Quarterly results include the final assays from the initial holes drilled at the beginning of the circa 11,000m program, which is the follow up program from the 2020 Q4 drilling campaign. This program will continue into Q3.

Drill statistics and completed holes are shown in Table 1 and Figure 1, respectively.

Table 1: Drill statistics for June Quarterly

Location	No of Holes	RC (m)	Diamond (m)	No of Samples	No Samples Submitted	No Samples Received	No of Samples Outstanding
East Zone	6		1290.7	1276	1097	782	494
West Zone	9	2020		2046	2046	2046	0
Cross-Cut	1		195.3	201	0	0	201

Several assays from the beginning of the planned drilling program have returned significant results and these have been used to define and update the remaining holes in the program. These are shown in Table 2.

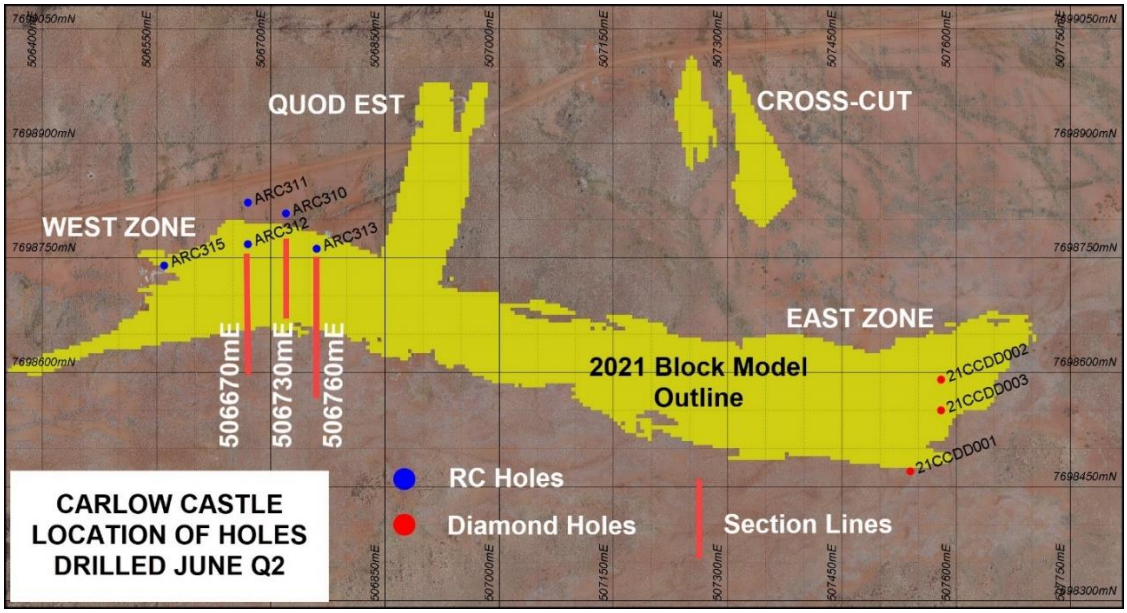


Figure 1: Location of drill collars drilled during the June Q2 period. Section lines are shown in red with corresponding section co-ordinates.

The rationale behind the new drilling program was to test the interpreted shallow plunging high-grade gold and copper shoots in and below the Carlow Castle Western Zone, the steeply dipping high-grade shoots on the eastern zone, the steep down-plunging gold shoots at Quod Est and the new interpretation of Cross-Cut.

Table 2: Carlow Castle drilling assay results averaged over significant drill intercept intervals bases on 1m assay samples, intersections defined by either >0.5g/t Au or >0.5%Cu, max 2m internal dilution. NSI = no significant intercept with values above lower cut off.

Hole No	Comment	From	To	Downhole Width (m)	True Width (m)	Au (g/t)	Cu (%)	Co (%)
ARC310		53	59	6	5.4	**14.97**	**7.09**	0.06
	Including	***54***	***57***	***3***	***2.7***	***13.92***	***5.11***	***0.03***
		112	113	1	0.9	1.42	0.05	0.03
		168	170	2	1.8	1.61	0.16	**0.13**
		225	226	1	0.9	1.37	0.06	0.01
ARC311		136	142	6	5.4	1.35	0.34	0.07
		154	155	1	0.9	**2.49**	0.49	0.02
		186	192	6	5.4	**2.61**	0.54	**0.14**
	Including	***187***	***188***	***1***	***0.9***	***6.27***	***1.07***	***0.05***
ARC312		9	10	1	0.9	1.61	**2.33**	0.05
		28	34	6	5.4	2.68	**1.10**	0.02
	Including	***31***	***34***	***3***	***2.7***	***4.34***	***1.75***	***0.01***
		56	61	5	4.5	1.66	0.26	0.04
		83	85	2	1.8	1.15	0.19	0.03
		114	115	1	0.9	**9.29**	0.67	**0.17**
		144	145	1	0.9	**2.63**	0.23	0.01
ARC313		35	36	1	0.9	1.11	0.05	0.01
		44	45	1	0.9	1.21	0.28	0.03
		82	83	1	0.9	1.06	**3.93**	0.01
		105	106	1	0.9	1.30	0.08	**0.18**
		110	112	2	1.8	**2.07**	0.44	**0.31**
		121	125	4	3.6	**2.09**	0.50	0.06
	Including	***124***	***125***	***1***	***0.9***	***5.76***	***1.74***	***0.07***
		147	148	1	0.9	1.35	0.14	0.10
		199	200	1	0.9	**5.17**	**0.38**	0.01
ARC315	NSI							

A reinterpretation of the structural setting and mineralising events have returned high-grade gold, copper and cobalt assays on the main shoots (Figure 2) and is defining the extent of the rich, lower grade gold-copper-cobalt "halo envelop" surrounding the internal high-grade zones.

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The Mineral Resource Estimate (MRE) completed by CSA Global and released in May, is being reviewed, considering the updated interpretation of the Carlow Castle system. This information, along with the updated interpretation will be incorporated into the new model and drive future drilling campaigns.

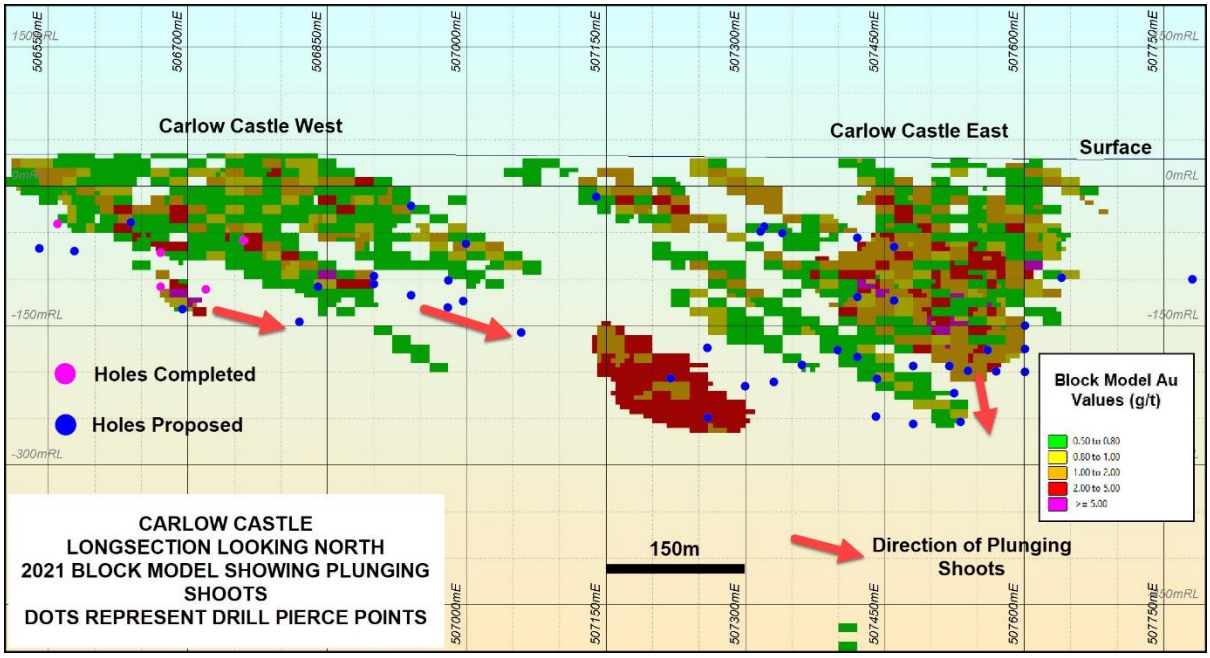


Figure 2: Longsection of Carlow Castle looking north showing the high-grade trends (hot colours) in the 2021 block model. The dots denote the target pierce points of the drill holes.

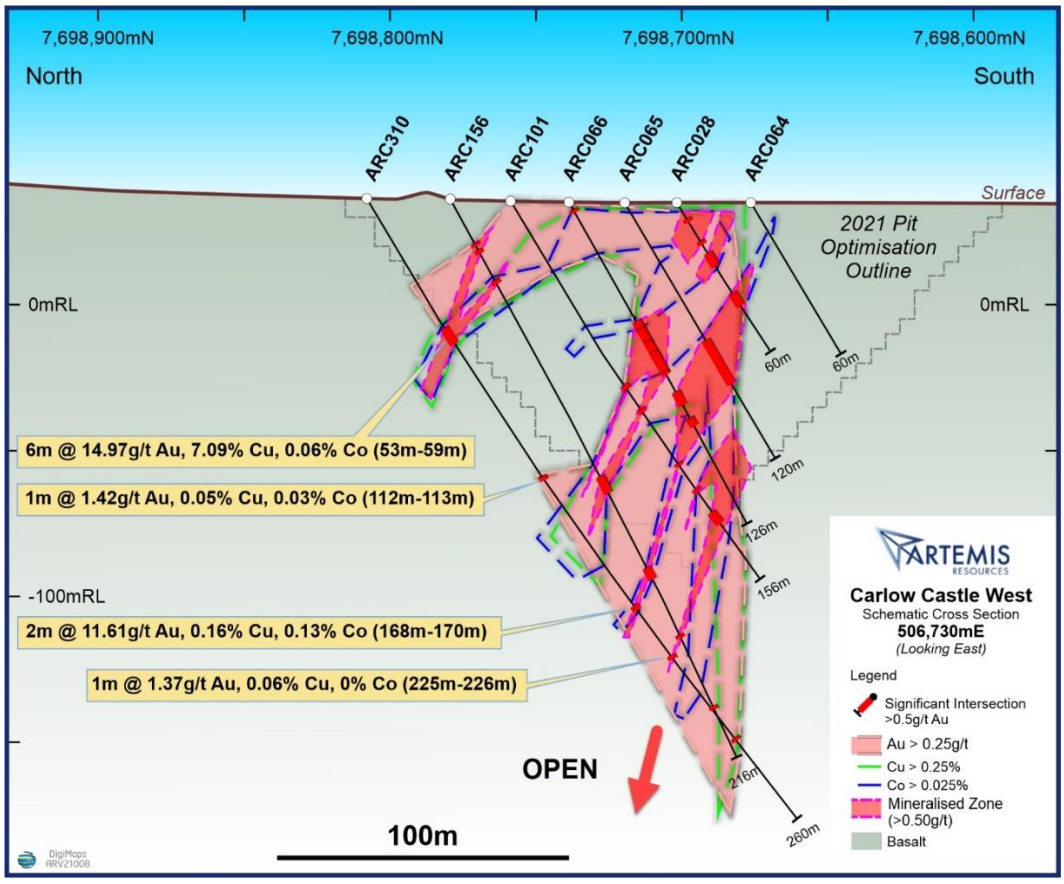


Figure 3: Section 506730mE, intersections for Hole ARC310. (Refer to Figure 1 for location)

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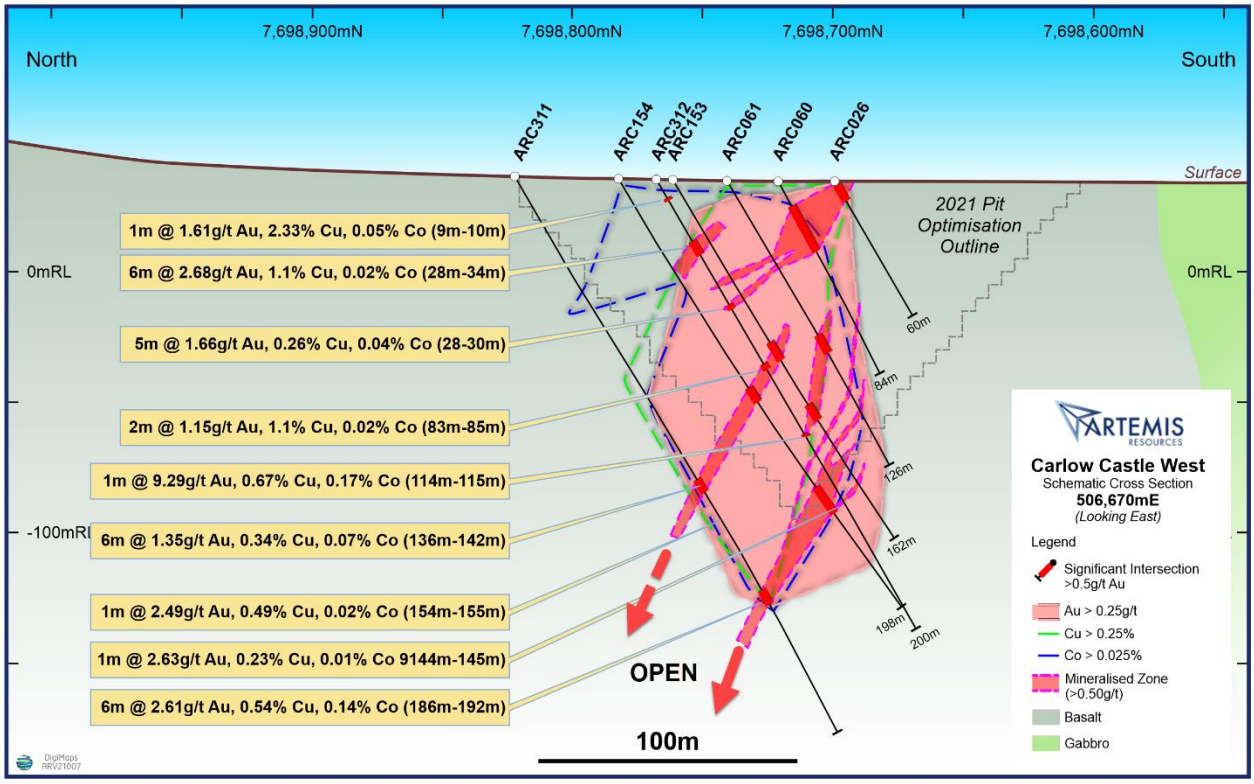


Figure 4: Section 506670mE showing intersections for holes ARC311 and ARC312 (refer to Figure 1 for location)

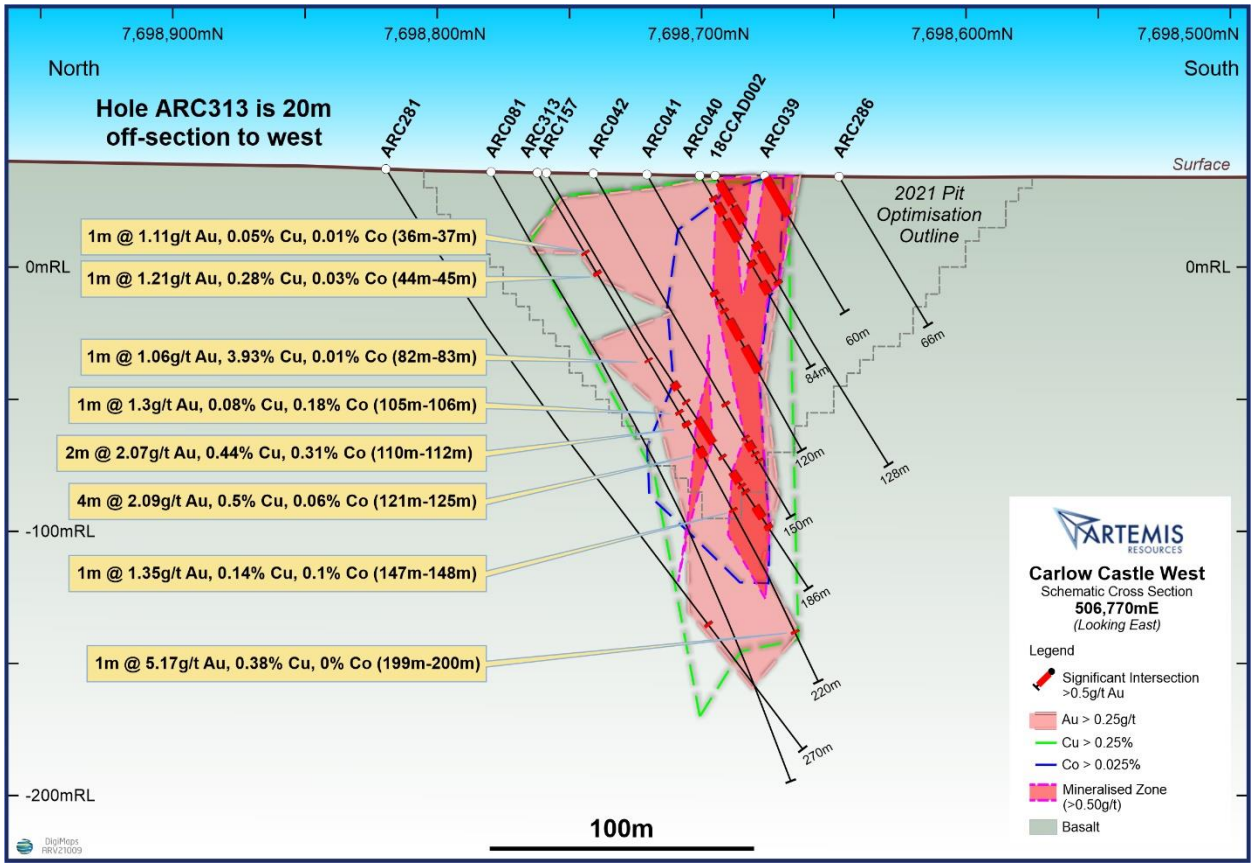


Figure 5: Section 506770mE showing intersections for hole ARC313 (Refer to Figure 1 for location)

Along with the potential in the Carlow Castle main zone, the Quod Est System located to the immediate north, is another area developing into a significant gold and copper resource, (refer to Figure 1 for location).

Quod Est mineralisation trends north to northeast, with a steeply dipping mineralisation plunge to the southeast, controlled by a gabbro/basalt contact. Significant results for Quod Est are included in the 23 April 2021 ASX release. Drilling at Quod Est is in progress.

Discovery of the Cross-Cut Zone by testing geophysical targets had intersected several high grade zones associated with north-westerly striking structures, (refer to Figure 1).

A new interpretation has been put forward, using airborne magnetic data and the SAM survey which suggests that Cross-Cut may be a series of *en-echelon* mineralised structures, as shown in Figure 6. Previous drilling had intersected significant copper and gold numbers, which are noted in the 23 April 2021 ASX release. Drilling at Cross-Cut is in progress.

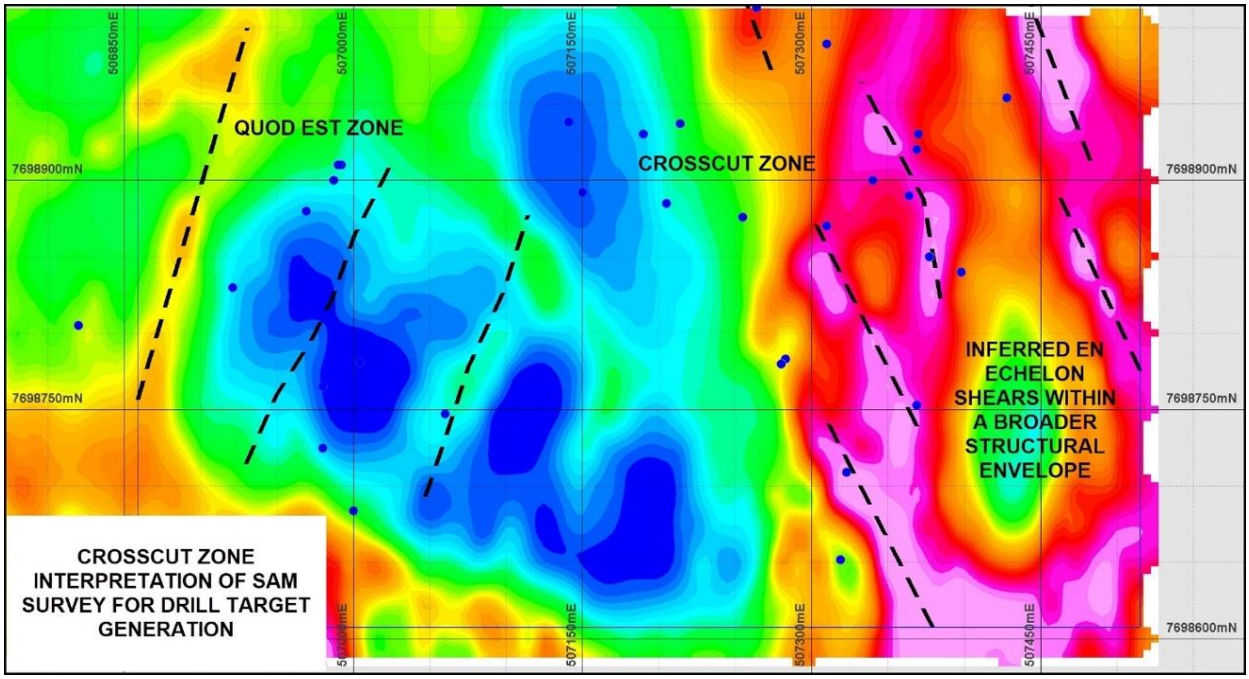


*Figure 6: Updated interpretation (plan view) of the Crosscut Zone showing the potential for repeated mineralised structures of an **en echelon** nature. Holes have been repositioned in the current drill program to test these features. Background image of SAM survey.*

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CARLOW CASTLE MINERAL RESOURCE ESTIMATE

During the quarter, the Mineral Resource for the Carlow Castle Project was updated by CSA Global using all data available as of 19 May 2021; this includes an additional 129 drill holes for 22,395 m since the 2019 Mineral Resource update. The additional drillholes were mainly at the eastern end of the Carlow Main zone and in the newly discovered Cross-Cut zone.

An open pit optimisation was completed to constrain the reported Mineral Resource. The updated Carlow Castle Mineral Resource is 14.3 million tonnes at 0.7 g/t Au, 0.4% Cu, and 0.05% Co for 320,000 ounces gold, 53,000 tonnes contained copper, and 7,000 tonnes contained cobalt.

Table 3 shows the updated resource numbers compared to the 2019 resources numbers.

Table 3. Comparison between 2021 and 2019 Mineral Resource estimates

Type	2021 Inferred				2019 Inferred			
	Tonnes (kt)	Au (g/t)	Cu (%)	Co (%)	Tonnes (kt)	Au (g/t)	Cu (%)	Co (%)
Oxide	4,400	0.4	0.3	0.04	5,100	2.1	0.6	0.1
Transitional	3,100	0.7	0.5	0.06	-	-	-	-
Fresh	6,900	0.9	0.4	0.06	2,800	0.7	0.6	0.05
Total	14,300	0.7	0.4	0.05	8,000	1.6	0.6	0.08

The 2021 Mineral Resource is materially different to the previously reported 2019 Mineral Resource, with a significant decrease in Au, Cu, and Co grades, and an increase in resource tonnes. The contained gold decreased by 98,000 ounces, contained copper increased 5,000 tonnes, and contained cobalt was approximately the same (Figures 7 and 8).

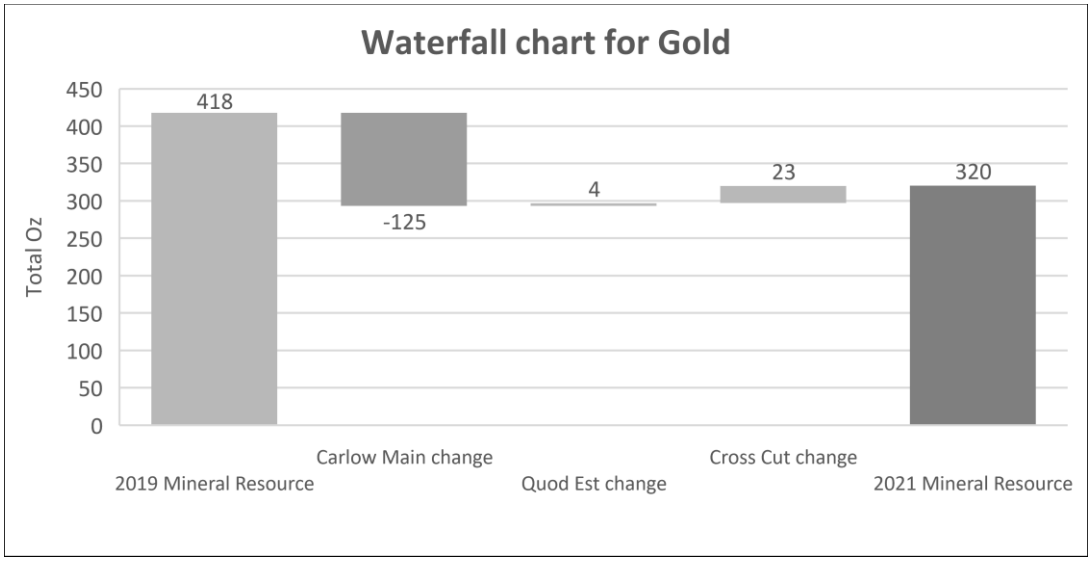


Figure 7. Waterfall chart of changes in the MRE for contained gold between 2019 and 2021 estimates

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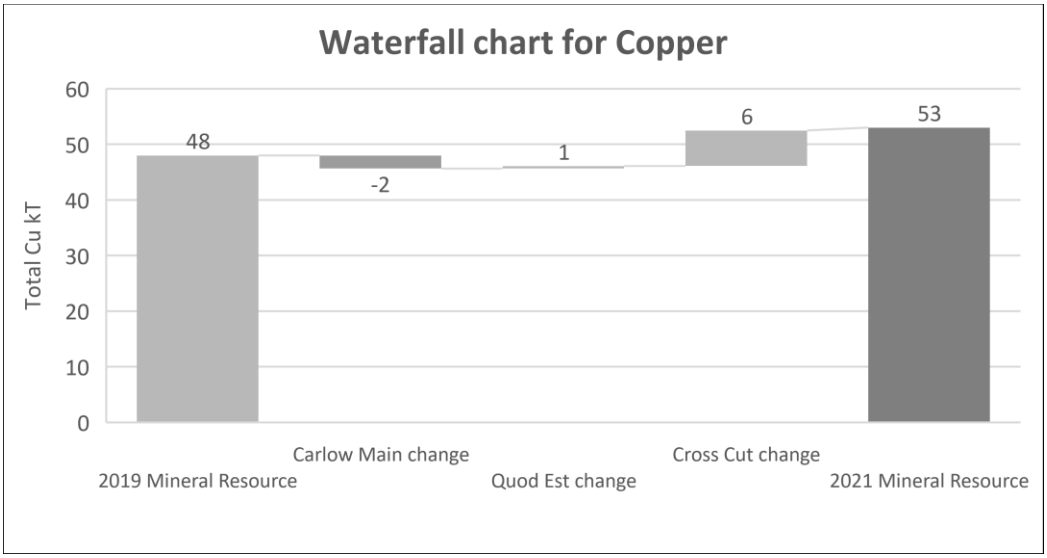


Figure 8. Waterfall chart of changes in the MRE for contained copper between 2019 and 2021 estimates.

Comparison between the 2019 and 2021 Mineral Resource

The 2021 Mineral Resource for Carlow Castle incorporated a significant amount of additional surface RC and diamond drilling. The decrease in resource grades and contained metal is a direct result of increased drilling below the -100mRL (approximately 140m below surface) as shown in Figure 9.

Below -100 mRL, the estimated mean gold grade decreased from 1.25 g/t Au in the 2019 model to 0.5 g/t Au in the 2021 model. Similarly, copper decreased from 0.3% Cu to 0.25% Cu, and cobalt from 0.05% Co to 0.03% Co. Material differences in the data and estimation methodology between the 2019 and 2020 Mineral Resource models are discussed below.

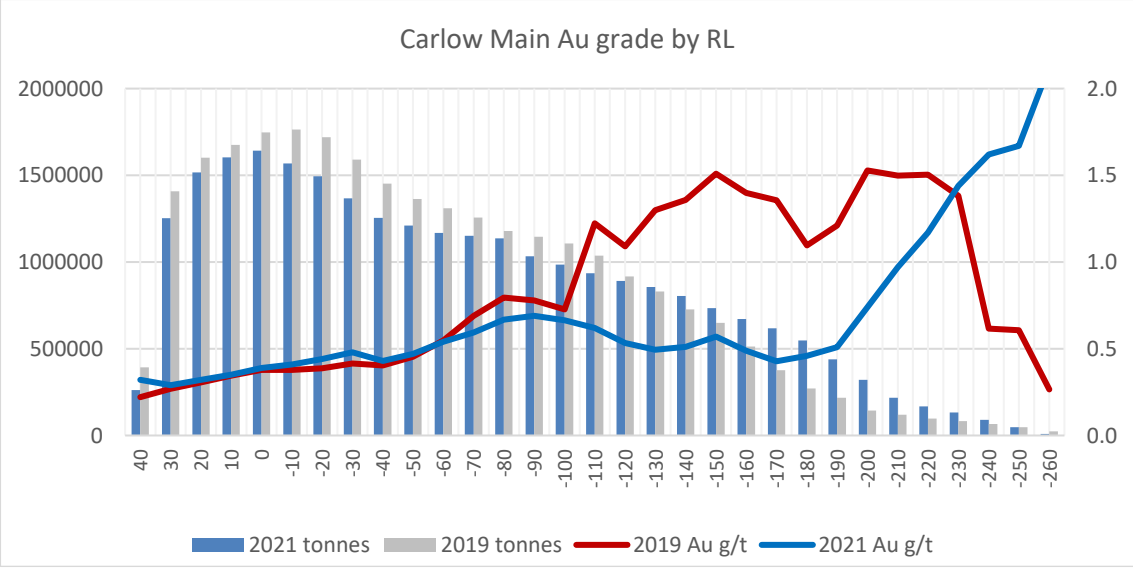


Figure 9. Carlow Main zone 2019 and 2021 model tonnes and Au grades by RL

Differences in the Input Datasets

Several very high-grade drill holes were drilled down dip in 2018: ARC133, ARC138, ARC139, and 18CCAD010. The 2021 Mineral Resource included several additional infill drillholes drilled across the mineralisation adjacent to ARC133, ARC138 and ARC139 and 18CCAD010 that reported lower Au, Cu, and Co grades and improved the confidence in the mineralisation interpretation (Figure 10).

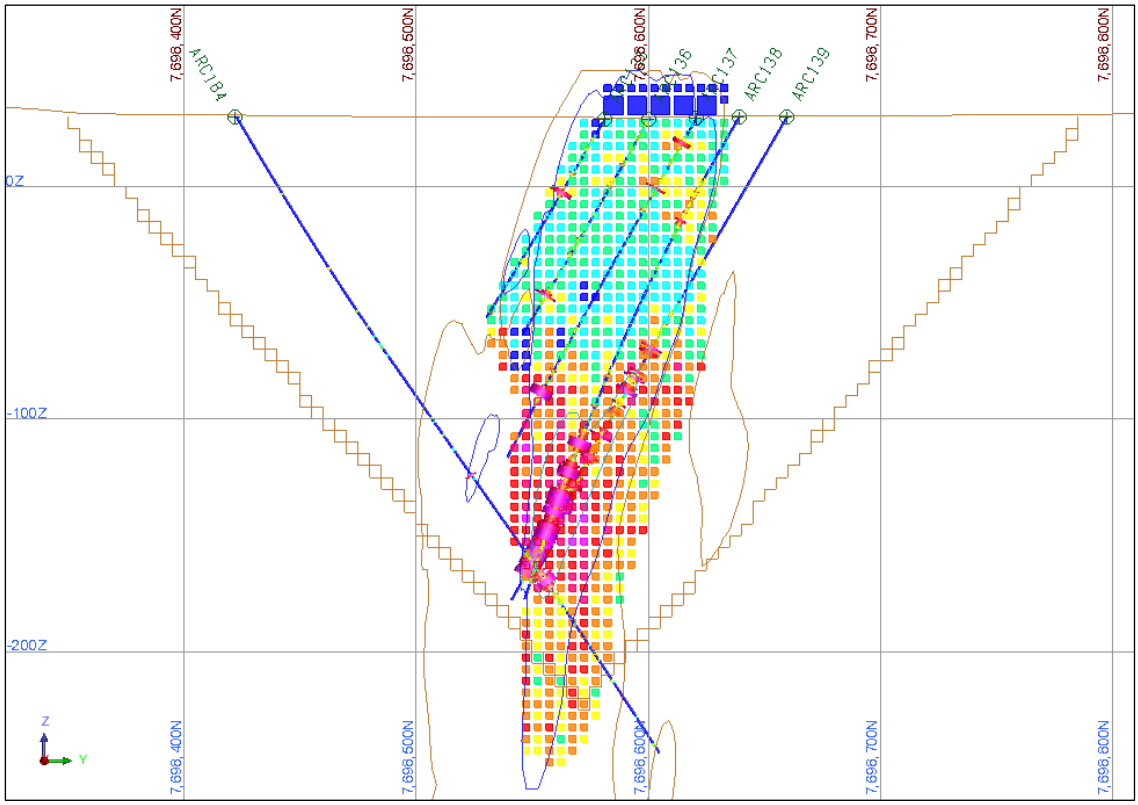


Figure 10. Cross-section 507 520 mE showing ARC138 and ARC139, 2019 block model, and 2019 Whittle shell

A comparison of the composite data for the Carlow Main zone showed the mean composite Au grade decreased from 0.60 g/t in 2019 to 0.55 g/t in 2021, while Cu composite grades increased from 2,935 ppm to 3,720 ppm, and Co composite grades stayed approximately the same. The changes in mean grades for Au and Cu are reflected in the Mineral Resource.

Differences in the Interpretation Approach

The 2019 mineralisation wireframe for Carlow Main used manual sectional interpretation on 40 m spacings at a nominal 500 ppm Cu cut-off. The 2021 model utilised a probabilistic indicator modelling method to model the complex and variable grade and geological continuity effectively. Nested indicator grade shells were generated at 200 ppm Cu, 500 ppm Cu, and 0.5 g/t Au cutoffs.

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The additional 0.5 g/t Au sub-domain was created for the 2021 model to constrain the influence of the high-grade down-dip drillholes. In areas with no infill drilling the 500 ppm Cu wireframes in 2019 and 2021 are generally comparable.

Differences in the Volume Covered

Infill drilling led to a refinement in the mineralisation interpretation and subsequent decrease in volume below -100 mRL. The decrease in volume was largely driven by infill drilling on four sections (507 380 mE; 507 500 mE; 507 540 mE; and 507 620 mE).

The additional drilling removed poorly constrained volume that had been projected down-dip in 2019, especially on the footwall.

Differences in the Estimation Parameters

The two models used different treatments of outlier grades. For the 2019 model, no top cuts were applied; grades above certain thresholds were restricted to a search distance of 10 m, or inside the OK panel in which they were situated. For the 2021 model, a top cut was applied to high grades before estimation.

Differences in the Open Pit Optimisation Parameters

Both the 2019 and 2021 models were constrained by a Whittle open pit optimisation to account for the reasonable prospects for eventual economic extraction (RPEEE) test of the JORC Code. The optimisation parameters for both models were identical except for increased commodity prices in 2021.

Differences in Mineral Resource Classification Approach

The resource classification followed similar approaches in the 2019 and 2021 models. In the 2019 model, the lower extents of the optimized resource shell were constrained by the extent of the mineralisation wireframe. The 2021 Whittle shell was not limited by the wireframe, but by grade and tonnage of mineralisation. Material below the -220 mRL was left unclassified based on limited drill data. The Carlow Main zone remains open at depth.

Differences in the Estimation Method

The change from a localised uniform conditioning (LUC) estimation method in 2019 to a global ordinary kriging (OK) method in 2021 was based on the improved mineralisation domaining and population statistics with infill drilling.

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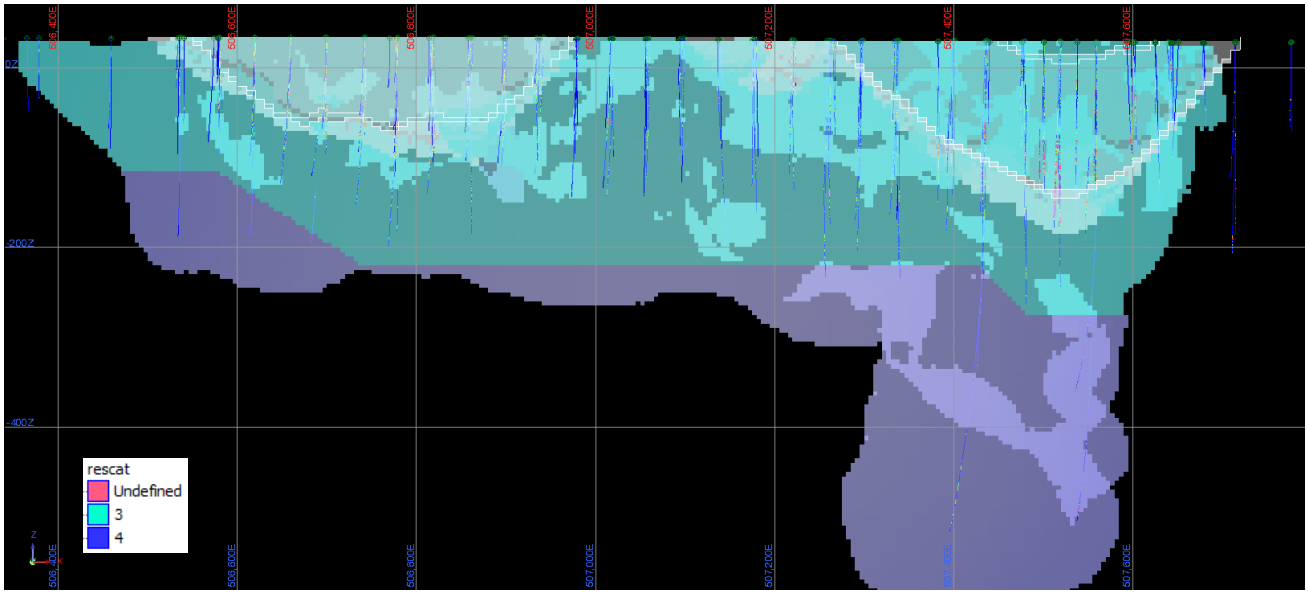


Figure 11. 2019 block model resource classification (Inferred – 3; Unclassified – 4) with 2019 Whittle shell

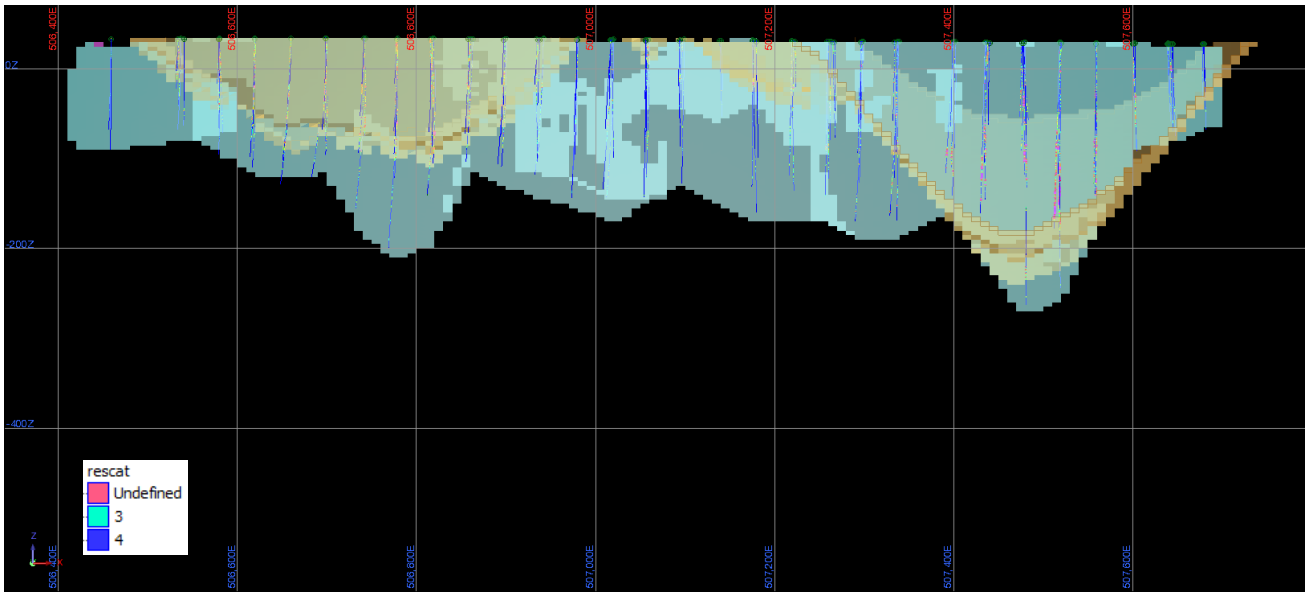


Figure 12. 2021 block model resource classification (Inferred – 3; Unclassified – 4) with 2021 Whittle shell

Summary of Findings from the 2021 and 2019 Resource Comparisons

- Some of the 2020 and 2021 drilling has drilled through parts of the 2019 Carlow Main zone resource model.
- This drilling has reduced the volume of the mineralisation and the contained metal below the -100mRL.
- Additional resource has been added in the newly discovered Cross-cut zone.

- The balance of the 2020-2021 drilling has extended the Carlow Main mineralisation at depth; none of this additional mineralisation is reported in the current Mineral Resource as it is below the optimized resource pit shell.
- Three drillholes that were drilled down-dip had a disproportionate effect on the Au grade below -100 mRL in the 2019 model; this has been rectified by the additional infill drilling and revised domaining.
- The change from LUC to OK has not significantly changed the grade-tonnage selectivity prediction, due to the additional data available for the 2021 model.
- The optimisation parameters for the 2021 model are the same as those used in 2019, except for higher commodity prices.
- The 2019 and 2021 Inferred Mineral Resiurce classification is justified given the changes described above.

Strategy for Carlow Castle

Following the Mineral Resource update for Carlow Castle, a detailed review of the current resource and exploration strategy has been conducted.

It is proposed that a structural review and interpretation be completed, and drill targets identified and tested. The new interpretation will include a re-modeling of Carlow Castle using previous drill data, current drilling data, assay results and mineralisation trends.

- Interpretation of the geology and structural setting;
- Remodel and generate additional drill targets;
- Step out drilling to add additional ounces to a currently increasing resource base;
- Regional review to stitch together data from various disciplines and generate new targets.

MUNNI MUNNI PGE PROJECT H1 DRILL PROGRAM

Reverse Circulation (RC) drilling of 15 drill holes for 2,740 metres has been completed in May, with drill holes spread through the entire upper portion of the mineralisation, to a maximum depth of 250 metres. Samples were processed at ALS Global.

Joint Venture Formation with Platina Resources Limited

Following a period of constructive dialogue, Artemis is pleased to have now executed a full Joint Venture Agreement and associated documents that allow for to formal formation of a Joint Venture over 100% of the Munni Munni Project with Platina Resources Limited in the ratio of beneficial interests, 70% ARV and 30% PGM.

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Drilling and Multi-elements Results

The RC drilling program was designed to confirm the PGE horizon located on the northern nose of the >20km long Munni Munni mafic intrusive Complex, on a 50 x 50 metre drill pattern.

A non-JORC resource estimation was calculated using historic holes which had defined the mineralised horizon. The recent drill program was designed to infill the historic drilling.

Holes 2MMRC0014 & 015 were targeted to test mineralisation along the poorly defined eastern side of the mafic intrusive Complex.

As the PGE horizon is essentially a stratigraphic zone, historical drilling has been widely spaced and very selectively assayed; Artemis has undertaken a broad multi-element analytical suite to improve the subtle lithological variations.

Location of Munni Munni tenements and completed drill hole collars are located in Figure 13.

Sections relating to the completed drilling are located in Figures 14 and 15.

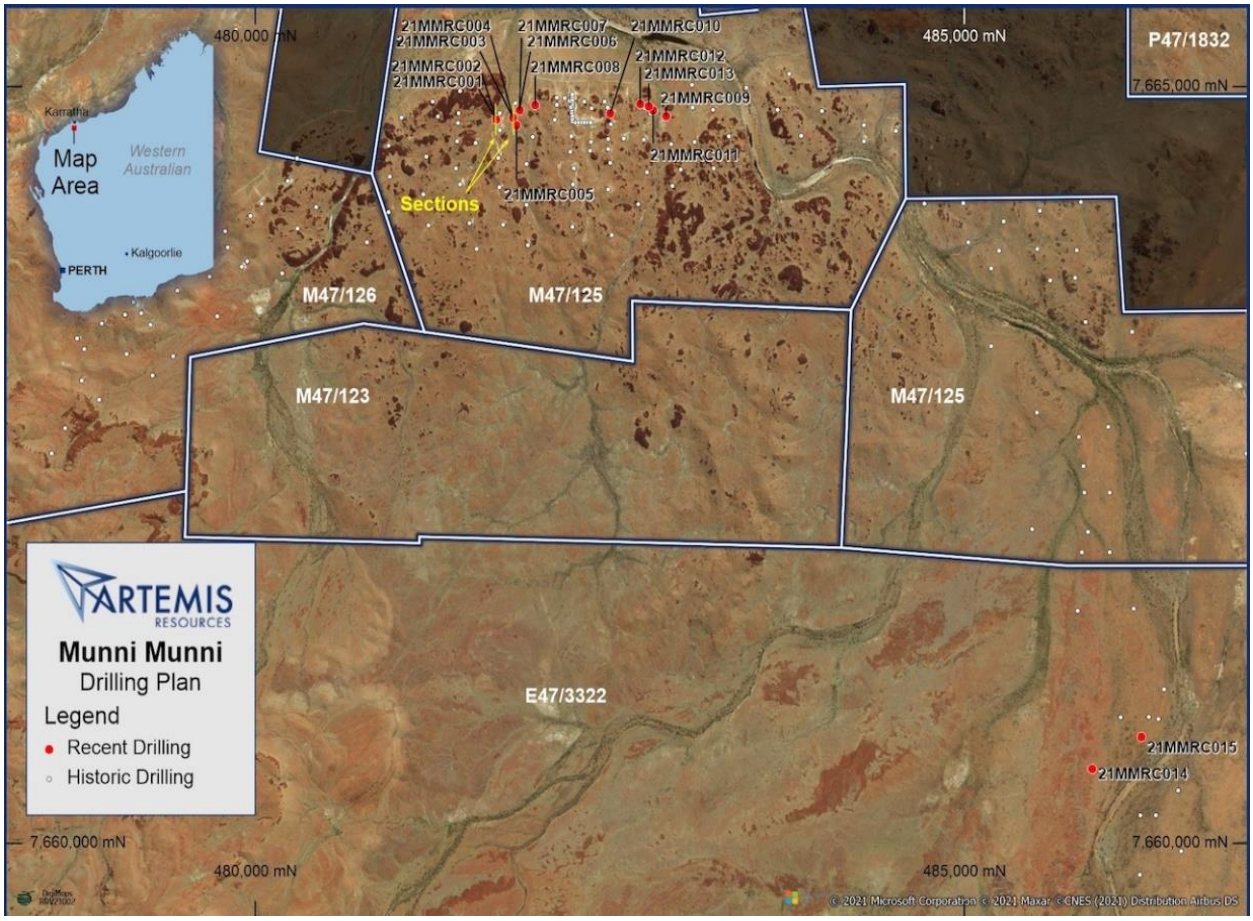


Figure 13: Munni munni location map highlighting recent drilling in red and section locations in yellow.

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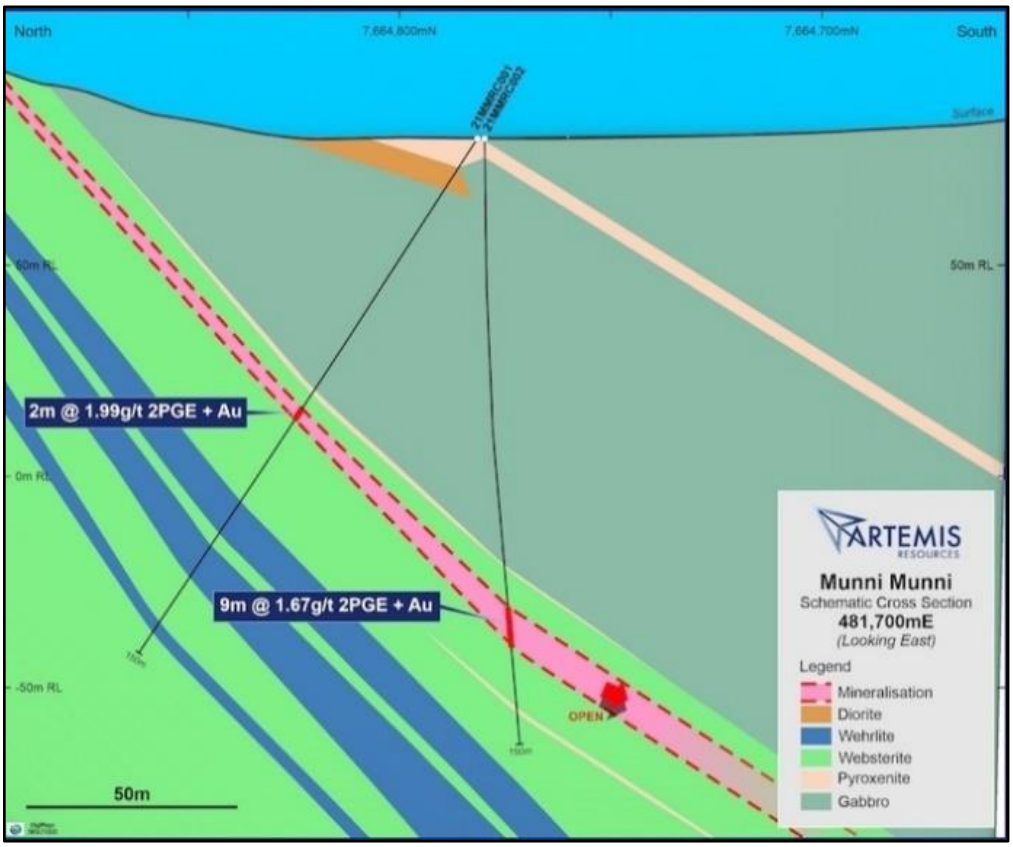


Figure 14: Section 481800mE – 2PGE + Au intercepts.

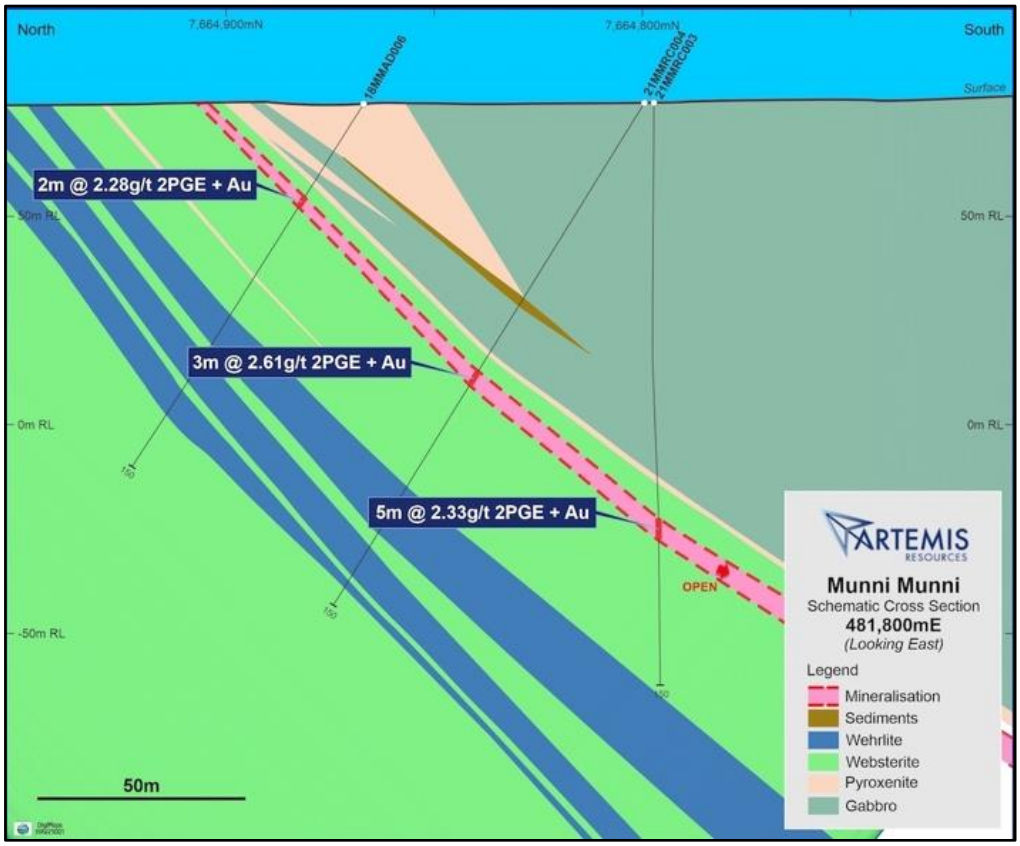


Figure 15: Section 481700mE – 2PGE + Au intercepts.

In the diamond drill core from 2018 essentially only gabbros and pyroxenites were recognised, likewise in the RC chips only gabbros, pyroxenites and sediments with various minor intrusive dykes were noted.

Holes 18MMAD006 with 21MMRC003 and 21MMRC004 show the direct correlation of the PGE results and the remarkable continuity and consistency of the lithochemistry.

The RC data shows slightly lower absolute results for the PGE but occurs in the same relative 'stratigraphic' position. Virtually all PGE occur within the websterite lithology with a lesser amount in the pyroxenite due the PGE occurring very close to the contact between the two units.

Significant results from the PGE zone in this drilling program include:

- 7m @ 2.20g/t 2PGE + Au (1.46g/t Pd, 0.67 g/t Pt, 0.07g/t Au) from 124m, 21MMRC005;
- 7m @ 2.35g/t 2PGE + Au (1.33g/t Pd, 0.84 g/t Pt, 0.18g/t Au), from 96m, 21MMRC006;
- 4m @ 2.45g/t 2PGE + Au (1.31g/t Pd, 0.85g/t Pt, 0.29g/t Au) from 60m, 21MMRC007;
- 5m @ 2.35g/t 2PGE + Au (1.36g/t Pd, 0.68g/t Pt, 0.31g/t Au) from 75m, 21MMRC008;
- 4m @ 2.87g/t 2PGE + Au (1.76g/t Pd, 0.89g/t Pt, 0.22g/t Au) from 115m, 2MMRC010.

RADIO HILL FIXED-LOOP ELECTROMAGNETIC (FLEM) SURVEY

Resource Potentials Pty Ltd (ResPot) completed a high-level review of Radio Hill project tenements M47/161 and M47/337 to determine what geophysical exploration datasets are available, highlight geophysical anomaly zones, identify anomalies and target areas of interest that remain untested, or are under- tested by drilling.

The aim is to provide recommendations for additional geophysical surveying, and then to plan, monitor, process and interpret new geophysical surveys carried out over target areas of interest. FLEM surveying was completed by GAP Geophysics in April 2021.

This study identified deep and untested conductor anomaly zones of interest identified from historic deep drilling and follow-up DHEM survey data and reports, with DHEM targets shown projected to surface on the map in Figure 16.

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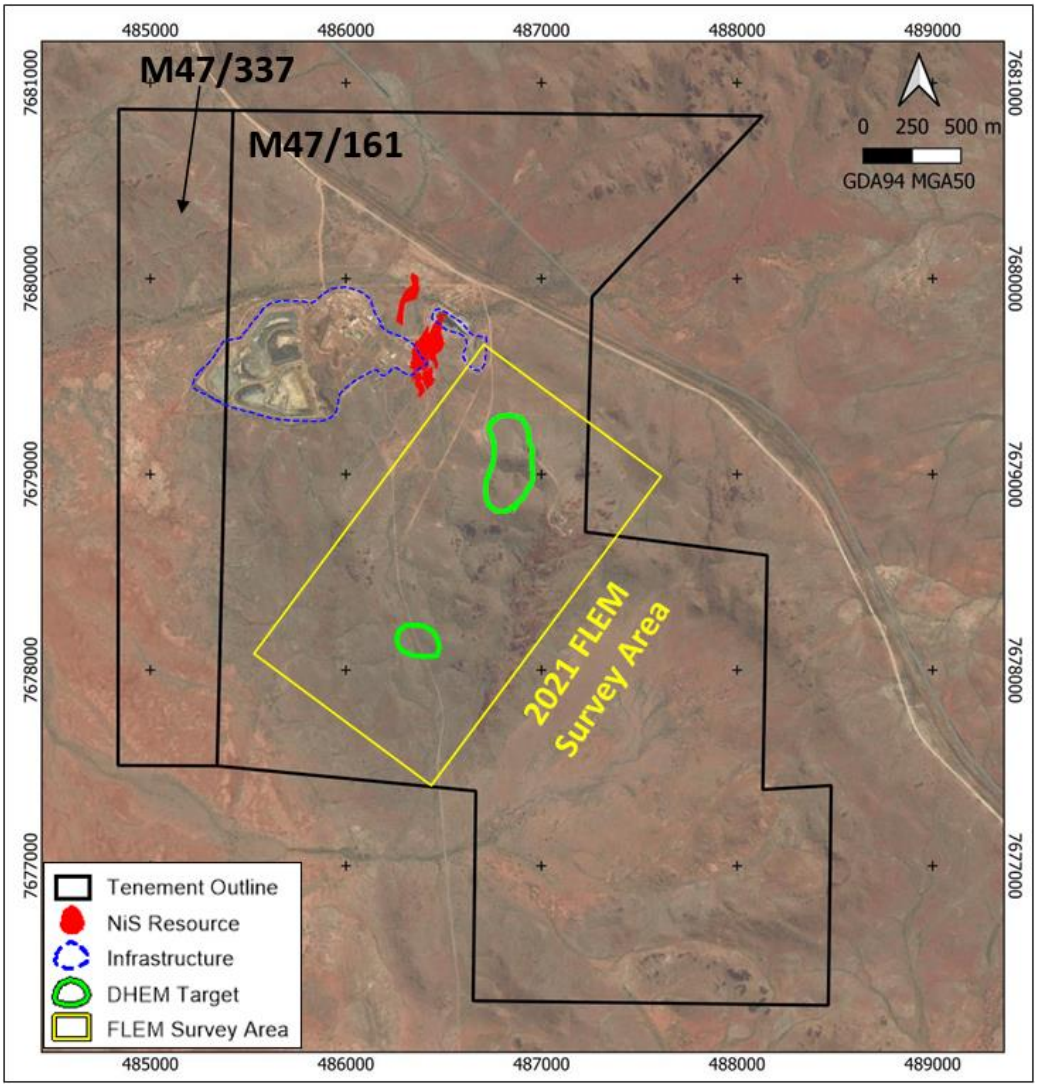


Figure 16: Radio Hill Project tenements M47/161 and M47/337 (black outlines), mine infrastructure (dashed blue outlines), and the Radio Hill resource wireframes projected to surface (red) over a satellite image. The recent FLEM survey coverage area is outlined in yellow.

The Radio Hill project area is still considered to hold potential for additional discoveries of Ni-Cu-Co-PGE sulphide deposits at depths >500m and to the south of the mined out NiS deposits, where long conduits likely follow the base of the intrusion. However, additional deposits are most likely located at least 600m below surface based on drilling and DHEM results and are therefore too hard to identify using airborne or surface-based EM survey methods.

Recommendations to this program are pending.

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WHUNDO GRADIENT-ARRAY INDUCED POLARISATION (GAIP) SURVEY

Artemis Resources hold mining rights to the Whundo VMS project tenements, located approximately 45km S of Karratha in Western Australia. The Whundo Zn-Cu-Pb-Ag VMS deposit has been mined in places and is now in care-and-maintenance status. The project area still holds some un-mined deposits and has potential for additional VMS deposits that remain to be discovered.

This study identified VMS mineralisation potential along a target trend located to the NE of the main Whundo deposit and covers the Yannery and Ayshia prospect areas. These prospect areas may host only weakly-conductive base metal mineralisation, such as sphalerite-rich or disseminated sulphide deposits, that were not identified using previous electromagnetic (EM) survey methods. Therefore, a new induced polarisation (IP) survey was planned and carried out over this area to identify chargeable sulphide mineralisation that was not detected by historic EM surveying. This is highlighted in green on Figure 17.

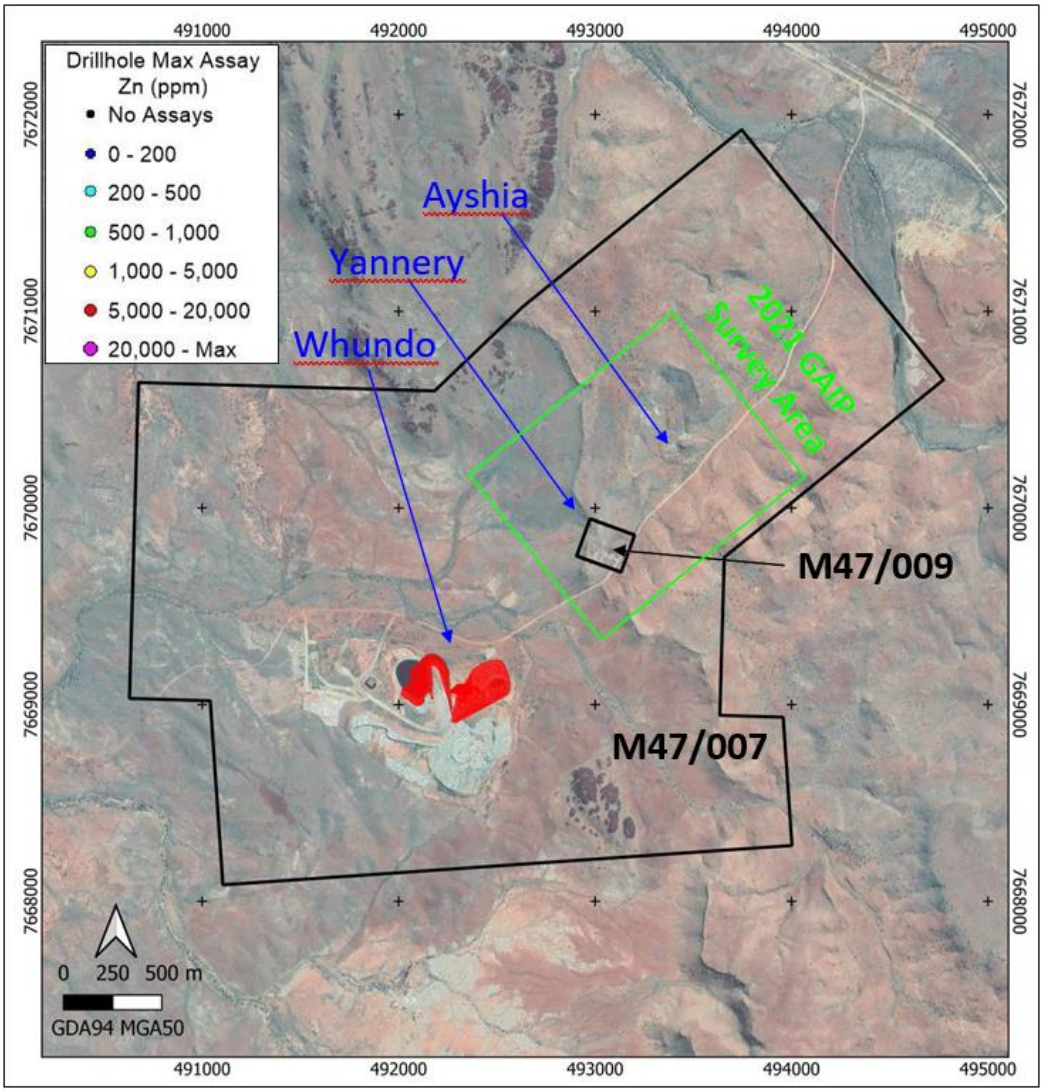


Figure 17: Whundo Project tenements M47/007 and M47/009 (black outlines), and the Whundo resource wireframe (red) over a satellite image. The recent GAIP survey area is outlined in green, and the known prospect locations are highlighted by blue arrows

A new GAIP survey area is recommended to be surveyed between the Whundo deposit and the recent GAIP survey area, as highlighted by the yellow square, (Figure 18).

This proposed GAIP survey area will cover a gap in survey coverage between Whundo and Yannery and cover the highest-amplitude chargeability anomaly located in the SW corner of the recent GAIP survey block.

Shallow RC drilling is recommended to test the chargeable and resistive target trend identified between Yannery and Ayshia prospects, as highlighted by the dashed black outline. This anomaly trend can be tested by RC drill transects planned across the trend. Untested VTEM target outlines to the NE and W of Whundo should also be RC drill tested. These targets are shown in Figure 18.

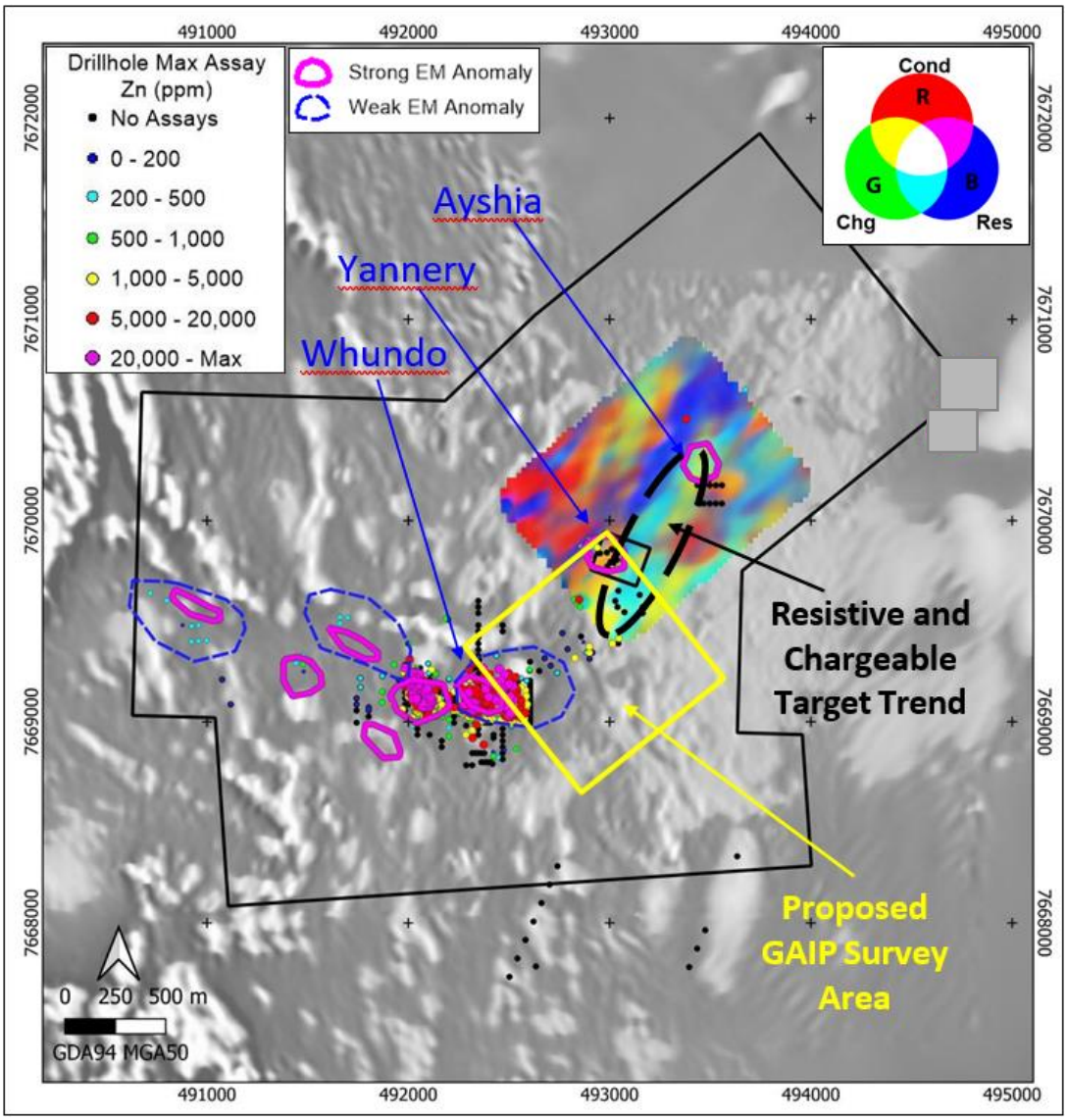


Figure 18: Whundo Project tenements M47/007 and M47/009 (black outlines), VTEM anomaly outlines from late-time VTEM data (pink), early-time anomalies (dashed blue), historic Whundo drillhole collar locations coloured by max Zn, and a semi-transparent colour GAIP ternary image where conductivity is red, chargeability is green and resistivity is blue, all overlying a greyscale derivative magnetic image background

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CORPORATE

Health and Safety

The Company continues to comply with all State guidelines to ensure the health and safety of its workforce, contractors, and the community in which it operates.

There is currently no significant impact on operations as a result of COVID-19.

Artemis has had no Occupational Health and Safety incidences during the quarter.

The Company ended the Quarter with a cash balance of $9.1m and liquid listed investments of circa $590,000.

Capital Raising

The Company raised $7 million at 6 cents a share in early June 2021 issuing 116.7 million new shares. The raise was strongly supported by European and Australian Institutional Investors.

Board of Directors

The Board welcomed Dr Simon Dominy as a Director on 1 July 2021. Dr Dominy is Adjunct Professor at the Western Australian School of Mines (WASM), Curtin University, and a Visiting Associate Professor at the Camborne School of Mines (CSM), University of Exeter, UK.

A mining geologist-engineer with over 25 years' experience, Dr Dominy has since 2015 been working with a number of private and listed entities developing/operating gold projects including: MG Gold Ltd; Novo Resources Corporation (TSV: NVO); Scotgold Resources Ltd (AIM: SGZ) and OCX Gold Group.

Between 2004-2014 he was an Executive Consultant/General Manager with the Snowden Group based in Australia and UK, including two years contracted out to LionGold Corporation (SGX: A78).

Simon is a Fellow of the Australasian Institute of Mining and Metallurgy ("FAusIMM") and the Australian Institute of Geoscientists ("FAIG").

Mr Boyd Timler resigned as a director on 24 May 2021.

Other

The Company spent ~$1.8 million on exploration in the quarter ended 30 June 2021, principally on the drilling programs at Carlow Castle and Munni Munni, and exploration planning at Paterson's outlined above.

Payments to Directors, related parties and their associates during the quarter amounted to $192,000, being salaries, superannuation and directors' fees.

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About Artemis Resources

Artemis Resources (ASX: ARV; FRA: ATY; US: ARTTF) is a Perth-based exploration and development company, led by an experienced team that has a singular focus on delivering shareholder value from its Pilbara gold projects – the Greater Carlow Gold Project in the West Pilbara and the Paterson Central exploration project in the East Pilbara.

For more information, please visit www.artemisresources.com.au

This report has been approved for release by the Board.

COMPETENT PERSONS STATEMENT PATERSONS RANGE:

The information in this announcement that relates to Exploration Results complies with the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC Code) and has been compiled and assessed under the supervision of Dr Jayson Meyers, a consultant to Artemis Resources Limited and a Director of Resource Potentials Pty Ltd. Dr Meyers is a Fellow of the Australasian Institute of Geoscientists. He has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the JORC Code. Dr Meyers consents to the inclusion in this announcement of the matters based on his information in the form and context in which it appears. Dr Meyers does not hold securities in the Company.

COMPETENT PERSONS STATEMENT WEST PILBARA:

The information in this announcement that relates to Exploration Results is based on information compiled or reviewed by Steve Boda, who is a Member of the Australasian Institute of Geoscientists (AIG). Mr Boda is an employee of Artemis Resources Limited. Mr Boda has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity which he is undertaking to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Mr Boda consents to the inclusion in the announcement of the matters based on his information in the form and context in which it appears.

COMPETENT PERSONS STATEMENT MINERAL RESOURCE ESTIMATION (MRE)

The information in this report that relates to Mineral Resources is based on information compiled by Mr Phil Jankowski, who is a Member of the Australasian Institute of Mining and Metallurgy. Mr Jankowski has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the Joint Ore Reserves Committee (JORC) 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Mr Jankowski consents to the inclusion in this website of the matters based on this information in the form and context in which it appears.

Tenement List - All tenements are located in Western Australia.

Project	Tenement	Status	Company
Purdy's Reward	L47/782	Pending	KML No 2 Pty Ltd
Carlow Castle	E47/1797	Live	KML No 2 Pty Ltd
Ruth Well	P47/1929	Live	KML No 2 Pty Ltd
	E47/3719	Live	KML No 2 Pty Ltd
	E47/3487[1]	Live	Elysian Resources Pty Ltd
	E47/3341[1]	Live	Hard Rock Resources Pty Ltd
47 Patch	E47/3361[1]	Live	Elysian Resources Pty Ltd
Elysian / Hard Rock	E47/3564[1]	Live	Elysian Resources Pty Ltd
	E47/3340[1]	Live	Hard Rock Resources Pty Ltd
	E47/3390[1]	Live	Hard Rock Resources Pty Ltd
	P47/1832[1]	Live	Hard Rock Resources Pty Ltd
	P47/1881[1]	Live	Hard Rock Resources Pty Ltd
	E47/3534[1]	Live	Jindalee Resources Pty Ltd
	E47/3535[1]	Pending	Jindalee Resources Pty Ltd
	P47/1833[1]	Pending	Jindalee Resources Pty Ltd
Whundo	L47/163	Live	Fox Radio Hill Pty Ltd
	M47/7	Live	Fox Radio Hill Pty Ltd
	M47/9	Live	Fox Radio Hill Pty Ltd
Radio Hill	M47/161	Live	Fox Radio Hill Pty Ltd
	M47/337	Live	Fox Radio Hill Pty Ltd
	L47/93	Live	Fox Radio Hill Pty Ltd
Weerianna	M47/223[2]	Live	Western Metals Pty Ltd
Silica Hills	L47/781	Pending	KML No 2 Pty Ltd

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	E47/1746	Live	KML No 2 Pty Ltd
Telfer	E45/5276	Live	Armada Mining Pty Ltd
Sing Well	P47/1622	Live	KML No 2 Pty Ltd
	P47/1112	Live	KML No 2 Pty Ltd
Nickol River	P47/1126	Live	KML No 2 Pty Ltd
	P47/1925	Live	KML No 2 Pty Ltd
Munni Munni	E47/3322[5]	Live	Karratha Metals Pty Ltd
	M47/123[5]	Live	Platina Resources Ltd
	M47/124[5]	Live	Platina Resources Ltd
	M47/125[5]	Live	Platina Resources Ltd
	M47/126[5]	Live	Platina Resources Ltd

1– 70% Artemis – Karratha Gold Joint Venture

2 – 80% Artemis

3 – 70% Artemis

4 – 70% Artemis – Joint Venture with Platina Resources

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Table 4:Carlow Drill Collar Survey June Q2 2021 (MGA50 Grid)

HoleID	Type	Easting GDA94	Northing GDA94	RL (m)	Dip	Azimuth Mag	Total Depth (m)
ARC310	RC	506720	7698808	37	-60.71	179.89	260
ARC311	RC	506670	7698822	37	-60.53	180.39	260
ARC312	RC	506670	7698768	36	-59.99	180.03	200
ARC313	RC	506760	7698762	36	-60.65	180.05	220
ARC315	RC	506560	7698740	35	-60.14	180	150
21CCDD001	DD	507540	7698470	30	-60.11	359.72	300.2
21CCDD002	DD	507580	7698590	30	-60.27	1.92	110.6
21CCDD003	DD	507580	7698550	30	-60.43	359.96	177.3

Table 5: Significant results for the Q2 June RC drilling at Carlow Castle. Results are >0.5g/t Au or >0.5% Cu

Hole No	From (m)	To (m)	Downhole Width (m)	Au (g/t)	Cu (%)	Co (%)
ARC310	34	35	1	0.300	0.014	0.042
ARC310	40	41	1	**0.900**	**1.585**	0.009
ARC310	53	54	1	**1.430**	**1.700**	**0.050**
ARC310	54	55	1	**47.300**	**11.250**	**0.065**
ARC310	55	56	1	**26.500**	**9.510**	**0.060**
ARC310	56	57	1	**9.700**	**9.900**	**0.057**
ARC310	57	58	1	**4.350**	**6.900**	**0.050**
ARC310	58	59	1	**0.530**	**3.250**	0.035
ARC310	59	60	1	0.320	0.266	0.009
ARC310	112	113	1	**1.420**	0.053	0.027
ARC310	113	114	1	0.380	**0.870**	**0.074**
ARC310	129	130	1	**0.670**	0.264	**0.141**
ARC310	136	137	1	0.320	0.145	0.007
ARC310	137	138	1	0.320	0.116	0.009
ARC310	138	139	1	0.450	0.090	0.034
ARC310	142	143	1	0.370	**0.640**	0.036
ARC310	143	144	1	0.330	0.159	0.012
ARC310	168	169	1	**1.650**	0.177	**0.102**
ARC310	169	170	1	**1.570**	0.136	**0.155**
ARC310	204	205	1	0.330	**0.573**	0.029
ARC310	214	215	1	0.450	0.068	**0.228**
ARC310	222	223	1	0.300	0.211	0.011
ARC310	225	226	1	**1.370**	0.063	0.003
ARC311	6	7	1	**0.550**	0.139	0.007
ARC311	45	46	1	**0.570**	0.180	0.021
ARC311	53	54	1	0.280	0.126	**0.060**
ARC311	56	57	1	0.480	0.181	**0.082**
ARC311	100	101	1	**0.540**	0.214	**0.066**
ARC311	109	110	1	0.320	0.090	**0.060**
ARC311	117	118	1	0.280	**0.715**	0.014
ARC311	132	133	1	0.330	0.047	0.010
ARC311	136	137	1	**2.550**	0.223	**0.058**
ARC311	139	140	1	**1.650**	**0.570**	**0.058**

Hole No	From (m)	To (m)	Downhole Width (m)	Au (g/t)	Cu (%)	Co (%)
ARC311	140	141	1	**2.870**	**0.565**	**0.157**
ARC311	141	142	1	**0.690**	0.269	**0.072**
ARC311	154	155	1	**2.490**	0.486	0.016
ARC311	175	176	1	0.460	0.068	0.012
ARC311	176	177	1	**0.570**	0.099	0.016
ARC311	181	182	1	0.340	0.090	0.008
ARC311	182	183	1	**0.780**	0.187	0.011
ARC311	186	187	1	**0.650**	0.155	0.024
ARC311	187	188	1	**6.270**	**1.075**	**0.054**
ARC311	189	190	1	**1.460**	0.106	**0.083**
ARC311	190	191	1	**5.930**	**1.630**	**0.610**
ARC311	191	192	1	**1.140**	0.199	**0.061**
ARC312	9	10	1	**1.610**	**2.330**	**0.053**
ARC312	28	29	1	**0.860**	0.340	0.025
ARC312	29	30	1	**0.840**	0.385	0.030
ARC312	30	31	1	**1.350**	**0.621**	0.015
ARC312	31	32	1	**6.950**	**0.570**	0.011
ARC312	32	33	1	**1.700**	**0.841**	0.013
ARC312	33	34	1	**4.370**	**3.830**	0.022
ARC312	35	36	1	0.320	0.297	0.011
ARC312	46	47	1	0.330	0.186	**0.053**
ARC312	47	48	1	0.420	0.196	0.045
ARC312	49	50	1	0.290	0.282	0.026
ARC312	53	54	1	0.480	0.363	0.030
ARC312	55	56	1	0.310	0.059	0.010
ARC312	56	57	1	**2.440**	0.125	0.015
ARC312	57	58	1	**1.450**	0.328	0.016
ARC312	59	60	1	0.260	0.066	0.018
ARC312	60	61	1	**4.010**	**0.713**	**0.118**
ARC312	66	67	1	**0.880**	0.051	**0.397**
ARC312	77	78	1	0.490	**0.563**	0.025
ARC312	78	79	1	0.480	**1.410**	0.018
ARC312	83	84	1	**0.760**	0.073	**0.050**
ARC312	84	85	1	**1.530**	0.304	0.014
ARC312	93	94	1	0.300	**0.664**	0.013
ARC312	105	106	1	**0.560**	0.295	0.013
ARC312	114	115	1	**9.290**	**0.673**	**0.169**
ARC312	115	116	1	0.380	0.098	0.014
ARC312	116	117	1	0.390	0.112	0.015
ARC312	118	119	1	**0.570**	0.049	0.022
ARC312	125	126	1	0.370	0.221	0.030
ARC312	134	135	1	0.330	0.099	0.023
ARC312	144	145	1	**2.630**	0.234	0.006
ARC313	14	15	1	0.460	0.058	0.010
ARC313	35	36	1	**1.110**	0.046	0.010
ARC313	43	44	1	0.480	0.128	0.034
ARC313	44	45	1	**1.210**	0.283	0.028
ARC313	82	83	1	**1.060**	**3.930**	0.010
ARC313	90	91	1	0.340	**2.110**	0.011
ARC313	103	104	1	0.320	0.222	0.030
ARC313	105	106	1	**1.300**	0.079	**0.185**
ARC313	110	111	1	**0.990**	0.421	**0.570**

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Hole No	From (m)	To (m)	Downhole Width (m)	Au (g/t)	Cu (%)	Co (%)
ARC313	111	112	1	**3.150**	0.463	0.047
ARC313	121	122	1	**2.170**	0.018	**0.083**
ARC313	122	123	1	0.360	0.156	**0.083**
ARC313	124	125	1	**5.760**	**1.740**	**0.071**
ARC313	130	131	1	0.370	0.050	0.007
ARC313	140	141	1	0.440	0.172	**0.062**
ARC313	147	148	1	**1.350**	0.145	**0.098**
ARC313	148	149	1	0.360	0.091	0.046
ARC313	151	152	1	**0.640**	0.393	**0.243**
ARC313	152	153	1	0.420	0.128	**0.090**
ARC313	170	171	1	0.280	**0.574**	0.013
ARC313	195	196	1	**0.730**	**2.070**	0.007
ARC313	199	200	1	**5.170**	0.376	0.002
ARC315	NSI					

Table 6: Drill Collar Locations for Munni Munni

Hole ID	Type	Easting	Northing	RL	Grid	Azimuth (True)	Dip	Depth
18MMAD001	DDH	482199.26	7664902.04	86.73	MGA-50	4.11	-60.1	100.5
18MMAD002	DDH	482660.00	7664952.82	81.86	MGA-50	5.17	-60.1	101.8
18MMAD003	DDH	482340.74	7664909.75	89.17	MGA-50	5.77	-60.2	100
18MMAD004	DDH	482454.88	7664874.92	85.70	MGA-50	4.47	-59.2	120
18MMAD005	DDH	481898.96	7664872.90	83.68	MGA-50	0	-70	100
18MMAD006	DDH	481796.57	7664865.99	82.57	MGA-50	0.84	-60.3	108.8
18MMAD007	DDH	482143.34	7664922.90	94.51	MGA-50	0	-80	110
18MMAD008	DDH	482454.50	7664875.00	85.70	MGA-50	0	-80	110
20MMRC001	RC	485794.94	7661174.67	96.57	MGA-50	90	-60	160
20MMRC002	RC	485863.85	7662228.67	92.18	MGA-50	90	-60	200
20MMRC003	RC	485901.19	7662571.11	91.25	MGA-50	90	-60	180
20MMRC004	RC	486293.89	7663240.68	89.82	MGA-50	90	-60	80
20MMRC005	RC	481923.45	7664887.17	82.84	MGA-50	0	-60	100
20MMRC006	RC	482201.58	7664896.23	86.94	MGA-50	0	-90	160
20MMRC007	RC	482492.96	7664856.56	88.47	MGA-50	180	-80	190
20MMRC008	RC	479730.23	7664005.47	102.58	MGA-50	330	-70	150
20MMRC009	RC	480200.52	7663223.59	104.73	MGA-50	0	-90	150
20MMRC010	RC	480309.48	7662943.32	106.57	MGA-50	0	-90	160
20MMRC011	RC	479598.19	7663830.25	123.01	MGA-50	320	-60	200
20MMRC012	RC	479696.24	7663809.66	112.06	MGA-50	330	-60	198
21MMRC001	RC	481699.73	7664781.70	83.18	MGA-51	0.00	-60	150
21MMRC002	RC	481699.72	7664779.73	83.07	MGA-52	0.00	-90	150
21MMRC003	RC	481814.44	7664795.24	83.58	MGA-53	0.00	-90	150
21MMRC004	RC	481814.52	7664797.22	83.51	MGA-54	0.00	-60	150
21MMRC005	RC	481844.03	7664739.96	84.73	MGA-55	0.00	-60	150
21MMRC006	RC	481862.44	7664843.06	83.49	MGA-56	0.00	-90	150
21MMRC007	RC	481864.87	7664843.26	83.67	MGA-57	30.00	-60	150
21MMRC008	RC	481974.29	7664875.13	86.89	MGA-58	20.00	-60	150
21MMRC009	RC	482895.77	7664802.80	82.58	MGA-59	0.00	-60	150
21MMRC010	RC	482502.76	7664821.49	98.79	MGA-60	350.00	-60	150
21MMRC011	RC	482798.12	7664827.12	82.19	MGA-61	0.00	-60	170
21MMRC012	RC	482713.67	7664884.68	85.61	MGA-62	0.00	-60	150
21MMRC013	RC	486247.37	7660700.45	98.29	MGA-63	0.00	-60	150
21MMRC014	RC	485899.50	7660489.58	99.18	MGA-64	0.00	-60	250
21MMRC015	RC	486247.366	7660700.47	98.29	MGA-65	0.00	-60	250

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Table 7: Significant Intersections for Munni Munni

Hole_ID	M From	M To	Width	Sample Type	Pd	Pt	Au	2PGE+Au	Co	Cu	Ni
18MMAD001	40.5	41	0.5	ASSAY 1/4	0.02	0.01	0.20	0.23	100	2660	1320
18MMAD001	41	41.5	0.5	ASSAY 1/4	**0.66**	0.49	**0.60**	**1.74**	130	4130	1910
18MMAD001	41.5	42	0.5	ASSAY 1/4	**2.00**	**1.85**	0.40	**4.25**	90	1430	950
18MMAD001	42	42.5	0.5	ASSAY 1/4	**2.13**	**1.34**	0.08	**3.55**	70	340	530
18MMAD001	42.5	43	0.5	ASSAY 1/4	**1.92**	**0.88**	0.04	**2.83**	70	210	530
18MMAD001	43	43.5	0.5	ASSAY 1/4	**1.15**	0.45	0.06	**1.66**	70	320	520
18MMAD001	43.5	44	0.5	ASSAY 1/4	**1.34**	0.36	0.24	**1.93**	90	1070	780
18MMAD001	44	44.5	0.5	ASSAY 1/4	**0.73**	0.14	0.04	0.91	70	380	540
18MMAD001	44.5	45	0.5	ASSAY 1/4	**0.95**	0.15	0.06	**1.16**	60	340	500
18MMAD001	45	45.5	0.5	ASSAY 1/4	**1.11**	0.17	0.12	**1.39**	100	1090	830
18MMAD001	45.5	46	0.5	ASSAY 1/4	**0.59**	0.08	0.06	0.73	70	520	570
18MMAD001	46	46.5	0.5	ASSAY 1/4	0.38	0.06	0.02	0.45	80	170	550
18MMAD001	46.5	47	0.5	ASSAY 1/4	0.50	0.41	0.02	0.93	80	120	510
18MMAD001	47	47.5	0.5	ASSAY 1/4	**1.28**	**0.76**	0.06	**2.10**	90	420	610
18MMAD001	47.5	48	0.5	ASSAY 1/4	0.01	0.01	0.01	0.03	80	190	530
18MMAD001	98	98.5	0.5	ASSAY 1/4	0.05	0.02	0.01	0.08	170	100	2260
18MMAD001	98.5	99	0.5	ASSAY 1/4	**0.60**	0.28	0.16	**1.04**	140	2080	2660
18MMAD001	99	99.5	0.5	ASSAY 1/4	0.01	0.00	0.00	0.01	90	100	1040
18MMAD002	22	22.5	0.5	ASSAY 1/4	0.01	0.00	0.03	0.04	110	3160	1540
18MMAD002	22.5	23	0.5	ASSAY 1/4	**0.59**	0.41	**0.72**	**1.71**	120	3430	1710
18MMAD002	23	23.5	0.5	ASSAY 1/4	**2.09**	0.85	**0.27**	**3.21**	80	1140	790
18MMAD002	23.5	24	0.5	ASSAY 1/4	**0.30**	0.04	**0.07**	**0.41**	90	890	730
										0.22	0.12
18MMAD003	34	34.5	0.5	ASSAY 1/4	**0.01**	0.01	**0.24**	**0.26**	160	4400	1960
18MMAD003	34.5	35	0.5	ASSAY 1/4	**0.07**	0.04	**0.47**	**0.58**	140	3420	1620
18MMAD003	35	35.5	0.5	ASSAY 1/4	**2.06**	2.01	**0.72**	**4.79**	180	3790	2010
18MMAD003	35.5	36	0.5	ASSAY 1/4	**2.71**	2.53	**0.22**	**5.46**	100	1250	940
18MMAD003	36	36.5	0.5	ASSAY 1/4	**2.14**	1.40	**0.29**	**3.83**	80	400	650
18MMAD003	36.5	37	0.5	ASSAY 1/4	**1.40**	0.46	**0.08**	**1.94**	80	240	610
18MMAD003	37	37.5	0.5	ASSAY 1/4	**1.62**	0.53	**0.15**	**2.30**	80	430	730
18MMAD003	37.5	38	0.5	ASSAY 1/4	**0.92**	0.29	**0.04**	**1.25**	160	2290	1370
18MMAD003	38	38.5	0.5	ASSAY 1/4	**0.93**	0.39	**0.17**	**1.48**	140	2070	1190
18MMAD003	38.5	39	0.5	ASSAY 1/4	**0.04**	0.02	**0.00**	**0.06**	80	260	560
18MMAD004	56.7	57	0.3	ASSAY 1/4	**0.11**	0.07	**0.02**	**0.20**	110	1160	620
18MMAD004	57	57.5	0.5	ASSAY 1/4	**0.75**	0.22	**0.07**	**1.05**	120	2090	1160
18MMAD004	57.5	58	0.5	ASSAY 1/4	**0.19**	0.14	**0.03**	**0.36**	90	580	710
18MMAD005	34	34.5	0.5	ASSAY 1/4	**0.01**	0.01	**0.23**	**0.25**	100	2880	1350
18MMAD005	34.5	35	0.5	ASSAY 1/4	**0.12**	0.09	**0.40**	**0.60**	110	3100	1360
18MMAD005	35	35.5	0.5	ASSAY 1/4	**1.80**	1.83	**0.52**	**4.15**	100	2600	1250
18MMAD005	35.5	36	0.5	ASSAY 1/4	**1.82**	1.79	**0.25**	**3.85**	80	930	780
18MMAD005	36	36.5	0.5	ASSAY 1/4	**2.05**	1.42	**0.10**	**3.57**	80	460	620
18MMAD005	36.5	37	0.5	ASSAY 1/4	**2.24**	1.34	**0.06**	**3.64**	80	380	620
18MMAD005	37	37.5	0.5	ASSAY 1/4	**1.71**	0.92	**0.04**	**2.67**	70	250	530
18MMAD005	37.5	38	0.5	ASSAY 1/4	**1.23**	0.53	**0.05**	**1.80**	80	340	590
18MMAD005	38	38.5	0.5	ASSAY 1/4	**1.57**	0.37	**0.16**	**2.10**	110	970	920
18MMAD005	38.5	39	0.5	ASSAY 1/4	**1.72**	0.24	**0.06**	**2.02**	80	260	610
18MMAD005	39	39.5	0.5	ASSAY 1/4	**0.75**	0.10	**0.04**	**0.88**	80	180	580
18MMAD005	59	59.5	0.5	ASSAY 1/4	**0.01**	0.00	**0.00**	**0.01**	60	180	330
18MMAD005	59.5	60	0.5	ASSAY 1/4	**0.41**	0.17	**0.06**	**0.64**	120	3990	1840
18MMAD005	60	60.5	0.5	ASSAY 1/4	**0.61**	0.35	**0.10**	**1.05**	110	2770	1480
18MMAD005	60.5	61	0.5	ASSAY 1/4	**0.87**	0.60	**0.19**	**1.65**	110	3020	1680
18MMAD005	61	61.5	0.5	ASSAY 1/4	**0.24**	0.14	**0.04**	**0.42**	90	1340	1090
										0.33	0.17

Hole_ID	M From	M To	Width	Sample Type	Pd	Pt	Au	2PGE+Au	Co	Cu	Ni
18MMAD005	65	65.5	0.5	ASSAY 1/4	**0.01**	0.00	**0.00**	**0.01**	40	60	200
18MMAD005	65.5	66	0.5	ASSAY 1/4	**0.30**	0.19	**0.05**	**0.53**	50	680	420
18MMAD005	66	66.5	0.5	ASSAY 1/4	**1.24**	0.75	**0.20**	**2.19**	130	3290	1880
18MMAD005	66.5	67	0.5	ASSAY 1/4	**1.41**	0.60	**0.18**	**2.19**	140	3310	2200
18MMAD005	67	67.5	0.5	ASSAY 1/4	**0.21**	0.11	**0.04**	**0.36**	80	630	1040
18MMAD005	67.5	68	0.5	ASSAY 1/4	**0.35**	0.18	**0.05**	**0.58**	90	760	1120
18MMAD005	68	68.5	0.5	ASSAY 1/4	**0.18**	0.10	**0.03**	**0.31**	90	570	1000
18MMAD005	68.5	69	0.5	ASSAY 1/4	**1.09**	0.63	**0.10**	**1.82**	130	2320	1630
18MMAD005	69	69.5	0.5	ASSAY 1/4	**0.19**	0.12	**0.05**	**0.36**	90	380	980
18MMAD006	27.5	28	0.5	ASSAY 1/4	**0.01**	0.00	**0.13**	**0.14**	120	3210	1400
18MMAD006	28	28.5	0.5	ASSAY 1/4	**0.76**	0.69	**0.33**	**1.78**	100	2330	1160
18MMAD006	28.5	29	0.5	ASSAY 1/4	**1.66**	1.21	**0.14**	**3.00**	80	420	560
18MMAD006	29	29.5	0.5	ASSAY 1/4	**1.49**	0.77	**0.06**	**2.32**	80	360	540
18MMAD006	29.5	30	0.5	ASSAY 1/4	**1.29**	0.67	**0.06**	**2.01**	80	350	540
18MMAD006	30	30.5	0.5	ASSAY 1/4	**0.76**	0.14	**0.07**	**0.97**	80	440	600
18MMAD006	30.5	31	0.5	ASSAY 1/4	**0.48**	0.09	**0.02**	**0.59**	80	390	580
18MMAD006	31	31.5	0.5	ASSAY 1/4	**1.10**	0.19	**0.08**	**1.37**	70	380	550
18MMAD006	31.5	32	0.5	ASSAY 1/4	**0.55**	0.26	**0.03**	**0.85**	70	260	530
18MMAD006	32	32.5	0.5	ASSAY 1/4	**1.16**	0.25	**0.11**	**1.51**	100	1070	740
18MMAD006	32.5	33	0.5	ASSAY 1/4	**0.32**	0.17	**0.04**	**0.53**	80	230	540
18MMAD006	33	33.5	0.5	ASSAY 1/4	**0.04**	0.01	**0.00**	**0.05**	70	150	500
18MMAD007	65	65.5	0.5	ASSAY 1/4	**0.06**	0.03	**0.36**	**0.45**	110	3440	1490
18MMAD007	65.5	66	0.5	ASSAY 1/4	**1.56**	1.60	**0.49**	**3.64**	100	2410	1160
18MMAD007	66	66.5	0.5	ASSAY 1/4	**1.98**	1.44	**0.09**	**3.50**	90	430	590
18MMAD007	66.5	67	0.5	ASSAY 1/4	**1.58**	0.55	**0.13**	**2.26**	90	770	700
18MMAD007	67	67.5	0.5	ASSAY 1/4	**0.91**	0.16	**0.14**	**1.21**	90	1320	900
18MMAD007	67.5	68	0.5	ASSAY 1/4	**0.55**	0.12	**0.04**	**0.71**	90	410	590
18MMAD007	68	68.5	0.5	ASSAY 1/4	**0.68**	0.11	**0.07**	**0.85**	80	850	700
18MMAD007	68.5	69	0.5	ASSAY 1/4	**0.64**	0.08	**0.04**	**0.76**	90	440	620
18MMAD007	69	69.5	0.5	ASSAY 1/4	**0.71**	0.23	**0.05**	**0.98**	90	380	620
18MMAD007	69.5	70	0.5	ASSAY 1/4	**0.34**	0.26	**0.01**	**0.61**	80	130	530
18MMAD007	70	70.5	0.5	ASSAY 1/4	**0.42**	0.25	**0.02**	**0.69**	90	240	560
18MMAD007	70.5	71	0.5	ASSAY 1/4	**0.02**	0.01	**0.00**	**0.03**	90	160	550
18MMAD008	81.5	82	0.5	ASSAY 1/4	**0.01**	0.00	**0.00**	**0.01**	60	260	470
18MMAD008	82	82.5	0.5	ASSAY 1/4	**0.67**	0.25	**0.07**	**0.99**	80	1520	950
18MMAD008	82.5	83	0.5	ASSAY 1/4	**1.46**	1.03	**0.33**	**2.81**	100	2080	1330
18MMAD008	83	83.5	0.5	ASSAY 1/4	**3.14**	2.15	**0.48**	**5.77**	120	2400	1690
18MMAD008	83.5	84	0.5	ASSAY 1/4	**2.66**	2.00	**0.45**	**5.11**	150	2570	2040
18MMAD008	84	84.5	0.5	ASSAY 1/4	**0.74**	0.72	**0.21**	**1.67**	90	1890	1200
18MMAD008	84.5	85	0.5	ASSAY 1/4	**0.73**	0.52	**0.13**	**1.39**	80	990	1140
18MMAD008	85	85.5	0.5	ASSAY 1/4	**0.08**	0.06	**0.01**	**0.14**	60	190	490
18MMAD008	85.5	86	0.5	ASSAY 1/4	**0.66**	0.47	**0.11**	**1.24**	90	1940	1170
18MMAD008	86	86.5	0.5	ASSAY 1/4	**0.64**	0.37	**0.09**	**1.10**	80	1850	1040
18MMAD008	86.5	87	0.5	ASSAY 1/4	**0.03**	0.02	**0.01**	**0.05**	60	130	520
18MMAD008	87	87.5	0.5	ASSAY 1/4	**0.18**	0.09	**0.03**	**0.30**	70	340	540
18MMAD008	87.5	88	0.5	ASSAY 1/4	**0.69**	0.57	**0.18**	**1.44**	100	1580	1130
18MMAD008	88	89	1	ASSAY 1/4	**0.14**	0.08	**0.02**	**0.24**	80	440	670
20MMRC003	133	134	1	RC	**0.25**	0.05	**0.04**	**0.33**	62	638	336
20MMRC003	134	135	1	RC	**0.48**	0.19	**0.12**	**0.78**	78	1590	613
20MMRC003	135	136	1	RC	**0.71**	0.25	**0.12**	**1.08**	90	2310	870
20MMRC003	136	137	1	RC	**0.08**	0.02	**0.05**	**0.15**	79	356	401

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Hole_ID	M From	M To	Width	Sample Type	Pd	Pt	Au	2PGE+Au	Co	Cu	Ni
20MMRC005	18	19	1	RC	**0.00**	0.00	**0.04**	**0.05**	95	1640	924
20MMRC005	19	20	1	RC	**0.34**	0.33	**0.23**	**0.90**	125	2810	1350
20MMRC005	20	21	1	RC	**1.74**	1.37	**0.20**	**3.30**	96	1450	981
20MMRC005	21	22	1	RC	**1.88**	1.03	**0.13**	**3.03**	85	861	752
20MMRC005	22	23	1	RC	**0.97**	0.20	**0.09**	**1.26**	94	887	794
20MMRC005	23	24	1	RC	**0.50**	0.09	**0.04**	**0.63**	82	497	616
20MMRC005	24	25	1	RC	**0.24**	0.17	**0.01**	**0.42**	82	177	521
20MMRC006	69	70	1	RC	**0.03**	0.01	**0.10**	**0.15**	100	1275	532
20MMRC006	70	71	1	RC	**0.62**	0.60	**0.30**	**1.51**	76	1520	846
20MMRC006	71	72	1	RC	**0.85**	0.61	**0.06**	**1.52**	85	802	423
20MMRC006	72	73	1	RC	**0.90**	0.29	**0.16**	**1.35**	96	1140	669
20MMRC006	73	74	1	RC	**0.62**	0.33	**0.12**	**1.06**	105	1500	695
20MMRC006	74	75	1	RC	**0.16**	0.08	**0.03**	**0.26**	81	355	605
20MMRC006	101	102	1	RC	**0.00**	0.00	**0.00**	**0.01**	59	296	143
20MMRC006	102	103	1	RC	**0.62**	0.39	**0.08**	**1.10**	131	2280	937
20MMRC006	103	104	1	RC	**0.22**	0.11	**0.04**	**0.37**	87	708	812
20MMRC007	121	122	1	RC	**0.01**	0.01	**0.14**	**0.16**	97	2280	1280
20MMRC007	122	123	1	RC	**0.49**	0.44	**0.33**	**1.26**	95	2810	1280
20MMRC007	123	124	1	RC	**1.70**	1.50	**0.17**	**3.37**	89	1090	736
20MMRC007	124	125	1	RC	**1.33**	0.76	**0.05**	**2.13**	81	511	527
20MMRC007	125	126	1	RC	**1.08**	0.40	**0.12**	**1.60**	82	874	722
20MMRC007	126	127	1	RC	**0.57**	0.17	**0.05**	**0.80**	75	416	572
20MMRC007	127	128	1	RC	**0.54**	0.16	**0.02**	**0.71**	76	380	594
20MMRC007	128	129	1	RC	**0.70**	0.22	**0.03**	**0.94**	76	260	573
20MMRC007	129	130	1	RC	**0.09**	0.04	**0.01**	**0.14**	74	133	528
20MMRC011	143	144	1	RC	**0.06**	0.04	**0.19**	**0.29**	88	1960	873
20MMRC011	144	145	1	RC	**0.87**	0.82	**0.42**	**2.11**	89	2360	1050
20MMRC011	145	146	1	RC	**0.78**	0.78	**0.14**	**1.69**	77	781	587
20MMRC011	146	147	1	RC	**0.83**	0.44	**0.09**	**1.35**	78	829	601
20MMRC011	147	148	1	RC	**0.95**	0.17	**0.07**	**1.20**	83	1460	853
20MMRC011	148	149	1	RC	**0.64**	0.08	**0.04**	**0.76**	75	1200	762
20MMRC011	149	150	1	RC	**0.48**	0.15	**0.05**	**0.68**	76	632	576
20MMRC011	150	151	1	RC	**0.21**	0.08	**0.01**	**0.30**	74	239	473
20MMRC012	193	194	1	RC	**0.01**	0.01	**0.14**	**0.15**	84	2710	1200
20MMRC012	194	195	1	RC	**0.37**	0.30	**0.15**	**0.82**	81	1060	756
20MMRC012	195	196	1	RC	**1.00**	0.60	**0.10**	**1.70**	79	909	651
20MMRC012	196	197	1	RC	**0.80**	0.37	**0.06**	**1.23**	73	659	544
20MMRC012	197	198	1	RC	**0.62**	0.21	**0.04**	**0.86**	73	656	556
21MMRC001	78	79	1	RC	**0.01**	0.01	**0.17**	**0.19**	117	3380	1485
21MMRC001	79	80	1	RC	**0.95**	1.01	**0.20**	**2.16**	87	1400	863
21MMRC001	80	81	1	RC	**0.59**	1.18	**0.05**	**1.82**	79	350	551
21MMRC001	81	82	1	RC	**0.17**	0.39	**0.02**	**0.58**	74	210	519
21MMRC001	82	83	1	RC	**0.01**	0.02	**0.01**	**0.04**	78	214	550
21MMRC002	115	116	1	RC	**0.01**	0.01	**0.19**	**0.21**	102	2470	1285
21MMRC002	116	117	1	RC	**0.11**	0.16	**0.33**	**0.61**	106	2970	1400
21MMRC002	117	118	1	RC	**1.37**	1.36	**0.35**	**3.07**	102	1980	1120
21MMRC002	118	119	1	RC	**1.20**	1.68	**0.11**	**2.99**	89	555	672
21MMRC002	119	120	1	RC	**1.00**	1.71	**0.07**	**2.78**	89	476	644
21MMRC002	120	121	1	RC	**0.59**	1.36	**0.06**	**2.01**	86	462	634
21MMRC002	121	122	1	RC	**0.16**	0.77	**0.08**	**1.01**	91	944	801
21MMRC002	122	123	1	RC	**0.09**	0.53	**0.02**	**0.64**	91	403	673

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Hole_ID	M From	M To	Width	Sample Type	Pd	Pt	Au	2PGE+Au	Co	Cu	Ni
21MMRC002	123	124	1	RC	**0.15**	0.88	**0.04**	**1.07**	88	359	644
21MMRC002	124	125	1	RC	**0.07**	0.35	**0.02**	**0.43**	80	185	574
21MMRC002	125	126	1	RC	**0.21**	0.73	**0.07**	**1.01**	90	625	735
21MMRC002	126	127	1	RC	**0.03**	0.15	**0.01**	**0.19**	77	155	578
21MMRC003	107	108	1	RC	**0.00**	0.01	**0.18**	**0.19**	98	2710	1310
21MMRC003	108	109	1	RC	**0.54**	0.61	**0.61**	**1.76**	112	3550	1580
21MMRC003	109	110	1	RC	**1.58**	1.52	**0.36**	**3.46**	98	1630	1020
21MMRC003	110	111	1	RC	**1.27**	1.64	**0.13**	**3.03**	85	632	661
21MMRC003	111	112	1	RC	**0.78**	1.43	**0.05**	**2.26**	81	376	579
21MMRC003	112	113	1	RC	**0.26**	0.80	**0.08**	**1.14**	85	624	687
21MMRC003	113	114	1	RC	**0.15**	0.70	**0.05**	**0.90**	94	1080	865
21MMRC003	114	115	1	RC	**0.11**	0.56	**0.02**	**0.68**	72	302	553
21MMRC003	115	116	1	RC	**0.07**	0.37	**0.01**	**0.45**	75	178	562
21MMRC003	116	117	1	RC	**0.06**	0.38	**0.01**	**0.46**	78	134	566
21MMRC003	117	118	1	RC	**0.15**	0.77	**0.01**	**0.93**	83	160	614
21MMRC003	118	119	1	RC	**0.54**	1.08	**0.02**	**1.63**	87	131	640
21MMRC003	119	120	1	RC	**0.03**	0.10	**0.00**	**0.13**	83	88	599
21MMRC004	80	81	1	RC	**0.01**	0.01	**0.16**	**0.18**	103	3080	1305
21MMRC004	81	82	1	RC	**0.68**	0.76	**0.39**	**1.82**	94	2430	1175
21MMRC004	82	83	1	RC	**1.38**	1.44	**0.26**	**3.08**	91	1300	871
21MMRC004	83	84	1	RC	**1.28**	1.49	**0.16**	**2.92**	88	836	726
21MMRC004	84	85	1	RC	**0.18**	0.67	**0.04**	**0.88**	84	369	571
21MMRC004	85	86	1	RC	**0.02**	0.04	**0.02**	**0.08**	84	187	520
21MMRC005	122	123	1	RC	**0.00**	0.01	**0.18**	**0.19**	102	3850	1710
21MMRC005	123	124	1	RC	**0.17**	0.19	**0.38**	**0.74**	104	3130	1460
21MMRC005	124	125	1	RC	**1.48**	1.56	**0.10**	**3.14**	79	836	705
21MMRC005	125	126	1	RC	**1.07**	1.73	**0.06**	**2.86**	74	326	543
21MMRC005	126	127	1	RC	**0.14**	0.98	**0.14**	**1.26**	95	1225	876
21MMRC005	127	128	1	RC	**0.19**	0.90	**0.05**	**1.14**	86	628	619
21MMRC005	128	129	1	RC	**0.07**	0.46	**0.04**	**0.57**	73	245	368
21MMRC005	129	130	1	RC	**1.45**	3.67	**0.12**	**5.23**	151	2610	1250
21MMRC005	130	131	1	RC	**0.33**	0.94	**0.02**	**1.29**	88	638	730
21MMRC005	131	132	1	RC	**0.17**	0.56	**0.02**	**0.75**	81	292	635
21MMRC005	132	133	1	RC	**0.01**	0.02	**0.00**	**0.03**	79	103	613
21MMRC006	94	95	1	RC	**0.00**	0.00	**0.03**	**0.03**	89	1560	981
21MMRC006	95	96	1	RC	**0.13**	0.21	**0.50**	**0.84**	120	4040	1725
21MMRC006	96	97	1	RC	**1.59**	1.56	**0.50**	**3.65**	100	2420	1250
21MMRC006	97	98	1	RC	**1.76**	1.69	**0.24**	**3.69**	85	1000	824
21MMRC006	98	99	1	RC	**1.20**	1.79	**0.10**	**3.08**	76	410	599
21MMRC006	99	100	1	RC	**0.72**	1.50	**0.05**	**2.26**	78	319	572
21MMRC006	100	101	1	RC	**0.31**	1.27	**0.22**	**1.80**	94	1010	828
21MMRC006	101	102	1	RC	**0.12**	0.53	**0.07**	**0.72**	73	331	587
21MMRC006	102	103	1	RC	**0.20**	0.97	**0.11**	**1.28**	78	391	613
21MMRC006	103	104	1	RC	**0.10**	0.58	**0.04**	**0.71**	77	295	583
21MMRC006	104	105	1	RC	**0.06**	0.33	**0.01**	**0.40**	80	209	587
21MMRC006	105	106	1	RC	**0.10**	0.57	**0.02**	**0.69**	81	268	588
21MMRC006	106	107	1	RC	**0.29**	1.02	**0.03**	**1.34**	81	302	591
21MMRC006	107	108	1	RC	**0.04**	0.11	**0.00**	**0.16**	79	139	575
21MMRC006	136	137	1	RC	**0.00**	0.01	**0.00**	**0.02**	90	310	290
21MMRC006	137	138	1	RC	**0.19**	0.45	**0.07**	**0.71**	101	2060	634
21MMRC006	138	139	1	RC	**0.03**	0.07	**0.01**	**0.11**	80	669	596
21MMRC006	139	140	1	RC	**0.55**	1.00	**0.10**	**1.65**	88	3870	939
21MMRC006	140	141	1	RC	**0.06**	0.08	**0.01**	**0.14**	105	975	1535

Hole_ID	M From	M To	Width	Sample Type	Pd	Pt	Au	2PGE+Au	Co	Cu	Ni
21MMRC007	59	60	1	RC	**0.03**	0.04	**0.28**	**0.35**	121	3230	1440
21MMRC007	60	61	1	RC	**1.81**	1.76	**0.32**	**3.89**	99	1900	982
21MMRC007	61	62	1	RC	**1.25**	2.02	**0.69**	**3.96**	89	1010	742
21MMRC007	62	63	1	RC	**0.19**	0.95	**0.14**	**1.28**	106	1470	917
21MMRC007	63	64	1	RC	**0.14**	0.52	**0.01**	**0.67**	82	252	584
21MMRC007	64	65	1	RC	**0.03**	0.04	**0.01**	**0.07**	89	257	647
21MMRC008	74	75	1	RC	**0.00**	0.00	**0.00**	**0.01**	69	148	509
21MMRC008	75	76	1	RC	**0.22**	0.38	**0.11**	**0.71**	86	1575	838
21MMRC008	76	77	1	RC	**0.61**	1.03	**0.22**	**1.85**	99	3120	1385
21MMRC008	77	78	1	RC	**0.75**	1.48	**0.33**	**2.55**	92	2960	1875
21MMRC008	78	79	1	RC	**1.25**	2.72	**0.64**	**4.60**	121	4950	3110
21MMRC008	79	80	1	RC	**0.60**	1.23	**0.30**	**2.13**	90	2600	1755
21MMRC008	80	81	1	RC	**0.09**	0.18	**0.03**	**0.30**	62	510	691
21MMRC008	81	82	1	RC	**0.03**	0.06	**0.01**	**0.10**	70	212	649
21MMRC008	82	83	1	RC	**0.06**	0.12	**0.03**	**0.20**	72	392	724
21MMRC008	83	84	1	RC	**0.16**	0.31	**0.08**	**0.56**	74	1105	986
21MMRC008	84	85	1	RC	**0.18**	0.36	**0.08**	**0.62**	93	916	1260
21MMRC008	85	86	1	RC	**0.02**	0.04	**0.01**	**0.07**	76	146	788
21MMRC008	86	87	1	RC	**0.64**	1.27	**0.30**	**2.22**	114	4180	2340
21MMRC008	87	88	1	RC	**0.35**	0.80	**0.17**	**1.32**	93	1930	1675
21MMRC008	88	89	1	RC	**0.24**	0.56	**0.13**	**0.94**	90	1295	1445
21MMRC008	89	90	1	RC	**0.19**	0.45	**0.09**	**0.73**	90	992	1380
21MMRC008	90	91	1	RC	**0.01**	0.03	**0.01**	**0.05**	71	135	836
21MMRC009	NSI										
21MMRC010	114	115	1	RC	**0.02**	0.10	**0.27**	**0.39**	119	3490	1590
21MMRC010	115	116	1	RC	**1.46**	1.35	**0.61**	**3.42**	141	3410	1735
21MMRC010	116	117	1	RC	**1.20**	2.21	**0.12**	**3.53**	73	418	646
21MMRC010	117	118	1	RC	**0.19**	0.80	**0.07**	**1.06**	71	361	599
21MMRC010	118	119	1	RC	**0.73**	2.66	**0.10**	**3.49**	97	817	925
21MMRC010	119	120	1	RC	**0.05**	0.17	**0.03**	**0.24**	77	277	595
			0	RC							
21MMRC010	131	132	1	RC	**0.01**	0.01	**0.01**	**0.03**	76	66	588
21MMRC010	132	133	1	RC	**1.05**	1.59	**0.25**	**2.89**	118	2190	1300
21MMRC010	133	134	1	RC	**0.05**	0.08	**0.01**	**0.14**	77	199	604
21MMRC010	141	142	1	RC	**0.05**	0.09	**0.01**	**0.15**	74	301	653
21MMRC010	142	143	1	RC	**0.21**	0.40	**0.05**	**0.66**	93	1420	1055
21MMRC010	143	144	1	RC	**0.01**	0.02	**0.01**	**0.03**	80	101	795
21MMRC011	141	142	1	RC	**0.00**	0.00	**0.07**	**0.07**	78	1710	757
21MMRC011	142	143	1	RC	**0.11**	0.21	**0.36**	**0.68**	98	3000	1260
21MMRC011	143	144	1	RC	**1.39**	1.94	**0.12**	**3.44**	82	609	602
21MMRC011	144	145	1	RC	**0.57**	1.40	**0.09**	**2.06**	80	533	588
21MMRC011	145	146	1	RC	**0.06**	0.27	**0.04**	**0.37**	85	787	726
21MMRC011	151	152	1	RC	**0.00**	0.01	**0.00**	**0.01**	82	154	559
21MMRC011	152	153	1	RC	**0.31**	0.74	**0.11**	**1.16**	101	2180	1115
21MMRC011	153	154	1	RC	**0.33**	0.84	**0.11**	**1.27**	106	3570	1255
21MMRC011	154	155	1	RC	**0.07**	0.14	**0.02**	**0.24**	76	688	649
21MMRC012	82	83	1	RC	**0.01**	0.10	**0.01**	**0.12**	101	1220	771
21MMRC012	83	84	1	RC	**0.31**	0.39	**0.10**	**0.80**	111	2180	1225
21MMRC012	84	85	1	RC	**0.13**	0.26	**0.03**	**0.42**	84	556	731
21MMRC012	85	86	1	RC	**0.08**	0.26	**0.02**	**0.36**	92	838	782
21MMRC012	86	87	1	RC	**0.05**	0.10	**0.03**	**0.18**	84	389	627

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Hole_ID	M From	M To	Width	Sample Type	Pd	Pt	Au	2PGE+Au	Co	Cu	Ni
21MMRC012	87	88	1	RC	**0.07**	0.12	**0.02**	**0.20**	86	302	620
21MMRC012	88	89	1	RC	**0.13**	0.31	**0.04**	**0.47**	102	826	775
21MMRC012	89	90	1	RC	**0.25**	0.55	**0.08**	**0.88**	99	1110	849
21MMRC012	90	91	1	RC	**0.28**	0.50	**0.08**	**0.85**	91	979	860
21MMRC012	91	92	1	RC	**0.83**	1.48	**0.36**	**2.66**	111	3690	1980
21MMRC012	92	93	1	RC	**1.03**	2.99	**0.42**	**4.44**	118	4300	2230
21MMRC012	93	94	1	RC	**0.22**	0.47	**0.06**	**0.76**	85	1100	920
21MMRC012	94	95	1	RC	**0.01**	0.04	**0.00**	**0.05**	80	278	594
21MMRC012	95	96	1	RC	**0.04**	0.07	**0.01**	**0.12**	91	901	732
21MMRC012	96	97	1	RC	**0.05**	0.10	**0.02**	**0.16**	93	891	752
21MMRC012	97	98	1	RC	**0.14**	0.19	**0.06**	**0.40**	104	1865	990
21MMRC012	98	99	1	RC	**0.04**	0.09	**0.02**	**0.14**	87	769	736
21MMRC012	99	100	1	RC	**0.26**	0.27	**0.09**	**0.62**	105	2140	1100
21MMRC012	100	101	1	RC	**0.21**	0.25	**0.07**	**0.53**	105	2220	1140
21MMRC012	101	102	1	RC	**0.29**	0.37	**0.31**	**0.97**	120	2870	1370
21MMRC012	102	103	1	RC	**0.12**	0.21	**0.05**	**0.38**	118	2250	1190
21MMRC012	103	104	1	RC	**0.19**	0.30	**0.07**	**0.56**	123	2530	1340
21MMRC012	104	105	1	RC	**0.12**	0.21	**0.04**	**0.37**	112	1780	1130
21MMRC012	133	134	1	RC	**0.00**	0.01	**0.00**	**0.01**	148	34	1980
21MMRC012	134	135	1	RC	**0.13**	1.09	**0.03**	**1.25**	167	1185	2350
21MMRC012	135	136	1	RC	**0.27**	1.07	**0.04**	**1.38**	148	512	2370
21MMRC012	136	137	1	RC	**0.01**	0.05	**0.00**	**0.07**	150	84	2040
21MMRC013	103	104	1	RC	**0.03**	0.05	**0.15**	**0.23**	88	2080	1000
21MMRC013	104	105	1	RC	**1.12**	1.06	**0.34**	**2.51**	88	1230	808
21MMRC013	105	106	1	RC	**0.77**	1.32	**0.06**	**2.14**	81	285	544
21MMRC013	106	107	1	RC	**0.30**	0.86	**0.07**	**1.23**	105	839	765
21MMRC013	107	108	1	RC	**0.15**	0.67	**0.06**	**0.88**	112	1090	918
21MMRC013	108	109	1	RC	**0.03**	0.05	**0.02**	**0.10**	108	1730	899
21MMRC013	109	110	1	RC	**0.04**	0.21	**0.03**	**0.28**	154	5250	1790
21MMRC013	110	111	1	RC	**0.03**	0.07	**0.01**	**0.11**	85	1010	736
21MMRC013	111	112	1	RC	**0.08**	0.18	**0.03**	**0.29**	76	517	592
21MMRC013	112	113	1	RC	**0.19**	0.41	**0.10**	**0.70**	97	1040	898
21MMRC013	113	114	1	RC	**0.16**	0.36	**0.07**	**0.59**	100	1260	928
21MMRC013	114	115	1	RC	**0.00**	0.02	**0.01**	**0.03**	66	122	466
21MMRC013	130	131	1	RC	**0.05**	0.10	**0.02**	**0.16**	53	274	445
21MMRC013	131	132	1	RC	**0.23**	0.49	**0.09**	**0.82**	86	1180	929
21MMRC013	132	133	1	RC	**0.01**	0.03	**0.00**	**0.04**	73	244	527
21MMRC014	NSI										
21MMRC015	99	100	1	RC	**0.13**	0.13	**0.06**	**0.32**	80	1670	576
21MMRC015	100	101	1	RC	**0.18**	0.75	**0.07**	**1.00**	88	1915	656
21MMRC015	101	102	1	RC	**0.27**	0.72	**0.14**	**1.13**	89	3200	1100
21MMRC015	102	103	1	RC	**0.20**	0.50	**0.10**	**0.80**	92	2420	915
21MMRC015	103	104	1	RC	**0.05**	0.22	**0.01**	**0.28**	94	621	489

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SECTION 1 SAMPLING TECHNIQUES AND DATA

(Criteria in this section apply to all succeeding sections.)

Criteria		Commentary
Sampling techniques	*Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.* *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.* *Aspects of the determination of mineralisation that are Material to the Public Report.* *In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.*	Reverse circulation drilling was used to obtain both 2m composite and one metre samples, using a 5 ¼" face sampling hammer. Samples were collected on a 2m composite basis to a prescribed depth predetermined by previous drilling, wireframing and assay data. Once the predetermined depth is achieved, the sampling reverts to one metre sample through the orezone to EOH. After composite sample results received, all samples that return a value of >0.1g/t Au will result in the resplitting of the one metre bulk bags at site using a 75:25 jones riffle splitter. These one metre samples are then submitted for analysis. All samples are pulverized to produce a 50g charge for fire assay. Drilling sampling techniques employed at the Artemis core facility include saw cut HQ (63mm) drill core samples. Both RC and HQ wireline core is currently being used to drill out the geological sequences and identify zones of mineralisation that may or may not be used in any Mineral Resource estimations, mining studies or metallurgical testwork. Duplicate samples were collected at the rig from a static cone splitter, with the primary and duplicate bag both simultaneously collected from separate chutes. For RC, the cyclone was cleared between rod changes to minimise contamination.
Drilling techniques	*Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).*	Reverse Circulation drilling completed by Topdrill. Drilling was completed using a truck mounted T685 Schramm rig mounted on 8x8 trucks This can produce 1000psi/2700CFM with an axillary booster which is capable of achieving dry samples at depths of around 300m.
Drill sample recovery	*Method of recording and assessing core and chip sample recoveries and results assessed.* *Measures taken to maximise sample recovery and ensure representative nature of the samples.* *Whether a relationship exists between sample recovery and grade and whether*	Recoveries are recorded on logging sheets along with encounters with water and whether the samples are dry, moist or wet. Drilling recoveries for Reverse Circulation drilling were >80% with some exceptions that maybe caused by loss of return through faults or encounters with water. >90% of samples returned dry.

Criteria		Commentary
	sample bias may have occurred due to preferential loss/gain of fine/coarse material.	Statistical analysis shows that no bias of grade exists due to recoveries
Logging	*Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.* *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.* *The total length and percentage of the relevant intersections logged.*	RC samples were collected from the static cone splitter as two samples, one bulk sample and one primary (analytical) sample. The bulk samples are one metre splits. These bags are then placed in neat rows of 50 bags each clear of the rig for safety reasons. A field technician mixes the bag by hand before taking a sample using a sieve and sieves the sample to remove fines. The sieved sample is then transferred to a wet sieve in a bucket of water, and the sample is sieved further until rock fragments are clearly visible. These rock fragments are then logged by the site geologist, taking note of colour, grainsize, rock type, alteration if any, mineralisation if any, veining if any, structural information if notable and any other relevant information. This information is then written down on pre-printed logging sheets, using codes to describe the attributes of the geology. A representative sample is transferred to pre-labelled chip trays into the corresponding depth from where the sample was drilled from. The remainder of the sample from the sieve is then transferred into a core tray that has been marked up by depths at metre intervals. An identification sheet noting the hole number and from-to depths that correspond to each tray is then written up and placed above the tray and a photograph is taken of the chips. The hole is logged in its entirety, hence 100% The geological data would be suitable for inclusion in a Mineral Resource Estimation (MRE)
Sub-sampling techniques and sample preparation	*If core, whether cut or sawn and whether quarter, half or all core taken.* *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.* *For all sample types, the nature, quality and appropriateness of the sample preparation technique.* *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* *Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance*	RC samples were collected on the drill rig using a cone splitter. If any mineralised samples were collected wet these were noted in the drill logs and database. The RC drilling rig is equipped with a rig-mounted cyclone and static cone splitter, which provided one bulk sample of approximately 20-30 kilograms, and a sub-sample of approximately 2-4 kilograms for every metre drilled. Field QC procedures involve the use of Certified Reference Materials (CRM's) as assay standards, along with duplicates and blank samples. The insertion rate of these was approximately 1:20. For RC drilling, field duplicates were taken on a routine basis at approximately 1:20 ratio using the

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Criteria		Commentary
	results for field duplicate/second-half sampling. *Whether sample sizes are appropriate to the grain size of the material being sampled.*	same sampling techniques (i.e. cone splitter) and inserted into the sample run. Primary and duplicates results have been compared. The sample sizes are appropriate, representative and are considered more than adequate to ensure that there are no particle size effects relating to the grain size of the mineralisation.
Quality of assay data and laboratory tests	*The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* *For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.* *Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.*	All samples were assayed by ALS-Chemex (ALS) in Perth, which is a National Association of Testing Authorities (NATA) Australia accredited organisation. The laboratory techniques below are for all samples submitted to ALS and are considered appropriate for the style of mineralisation defined within the Carlow Castle Project area The sample preparation followed industry best practice. Fire assay samples were dried, coarse crushing to ~10mm, split to 300g subsample, followed by pulverisation in an LM5 or equivalent pulverising mill to a grind size of 85% passing 75 micron. This fraction was split again down to a 50g charge for fire assay Both 30g and 50g sample sizes were chosen for analysis of gold, with fire assay (Au-AA26) with ICP finish and determination by AAS. The limit of 100 g/t was not reached for any samples. The larger sample size of 50g was predominantly selected to provide greater confidence in the analyses. All samples were dried, crushed, pulverised and split to produce a sub-sample of 50g which is digested and refluxed with hydrofluoric, nitric, hydrochloric and perchloric acid (4 acid digest). This digest is considered a total dissolution for most minerals. Analytical analysis is performed using ICP-AES Finish (ME-ICP61A) for Ag, Al, As, Ba, Be, Bi, Ca, Cd, Co, Cr, Cu, Fe, Ga, K, La, Mg, Mn, Mo, Na, Ni, P, Pb, S, Sb, Sc, Sr, Th, Ti, Tl, U, V, W, Zn. The original assay technique used for copper and cobalt was 0.25 g sample with four acid digest and ICP-AES finish. When the upper limits of the range recommended by the lab were exceeded, a method more appropriate method was used to re-assay another sample of the pulp. For assays that reached the limits of 1% for the 30 g, the laboratory method ME-ICP61A was triggered, using 0.40 g samples with the same liberation and finish techniques. Standards are matrix matched by using previous pulps from drilling programs and homogenised using certified laboratories. Standards were analysed by round robins to determine grade.

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Criteria		Commentary
		Standards were routinely inserted into the sample run at 1:20. Laboratory standards and blank samples were inserted at regular intervals and some duplicate samples were taken for QC checks.
Verification of sampling and assaying	*The verification of significant intersections by either independent or alternative company personnel.* *The use of twinned holes.* *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.* *Discuss any adjustment to assay data.*	Sampling was undertaken by field assistants supervised by experienced geologists from Artemis Resources. Significant intercepts were checked by senior personnel who confirmed them as prospective for gold mineralisation. No twin holes using RC was completed in this program. Electronic data capture on excel spreadsheets which are then uploaded as .csv files and routinely sent to certified database management provider. Routine QC checks performed by Artemis senior personnel and by database management consultant. PDF laboratory certificates are stored on the server and are checked by the Exploration Manager.
Location of data points	*Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* *Specification of the grid system used.* *Quality and adequacy of topographic control.*	A Garmin GPSMap62 hand-held GPS was used to define the location of the initial drill hole collars. Standard practice is for the GPS to be left at the site of the collar for a period of 5 minutes to obtain a steady reading. Collar locations are considered to be accurate to within 5m. A high-quality downhole north-seeking multi-shot or continuous survey gyro-camera was used to determine the dip and azimuth of the hole at 30m intervals down the hole The topographic surface was calculated from the onsite mine survey pickups and subsequently verified by RTK GNSS collar surveys. Zone 50 (GDA 94). Surface collar coordinates are surveyed via RTK GNSS with 1cm accuracy by a professional surveying contractor.
Data spacing and distribution	*Data spacing for reporting of Exploration Results.* *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.* *Whether sample compositing has been applied.*	In certain areas, current drill hole spacing is variable and dependent on specific geological, and geochemical targets. A nominal 40x20m drill spacing is considered adequate to establish the degree of geological and grade continuity appropriate for JORC (2012) classifications applied. No sample compositing to date has been used for drilling completed by Artemis. All results reported are the result of 1 metre downhole sample intervals.

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Criteria		Commentary
Orientation of data in relation to geological structure	*Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	Drill holes were designed to be perpendicular to the strike of known mineralisation. Due to the structural and geological complexity of the area, mineralisation of unknown orientation can be intersected.
Sample security	*The measures taken to ensure sample security.*	The chain of custody is managed by the supervising geologist who places calico sample bags in polyweave sacks. Up to 10 calico sample bags are placed in each sack. Each sack is clearly labelled with: Artemis Resources Ltd Address of laboratory Sample range Samples were delivered by Artemis personnel to the transport company in Karratha and shrink wrapped onto pallets. The transport company then delivers the samples directly to the laboratory.
Audits or reviews	*The results of any audits or reviews of sampling techniques and data.*	Data is validated upon up-loading into the master database. Any validation issues identified are investigated prior to reporting of results.

SECTION 2 REPORTING OF EXPLORATION RESULTS

(Criteria listed in the preceding section also apply to this section.)

Criteria		Commentary
Mineral tenement and land tenure status	*Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.* *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.*	Drilling by Artemis was carried out on E47/1797 – 100% owned by Artemis Resources Ltd. This tenement forms a part of a broader tenement package that comprises the West Pilbara Project. This tenement is in good standing.
Exploration done by other parties	*Acknowledgment and appraisal of exploration by other parties.*	The most significant work to have been completed historically in the Carlow Castle area, including the Little Fortune and Good Luck prospects, was completed by Open Pit Mining Limited between 1985 and 1987, and subsequently Legend Mining NL between 1995 and 2008. Work completed by Open Pit consisted of geological mapping, geophysical surveying (IP), and RC drilling and sampling.

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Criteria		Commentary
		Work completed by Legend Mining Ltd consisted of geological mapping and further RC drilling. Legend also completed an airborne ATEM survey over the project area, with follow up ground-based FLTEM surveying. Re-processing of this data was completed by Artemis and was critical in developing drill targets for the completed RC drilling. Compilation and assessment of historic drilling and mapping data completed by both Open Pit and Legend has indicated that this data is compares well with data collected to date by Artemis. Validation and compilation of historic data is ongoing. All exploration and analysis techniques conducted by both Open Pit and Legend are considered to have been appropriate for the style of deposit.
Geology	*Deposit type, geological setting and style of mineralisation.*	The Carlow Castle Co-Cu-Au prospect includes a number of mineralised shear zones, located on the northern margin of the Andover Intrusive Complex. Mineralisation is exposed in numerous workings at surface along quartz-rich shear zones. Both oxide and sulphide mineralisation are evident at surface associated with these shear zones. Sulphide mineralisation appears to consist of Chalcopyrite, chalcocite, cobaltite, pyrrhotite and pyrite
Drill hole Information	*A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:* *easting and northing of the drill hole collar* *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar* *dip and azimuth of the hole* *down hole length and interception depth* *hole length.* *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*	Drill hole information is contained within this release.
Data aggregation methods	*In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.* *Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation*	All intervals reported are composed of 1 metre down hole intervals for Reverse Circulation drilling. Aggregated intercepts do include reported lengths of higher-grade internal intercepts. No upper or lower cut-off grades have been used in reporting results. No metal equivalent calculations are used in this report.

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Criteria		Commentary
	should be stated and some typical examples of such aggregations should be shown in detail. *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	
Relationship between mineralisation widths and intercept lengths	*These relationships are particularly important in the reporting of Exploration Results.* *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.* *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').*	The mineralisation in the Carlow Castle Western Zone strikes generally E-W and dips to the north at approximately -75 to -80 degrees. The drill orientation was 180 -60 dip. Drilling is believed to be generally perpendicular to strike. Given the angle of the drill holes and the interpreted dip of the host rocks and mineralisation, reported intercepts approximate true width. True thicknesses are calculated from interpretation deriving from orientation of high-grade intervals, orientation of the main mineralised trend and its dip. This is an estimation only and can change according to additional information.
Diagrams	*Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.*	Appropriate plans are shown in the text.
Balanced reporting	*Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	This release reports the results of five RC holes. The significant results tabulated in the release are reported at a base grade of >0.5 g/t Au or >0.5% Cu. Internal dilution of up to 2 m may be included in an intersection.
Other substantive exploration data	*Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	Targeting for the RC drilling completed by Artemis was based on compilation of historic exploration data, and the surface expression of the targeted mineralised shear zones and associated historic workings.
Further work	*The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).* *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	Further work (RC and diamond drilling) is justified to locate extensions to mineralisation both at depth and along strike.

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SECTION 3 – Estimation and Reporting of Mineral Resources

Criteria	JORC Code explanation	Commentary
Database integrity	*Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.*	Geophysical files were uploaded from the data logging device to the contractor's central storage database and then provided in both raw and corrected/filtered format in CSV, LAS and PDF format. This has removed the potential for transcription errors and for reference checks. Core logging was completed by Artemis on site using project-specific logging codes and a database management system; DataShed™, with primary key fields and look-up tables. Collar survey, down hole survey and assay files were loaded from source files using templates to load into predefined tables. These measures enforced strict referential integrity and validation rules to prevent corruption errors. The Competent Person found no material errors and deemed the database was fit for the purpose of Mineral Resource estimation.
	Data validation procedures used.	The Competent Person checked the drillhole files for the following errors prior to Mineral Resource estimation: • Absent collar data • Multiple collar entries • Questionable downhole survey results • Absent survey data • Overlapping intervals • Negative sample lengths • Sample intervals which extended beyond the hole depth defined in the collar table. • Assay values reported as negative detection limits were updated to half detection limits.
Site visits	*Comment on any site visits undertaken by the Competent Person and the outcome of those visits.*	The Competent Person has not visited the site, but has relied on information from colleague Mr Matt Clark, Senior Resource Geologist, collected during a site visit in April 2021.
	If no site visits have been undertaken, indicate why this is the case.	The Competent Person considers that the information provided to him by colleague Mr Matt Clark allows him to appropriately consider the necessary factors in establishing Mineral Resources for the confidence estimated.
Geological interpretation	*Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.*	The host lithologies at Carlow Castle are basalt and gabbro, with mineralisation predominantly in basalt with a strong lithological control on mineralisation between basalt and gabbro. The dominant control on mineralisation is by structures potentially far smaller than the drill hole spacing and smaller than which can be explicitly modelled. Therefore, the geological model consisted of waste and mineralisation.
	Nature of the data used and of any assumptions made.	No material assumptions have been made which affect the MRE reported herein.
	The effect, if any, of alternative interpretations on Mineral Resource estimation.	The Competent Person is confident any alternative interpretations would result in globally immaterial differences in the Mineral Resource estimate.
	The use of geology in guiding and controlling Mineral Resource estimation.	Mineralisation generally shows a continuous grade distribution from un-mineralised through to high grade, with minor inflection points within the log-probability plot

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	The factors affecting continuity both of grade and geology.	for the distribution. One such inflection occurs at 200 ppm Cu, on which definition of mineralisation lodes were based. A second cut-off at 500 ppm correlated with high-grade copper, gold, and cobalt, and also correlated with structural measurements defined by structural logging and modelling. The geological model includes a shallow, approximately 3 m thick overburden surface and an oxide horizon that averages 40 m depth. Transitional material is typically 10 to 20 m thick and extends down to 100 m depth in the eastern section of Carlow Main.
Dimensions	*The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.*	The Carlow Main lodes have been modelled as a set of anastomosing fingers extending off and conjoining a major central zone that follows a broad sigmoidal curve whose average centreline at 769,660 mN strikes 1,200m east-west. The anastomosing lodes vary in thickness from 5 m where they pinch to 90 m in the thickest portion. The high-grade 500 ppm copper shell averages 30-40m thick, within the low-grade 200 ppm copper wireframe that extends up to 50 m to the north and south. At the western end, mineralisation dips steeply north, and at the eastern end it dips steeply south. Mineralisation in Carlow Main has been interpreted to a maximum of 630 m below surface, averaging 280 m. The Quod Est and Cross Cut mineralisation have been modelled similarly with low-grade 200 ppm copper shell and inner high-grade 500 ppm grade shells. Quod Est and Cross-Cut lodes have been interpreted as a steeply east dipping lodes. The major lode at Quod Est outcrops and strikes NNE, bifurcates at its southern third, and measures about 200 m overall, with maximum depth of 180 m. The Cross Cut mineralisation has been interpreted as two lode structures that strike 150 m NNE and dip steeply east, to a maximum depth of 180 m.
Estimation and modelling techniques	*The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen, include a description of computer software and parameters used*	The Mineral Resources were estimated within nine estimation domains, representing Carlow Castle Main, Quod Est and Cross Cut, formed from the mineralisation model interpreted at nominal cut-offs of 200 ppm and 500 ppm Cu. The domains were further split into overburden, oxide and fresh by the oxidation wireframes. A small volume wireframe was modelled in the eastern section of Carlow Main based on a 0.5 g/t Au cut-off to control the influence of high-grade holes that were drilled subparallel to mineralisation. All geological modelling was undertaken using Leapfrog Geo software. Estimation domains were modelled using indicator interpolants and the nominal 200 ppm Cu, 500 ppm Cu, and 0.5 g/t Au cut-off grades. Statistics, grade and density estimates, and variography, were undertaken in Supervisor software, and composite selection and block coding, undertaken in Surpac software, used the combined domains as hard boundaries. Samples were composited to 1 m intervals based on assessment of the raw drillhole sample interval lengths. Quantitative Kriging Neighbourhood Analysis (QKNA) was undertaken using Supervisor software to assess the effect

Criteria	JORC Code explanation	Commentary
		of changing key kriging neighbourhood parameters on block grade and density estimates. Kriging Efficiency and Slope of Regression were determined for a range of block sizes, minimum and maximum samples, search dimensions and discretisation grids. A two-pass search ellipse strategy was adopted, whereby the first pass equated to the full range of the relevant variogram model for each domain, with a minimum of 8 samples, maximum of 20 samples and a maximum of 6 samples per hole. The second pass search ellipse was between 2 to 3.5-times the variogram model range, with a minimum of 8 samples, maximum of 16 samples and a maximum of 6 samples per hole. All blocks were filled in the first two passes. A 20 mE x 10 mN x 10 mRL parent cell size was constructed covering the full volume of the mineralisation and additional space for mine infrastructure planning. Sub-celling was employed to 5 mE x 5 mN x 5 mRL to improve block volume fitting to the complex wireframe. Mineralisation domains were coded in the block model below the overburden surface, and further coded by oxidation domain. High grade cuts were used to constrain outliers in the dataset as described above. Grade interpolation for Au, Cu, Co, As, S was completed using ordinary kriging (OK) into the parent block cells. The search employed a dynamic anisotropy to allow the ellipse to rotate along the sinusoidal mineralisation domains.
	The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.	Several previous historical resource estimates have been completed previously. These reports were available to the Competent Person. These did not necessarily cover the same area as this Mineral Resource update and were volumetrically smaller in their extent. Further; while these Previous Mineral Resources are quoted below, the approach taken to modelling and estimation differs fundamentally from that of the current estimate Consequently, the models are not directly comparable. In 2018, Mr Philip Jones estimated Mineral Resources reported in accordance with the JORC Code for Carlow South using drilling data provided by Artemis to model mineralisation wireframes that were based on a total net smelter return of >$30 using the following metal factors: • Copper: Price: $4.473/lb; Recoveries: 75% (mining and metallurgical recovery) • Gold: Price: $USD1282.10/oz; Recoveries: 90% (mining and metallurgical) • Cobalt: Price: $54,500/t; Recoveries: 75% mining and metallurgical In January 2019 Al Maynard & Associates estimated Inferred Mineral Resources at Carlow Castle South and Quod Est of 7.7 Mt @ 0.51% Cu, 1.06 g/t Au and 0.08% Co. Four domains, based on the strike of the mineralisation, were used in the modelling. High grade cuts were also applied using mean grades +2SD of copper, gold and cobalt per domain. Grades were interpolated by Inverse Distance Squared (ID^2).

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		In November 2019, CSA Global estimated Inferred Mineral Resources at Carlow Castle South and Quod Est of 8 Mt @ 0.6% Cu, 1.6 g/t Au and 0.08% Co, reported above a lower cut-off of 0.3% Cu, and within a theoretical optimised pit shell. Two estimation domains for Carlow Main and Quod Est were used in the modelling based on a lower cut-off grade of 500 ppm copper. Grade interpolation was completed initially by ordinary kriging into panels, with post-processing using localised uniform conditioning (LUC) within the panels to derive an estimate at the smaller selective mining unit (SMU) scale. Grade limiting was employed in the panel estimates to restrict the influence of very high grades to 10 m. The optimised pit shell used for the Mineral Resource reporting used the following parameters: • 50° overall slope angle • Oxide and Fresh used same recoveries/processing costs • $48.1/t processing cost • 85% copper recovery • 94.8% gold recovery • 73% cobalt recovery • Mining costs $/t incremented by depth ranging from $2.57 through to $5.77 inclusive. • Copper: $9000/t • Gold: $2000/oz • Cobalt: $48,000/t
	The assumptions made regarding recovery of by-products.	The co-products, gold and cobalt, are assumed to be recoverable within the mineralisation wireframe volumes that have been modelled on a copper grade cut-off. The metallurgical testwork for gold and cobalt may not be representative of the material reported as Mineral Resources. However, the metallurgical testwork results show that gold and cobalt can be recovered.
	Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulphur for acid mine drainage characterisation).	Arsenic and sulphur have been estimated, although it is unknown at this stage of the project if they are deleterious for copper, gold and cobalt.
	In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.	The dimensions of the parent block used for estimation represents approximately half the drillhole spacing in the X orientation and one quarter the spacing in the Y orientation.
	Any assumptions behind modelling of selective mining units.	SMU units were not modelled. The parent block size of 10 m in the Z direction is approximately twice the size of assumed SMU of 5 m high mining benches. The assumed SMU has been determined based on the assumption of a production scenario utilising small to medium size earthmoving equipment (for reference; 125 tonne excavator, plus CAT 777 or equivalent haul trucks). In the experience of the Competent Person, this

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		equipment selection may be considered typical for a deposit of the size and style of Carlow Castle.
	Any assumptions about correlation between variables	No assumptions have been made regarding the correlation of variables.
	Description of how the geological interpretation was used to control the resource estimates.	Logged geology, alteration and structural controls were used in the interpretation of lodes within the resource model. Hard boundaries were used for estimation between mineralised domains.
	Discussion of basis for using or not using grade cutting or capping.	For the estimate of grades, high-grade cuts were applied to reduce the influence of extreme outliers. These values, determined by statistical analysis including review of CV values, histograms, log-probability plots and mean-variance plots.
	The process of validation, the checking process used, the comparison of model data to drillhole data, and use of reconciliation data if available.	Standard model validation was completed using numerical methods (histogram and swath plots) and validated visually in section and 3D against the input raw drillhole data, composites and blocks.
Moisture	*Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	Tonnages have been estimated on a dry basis.
Cut-off parameters	*The basis of the adopted cut-off grade(s) or quality parameters applied.*	The Mineral Resources were reported at a 0.3 ppm Au.Eq cut-off, within a Whittle™ theoretical optimisation that used the following factors: • 50° overall slope angle • Oxide, Transitional and Fresh used same recoveries / processing costs • $48.1 / tonne processing (includes refining, insurance and G&A) • Recoveries, which in Artemis' opinion have a reasonable potential to be achieved, are: • 85% Cu recovery • 94.8% Au recovery • 73% Co recovery • Mining Costs $ / tonne incremented by depth (coded into each block in the model by RL), ranging from $2.57 through to $5.77 inclusive • Prices: ○ Cu $9,400 / tonne ○ Au $2,200 / oz ○ Co $50,000 / tonne • 2.5% royalty per ounce payable on gold produced. 5% royalties per tonne payable on both copper and cobalt produced. • Au.Eq was calculated from a combined weighted grade of Au, Cu, Co using the same commodity prices and metallurgical recoveries as the optimisation. Au.Eq = Au (ppm) + Cu (%)x1.19 + Co (%) x 5.44
Mining factors or assumptions	*Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for*	Open pit mining is considered as the appropriate method for future studies, and the Competent Person believes that there are reasonable prospects for eventual economic extraction based on the outputs of the Whittle optimisation completed.

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Criteria	JORC Code explanation	Commentary
	eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.	A minimum mining width of 2 m was applied (downhole composite width). No other mining assumptions were made. Detailed mining assumptions such as dilution and minimum mining widths will be included in any optimisation, detailed mine planning and Life of Mine plan.
Metallurgical factors or assumptions	*The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.*	Preliminary metallurgical testwork was conducted by ALS Metallurgy in 2019 focussing on the metallurgical amenability of selected samples to a conventional gravity gold, cyanide leach and flotation processes. Results are detailed below: Gold • 48% of gold by testwork on metallurgical samples was recovered using gravity separation, and most of the balance of the non-gravity gold is recoverable in sulphide concentrates as a by-product using standard flotation. Copper • Quick floating copper minerals produced a high-grade, premium copper concentrate of approximately 30% Cu. • Deleterious elements including arsenic may be managed with a light concentrate polishing using regrind or blend control. Recoveries depended on mineralogy, with 77–85% copper recoveries achieved. • Unrecovered copper minerals are predominantly represented by non-floating silicates or secondary oxide copper minerals. Cobalt • Cobalt recoveries ranged from 73–79%. Saleable Cobalt concentrate grades ranging 2.3–5.3% Co were produced. Cobaltite (CoAsS) is the dominant cobalt bearing mineral and is therefore intrinsically linked to arsenic affecting its sale price. Artemis believe the gold recovered by metallurgical testwork could be sold in concentrates as a credit or recovered on site using a cyanide leach process. Acid soluble copper testwork has been completed for oxide and transitional ore and estimated in the block model by inverse distance (ID2) to guide additional metallurgical sampling. CSA Global recommend additional metallurgical programs across the Mineral Resource incorporating results from acid soluble copper and multi-element analysis. Further geometallurgical testwork to develop quantitative mineralogy and rock mass studies is also recommended.
Environmental factors or assumptions	*Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the*	No assumptions regarding possible waste and process residue disposal options have been made. Sulphur and arsenic have been estimated into the model to allow the assessment of potentially acid forming minerals and other environmentally sensitive residue.

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	determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered, this should be reported with an explanation of the environmental assumptions made.	
Bulk density	*Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.*	For mineralisation, downhole geophysical gamma density was used to estimate density by OK using the relevant variogram and estimation parameters for each statistical domain. Only sample points that had a calliper measurement of not more than 20% of the nominal hole diameter for each hole type were included in the analysis and data for estimation. The gamma density was visually correlated point-by-point to each overlapping water immersion determination of specific gravity on HQ3 core, which found a strong correlation. The size and range of lengths of density determinations are considered by the Competent Person to be robust. A correlation of 0.05 was calculated between sample lengths and density determinations, confirming that the sample length has no impact on the density. The gamma-density of the RC hole is weakly low-biased compared to the diamond core density, while the gamma-density of the diamond hole is very weakly high-biased. Sample points were composited to 1 m length prior to estimation. Waste densities were applied from nominal values.
	The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc.), moisture and differences between rock and alteration zones within the deposit.	The gamma determines a quantitative, in situ measurement of density that accounts for void spaces. The measurements have been calibrated to regular calibration holes in iron ore deposits in the Pilbara, and on materials at the contractor's facility. The water immersion method measurements were determined by measuring the weight of part or the entire sample in air and water and then applying the formula bulk density = weight_air/(weight_air-weight_water). Samples of drill core were sealed with a masonry sealant/wax and allowed to dry prior to bulk density determination. The estimate of density was undertaken within oxidation domains in the mineralisation.
	Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.	The gamma density data were considered sufficient in number for all material types, quantitative and unbiased when large calliper deviations from the nominal hole diameter were removed. Calibration was undertaken using comparison to other holes and to density measured by water immersion. The approach adopted is considered robust.
Classification	*The basis for the classification of the Mineral Resources into varying confidence categories.*	The MRE was classified as Inferred based on the level of geological understanding of the mineralisation, quality of samples, density data, drillhole spacing, historical nature of the drilling, detail of metallurgical information available

Criteria	JORC Code explanation	Commentary
		for soluble / insoluble copper speciation and sampling and assaying processes.
	Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).	The classification reflects the overall level of confidence in mineralised domain continuity based the mineralisation drill sample data numbers, spacing and orientation. Overall mineralisation trends are reasonably consistent within the various lithotypes over numerous drill sections.
	Whether the result appropriately reflects the Competent Person's view of the deposit.	The Mineral Resource classifications applied appropriately reflect the view of the Competent Person.
Audits or reviews	*The results of any audits or reviews of Mineral Resource estimates.*	Internal audits were completed by CSA Global which verified the technical inputs, methodology, parameters and results of the estimate.
Discussion of relative accuracy/ confidence	*Where appropriate, a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.*	The accuracy of the MREs is communicated through the classification assigned to the various parts of the deposits. The MREs have been classified in accordance with the JORC Code (2012 Edition) using a qualitative approach. All factors that have been considered have been adequately communicated in Section 1 and Section 3 of this table. The MRE statement relates to a global estimate of in-situ tonnes and grade.
	The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.	The accuracy of the MREs is communicated through the Inferred classification assigned to the deposit. The MRE has been classified in accordance with the JORC Code. All factors that have been considered have been adequately communicated in Section 1, Section 2 and Section 3 of this table. The MRE statement relates to a global estimate of in-situ tonnes and grade.
	These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.	No production data are available.

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