ASX ANNOUNCEMENT

21 March 2023

A.B.N. 11 009 341 539

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EKJV Mineral Resource and Ore Reserve Statement

ASX:TBR

Board of Directors

Mr Otakar Demis
Chairman & Joint Company Secretary

Mr Anton Billis
Managing Director

Mr Gordon Sklenka
Non-Executive Director

Mr Stephen Buckley
Company Secretary

Tribune Resources Ltd (**ASX code: TBR**) has pleasure in providing the attached EKJV Mineral Resource and Ore Reserve Statement (**Statement**) as provided by Evolution Mining Limited.

The information contained within the attached Statement has been prepared by Evolution Mining and Tribune makes no comment on its accuracy or completeness.

The EKJV is located 25km west north west of Kalgoorlie and 47km north east of Coolgardie. The EKJV is between Rand (12.25%), Tribune Resources Ltd (36.75%) and Evolution Mining Limited (51%).

This report has been released with the approval of the Board of Tribune Resources Limited.

-ENDS-

For further information, please contact:

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East Kundana Joint Venture

Mineral Resource and Ore Reserve Statement

December 31, 2022

Competent Persons Statement

The information in this Mineral Resource & Ore Reserves statement that relates to the December 31, 2022 reported MGO Mineral Resources is based on information compiled by Bradley Daddow who is a Competent Person employed by Evolution Mining on a full-time basis. Mr Daddow is a Member of the Australasian Institute of Geoscientists and has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity which he has undertaken to qualify as a Competent Person as defined in the 2012 Edition of the "Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves". Mr Daddow consents to the inclusion in this report of the matters based on his information in the form and context in which it appears. A signed consent form is contained within Appendix B.

The information in this Mineral Resource & Ore Reserves statement that relates to the December 31, 2022 reported MGO Ore Reserves has been compiled as follows:

The information in this Mineral Resource & Ore Reserves statement that relates to the December 31, 2022 reported MGO Ore Reserves is based on information compiled by Blake Callinan who is a Competent Person employed on a full-time basis by Evolution Mining and is a Member of the Australasian Institute of Mining and Metallurgy. Mr Callinan has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity which he has undertaken to qualify as a Competent Person as defined in the 2012 Edition of the "Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves". Mr Callinan consents to the inclusion in this report of the matters based on his information in the form and context in which it appears. A signed consent form is contained within Appendix B.

Evolution Mining employees acting as a Competent Person may hold equity in Evolution Mining Limited and may be entitled to participate in Evolution's executive equity long-term incentive plan, details of which are included in Evolution's annual Remuneration Report. Annual replacement of depleted Ore Reserves is one of the performance measures of Evolution's long-term incentive plans.

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East Kundana Joint Venture (EKJV) Mineral Resource Statement

The East Kundana Joint Venture (EKJV) Mineral Resource statement included with this announcement has been prepared in accordance with the 2012 Edition of the "Australasian Code for reporting of Exploration Results, Mineral Resources and Ore Reserves" (the JORC Code 2012) and the ASX Listing Rules.

This Material Information summary has been provided for the East Kundana Joint Venture (EKJV) Mineral Resource pursuant to ASX Listing Rules 5.8 and 5.9 and the Assessment and Reporting Criteria in accordance with JORC Code 2012 requirements. The Assessment and Reporting Criteria in accordance with JORC Code 2012 – Table 1 is presented in Appendix A.

The December 2022 EKJV Mineral Resource is estimated at 11.0 million tonnes at 4.80g/t gold for 1.7 million ounces of contained gold (Table 1), a net increase of 82,000 ounces of gold (+5%) compared to the December 2021 estimate of 9.1 million tonnes at 5.41g/t gold for 1.6 million ounces of contained gold (Table 2).

The Mineral Resource was reported within A$2,200/oz optimised mining shapes and is inclusive of Ore Reserves but excludes mined areas and areas sterilised by mining activities.

Table 1. East Kundana Joint Venture (EKJV) Total Mineral Resource reported to 31st December 2022

Prospect	Type	Cut-Off	Measured			Indicated			Inferred			Total Resource		
			Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)
Hornet OP	OP	0.32	-	-	-	0.17	3.42	19	0.18	1.55	9	0.35	2.47	28
Golden Hind	OP	0.32	-	-	-	0.21	2.53	18	0.00	0.60	0	0.22	2.53	18
Pegasus	OP	0.31	-	-	-	0.01	19.80	5	0.00	0.90	0	0.01	15.77	5
Hornet	UG	2.44	0.04	4.19	6	0.45	3.64	52	1.00	4.12	133	1.49	3.98	191
Pegasus-Drake	UG	2.44	0.19	6.77	42	1.34	7.31	315	0.25	3.81	31	1.79	6.75	389
Pode/Hera	UG	2.44	0.51	5.02	97	0.79	3.75	116	0.37	3.17	46	1.68	4.80	259
Raleigh	UG	2.44	0.39	7.20	91	0.63	6.36	129	0.30	3.85	37	1.32	6.04	257
Raleigh-Sadler	UG	2.44	-	-	-	0.19	6.40	38	0.03	4.90	4	0.22	5.96	42
Golden Hind	UG	1.71	-	-	-	0.14	4.07	18	0.25	3.65	30	0.39	3.80	48
Rubicon-Nugget	UG	2.44	0.36	3.88	45	0.83	3.91	104	0.08	4.54	12	1.27	3.94	161
Falcon	UG	2.44	-	-	-	-	-	-	0.27	5.02	44	0.27	5.02	44
Star Trek	UG	2.44	-	-	-	-	-	-	1.55	4.19	209	1.55	4.19	209
Stockpiles	SP		-	-	-	0.19	1.52	9	-	-	-	0.19	1.52	9
TOTAL (100%) EKJV			**1.51**	**5.80**	**281**	**4.95**	**5.17**	**823**	**4.29**	**4.01**	**554**	**10.75**	**4.80**	**1,659**

Data is reported to significant figures to reflect appropriate precision and may not sum precisely due to rounding.
Mineral Resources are Reported inclusive of Ore Reserves

Table 2. Comparison of December 2022 and December 2022 East Kundana Joint Venture (EKJV) Mineral Resource

Period	Measured			Indicated			Inferred			Total		
	Tonnes (Mt)	Grade Au (g/t)	Gold Metal (koz)	Tonnes (Mt)	Grade Au (g/t)	Gold Metal (koz)	Tonnes (Mt)	Grade Au (g/t)	Gold Metal (koz)	Tonnes (Mt)	Grade Au (g/t)	Gold Metal (koz)
Dec-21	1.69	6.63	360	5.07	5.40	880	2.31	4.53	337	9.07	5.41	1,577
Dec-22	1.51	5.80	281	4.95	5.17	823	4.29	4.01	554	10.75	4.80	1,659
Absolute Change	0.18	0.83	79	0.12	0.23	57	1.98	0.52	217	1.68	0.61	82
Relative Change	-11%	-13%	-25%	-2%	-4%	-7%	60%	-12%	49%	17%	-12%	5%

Data is reported to significant figures to reflect appropriate precision and may not sum precisely due to rounding.
Mineral Resources are Reported inclusive of Ore Reserves

Evolution Mining reported a 31 December 2022 Mineral Resource of 5.5 million tonnes at 4.79g/t gold for 843,000 ounces of contained gold, being the Evolution share of the total EKJV resource of 11.0 million tonnes at 4.80g/t gold for 1.7 million ounces of contained gold (Table 1). This figure was adjusted from the EKJV 31 December 2021 Mineral Resource (1.60 million ounces) due to revised costs and design parameters, revised gold price assumption, mining depletion and stockpile adjustment. The UG Mineral Resource at Falcon and Star Trek Underground are new additions to the 31 December 2022 Mineral Resource statement.

The design changes are attributable to:

- Assumed gold price change from A$2,000/oz. to A$2,200/oz.
- Reduced processing costs based on development of a 4.2 million tonne per annum plant (Future Growth Project)
- Underground mining costs increased in line with review of actual costs
- Sustaining capital and haulage costs excluded
- Open Pit metallurgical recovery increased to 93.5% to better reflect actual performance at deposit grades (previously 86% recovery was calculated using a 0.5g/t gold cut-off grade.)

A stockpile adjustment of –60,000 tonnes and -0.29g/t gold for –5,000 ounces of gold has been included in the reported December 31, 2022 Mineral Resource.

The December 31, 2022 EKJV Mineral resource includes the following updated geological models:

- Hornet (EKJV), November 2022 Resource Update
- Pegasus & Drake (EKJV), March 2022 Resource Update
- Pode & Hera (EKJV), October 2022 Resource Update
- Rubicon (EKJV), November 2022 Resource Update
- Falcon (EKJV), July 2022 Resource Update
- Star Trek (EKJV), November 2022 Resource Update
- Raleigh (EKJV), November 2022 Resource Update

The following geological models remain unchanged from the December 31, 2022 Evolution Mining Resource Statement:

- Hornet OP (EKJV) 2021
- Golden Hind OP (EKJV) 2021

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East Kundana Joint Venture (EKJV) Ore Reserve Statement

The East Kundana Joint Venture Ore Reserve statement included with this announcement has been prepared in accordance with the 2012 Edition of the "Australasian Code for reporting of Exploration Results, Mineral Resources and Ore Reserves" (the JORC Code 2012) and the ASX Listing Rules.

This Material Information summary has been provided for the East Kundana Joint Venture Ore Reserve pursuant to ASX Listing Rules 5.8 and 5.9 and the Assessment and Reporting Criteria in accordance with JORC Code 2012 requirements. The Assessment and Reporting Criteria in accordance with JORC Code 2012 – Table 1 is presented in Appendix A.

The December 2022 East Kundana Joint Venture (EKJV) Ore Reserve estimate is 2.9 million tonnes at 5.35g/t gold for 503,000 ounces of contained gold (Table 3). This is a decrease of –44,000 ounces (-8%) compared to the December 2021 estimate of 3.5 million tonnes at 4.84g/t gold for 547,000 ounces of contained gold (Table 4).

Ore Reserves use a $1,600 per ounce gold price assumption for generating cut-off grades that are used in optimisations in line with Evolution Mining Strategic Planning Standards. The reported Ore Reserve is defined within appropriately designed open pit shapes or underground stope shapes which have considered relevant modifying factors and include planned dilution and ore loss.

Table 3. MGO Total Ore Reserve reported as of 31st December 2022

Deposit	Type	COG	Proved			Probable			Total Reserve		
			Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)
Hornet	OP	0.64	-	-	-	0.07	3.65	8	0.07	3.65	8
Golden Hind	OP	0.64	-	-	-	0.08	5.03	14	0.08	5.03	14
RHP	UG	3.83	0.62	6.13	122	1.36	5.44	239	1.98	5.66	361
Raleigh	UG	3.83	0.02	3.19	2	0.77	4.82	119	0.79	4.77	121
TOTAL EKJV 100%			**0.64**	**6.02**	**125**	**2.28**	**5.16**	**379**	**2.92**	**5.35**	**503**

Data is reported to significant figures to reflect appropriate precision and may not sum precisely due to rounding.

Table 4. Comparison of December 2022 and December 2021 MGO Ore Reserves

Period	Proved			Probable			Total		
	Tonnes (Mt)	Grade Au (g/t)	Gold Metal (koz)	Tonnes (Mt)	Grade Au (g/t)	Gold Metal (koz)	Tonnes (Mt)	Grade Au (g/t)	Gold Metal (koz)
Dec 2021	1.22	4.93	194	2.30	4.79	353	3.52	4.84	547
Dec 2022	0.64	6.02	125	2.28	5.16	379	2.92	5.35	503
Absolute Change	-0.58	1.09	-69	-0.01	0.38	25	-0.59	0.52	-44
Relative Change	-47%	22%	-36%	-1%	8%	7%	-17%	11%	-8%

Data is reported to significant figures to reflect appropriate precision and may not sum precisely due to rounding.

Changes to the Ore Reserve estimate are attributable to:

- Depletion (including stockpiles) of -63,000 ounces of gold
- Additions of 10,000 ounces of gold
- Design changes of 13,000 ounces of gold (primarily due to increased gold price and increased process recovery offset against increased production costs)
- New data (predominantly from drilling in the Hera Lode of 1,500 ounces of gold)

Rand Mining and Tribune Resources Joint Venture Partners

Evolution Mining holds a 51% interest in the EKJV Mineral Resource, except for Raleigh which is 50%. The below tables summarise the Rand Mining and Tribune Resources attributed Mineral Resource and Ore Reserves.

Table 5: East Kundana Joint Venture (EKJV) Total Mineral Resource reported to 31st December 2022

Rand and Tribune Attributable Mineral Resource

Prospect	Type	Equity	Cut-Off	Measured			Indicated			Inferred			Total Resource		
				Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)
Hornet OP	OP	49%	0.32	-	-	-	0.08	3.42	9	0.09	1.55	4	0.17	2.47	14
Golden Hind	OP	49%	0.32	-	-	-	0.11	2.53	9	0.00	0.60	0	0.11	2.53	9
Pegasus	OP	49%	0.31	-	-	-	0.00	19.80	3	0.00	0.90	0	0.01	15.77	3
Hornet	UG	49%	2.44	0.02	4.19	3	0.22	3.64	26	0.49	4.12	65	0.73	3.98	93
Pegasus-Drake	UG	49%	2.44	0.10	6.77	21	0.66	7.31	154	0.12	3.81	15	0.88	6.75	190
Pode/Hera	UG	49%	2.44	0.25	5.02	47	0.39	3.75	57	0.18	3.17	22	0.82	4.80	127
Raleigh	UG	50%	2.44	0.20	7.20	46	0.31	6.36	64	0.15	3.85	19	0.66	6.04	128
Raleigh-Sadler	UG	50%	2.44	-	-	-	0.09	6.40	19	0.02	4.90	2	0.11	5.96	21
Golden Hind	UG	49%	1.71	-	-	-	0.07	4.07	9	0.12	3.65	15	0.19	3.80	23
Rubicon-Nugget	UG	49%	2.44	0.18	3.88	22	0.41	3.91	51	0.04	4.54	6	0.62	3.94	79
Falcon	UG	49%	2.44	-	-	-	-	-	-	0.13	5.02	22	0.13	5.02	22
Star Trek	UG	49%	2.44	-	-	-	-	-	-	0.76	4.19	102	0.76	4.19	102
Stockpiles	SP	49%		-	-	-	0.09	1.52	5	-	-	-	0.09	1.52	5
TOTAL Rand and Tribune				**0.74**	**5.81**	**139**	**2.44**	**5.17**	**405**	**2.11**	**4.01**	**272**	**5.28**	**4.80**	**816**

Data is reported to significant figures to reflect appropriate precision and may not sum precisely due to rounding.

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Table 6. East Kundana Joint Venture (EKJV) Total Ore Reserve reported to 31st December 2022

Rand and Tribune Attributable Mineral Resource

Deposit	Type	Equity	Cut-off	Proved			Probable			Total Reserve		
				Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)
Hornet	OP	49%	0.64	-	-	-	0.03	3.65	4	0.03	3.65	4
Golden Hind	OP	49%	0.64	-	-	-	0.04	5.03	7	0.04	5.03	7
RHP	UG	49%	3.83	0.30	6.13	60	0.67	5.44	117	0.97	5.66	177
Raleigh	UG	50%	3.83	0.01	3.19	1	0.38	4.82	59	0.39	4.77	61
TOTAL R and T				**0.32**	**6.02**	**61**	**1.13**	**5.16**	**187**	**1.44**	**5.35**	**248**

Data is reported to significant figures to reflect appropriate precision and may not sum precisely due to rounding.

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1. APPENDIX A: TABLE 1 – ASSESSMENT AND REPORTING CRITERIA, JORC CODE 2012

1.1 Golden Hind: Mineral Resource – 31 December 2022

Section 1: Sampling Techniques and Data

Criteria	Commentary
Sampling *techniques*	• Sampling was completed using a combination of Reverse Circulation (RC), Rotary Air Blast (RAB) and Diamond (DD) drilling. RAB drilling was excluded in resource estimation work. •
	• RC samples were split using a rig-mounted cone splitter on 1 m intervals to obtain a sample for assay. • Diamond core was placed in core trays for logging and sampling. Half core samples were nominated by the geologist from diamond core with a minimum sample width of either 20 cm (HQ) or 30 cm (NQ2).
	• RC sampling was split using a rig mounted cone splitter to deliver a sample of approximately 3 kg. • DD drill core was cut in half using an automated core saw, where the mass of material collected will vary on the hole diameter and sampling interval. • All samples were delivered to a commercial laboratory where they were dried, crushed to 90% passing 3 mm if required, at this point large samples may be split using a rotary splitter, pulverisation to 90% passing 75 µm, a 40 g charge was selected for fire assay.
Drilling techniques	• Both Reverse Circulation and Diamond Drilling techniques were used to drill the Golden Hind deposit. • Surface diamond drillholes were predominantly completed using HQ2 (63.5 mm) coring. • Historically, core was orientated using the Reflex ACT Core orientation system. • RC Drilling was completed using a 5.75” drill bit, downsized to 5.25” at depth. • In limited cases, RC pre-collars were drilled, followed by diamond tails. Pre-collar depth was determined in the drill design phase.
Drill sample recovery	• Any core loss in diamond drilling is recorded on the core block by the driller. This is captured by the logging geologist and entered as an interval into the hole log. • Moisture content and sample recovery is recorded for each RC sample

	Golden Hind		
	Number of Holes	Total metres	Number of Samples
DD	30	7976	3349
RC	111	10038	9450
RC_DD	18	6034	1546
TOTAL	**159**	**24047**	**14345**

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Criteria	Commentary
	• For diamond drilling, the contractors adjust their rate of drilling and method if recovery issues arise. All recovery is recorded by the drillers on core blocks. This is checked and compared to the measurements of the core by the geological team. Any issues are communicated back to the drilling contractor.
	Triple-tube drilling techniques have been employed by the drilling contractor in order to alleviate reduced recovery, due in part to the nature of the material being drilled and to the drill orientation oblique to the target structure. In order to mitigate the impacts on the estimate, samples which have logged core loss through the ore zone are ***excluded***.
Logging	• All diamond core is logged for regolith, lithology, veining, alteration, mineralisation, and structure. Structural measurements of specific features are also taken through oriented zones. • RC sample chips are logged in 1 m intervals for the entire length of each hole. Regolith, lithology, alteration, veining, and mineralisation are all recorded. • All logging codes for regolith, lithology, veining, alteration, mineralisation, and structure is entered into the AcQuire database using suitable pre-set dropdown codes to remove the likelihood of human error.
	• All core logging is qualitative with mineralised zones assayed for quantitative measurements. Every core tray is photographed wet.
	• In all instances, the entire drill hole is logged.
Sub-sampling techniques and sample preparation	• Diamond core is cut using an automated core saw. In most cases, half the core is taken for sampling with the remaining half being stored for later reference. Full core sampling is taken where data density of half core stored is sufficient for auditing purposes.
	• For recent RC drilling (2015 onwards), RC samples were split using a rig-mounted cone splitter to collect a sample 3 - 4 kg in size from each 1 m interval. These samples were utilised for any zones approaching known mineralisation and from any areas identified as having anomalous gold. Outside known mineralised zones, spear samples were taken over a 4 m interval for composite sampling.
	• For recent data (2015 onwards), preparation of samples was conducted at Bureau Veritas' Kalgoorlie facilities. Sample preparation commences with sorting, checking, and drying at less than 110°C to prevent sulphide breakdown. Samples are jaw crushed to a nominal -6 mm particle size. If the sample is greater than 3 kg a Boyd crusher with rotary splitter is used to reduce the sample size to less than 3 kg (typically 1.5 kg) at a nominal <3 mm particle size. • The entire crushed sample (if less than 3 kg) or sub-sample is then pulverized to 90% passing 75 µm, using a Labtechnics LM5 bowl pulveriser. 300 g pulp subsamples are then taken with an aluminium scoop and stored in labelled pulp packets. • The sample preparation is considered appropriate for the deposit.

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Criteria	Commentary
	• For recent data (2015 onwards), procedures are utilised to guide the selection of sample material in the field. Standard procedures are used for all processes within the laboratory. Grind checks are performed at both the crushing stage (3 mm) and pulverising stage (75 µm), requiring 90% of material to pass through the relevant size.
	• No umpire assays have been completed in this reporting period.
	• The sample sizes are considered appropriate for the material being sampled.
Quality of assay data and laboratory tests	• For recent data, a 40 g fire assay charge for is used with a lead flux in the furnace. The prill is totally digested by HCl and HNO3 acids before Atomic Absorption Spectroscopy (AAS) determination for gold analysis.
	• No geophysical tools were used to determine any element concentrations.
	• For recent data (2015 onwards), certified reference materials (CRMs) are inserted into the sample sequence randomly at a rate of 1 per 20 samples to ensure correct calibration. Any values outside of three standard deviations are re-assayed with a new CRM. • Blanks are inserted into the sample sequence at a rate of 1 per 20 samples. The insertion points are selected at random, except where high grade mineralisation is expected. In these cases, a Blank is inserted after the high-grade sample to test for contamination. Results greater than 0.2 g/t are investigated, and re-assayed if appropriate. New pulps are prepared if anomalous results cannot be resolved. • Barren flushes are regularly inserted after anticipated high gold grades at the pulverising stage. • No field duplicates were submitted for diamond core. • Pulp duplicates are requested after any ore zone. These are indicated on the sample sheet and the submission sheet. • When visible gold is observed in core, a quartz flush is requested after the sample. • Laboratory performance was monitored using the results from the QA samples mentioned above. This was supplemented by the internal QA samples used by the laboratories, which included pulp duplicates and CRMs. • The QA studies indicate that accuracy and precision are within industry accepted limits.
Verification of sampling and assaying	• All significant intersections are verified by another geologist during the drill hole validation process, and later by a Competent person to be signed off.
	• No twinned holes were drilled for this data set. Re-drilling of some drillholes has occurred due to issues downhole (e.g., bogged rods). These have been captured in the database as an ‘A’ suffix. Re-drilled holes are sampled whilst the original drillhole is logged but not sampled.
	• Geological logging and sampling are directly recorded into AcQuire. Assay files are received in .csv format and loaded directly into the database using an Acquire importer object. Assays are then processed through a form in AcQuire for QAQC checks. Hardcopy and non-editable electronic copies of these are stored.

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Criteria	Commentary
	• No adjustments are made to this assay data.
Location of data points	• As a majority of the data in the Golden Hind data set is historic, it is unknown what QC procedures have been used. • For more recent data (2015 onwards), planned hole collars are pegged using a Differential GPS by the field assistants. • The final collar is picked up after hole completion by Cardno Survey with a Real Time Kinematic Differential Global Positioning System (RTKDGPS) in the MGA 94_51 grid. • During drilling single-shot surveys are conducted every 30 m to ensure the hole remains close to design. This is performed using the Reflex Ez-Trac system which measures the gravitational dip and magnetic azimuth results are uploaded directly from the Reflex software export into the Acquire database. • At the completion of diamond drilling the Deviflex RAPID continuous in-rod survey instrument taking readings every 2 seconds, In and Out runs and reported in 3 m intervals was also used along with DeviSight GPS compass for surface alignment application True North Azimuth, DIP, latitude and longitude coordinates for set up.
	• Collar coordinates are recorded in mine grid (Kundana 10) and transformed into MGA94_51.
	• Quality topographic control has been achieved through Lidar data and survey pickups of holes over the last 15 years.
Data spacing and distribution	• Drillhole spacing varies across the deposit, with majority of drilling between 120 m x 120 m down to 20 m x 20 m
	• The data spacing and distribution is considered sufficient to support the resource estimate.
	• No sample compositing has been applied.
Orientation of data in relation to geological structure	• Most of the structures in the Kundana area dip steeply (80°) to the west (local grid). Golden Hind dips at a shallower angle of 55° to the west. Diamond drilling was designed to target the ore bodies perpendicular to this orientation to allow for a favourable intersection angle.
	• No sampling bias is considered to have been introduced by the drilling orientation. Where drillholes have been particularly oblique, they have been flagged as unsuitable for resource estimation.
Sample security	• Prior to laboratory submission, samples are stored in a secure yard. Once submitted to the laboratories they are stored in a secure fenced compound, tracked through their chain of custody and via audit trails.
Audits or reviews	• No independent audits have been undertaken of the data and sampling practices.

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Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	Commentary
Mineral tenement and land tenure status	• All information in this report is located within M16/309 which is held by The East Kundana Joint Venture (EKJV). The EKJV is majority owned and managed by Evolution Mining (51%). The minority holding in the EKJV is held by Tribune Resources Ltd (36.75%) and Rand Mining Ltd (12.25%). • The tenement on which the Golden Hind deposit is hosted is subject to three royalty agreements. The agreements are the Kundana-Hornet Central Royalty, the Lake Grace Royalty and the Kundana Pope John Agreement No. 2602-13.
	• No known impediments exist, and the tenements are in good standing.
Exploration done by other parties	• No other parties performed exploration work at Golden Hind during the reporting period. Previous exploration by other parties is summarised in open file annual reports which are available from the DMIRS.
Geology	• The Kundana gold camp is situated within the Norseman-Wiluna Greenstone Belt, in an area dominated by the Zuleika shear zone, which separates the Coolgardie domain from the Ora Banda domain. • Golden Hind mineralisation is located along the Strzelecki-Raleigh structure. The majority of mineralisation consists of narrow, laminated quartz veining on the contact between volcanogenic sedimentary rock unit and andesite/gabbro (RMV).
Drill hole Information	• A summary of the data present in the Golden Hind deposit can be found above. • The collar locations are presented in plots contained in the December 2022 resource report. • Drillholes vary in survey dip from -73 degrees to +18 degrees, with hole depths ranging from 18 m to 537 m, and having an average depth of 151 m. The assay data acquired from these holes are described in the December 2022 resource report. • All of the drill hole data were used directly or indirectly for the preparation of the resource estimates described in the resource report.
	• No material information has been excluded from this report.
Data aggregation methods	• All reported assay results have been length weighted to provide an intersection width. A maximum of 2 m of low-grade material (considered < 2.0 g/t) between mineralised samples has been permitted in the calculation of these widths. Typically grades over 2.0 g/t are considered significant, however, where wide zones of low grade are intersected in areas of known mineralisation these will be reported. No top-cutting is applied when reporting intersection results.
	• Where an intersection incorporates short lengths of high grade results these intersections will be reported in addition to the aggregate value. These will typically take the form of ##.#m @ ##.##g/t including ##.#m @ ##.##g/t.

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Criteria	Commentary
	• No metal equivalent values have been used for the reporting of these exploration results.
Relationship between mineralisation widths and intercept lengths	• True widths have been calculated for intersections of the known ore zones based on existing knowledge of the nature of these structures.
	• Both the downhole width and true width have been clearly specified when used.
	• Where a true widths cannot be estimated, the intercepts are clearly labelled as down hole thickness.
Diagrams	• Appropriate plans and section have been included at the end of this Table and in the body of the December 2022 resource report.
Balanced reporting	• Both high and low grades have been reported accurately, clearly identified with the drill hole attributes and 'From' and 'To' depths.
Other substantive exploration data	• No other material exploration data has been collected for this area.
Further work	• There are plans for further drilling at Golden Hind to extend the Indicated Resource to the north and investigate the potential for Underground mining below the current planned Open Pit. • Further work will include mining studies appropriate to EVNs current open-cut and underground mining methods. If mining studies yield a positive result, infill resource definition is planned to convert Inferred Mineral Resource category to Indicated Mineral Resource category and to test for extensions to mineralisation along strike and down-dip that would likely impact the economic outcome. • A feasibility study is progressing to determine the economics of reducing the Mungai Processing facility unit cost by increasing throughput from 2.0Mpta to 4.2Mtpa. This will likely reduce COGs for the MGO Mineral Resource Statement.
	• Appropriate diagrams accompany this release.

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Section 3: Estimation and Reporting of Mineral Resources

(Criteria listed in the preceding section also apply to this section.)

Criteria	Commentary
Database integrity	• Sampling and logging data is either recorded on paper and manually entered into a database system or captured digitally via a logging laptop and directly loaded into the database system. There are checks in place to avoid duplicate holes and sample numbers. Where possible, raw data is loaded directly into the database from laboratory and survey-tool derived files.
	• The complete exported data base including drill and face samples is brought into Datamine RM and checked visually for any apparent errors i.e., holes or faces sitting between levels or not on surface DTM's. Multiple checks are then made on numerical data including: • Empty table checks to ensure all relevant fields are populated. • Unique collar location check. • Distances between consecutive surveys is no more than 50m for drill-holes. • Differences in azimuth and dip between consecutive surveys of no more than 0.3 degrees. • The end of hole extrapolation from the last surveyed shot is no more than 30 m. • Errors are corrected where possible. When not possible the data is resource flagged as "No" in the database and the database is re-exported. This data is not used in the estimation process. • In addition to being validated, drill holes are assigned a Data Class, which provides a secondary level of confidence in the quality of the data. A review of all the historic data for Golden Hind was undertaken in 2019 and Data Class (DC) values from 0 - 3 assigned, criteria summarised below: • DC 3 = Recent data; all data high quality, validated and all original data available. • DC 2 = Historic data; may or may not have all data in AcQuire or hard copy available but has proximity to recent drilling which confirms the dip, width and tenor. Used to assist in classification OR Recent data; minor issues with data such as QAQC fail but not proximal to the ore zone. • DC 1 = Historic data; same criteria as DC 2 but cannot be verified with recent drilling, i.e., too far away or too dissimilar dip, width and/or tenor to recent drilling. Not to be used in Resource estimate. • DC 0 = Historic data; no original information or new drilling in proximity to verify. Not to be used in Resource estimate.
Site visits	• The geological interpretations underpinning these Resource models have been prepared by geologists working in adjacent mines and in direct, daily contact with similar ore bodies. The estimation of grades was undertaken by personnel familiar with the orebody and the general style of mineralisation encountered. The Senior Resource Geologist, a Competent Person for reviewing and signing off on estimations of the Golden Hind lode maintained a presence throughout the process.
	• Site visits have been undertaken.

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Criteria	Commentary
Geological interpretation	• The interpretation of the Golden Hind deposit has been carried out using a systematic approach to ensure continuity of the geology and estimated mineral resource. The confidence in the geological interpretation is high and is supported with information acquired from drilling. Towards the northern end of the mineralisation, the structure between Raleigh and Golden Hind is not as well defined. This will be accounted for in MRE classifications applied. • The interpretation of the Golden Hind mineralisation wireframe was conducted using the sectional interpretation method in Vulcan software. Sectional interpretation was completed in vertical east-west sections at approximately 10 m spacing where the drill density was good, and at approximately 40 m spacing in the North where the drill density data was sparser. Wireframes were checked for unrealistic volumes and updated where appropriate.
	• All available geological data was used in the interpretation including drill holes and regional structural models.
	• Due to the consistency of the structure conveyed by this dataset and knowledge from the adjacent Raleigh deposit, no alternative interpretations have been considered.
	• Golden Hind is an extension of the Raleigh Main Vein (RMV) hosted in the Strzelecki Structure and located to the south of the Raleigh mining area. The continuity of the RMV from Raleigh to Golden Hind is not well understood and the northern extent. • The interpretation of the Raleigh Main Vein (RMV) is based on the presence of quartz veining and continuity between sections on the main Raleigh structure. The RMV was constrained to high-grade intercepts with all holes with available photography reviewed for lithology logging. • The RMS was identified as a lower-grade halo surrounding the RMV, usually hosted in brecciated volcaniclastics or andesite. The RMS is not always present and is modelled as coincident with the RMV when halo grades were absent, to eliminate overestimation of the volume.
	• Grade continuity is affected when the percentage of quartz decreases within the main Raleigh structure and only a sheared structure remains. This results in lower grade in areas where only shear is present and higher grade where quartz veining is developed.
Dimensions	• The Golden Hind structure is approximately 1500 m long and is limited by limited drilling to the north and diamond drilling at depth. The Golden Hind mineralisation occurs in a major regional shear system, the Strzelecki structure that extends over tens of kilometres. • The Golden Hind RMV varies in width but is typically in the range of 0.1 m to 1 m. • Mineralisation is known to occur from the base of cover to around 900 m below surface in the region.

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Criteria	Commentary
Estimation and modelling techniques	• All Golden Hind mineralisation used 1.0 m composites with direct grade estimation of gold. The primary method of estimation was by categorical indicated kriging (CIK) (unless otherwise stated), utilising a three-pass search strategy using Datamine Studio RM software. Details of the estimation parameters for each mineralisation zone are summarised below. • RMV divided into two data density subdomains based on near-surface, high-density RC drilling and sparser RC and DD drilling at depth. A binary estimate is completed on composited data set with indicators (0 or 1) applied based on grade cut-off (> 0.8 g/t). Estimate returns result between 0 and 1. Cut-off of 0.70 chosen to ascertain two grade subdomains (high grade and low grade) for final gold estimate. Data sets top cut to 30 g/t and 25 g/t (high grade subdomain, high- and low-density subdomains respectively) or 2 g/t and 0.8 g/t (low grade subdomain, high- and low-density subdomains respectively) using the hard top-cut approach. Same variogram and search parameters used for both high- and low-grade subdomains. Variograms indicate grade continuity plunging steeply to the north. Searches were completed in three passes. Search ranges of 180 m in dir1, 100 m in dir2 and 25 m in dir3 were used for the high data density subdomain and 280 m in dir1, 160 m in dir2 and 40 m in dir3 for the low data density subdomain. • RMS divided into two data density subdomains based on near-surface, high-density RC drilling and sparser RC and DD drilling at depth. Variography attempted for the RMS lode but completed with low confidence. ID2 has been used for grade interpolation, with no top-cutting required due to low coefficients of variance within the RMS lode. Searches were completed in three passes. Search ranges of 60 m in dir1, 40 m in dir2 and 20 m in dir3 were used for the high data density subdomain and 80 m in dir1, 40 m in dir2 and 30 m in dir3 for the low data density subdomain
	• All mineralisation zones had check estimates using ID2 and Nearest Neighbour completed as a comparison.
	• No assumptions have been made regarding recovery of any by-products.
	• No deleterious elements have been considered and therefore estimated for this deposit.
	• The data spacing varies considerably within the deposit ranging from closed spaced drilling 20 m (along strike) and 20 m (down dip) through to more widely spaced intercepts at over 80 m (along strike) and 80 m (down dip). • As such, the block sizes varied depending on sample density. In areas of where the close spaced data existed, a 10 m x 10 m x 10 m block size was chosen. For lower density drilling with wider spacing a block size of 20 m x 20 m x 20 m was selected. • All the varying block sizes are added together after being estimated individually. • Search ellipse dimensions were derived from the variogram model ranges.
	• No selective mining units are assumed in this estimate.
	• No other elements other than gold have been estimated.

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Criteria	Commentary
	• Closed volume wireframes have been created using sectional interpretation. These were used to define the RMV, and RMS mineralised zones based on the shearing intensity, veins and gold grade. • RMV (Golden Hind) is a steeply dipping structure with quartz veining evident from drilling. • RMS (Golden Hind) is a steeply dipping sheared lower grade structure usually hosted in brecciated volcaniclastics. • For mine planning purposes a waste model is created by making a waste solid wireframe approximately 30 m either side of the mineralisation. A default grade of 0.1 g/t is assigned and the same resource classification as the adjacent ore lode is applied to ensure consistency in MSO Resource Classification reporting.
	• Top cuts were applied to the composited sample data with the intention of reducing the impact of outlier values on the average grade. • The top cut values are applied in several steps, using a technique called influence limitation top cutting. A top cut (AU) and non-top cut (*_NC) variable is created, as well as a spatial variable (*_IL) which only has values where the top cut values appear. For example, where gold requires a topcut, the following variables will be created and estimated: • AU (top cut gold). • AU_NC (non- top-cut gold). • AU_IL (spatial variable; values present where AU data is top cut). • The top-cut and non-top cut values are estimated using search ranges based on the variogram, and the *_IL values estimated using very small ranges (e.g., 5 m x 5 m x 5 m). Where the *_IL values produce estimated blocks within these restricted ranges, the *_NC estimated values replace the original top cut estimated values (AU).
	• Statistical measures of estimation performance, such as the Slope of Regression have been used to assess the quality of the estimation for each domain. • Differences in the global grade of the declustered, top-cut composite data set and the average model grade were within 10%, or justification for a difference outside 10% was explicable. • Swath plots comparing declustered, top-cut composites to block model grades are prepared and reviewed. Plots are also prepared summarising the critical model parameters. • Visually, block grades are assessed against drill hole data.
Moisture	• The tonnes have been estimated on a dry basis.

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<table>
<tr><th>Criteria</th><th>Commentary</th></tr>
<tr><td>Cut-off parameters</td><td>

The cut-off grades were estimated using projected site mining costs, processing costs and site general administration costs.
a gold price of A$2,200/oz was utilised.
The cut-off grades applied to the deposit areas are listed below:

<table>
<tr><th>Deposit</th><th>COG (g/t Au) (m)</th></tr>
<tr><td>Open Pits (excl Boundary)</td><td>0.40 g/t Au</td></tr>
<tr><td>Raleigh & Raleigh North UG</td><td>2.44 g/t Au</td></tr>
<tr><td>East Kundana JV UG</td><td>2.44 g/t Au</td></tr>
</table>
</td></tr>
<tr><td>Mining factors or assumptions</td><td>

The Mineral Resource estimations for open pit resource have been reported within pit optimisation shells generated in Whittle software. Mining costs are based on regolith type and depth below surface. For Mineral Resources, no dilution or recovery factors have been applied. Mining selectivity of 10m (x) by 10m (y) by 5m (z) has been applied.
The Mineral Resource estimations for underground have been reported within Mining Shape Optimiser objects (MSOs) generated in Datamine or Deswik software. These shapes assume a minimum mining width of 2.5 m with a minimum footwall and hanging-wall slope of 50 to 80 degrees. The minimum strike of the panels is 10.0m and a vertical extent of 5.0m. No external dilution has been applied to the shapes however internal dilution has been applied where required (no estimated grade or sub Inferred Mineral Resource blocks) at 0.0 g/t.
All Mineral Resources have been depleted by prior mining. The prior mining is represented by detailed surveys completed over the life of the project. These surveys are represented by 3D models which have been used to flag blocks as mined or not. MSO’s are also validated and removed if they are considered to be sterilised (low likelihood of being mined) by current mine development.

</td></tr>
<tr><td>Metallurgical factors or assumptions</td><td>

Reasonable assumptions for metallurgical extraction factored into the resource estimate are based on previous processing of the ore from the nearby deposits at Kundana, Kunanalling and Carbine through the various historic and operational CIP/CIL processing facilities within the district (including the Mungari Mill).
Where a deposit has not been previously mined or processed, preliminary deportment and geo-metallurgical studies are completed on ore types to generate metallurgical factors and assumptions to be included in the resource estimate.
Target gold recoveries range from 86% to 95% recovery.

</td></tr>
<tr><td>Environmental factors or assumptions</td><td>

No significant environmental factors are expected to be encountered regarding the disposal of waste or tailing material. This expectation is based on previous mining and milling history of existing open pit operations with the project area.
Mungari Gold Operations has in place regulatory permits and approvals to continue operations.
A site Environmental team monitors ongoing compliance with approvals and maintains the site in good standing with regulators.

</td></tr>
<tr><td>Bulk density</td><td>

A thorough investigation into density values for the various lithological units at Golden Hind was completed and the mean densities by lithology were coded into the database. Where there were no measurements for a specific lithology, a default value of 2.7 t/m³ was applied. Density was then estimated by Ordinary Kriging or ID2, using the associated gold estimation parameters for that domain. Post estimation, default density values for the oxide and transition zones were applied, based on regional averages.

</td></tr>
</table>

Criteria	Commentary
	• No voids are encountered in the ore zones and underground environment as Golden Hind is unmined.
	• The average bulk density of individual lithologies is based on 502 bulk density measurements at the Golden Hind deposit. Assumptions were based on regional averages for the default density applied to oxide (1.8 t/m³) and transitional (2.3 t/m³) material, due to lack of data in this area.
Classification	• Classification is based on a series of factors including: • Geologic grade continuity • Density of available drilling • Statistical evaluation of the quality of the kriging estimate • Confidence in historical data, based on the new Data Class system
	• All relevant factors have been given due weighting during the classification process.
	• The resource model methodology is appropriate, and the estimated grades reflect the Competent Persons view of the deposit.
Audits or reviews	• The Resource model has been subjected to internal peer reviews.
Discussion of relative accuracy/ confidence	• The mineral resource estimate is considered robust and representative of the Golden Hind style of the RMV mineralisation. The application of geostatistical methods has helped to increase the confidence of the model and quantify the relative accuracy of the resource.
	• This resource report relates to the Golden Hind deposit. The model will show local variability even though the global estimate reflects the total average tonnes and grade.
	• No reconciliation factors are applied to the resource post-modelling.

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1.2 Drake, Pegasus, Rubicon and Hornet: Mineral Resource – 31 December 2022

Section 1: Sampling Techniques and Data

Criteria	Commentary
Sampling techniques	• Several sample types were used to collect material for analysis; underground and surface diamond drilling (DD), surface reverse circulation drilling (RC) and face channel (FC) sampling. Rotary air blast (RAB) holes were excluded from the estimate. Where sufficient DD holes were present, RC holes were also excluded. Tabulated statistics below include the Pode and Hera trend. A more detailed breakdown will be made available in the Drake, Pegasus, Rubicon and Hornet 2022 Resource Report.

	RHP, Drake, Pode,Hera		
Type	No.of Holes	Total Metres	No. of Samples
DD	4,770	869,035	571,408
FS	12,829	62,292	127,950
RC	1,307	124,002	11,534
RCDD	62	21,433	1,144
TOTAL	18,968	1,076,762	712,036

	• DD drilling is sampled within geological boundaries with a minimum (0.3 m) and maximum (1.0 m) sample length. Face channel sampling is constrained within geological and mineralised boundaries with a minimum (0.2 m) and maximum (1.0 m) channel sample length. In some cases, smaller samples (0.1 m – 0.2 m) have been taken to account for smaller structures in the face.
	• DD drill core was nominated for either half core or full core sampling. Core designated for half core was cut using an automated core saw. The mass of material collected was dependent on the drillhole diameter and sampling interval selected. Core designated for full core was broken with a rock hammer if sample segments were too large to fit into sample bags. • A sample size of at least 3 kg of material was targeted for each face sample interval. • All samples were delivered to a commercial laboratory where they were dried and crushed to 90% of material ≤3 mm. At this point large samples were split using a rotary splitter, then pulverised to 90% ≤75 µm. • A 40 g charge was selected for fire assay for all recent samples. Historically, charge weights of 50 g have also been used.
Drilling techniques	• Both Reverse Circulation and Diamond Drilling techniques were used to drill the Kundana deposits. • Surface diamond drill holes were completed using HQ2 (63.5 mm) core, whilst underground diamond drill holes were completed using NQ2 (50.5mm) core. • Historically, core was orientated using the Reflex ACT Core orientation system. Currently, core is oriented using the Boart Longyear Trucore Core Orientation system. • RC Drilling was completed using a 5.75” drill bit, downsized to 5.25” at depth.

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Criteria	Commentary
	• In many cases, RC pre-collars were drilled, followed by diamond tails. Pre-collar depth was determined in the drill design phase depending on the target being drilled and production constraints.
Drill sample recovery	• For DD drilling, any core loss is recorded on the core block by the driller. This is captured by the logging geologist and entered as an interval into the hole log.
	• Contractors adjust the rate and method of drilling if recovery issues arise. All recovery is recorded by the drillers on core blocks. This is checked and compared to the measurements of the core by the geological team. Any issues are communicated back to the drilling contractor.
	• Recovery was excellent for diamond core and no relationship between grade and recovery is observed. Average recovery across the Kundana camp is at 99%.
Logging	• All diamond core is logged for lithology, veining, alteration, mineralisation, and structural data. Structural measurements of specific features are also taken through oriented zones. • Logging is entered in AcQuire using a series of drop-down menus which contain the appropriate codes for description of the rock. • All underground faces are logged for lithology and mineralisation. Logging is captured on a face sample sheet underground which is then transferred to AcQuire. Faces are then input into AcQuire using a series of drop-down menus which contain appropriate codes for description of the rock.
	• All core logging is qualitative with mineralised zones assayed for quantitative measurements. Every core tray is photographed wet. • All underground faces are logged and sampled to provide both qualitative and quantitative data. Faces are washed down and photographed before sampling is completed.
	• For all drill holes, the entire length of the hole is logged.
Sub-sampling techniques and sample preparation	• Diamond core is cut using an automated core saw. Sampling and cutting methodology is dependent on the type of drilling completed. Half core is utilised for exploration drilling. Some exploration drill holes have been whole core sampled and all Grade Control drilling is whole core sampled.
	• RC samples are split using a rig-mounted cone splitter to collect a sample 3 - 4 kg in size from each 1 m interval. These samples were from any zone approaching known mineralisation and from any areas identified as having anomalous gold. Outside known mineralised zones spear samples were taken over a 4 m interval for composite sampling.
	• Preparation of samples was conducted at Bureau Veritas' Kalgoorlie facilities; commencing with sorting, checking, and drying at less than 110°C to prevent sulphide breakdown. Samples are jaw crushed to a nominal -6 mm particle size. If the sample is greater than 3

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Criteria	Commentary
	kg a Boyd crusher with rotary splitter is used to reduce the sample size to less than 3 kg (typically 1.5 kg) at a nominal <3 mm particle size. • The entire crushed sample (if less than 3 kg) or sub-sample is then pulverized to 90% ≤75 µm, using a Labtechnics LM5 bowl pulveriser. 400 g Pulp subsamples are then taken with an aluminium scoop and stored in labelled pulp packets. • The sample preparation is considered appropriate for the deposit.
	• Standard procedures are used for all processes within the laboratory. Grind checks are performed at both the crushing stage (3 mm) and pulverising stage (75 µm), requiring 90% of material to pass through a sieve of relevant size.
	• Umpire sampling is performed monthly, where 3% of the samples are sent to the umpire laboratory for processing. • Umpire samples of faces were analysed using a 40 g charge weight.
	• The sample sizes are considered appropriate for the material being sampled.
Quality of assay data and laboratory tests	• A 40 g fire assay charge for diamond drillholes and a 40 g charge for face samples is used with a lead flux in the furnace. The prill is totally digested by HCl and HNO3 acids before Atomic Absorption Spectroscopy (AAS) determination for gold analysis.
	• No geophysical tools were used to determine any element concentrations
	• Certified reference materials (CRMs) are inserted into the sample sequence at a rate of 1 per 20 samples to ensure correct calibration. Any values outside of 3 standard deviations are re-assayed with a new CRM. • Blanks are inserted into the sample sequence at a rate of 1 per 20 samples. The insertion points are selected at random, except where high grade mineralisation is expected. In these cases, a Blank is inserted after the high-grade sample to test for contamination. Results greater than 0.2 g/t if received are investigated, and re-assayed if appropriate. New pulps are prepared if anomalous results cannot be resolved. • Barren flushes are regularly inserted after anticipated high gold grades at the pulverising stage. • No field duplicates were submitted for diamond core. • Pulp duplicates are requested after any ore zone. These are indicated on the sample sheet and the submission sheet. • When visible gold is observed in core, a quartz flush is requested after the sample. • Laboratory performance was monitored using the results from the QA samples mentioned above. This was supplemented by the internal QA samples used by the laboratories, which included pulp duplicates and CRMs.+ • The QA studies indicate that accuracy and precision are within industry accepted limits.
Verification of sampling and assaying	• All significant intersections are verified by another geologist during the drill hole validation process, and later by a competent person to be signed off.

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Criteria	Commentary
	• No specific twinned holes were drilled. Re-drilling of some drillholes has occurred due to issues downhole (e.g., bogged rods). These have been captured in the database with an 'A' suffix. Re-drilled holes are sampled, whilst the original drillhole is logged but not sampled.
	• Geological logging and sampling are directly recorded into AcQuire. Assay files are received in .csv format and loaded directly into the database using an AcQuire importer object. Assays are then processed through a form in AcQuire for QAQC checks. Hardcopy and non-editable electronic copies of these are stored.
	• No adjustments have been made to this assay data.
Location of data points	• Planned holes are marked up by the mine survey department using a total station survey instrument in mine grid (Kundana 10). The actual hole position is then located by the mine survey department once drilling is completed. • Holes are lined up on the collar point using the DHS Minnovare Azimuth Aligner. Planned azimuths and dips of the holes are downloaded to the aligner which is then placed on the rod string to align the hole for drilling. • During drilling, single shot surveys are conducted at the 30 m mark to check azimuth aligner set up and track off collar deviation. The Deviflex tool is used at 50 m intervals to track the deviation of the hole and to ensure it stays close to design. This is a relative change tool which measures the change in orientation along the path of the hole at 3 m intervals. The Deviflex tool is referenced back to the azimuth aligner measurement to provide a non-magnetic survey in true North. At the completion of the hole, a final Deviflex survey is completed taking measurements for the entire hole. Results are uploaded from the Deviflex software into cloud service. This data is then reviewed, downloaded, and imported into the Acquire database. The download from the Deviflex service utilises an average of all the Deviflex surveys taken over the entire hole. These are review and validated and erroneous surveys discarded. • Prior to the overshot mounted Deviflex tool being available, a combination of magnetic and Deviflex single shot surveys were used and 30 m intervals whilst drilling. A final end of hole multi shot Deviflex survey was taken to provide a continuous non-magnetic survey of the entire hole trace.
	• Collar coordinates are recorded in mine grid (Kundana 10) and transformed into MGA94_51.
	• Quality topographic control has been achieved through Lidar data and survey pickups of holes over the last 15 years.
Data spacing and distribution	• Drill hole spacing varies across the deposit. Resource Targeting drilling at an 80 m x 80 m nominal spacing is infilled during Resource Definition down to an average of 30 m x 30 m. Grade control drilling follows development and is generally comprised of stab drilling from the development drive at 10 m to 15 m spaced centres.
	• The data spacing and distribution is considered sufficient to support the Resource and Reserve estimates.
	• No sample compositing has been applied.

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Criteria	Commentary
Orientation of data in relation to geological structure	• Most of the structures in the Kundana area dip steeply (80°) to the west (local grid). Diamond drilling was designed to target the ore bodies perpendicular to this orientation to allow for a favourable intersection angle. Instances where this was not achievable (primarily due to drill platform location), drilling was not completed, or re-designed once a more suitable platform became available. • Drill holes with low intersection angles are excluded from resource estimation where more suitable data is available.
	• No sampling bias is considered to have been introduced by the drilling orientation. Where drillholes have been particularly oblique, they have been flagged as unsuitable for resource estimation.
Sample security	• Prior to laboratory submission samples are stored in a secure yard. Once submitted to the laboratories they are stored in a secure fenced compound, tracked through their chain of custody and via audit trails.
Audits or reviews	• No recent audits have been undertaken of the data and sampling practices.

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Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	Commentary
Mineral tenement and land tenure status	• All holes mentioned in this report are located on the M16/309 Mining lease held by the East Kundana Joint Venture (EKJV). The EKJV is majority owned and managed by Evolution Mining (51%). The minority holding in the EKJV is held by Tribune Resources Ltd (36.75%) and Rand Mining Ltd (12.25%). • The tenement on which the Rubicon, Hornet, Pegasus, and Drake deposits are hosted (M16/309) is subject to three royalty agreements. The agreements that are on M16/309 are the Kundana- Hornet Central Royalty, the Lake Grace Royalty and the Kundana Pope John Agreement No. 2602-13.
	• No known impediments exist, and the tenements are in good standing.
Exploration done by other parties	• The first reference to the mineralisation style encountered at the Kundana project was the mines department report on the area produced by Dr. I. Martin (1987). He reviewed work completed in 1983 – 1984 by a company called Southern Resources, who identified two geochemical anomalies, creatively named Kundana #1 and Kundana #2. The Kundana #2 prospect was subdivided into a further two prospects, dubbed K2 and K2A. • Between 1987 and 1997, limited work was completed. • Between 1997 and 2006, Tern Resources (subsequently Rand Mining and Tribune Resources) and Gilt-edged Mining focused on shallow open pit potential with production from the Rubicon open pit commenced in 2002. • In 2011, Pegasus was highlighted by an operational review team and follow-up drilling was planned through 2012.
Geology	• The Kundana camp is situated within the Norseman-Wiluna Greenstone Belt, in an area dominated by the Zuleika shear zone, which separates the Coolgardie domain from the Ora Banda domain. • K2-style mineralisation (Pegasus, Rubicon, Hornet, Drake) consists of narrow vein deposits hosted by shear zones located along steeply dipping overturned lithological contacts. The K2 structure is present along the contact between a black shale unit (Centenary Shale) and intermediate volcaniclastics (Black Flag Group). • Minor mineralisation, termed K2B, also occurs further west, on the contact between the Victorious basalt and Bent Tree Basalt (both part of the regional upper Basalt Sequence). Additional mineralised structures include the K2E and K2A veins, Polaris/Rubicon Breccia (Silicified and mineralised Shale) and several other HW lodes adjacent to the main K2 structure. • A 60° W dipping fault offsets the K2B contact and exists as a zone of vein-filled brecciated material hosting the Pode-style mineralisation in the Nugget lode at Rubicon.
Drill hole Information	• A summary of the data present in the RHP deposits can be found above. • The collar locations are presented in plots contained in the December 2022 resource report.

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Criteria	Commentary
	• Drill holes vary in survey dip from +44 to -89 degrees, with hole depths ranging from 10 m to 1,413 m with an average depth of 233 m. The assay data acquired from these holes are described in the December 2022 resource report. • All validated drill hole data was used directly or indirectly for the preparation of the resource estimates described in the resource report.
	• The exclusion of any drill hole data is not material to this report
Data aggregation methods	• All reported assay results have been length weighted to provide an intersection width. A maximum of 2 m of barren material (considered <2 g/t) between mineralized samples has been permitted in the calculation of these widths. Typically grades over 2 g/t are considered significant, however where low grades are intersected in areas of known mineralisation, these will be reported. No top-cutting is applied when reporting intersection results.
	• Where an intersection incorporates short lengths of high grade results these intersections will be reported in addition to the aggregate value. These will typically take the form of ##.#m @ ##.#gpt including ##.#m @ ##.#gpt.
	• No metal equivalent values have been used for the reporting of these exploration results
Relationship between mineralisation widths and intercept lengths	• True widths have been calculated for intersections of the known ore zones, based on existing knowledge of the nature of these structures.
	• Both the downhole width and true width have been clearly specified when used.
	• Both the downhole width and true width have been clearly specified when used.
Diagrams	• Appropriate plans and section have been included at the end of this table and in the December 2022 resource report.
Balanced reporting	• Both high and low grades have been reported accurately, clearly identified with the drill hole attributes and ‘From’ and ‘To’ depths.
Other substantive exploration data	• Fifteen geotechnical holes were drilled targeting several different areas through lower Rubicon and Pegasus. Holes have been designed for seismic monitoring. Holes were geologically logged to ensure no mineralisation was intersected. Where mineralisation was intersected, appropriate sampling was completed.
Further work	• Drilling will continue in various parts of the mine with the intention of extending areas of known mineralisation. Areas of focus across RHP will be those down dip of current high-grade trends on the K2 ahead of development. GC drilling will also be conducted as required on a level-by-level basis. • Further work will include mining studies appropriate to EVNs current open-cut and underground mining methods. If mining studies yield a positive result, infill resource definition is planned to convert Inferred Mineral Resource category to Indicated Mineral Resource category and to test for extensions to mineralisation along strike and down-dip that would likely impact the economic outcome.

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Criteria	Commentary
	• A feasibility study is progressing to determine the economics of reducing the Mungai Processing facility unit cost by increasing throughput from 2.0Mpta to 4.2Mtpa. This will likely reduce COGs for the MGO Mineral Resource Statement.
	• Appropriate diagrams accompany this release and are detailed in the December 2022 resource report.

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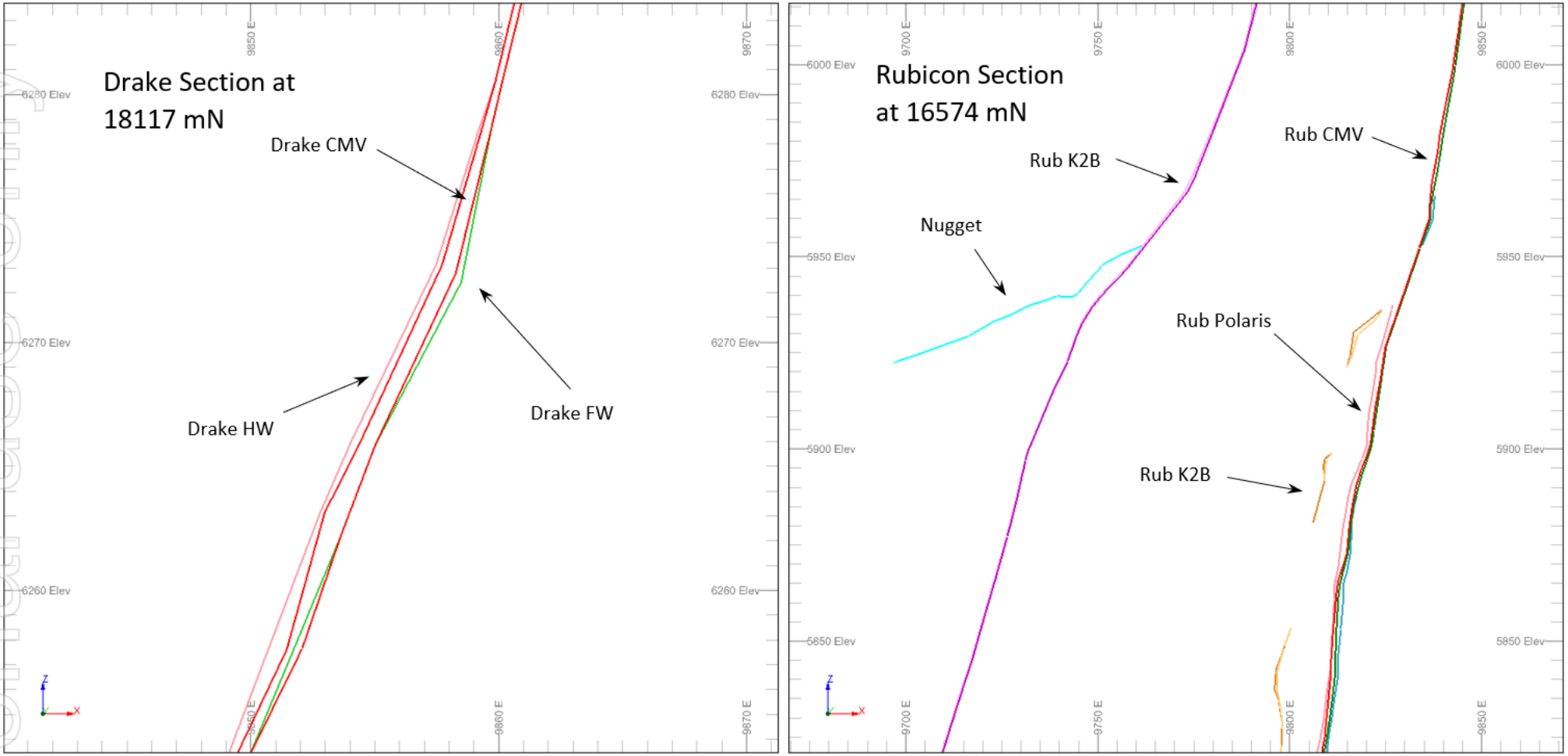


Figure 1. Cross section views of Drake and Rubicon ore lodes

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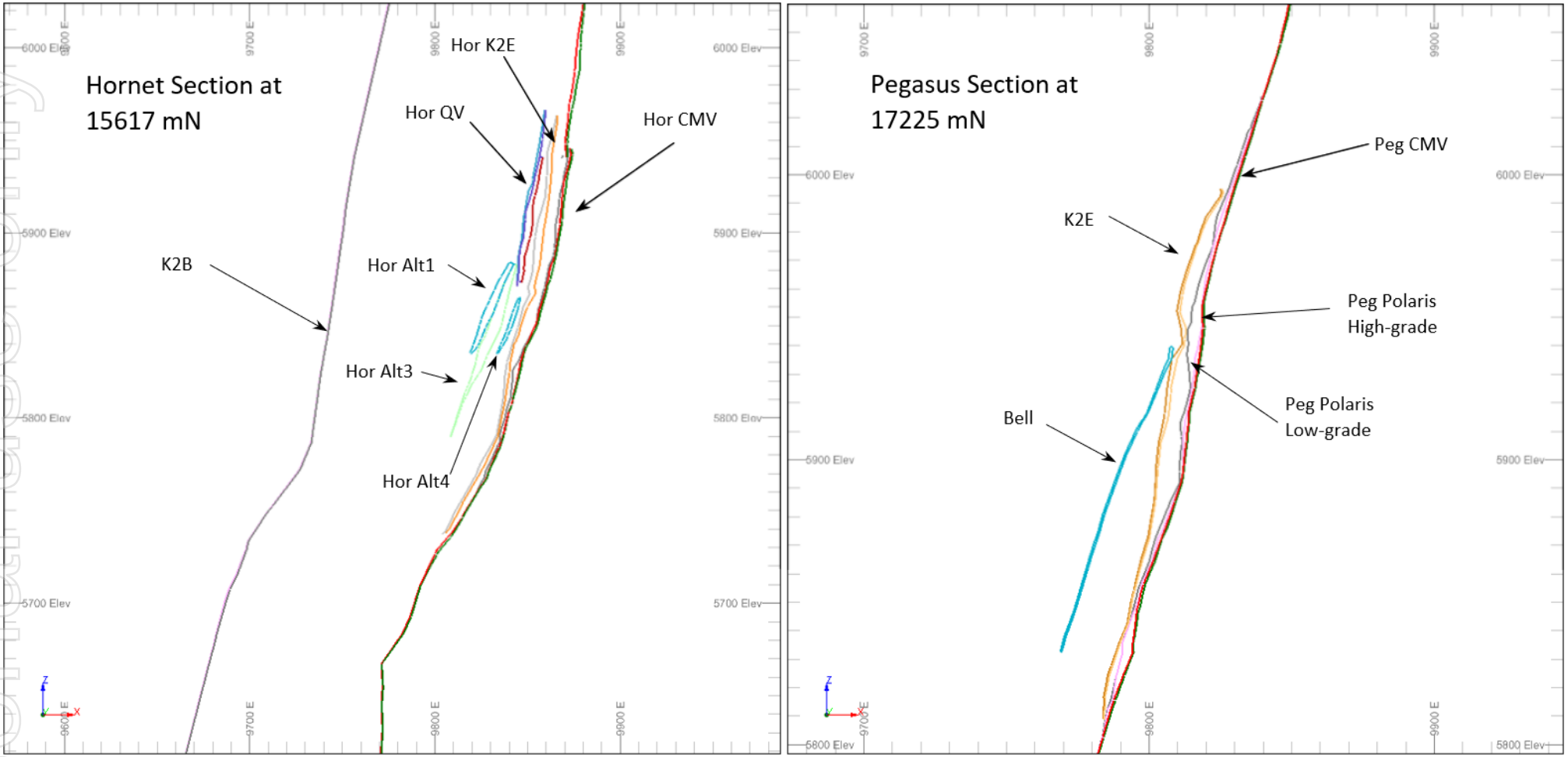


Figure 2. Cross section views of Pegasus and Hornet ore lodes.

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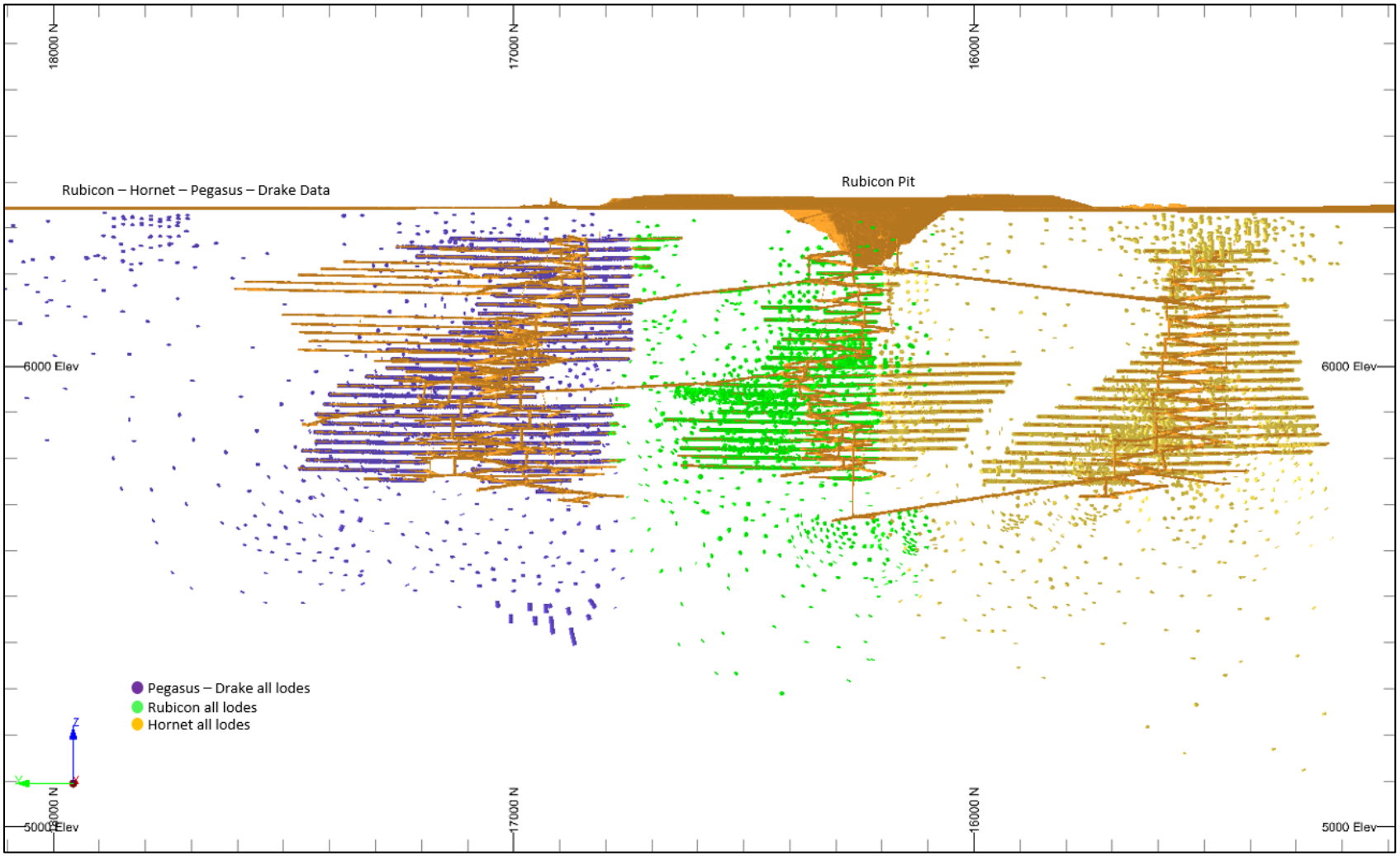


Figure 3. Long section views of Drake, Pegasus, Rubicon and Hornet ore lodes and data used in resource estimations.

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Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	Commentary
Database integrity	• Sampling and logging data are either recorded on paper and manually entered into a database system or captured digitally via a logging laptop and directly loaded into the database system. There are checks in place to avoid duplicate holes and sample numbers. Where possible, raw data is loaded directly into the database from laboratory and survey-tool derived files.
	• The complete exported data base including drill and face samples is brought into Datamine and checked visually for any apparent errors i.e., holes or faces sitting between levels or not on surface DTM's. Multiple checks are then made on numerical data. This includes: • Empty table checks to ensure all relevant fields are populated. • Unique collar location check. • Distances between consecutive surveys is no more than 60m for drill-holes. • Differences in azimuth and dip between consecutive surveys of no more than 0.3 degrees. • The end of hole extrapolation from the last surveyed shot is no more than 30 m. • Underground face sample lines are not greater than +\- 5 degrees from horizontal. • Errors are corrected where possible. When not possible the data is resource flagged as "No" in the database and the database is re-exported. This data will not be used in the estimation process. • Several drilling programs completed between 2014 and 2016 had erroneous metre depths recorded by the drillers, therefore these drill holes have been omitted from the ore wireframe interpretations and flagged as invalid. However, where there were no QAQC issue with the assays, the correct intervals have been recorded, the translation in the easting direction required for them to be in the 'correct' location (based on development above and below) applied and these intervals were appended to the data set before compositing. • The sample translation method has been applied to surface drilling in between development levels which are deemed to cause an unrealistic kink in the wireframe interpretation. This is only done after a thorough investigation of the surrounding data to ensure that no secondary veining is present in the footwall or hanging wall and that no separate lodes are missed. • In addition to being Resource Flagged as "Yes" or "No", drill holes are assigned a Data Class, which provides a secondary level of confidence in the data quality. Data Class (DC) values range from 0 to 3, with criteria summarised below: • DC 3 = Recent data - all data high quality, validated and all original data available. • DC 2 = Historic data - may or may not have all data in AcQuire or hard copy available but has proximity to recent drilling which confirms the dip, width and tenor which is used to assist in classification Or Recent data - minor issues with data but away from the ore zone. • DC 1 = Historic data - same criteria as DC 2 but cannot be verified with recent drilling, i.e., too far away, or dissimilar dip, width and/or tenor to recent drilling. Not used in Resource estimate. • DC 0 = Historic data - no original information or new drilling in proximity to verify. Not used in Resource estimate.
Site visits	• The geological interpretations underpinning these resource models were prepared by geologists working in the mine who were in direct, daily contact with the ore body. The estimation of grades was undertaken by personnel familiar with the ore body and the general style of mineralisation encountered. The Senior Resource Geologist, a Competent Person for reviewing and signing off on the RHP and Drake estimates, maintained a site presence throughout the process.
	• Site visits are completed for the commercial laboratories that undertake the sub-sampling and analysis to ensure sample chain of custody

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Criteria	Commentary
Geological interpretation	• The interpretation of the RHP and Drake deposits were carried out using a systematic approach to ensure continuity of the geology and estimated mineral resource. The confidence in the geological interpretation is high and is supported with information acquired during ore development as well as from underground and surface diamond drilling. • The interpretation of all RHP and Drake mineralised wireframes was conducted using the sectional interpretation method in Datamine RM software. All lodes have been interpreted in plan-view section. Where development levels were present, sectional interpretation was completed at approximately 5 m spacing. Where only drilling data was present, sectional interpretation was completed at approximately 10 m - 20 m spacing. Checks were made to ensure that the wireframed volume agreed with the true ore widths of drill hole intersections. As a rule, wireframe extrapolation was limited to one half of the average drill spacing.
	• All available geological data was used in the interpretation including mapping, drill holes, underground face channel data, 3D photogrammetry and structural models.
	• Alternative interpretations are not considered, the mineralisation is well defined and understood from underground exposures.
	• The interpretation of the RHP and Drake mineralisation is based on the presence of mineralised structure (veining and shear), ore-bearing mineralogy (gold and associated sulphides), assayed samples and continuity between sections.
	• Individual RHP and Drake mineralised structures are thought to be reasonably continuous at the current drill spacing, as similar mineralisation styles, structures and grade tenor exists between adjacent drillholes. • Post-mineralisation dextral offsetting faults (locally called D4 structures) affect the continuity of the K2 structure. These structures are steep-dipping, and the general trend is NNW-SSE. The largest is the Mary fault with a ~600 m offset. The White Foil and Poseidon faults form the bounding structures between the Hornet/Rubicon and Rubicon/Pegasus mine areas, respectively. Offset on these structures varies between 1 and 10 m. Many smaller scale faults exist within the mining areas (especially at the southern end of Hornet) although none have a material impact on the Resource model.
Dimensions	• The strike length of the different ore systems varies from ~100 m to 600 m, with the individual Rubicon Hornet, Pegasus, and Drake CMV structures having the longest strike lengths. The individual ore bodies occur in a major regional Zuleika shear system extending over tens of kilometres. • Ore body widths are typically in the range of 0.2 – 3.0 m. The widest orebody is Rubicon Nugget at approximately 7 m. The narrowest is the K2B (present at Rubicon, Hornet and Pegasus) at approximately 0.5 m. The main CMV structure has an average thickness of 0.65 m. • Mineralisation is known to occur from the base of cover to ~1,000 m below surface. The structure is open at depth.
Estimation and modelling techniques	• RHP and Drake mineralised zones with high data-density use direct grade estimation by Ordinary Kriging (unless otherwise stated) supported by composited sample data. Composite lengths of 1 m were used for all lodes, determined from statistical analysis of all sample lengths in the estimation dataset. In smaller mineralised zones where construction of a coherent variogram was not possible, Inverse Distance has been used. All estimation was completed using Datamine RM software. Details of estimation by ore lode is summarised below: • CMV (Rubicon, Hornet and Pegasus) - divided into two grade subdomains based on data density: high density around development levels and lower density for the remainder. Each domain was analysed for top cuts and had variography completed separately. The high-density domain has search ranges between 30 m - 90 m in direction 1, 20 m - 65 m in direction 2 and 15 m - 30 m in direction 3. The low-density domain has search ranges between 50 m – 200 m for direction 1 and 30 m – 150 m for direction 2 and 18 m - 100 m in direction 3, Three passes were used for estimation with distances based on variography. Estimation was completed using a soft boundary between the high and low-density domains and between adjacent CMV domains. Restrictions by drill hole have been applied to the high-density domain and restrictions by drill hole type have been applied to the low-density domain. Rubicon CMV utilised a lower cut estimation (outline below) and

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Criteria	Commentary
	was restricted on a high-grade low-grade flag. This low cut estimation was applied to samples < 3g/t and using a search of 30 m in direction 1 and 20 m in direction 2. • Hornet CMV contains two additional subdomains, one based on grade and the other on the weathering profile. The low-grade domain that was analysed for top cuts and had variography completed separately. It indicates grade continuity with search ranges of 90 m in direction 1 and 60 m in direction 2. Three search passes were used. Restrictions by drill hole have been applied. A semi-soft boundary has been applied between the fresh and weathered domains of the Hornet CMV as boundary analysis suggested neither a completely hard nor completely soft boundary. The weathering domain was analysed for top cuts and had variography completed separately, there was insufficient data for variographic analysis therefore ID2 was used for estimation. Three search passes were used. Restriction by drill hole was applied. • Polaris (RHP) - Rubicon Polaris is divided into two subdomains based on data density: high density around development levels and lower density distant to development. For high density and low density domains in Rubicon Polaris has search distances of 45 m & 50 m in direction 1, 25 m & 35 m in direction 2 and 15 m in direction 3. Pegasus Polaris is divided into an additional two subdomains based on grade. These separate domains have separate variography and topcuts. The high grade domain uses search distances of 30 m for direction 1, 30 m for direction 2 and 15 m for direction 3. The low grade domain uses search distances of 20 m for direction 1, 15 m for direction 2 and 10 m for direction 3. Hornet Polaris comprises two domains; Polaris North situated proximal to northern Hornet development and Polaris situated proximal to southern Hornet development. Each domain was analysed for top cuts and had variography completed separately. Rubicon Polaris is a singular lode and has search distances of 40 m for direction 1 and 30 m for direction 2 in the high data density domain and 110 m for direction 1 and 90 m for direction 2 in the low data density domain. Pegasus Polaris has search distances of 50 m for direction 1 and 35 m for direction 2 in the high grade domain and search distances of 40 m for direction 1 and 30 m for direction 2 in the low-grade domain. Hornet Polaris has search distances of 45 m for direction 1 and 30 m for direction 2 in Polaris North and 45 m for direction 1 and 40 m for direction 2 in Polaris. Three search passes were used in all domains. Restrictions by drill hole were applied to both Hornet Polaris domains. No restrictions were applied to Pegasus Polaris domains. • K2E (RHP) - Rubicon K2E is divided into two subdomains based on data density: high density around development levels and lower density distant to development. Pegasus K2E is divided into two domains (K2E and K2E Lower) based on two spatially separate areas of similar data density. Hornet K2E comprises two domains: A northern Hornet K2E proximal to northern Hornet development and a Hornet K2E proximal to southern Hornet development. Each domain was analysed for top cuts and had variography completed separately. Rubicon K2E has search distances of 35 m for direction 1 and 35 m for direction 2 in the high data density domain and 165 m for direction 1 and 85 m for direction 2 in the low data density domain. Pegasus K2E has search distances of 50 m for direction 1 and 30 m for direction 2 for both the upper and lower domains. Hornet K2E domains have search distances of 40 m for direction 1 and 20 m for direction 2 for the high data density domain and 65 m for direction 1 and 40 m for direction 2 in the low density domain. Three search passes were used in all domains. Restrictions by drill hole type were applied to both domains in the Rubicon K2E. Restrictions by drill hole were applied to Pegasus and Hornet K2E. • K2B (Rubicon and Hornet) - Rubicon and Hornet K2B divided into two subdomains based on data density. Each domain was analysed for top cuts and had variography completed separately. All Rubicon K2B domains have search distances of 70 m for direction 1 and 40 m for direction 2. Hornet K2B has search distances of 80 m for direction 1 and 60 m for direction 2 for the high-density subdomain and 250 m for direction 1 and 200 m for direction 2 for the low-density subdomain. Three search passes were used in all domains. Estimation was completed using a soft boundary between the high and low-density subdomains. No restrictions by drill hole or drill hole type have been applied. • Nugget (Rubicon)- includes one domain which was top cut and had variography analysis completed with ranges of 80 m in direction 1 and 40 m in direction 2. Restriction by drill hole was applied.

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Criteria	Commentary
	• Footwall (Rubicon and Hornet) – Rubicon footwall is divided into two subdomains based on data density: high density around development levels and lower density for the remainder. High data density uses search directions of 20 m for direction 1 and 2. The lower data density domain has search distances of 60 m for direction 1 and 55 m for direction 2. Each domain was analysed for top cuts and had variography completed separately. Hornet footwall comprises two domains in upper and lower levels – Hornet foot wall and hornet footwall upper. Hornet footwall domain has a search distance of 40 m for direction 1 and 30 m for direction 2. Hornet Footwall upper had uses search distances of 40 m in direction 1 and 20 m in direction 2. Three search passes were used in all domains. Estimation was completed using a soft boundary between the Rubicon footwall high and low-density subdomains. Restriction by drill hole type was applied to both Rubicon and Hornet footwall restriction by drillhole ID was used for Hornet footwall upper. • Bell (Pegasus) – includes one domain which was not top cut and had variography analysis with ranges of 50 m in direction 1 and 15 m in direction 2. Three search passes were used. Restriction by drill hole was applied. • FWVN (Pegasus) – includes one domain which was not top cut. There was insufficient data for variographic analysis therefore ID2 was used for estimation. Pegasus CMV variography with NNW plunge direction was used for rotation angles in the ID2 estimate. Three search passes were used. Restriction by drill hole was applied. • INTW (Pegasus) – includes one domain which was top cut. There was insufficient data for variographic analysis therefore isotropic search was used for estimation. Three search passes were used. Restriction by drill hole was applied. • CMV (Drake)- divided into two subdomains based on data density: high density near surface and lower density at depth. Both domains were analysed for top cuts and had variography completed. Each domain has a search distance of 200 m for direction 1 and 150 m for direction 2. Three search passes were used. Estimation was completed using a soft boundary between the high and low-density domains and between adjacent CMV domains (Moonbeam to the north and Pegasus to the south). No restrictions by drill hole or drill hole type have been applied. • Halo (Drake) – divided into the Hanging wall (HW) and Footwall (FW) domains either side of the Drake CMV. Both domains were analysed for top cuts separately. Drake CMV variography was used. Three search passes were used. No restrictions by drill hole or drill hole type have been applied. • HORVQ, ALT1, ALT2, ALT3, ALT4, ALT5, LEAF, HONEY (Hornet) – all comprised single estimation domains and had variographic analysis completed. All domains used ranges of 20 m – 80 m in direction 1 and 20 m – 50 m in direction 2. Three search passes were used. All lodes were restricted by drillhole. • Caesar (Rubicon) comprised of one estimation domain and had variographic analysis completed. This domain used ranges of 130 m for direction 1 and 80 m for direction 2. • RK2BFW (Rubicon) comprised of one estimation domain. There was insufficient data for variographic analysis therefore ID2 search was used. This domain used ranges of 15 m for direction 1 and 7.5 m for direction 2. This estimate was restricted by drillhole. • Hophw & hopfw (Hornet) Hornet open pit foot wall and Hornet open pit hanging wall each consisted of a single estimation domain. These has separate top cut and variographic analysis. Both HOPFW and HOPHW used search ranges of 70 m for direction 1 and 40 m for direction 2. • SPGN (Hornet) comprised of one estimation domain, which was top cut and had variography analysis completed with ranges of 50 m in direction 1 and 30 m in direction 2. • F18 (Hornet) comprised of one estimation domain, which was top cut, there was insufficient data for variographic analysis therefore ID2 was used for estimation. Three search passes were used. No restrictions by drill hole or drill hole type have been applied. • MFZ (Hornet) comprised of one estimation domain, which was top cut. There was insufficient data for variographic analysis therefore ID2 was used for estimation. Hornet CMV variography orientation was used for rotation angles in the ID2 estimate. Estimation was completed using a soft boundary between adjacent CMV domains. This estimate was restricted by drillhole.

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Criteria	Commentary
	• Check estimates have been completed for all lodes. These include Inverse Distance (ID) and Nearest Neighbour (NN) estimates. Isotropic searches have also been tested to corroborate chosen search orientations. • All mineralised zones at RHP and Drake for the current estimate were compared with previous grade and resource models. This allowed a comparison of tonnes and gold grade for each zone and an overall global comparison.
	• No assumptions have been made.
	• No deleterious elements were estimated in these models.
	• Block sizes varied depending on sample density. In areas of high data density (underground face samples with average spacing of 3 m – 4 m) a 5 m x 5 m x 5 m block size was chosen. Low density drill spacing is defined as approximately 30 m or greater and a 10 m x 10 m x 10 m block size was chosen. • Estimates were completed with soft boundaries between varying block size estimates unless a geological feature and contact analysis indicated a hard boundary was required and added together following individual estimation for final validations. • Search ellipse dimensions were derived from the variogram model ranges, or isotropic ranges based on data density where insufficient data was present for variography analysis.
	• Selective mining units were not used during the estimation process.
	• All variables were estimated independently of each other. Density has used estimation parameters based on the equivalent gold estimation for that domain.
	• Hanging wall and footwall wireframe surfaces were created using sectional interpretation. These were used to define the RHP and Drake mineralised zones based on the geology (usually a quartz vein) and gold grade. • CMV (RHP and Drake) - Steeply dipping structure with quartz veining evident from drilling and development. • MFZ (Hornet) – Faulted and stepped CMV-style mineralisation in the Mary Fault Zone. Laminated quartz-vein present but fractured by late-stage faulting. • Polaris (RHP)- Steeply dipping silicified shale structure in the hanging-wall of the CMV with quartz stringers evident from drilling and underground development. • K2E (RHP)- Steeply dipping hangingwall structure with quartz veining evident from drilling and underground development. • K2B (Rubicon/Hornet)- Steeply dipping hangingwall structure with quartz veining evident from drilling and underground development. • Bell/Nugget/Nugget3 (Pegasus/Rubicon) – Low angled dilatational fault zones with quartz veining evident from drilling and underground development. • Honey, Alteration 1/2/3/4/5, HORVQ/Caesar/F18/SPGN (Hornet hangingwall mineralised zones) - Sheared and silicified shale with quartz stringers evident from drilling and underground development. • Halo (Drake)- Steeply dipping hangingwall and footwall brecciated veining and shearing directly adjacent to the Drake CMV. • For mine planning purposes a waste model is created by projecting the hanging wall and footwall surfaces 15 m either side. A default grade of 0.1 g/t is assigned and the same resource classification as the adjacent ore lode is applied.
	• Top cuts were applied to the composited sample data with the intention of reducing the impact of outlier values on the average grade. Top cuts vary by domain (ranging from 4 g/t to 250 g/t for individual domains). • The top cut values are applied in several steps, using influence limitation top capping. A top cut (AU) and non-top cut (*_NC) variable is created, as well as a spatial variable (*_IL) which only has values where the top cut values appear; this applies to gold top cutting only. For example, where gold requires a top cut, the following variables will be created and estimated: • AU (top cut gold). • AU_NC (non- top-cut gold).

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<table>
<tr><th>Criteria</th><th>Commentary</th></tr>
<tr><td></td><td>
• AU_IL (spatial variable; values present where AU data is top cut).
• The top-cut and non-top cut values are estimated using search ranges based on the modelled gold variogram, and the *_IL values estimated using very small ranges (e.g.,5 m x 5 m x 5 m). Where the *_IL values produce estimated blocks within these restricted ranges, the *_NC estimated values replace the original top cut estimated values (AU).
• The same principle has been applied to produce a ‘lower-cut’ to the composited sample data with the intention of limiting the impact of high-grade samples on genuine low-grade areas, especially where there is an order of magnitude difference in assayed grade. A spatial variable (*_LC) is created using the non-top cut (*_NC) variable which only has values where the low-cut values appear; this applies to gold low cutting only. For example, where gold requires a low cut, the following variables will be created and estimated:
• AU_NC (non- cut gold).
• AU_LC (spatial variable; values present where AU data is low-cut).
• The non-top cut values are estimated using search ranges based on the modelled gold variogram, and the *_LC values estimated using small ranges (e.g.,30 m x 20 m x 15 m). Where the *_LC values produce estimated blocks within these restricted ranges, the *_LC estimated values replace the original top cut estimated values (AU). Multiple iterations are tested with different search distance and minimum sample fulfillments applied.
• A hard top cut is applied instead of/as well in the following situations:
• If there are extreme outliers within an ore domain.
• If the area has a history of poor reconciliation (i.e., overcalling).
</td></tr>
<tr><td></td><td>
• Statistical measures of Kriging error, such as Kriging Efficiency and Slope of Regression, are used to assess the quality of the estimation for each domain.
• Differences between the declustered, top-cut composite data set and the average model grade must be within 10%.
• Swath plots comparing declustered, top-cut composites to block model grades are created and visual plots are prepared summarising the critical model parameters.
• Visually, block grades are assessed against drill hole and face data.
</td></tr>
<tr><td>Moisture</td><td>• Tonnages are estimated on a dry basis.</td></tr>
<tr><td>Cut-off parameters</td><td>
• The cut-off grades were estimated using projected site mining costs, processing costs and site general administration costs.
• a gold price of A$2,200/oz was utilised.
• The cut-off grades applied to the deposit areas are listed below:
<table>
<tr><th>Deposit</th><th>COG (g/t Au) (m)</th></tr>
<tr><td>Open Pits (excl Boundary)</td><td>0.40 g/t Au</td></tr>
<tr><td>Raleigh & Raleigh North UG</td><td>2.44 g/t Au</td></tr>
<tr><td>East Kundana JV UG</td><td>2.44 g/t Au</td></tr>
</table>
•
</td></tr>
<tr><td>Mining factors or assumptions</td><td>• The Mineral Resource estimations for open pit resource have been reported within pit optimisation shells generated in Whittle software. Mining costs are based on regolith type and depth below surface. For Mineral Resources, no dilution or recovery factors have been applied. Mining selectivity of 10m (x) by 10m (y) by 5m (z) has been applied.</td></tr>
</table>

Criteria	Commentary
	• The Mineral Resource estimations for underground have been reported within Mining Shape Optimiser objects (MSOs) generated in Datamine or Deswik software. These shapes assume a minimum mining width of 2.5 m with a minimum footwall and hanging-wall slope of 50 to 80 degrees. The minimum strike of the panels is 10.0m and a vertical extent of 5.0m. No external dilution has been applied to the shapes however internal dilution has been applied where required (no estimated grade or sub Inferred Mineral Resource blocks) at 0.0 g/t. • All Mineral Resources have been depleted by prior mining. The prior mining is represented by detailed surveys completed over the life of the project. These surveys are represented by 3D models which have been used to flag blocks as mined or not. MSO's are also validated and removed if they are considered to be sterilised (low likelihood of being mined) by current mine development.
Metallurgical factors or assumptions	• Reasonable assumptions for metallurgical extraction factored into the resource estimate are based on previous processing of the ore from the nearby deposits at Kundana, Kunanalling and Carbine through the various historic and operational CIP/CIL processing facilities within the district (including the Mungari Mill). • Where a deposit has not been previously mined or processed, preliminary deportment and geo-metallurgical studies are completed on ore types to generate metallurgical factors and assumptions to be included in the resource estimate. • Target gold recoveries range from 86% to 95% recovery.
Environmental factors or assumptions	• No significant environmental factors are expected to be encountered regarding the disposal of waste or tailing material. This expectation is based on previous mining and milling history of existing open pit operations with the project area. • Mungari Gold Operations has in place regulatory permits and approvals to continue operations. • A site Environmental team monitors ongoing compliance with approvals and maintains the site in good standing with regulators.
Bulk density	• A thorough investigation into average density values for the various lithological units at RHP and Drake was completed and the mean densities by lithology were coded into the database. Where there were no measurements for a specific lithology and default of 2.8 t/m3 was applied. Density was then estimated by Ordinary Kriging using the associated gold estimation parameters for that domain. Post estimation, default density values for the oxide and transitional zones were applied, based on regional averages.
	• No significant voids are encountered in the ore zones and underground environment
	• Assumptions on the average bulk density of individual lithologies, based on 7,543 bulk density measurements at RHP and Drake. Assumptions were also made based on regional averages, on the default densities applied to oxide (1.8 t/m^3) and transitional (2.3 t/m^3) material, due to a lack of data in these zones.
Classification	• Classification is based on a series of factors including: • Geologic grade continuity. • Density of available drilling. • Statistical evaluation of the quality of the kriged estimate. • Confidence in historical data, based on the new Data Class system.
	• All relevant factors have been given due weighting during the classification process.
	• The resource estimation methodology is considered appropriate, and the estimated grades reflect the Competent Persons view of the deposit.
Audits or reviews	• All resource models have been subjected to internal peer review.
Discussion of relative accuracy/ confidence	• These mineral resource estimates are considered as robust and representative of the RHP and Drake styles of mineralisation. The relative accuracy of the Mineral Resource estimate is reflected in the reporting of the Mineral Resource as per the guidelines of the 2012 JORC Code.
	• The statement relates to global estimates of tonnes and grade.

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Criteria	Commentary
	• No reconciliation factors are applied to the resource post-modelling.

1.3 Pode and Hera: Mineral Resource – 31 December 2022

Section 1: Sampling Techniques and Data

Criteria	Commentary
Sampling techniques	• A combination of sample types was used to collect material for analysis; underground and surface diamond drilling (DD), surface Reverse Circulation drilling (RC) and face channel (FC) sampling. Tabulated statistics below include the Hornet, Rubicon, Pegasus, Drake trend. A more detailed breakdown will be made available in the Pode/Hera 2022 Resource Report.

	RHP, Drake, Pode,Hera		
Type	No.of Holes	Total Metres	No. of Samples
DD	4,770	869,035	571,408
FS	12,829	62,292	127,950
RC	1,307	124,002	11,534
RCDD	62	21,433	1,144
TOTAL	18,968	1,076,762	712,036

	• DD drilling is sampled within geological boundaries with a minimum (0.3 m) and maximum (1.0 m) sample length. Face channel sampling is constrained within geological and mineralised boundaries with a minimum (0.2 m) and maximum (1.0 m) channel sample length. In some cases, smaller samples (0.1 m – 0.2 m) have been taken to account for narrower structures in the face. Where possible, face sampling is conducted from channels perpendicular to the vein structure.
	• DD drill core was nominated for either half core or full core sampling. Samples designated for half core were cut using an automated core saw. The mass of material collected was dependent on the drillhole diameter and sampling interval selected. • A sample size of at least 3 kg of material was targeted for each face sample interval. • All samples were delivered to a commercial laboratory where they were dried and crushed to 90% of material ≤3 mm. At this point, samples greater than 3 kg were split using a rotary splitter, then pulverised to 90% ≤75 µm. • A 40 g charge was selected for fire assay for all recent samples. Historically, charge weights of 50 g have also been used.
Drilling techniques	• Both Reverse Circulation and Diamond Drilling techniques are used to drill the Kundana deposits. • Surface diamond drillholes were completed using HQ2 (63.5 mm), whilst underground diamond drillholes were completed using NQ2 (50.5 mm). • Historically, core was orientated using the Reflex ACT Core orientation system. Currently, core is orientated using the Boart Longyear Trucore Core Orientation system. • RC Drilling was completed using a 5.75” drill bit, downsized to 5.25” at depth. • In many cases RC pre-collars were drilled, followed by diamond tails. Pre-collar depth was determined in the drill design phase.
Drill sample recovery	• For DD drilling, any core loss is recorded on the core block by the driller. This is then captured by the logging geologist and entered as an interval into the hole log.

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Criteria	Commentary
	• Contractors adjust the rate and method of drilling if recovery issues arise. All recovery is recorded by the drillers on core blocks. This is checked and compared to the measurements of the core by the geological team. Any issues are communicated back to the drilling contractor.
	• Recovery was excellent for diamond core and no relationship between grade and recovery was observed. Average recovery across the Kundana camp is at 99%. No specific areas within Pode had issues with recovery.
Logging	• All diamond core is logged for lithology, veining, alteration, mineralisation, and structural data. Structural measurements of specific features are also taken through oriented zones. • Logging is entered in AcQuire using a series of drop-down menus which contain the appropriate codes for description of the rock. • All underground faces are logged for lithology and mineralisation. Logging is captured on a face sample sheet underground which is then transferred to AcQuire. Faces are then input into AcQuire using a series of drop-down menus which contain appropriate codes for description of the rock.
	• All core logging is qualitative with mineralised zones assayed for quantitative measurements. Every core tray is photographed wet. • All underground faces are logged and sampled to provide both qualitative and quantitative data. Faces are washed down and photographed before sampling is completed.
	• For all drillholes, the entire length of the hole is logged.
Sub-sampling techniques and sample preparation	• Diamond core is cut using an automated core saw. Sampling and cutting methodology is dependent on the type of drilling completed. Half core is utilised for exploration drilling and Resource Definition drilling. Grade Control and rare Resource Definition drill holes are whole core sampled.
	• RC samples are split using a rig-mounted cone splitter to collect a sample 3 - 4 kg in size from each 1m interval. These samples were utilised for any zones approaching known mineralization and from any areas identified as having anomalous gold. Outside known mineralised zones spear samples were taken over a 4 m interval for composite sampling.
	• Preparation of samples was conducted at Bureau Veritas' Kalgoorlie facilities; commencing with sorting, checking, and drying at less than 110°C to prevent sulphide breakdown. Samples are jaw crushed to a nominal -6 mm particle size. If the sample is greater than 3 kg a Boyd crusher with rotary splitter is used to reduce the sample size to less than 3 kg (typically 1.5 kg) at a nominal <3 mm particle size. • The entire crushed sample (if less than 3 kg) or sub-sample is then pulverized to 90% ≤75 µm, using a Labtechnics LM5 bowl pulveriser. 400 g Pulp subsamples are then taken with an aluminium scoop and stored in labelled pulp packets. • The sample preparation is considered appropriate for the deposit.
	• Standard procedures are used for all processes within the laboratory. Grind checks are performed at both the crushing stage (3 mm) and pulverising stage (75 µm), requiring 90% of material to pass through the relevant size.
	• Umpire sampling is performed monthly, where 3% of the samples are sent to the umpire laboratory for processing. Umpire samples of faces were analysed using a 40g charge weight.
	• The sample sizes are considered appropriate for the material being sampled.
Quality of assay data and laboratory tests	• A 40 g fire assay charge for diamond drillholes and a 40 g charge for face samples is used with a lead flux in the furnace. The prill is totally digested by HCl and HNO3 acids before Atomic Absorption Spectroscopy (AAS) determination for gold analysis.
	• No geophysical tools were used to determine element concentrations.

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Criteria	Commentary
	• Certified reference materials (CRMs) are inserted into the sample sequence randomly at a rate of 1 per 20 samples to ensure correct calibration. Any values outside of 3 standard deviations are re-assayed with a new CRM. • Blanks are inserted into the sample sequence at a rate of 1 per 20 samples. The insertion points are selected at random, except where high grade mineralisation is expected. In these cases, a Blank is inserted after the high-grade sample to test for contamination. Results greater than 0.2 g/t if received are investigated, and re-assayed if appropriate. New pulps are prepared if anomalous results cannot be resolved. • Barren flushes are regularly inserted after anticipated high gold grades at the pulverising stage. • No field duplicates were submitted for diamond core or face samples. • Pulp duplicates are requested after any ore zone. These are indicated on the sample sheet and the submission sheet. • When visible gold is observed in core, a quartz flush is requested after the sample. • Laboratory performance was monitored using the results from the QA samples mentioned above. This was supplemented by the internal QA samples used by the laboratories, which included pulp duplicates and CRMs. • The QA studies indicate that accuracy and precision are within industry accepted limits.
Verification of sampling and assaying	• All significant intersections are verified by another geologist during the drill hole validation process, and later by a Competent Person to be signed off.
	• No twinned holes were drilled at Pode. Re-drilling of some drillholes has occurred due to issues downhole (e.g., bogged rods). These have been captured in the database with an 'A' suffix. Re-drilled holes are logged and sampled, whilst the original drillhole is logged, but not sampled.
	• Geological logging and sampling are recorded directly into AcQuire. Assay files are received in .csv format and loaded directly into the database using an AcQuire importer object. Assays are then processed through a form in AcQuire for QAQC checks. Hardcopy and noneditable electronic copies are stored.
	• No adjustments have been made to this assay data.
Location of data points	• Planned holes are marked up by the mine survey department using a total station survey instrument in mine grid (Kundana 10). The actual hole position is then located by the mine survey department once drilling is completed. In some cases, drillhole collar points are measured off survey stations if a mark-up cannot be completed. • Holes are lined up on the collar point using the DHS Azimuth Aligner. Planned azimuths and dips of the holes are downloaded to the aligner which is then placed on the rod string to align the hole for drilling. • During drilling, single shot surveys are conducted every 30 m to track the deviation of the hole and to ensure it stays close to design. This is performed using the DeviShot camera which measures the gravitational dip and magnetic azimuth. Results are uploaded from the Devishot software into a .csv format which is then imported into the Acquire database. At the completion of the hole, a Multishot (using the Deviflex non-magnetic strain gauge instrument) survey is completed, taking measurements every 3 m to ensure accuracy of the hole. This is converted to csv format and imported into the Acquire database.
	• Collar coordinates are recorded in mine grid (Kundana 10) and transformed into MGA94_51.
	• Quality topographic control has been achieved through Lidar data and survey pickups of holes over the last 15 years.
Data spacing and distribution	• Drillhole spacing varies across the deposit. Resource Targeting drilling at an 80 m x 80 m nominal spacing is infilled during Resource Definition drilling down to an average of 30 m x 30 m. Grade Control drilling follows development and is generally comprised of stab drilling from the development drive at 10 m to 15 m drill centres.
	• The data spacing and distribution is considered sufficient to support the resource and reserve estimates.
	• No sample compositing has been applied.

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Criteria	Commentary
Orientation of data in relation to geological structure	• Pode structures in the Kundana area dip on average (50°) to the west (local grid). Diamond drilling was designed to target the orebodies perpendicular to this orientation to allow for a favourable intersection angle. In instances where this was not possible (primarily due to drill platform location), drilling was not completed, or re-designed once a more suitable platform became available. • Drillholes with extremely poor intersection angles are excluded from resource estimation. • No sampling bias is considered to have been introduced by the drilling orientation.
Sample security	• Prior to laboratory submission samples are stored in a secure yard. Once submitted to the laboratories they are stored in a secure fenced compound, tracked through their chain of custody and via audit trails.
Audits or reviews	• No audits have been undertaken of the data and sampling practices.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	Commentary
Mineral tenement and land tenure status	• The Pode deposit is located within the M16/309 and M16/326 mining leases held by the East Kundana Joint Venture (EKJV). The EKJV is majority owned and managed by Evolution Mining (51%). The minority holding in the EKJV is held by Tribune Resources Ltd (36.75%) and Rand Mining Ltd (12.25%). • The tenement on which the Pode deposits are hosted (M16/309) is subject to three royalty agreements. The agreements that are on M16/309 are the Kundana-Hornet Central Royalty, the Lake Grace Royalty and the Kundana Pope John Agreement No. 2602-13. • No known impediments exist, and the tenements are in good standing.
Exploration done by other parties	• The first reference to the mineralization style encountered at the Kundana project was the mines department report on the area produced by Dr. I. Martin (1987). He reviewed work completed in 1983 – 1984 by a company called Southern Resources, who identified two geochemical anomalies, creatively named Kundana #1 and Kundana #2. The Kundana #2 prospect was subdivided into a further two prospects, dubbed K2 and K2A. • Between 1987 and 1997, limited work was completed. • Between 1997 and 2006 Tern Resources (subsequently Rand Mining and Tribune Resources), and Gilt-Edged Mining focused on shallow open pit potential, which was not considered viable for Pegasus, however the Rubicon open pit was considered economic, and production commenced in 2002. • In 2011, Pegasus was highlighted by an operational review team and follow-up drilling was planned through 2012.

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Criteria	Commentary
Geology	• The Kundana camp is situated within the Norseman-Wiluna Greenstone Belt, in an area dominated by the Zuleika shear zone, which separates the Coolgardie domain from the Ora Banda domain. • K2-style mineralisation (Pegasus, Rubicon, Hornet, Drake) consists of narrow vein deposits hosted by shear zones located along steeply dipping overturned lithological contacts. The K2 structure is present along the contact between a black shale unit (Centenary Shale) and intermediate volcaniclastics (Black Flag Group). • Minor mineralisation, termed K2B, also occurs further west, on the contact between the Victorious basalt and Bent Tree Basalt (both part of the regional upper Basalt Sequence). Additional mineralisation includes the K2E and K2A veins, Polaris/Rubicon Breccia (Silicified and mineralised Shale) and several other HW lodes adjacent to the main K2 structure. • A 60° W dipping fault, offsets this contact and exists as a zone of vein-filled brecciated material hosting the Pode-style mineralisation at Pegasus and the Nugget lode at Rubicon.
Drill hole Information	• A summary of the data present in the Pode deposits can be found above. • The collar locations are presented in plots contained in the December 2022 resource report. • Drillholes vary in survey dip from +53 to -84 degrees, with hole depths ranging from 8 m to 1,413 m. Average hole depth is 248 m. The assay data acquired from these holes are described in the December 2022 resource report. • All validated drill hole data was used directly or indirectly for the preparation of the resource estimates described in the resource report.
	• The exclusion of the drill hole information does not materially detract from the understanding of this report.
Data aggregation methods	• All reported assay results have been length weighted to provide an intersection width. A maximum of 2 m of barren material (considered < 2 g/t) between mineralized samples has been permitted in the calculation of these widths. Typically grades over 2.0 g/t are considered significant, however, where low grades are intersected in areas of known mineralisation these will be reported. No top-cutting is applied when reporting intersection results.
	• Where an intersection incorporates short lengths of high grade results these intersections will be reported in addition to the aggregate value. These will typically take the form of ##.#m @ ##.##g/t including ##.#m @ ##.##g/t.
	• No metal equivalent values have been used for the reporting of these exploration results.
Relationship between mineralisation widths and intercept lengths	• True widths have been calculated for intersections of the known ore zones based on existing knowledge of these structures.
	• Both the downhole width and true width have been clearly specified when used.
	• Not applicable.
Diagrams	• Appropriate plans and section have been included at the end of this table and in the December 2022 resource report.
Balanced reporting	• Both high and low grades have been reported accurately, clearly identified with the drill hole attributes and ‘From’ and ‘To’ depths.
Other substantive exploration data	• No other material exploration data has been collected for this area.
Further work	• Further drilling will continue to define the extents of the Pode-style mineralisation. • Further work will include mining studies appropriate to EVNs current open-cut and underground mining methods. If mining studies yield a positive result, infill resource definition is planned to convert Inferred Mineral Resource category to Indicated Mineral Resource category and to test for extensions to mineralisation along strike and down-dip that would likely impact the economic outcome. • A feasibility study is progressing to determine the economics of reducing the Mungai Processing facility unit cost by increasing throughput from 2.0Mpta to 4.2Mtpa. This will likely reduce COGs for the MGO Mineral Resource Statement.
	• Appropriate diagrams accompany this release.

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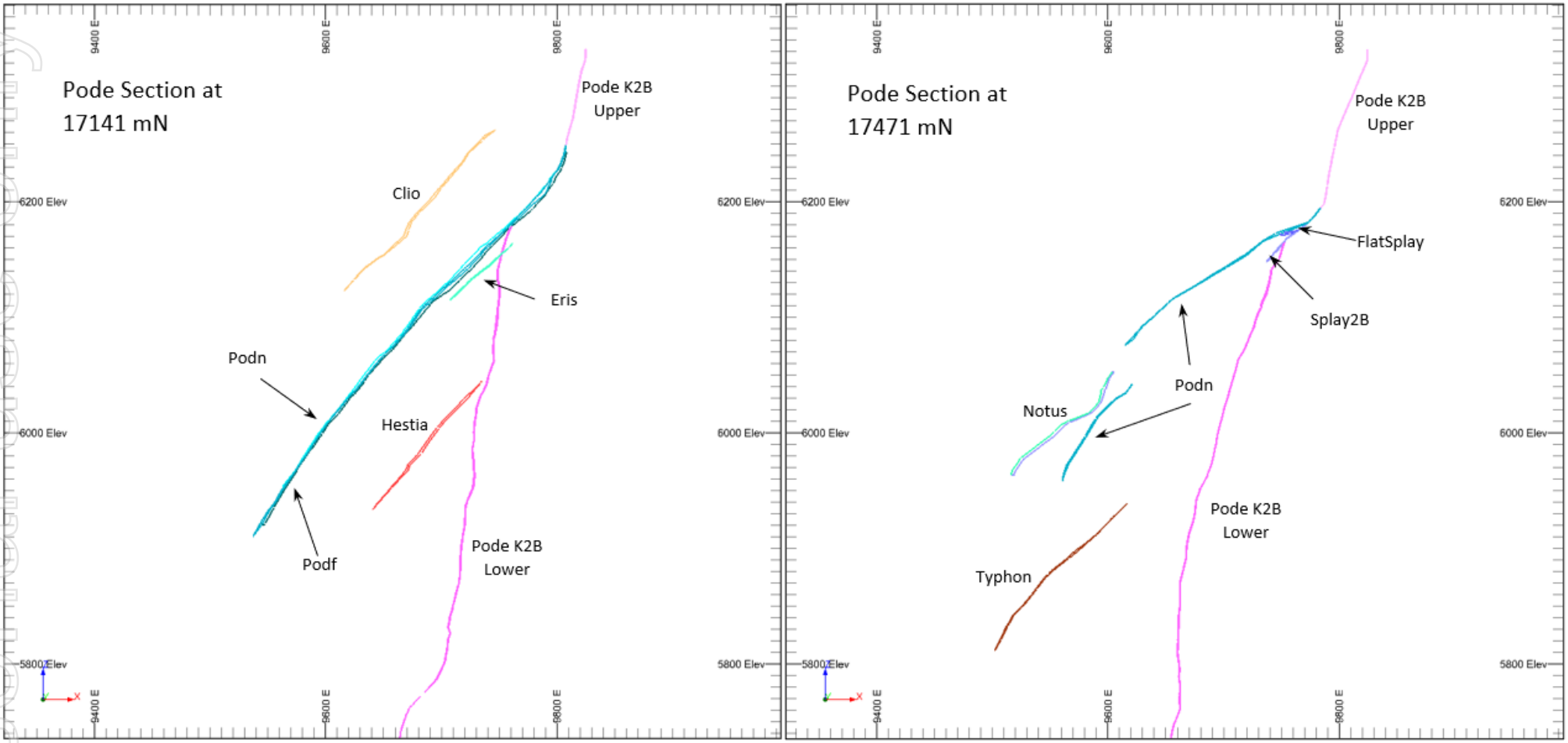


Figure 1. Cross section views of Pode ore lodes

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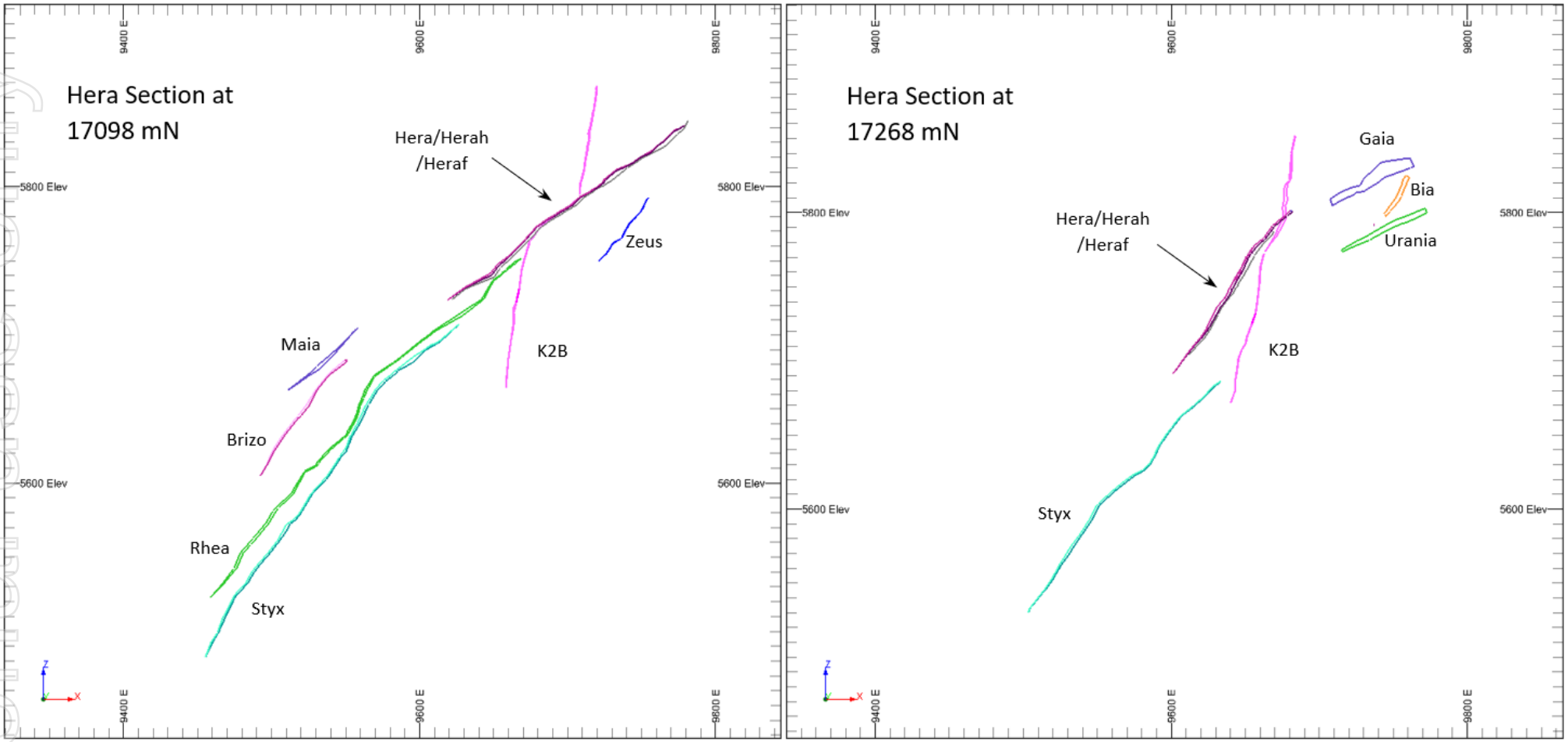


Figure 2. Cross section views of Hera ore lodes

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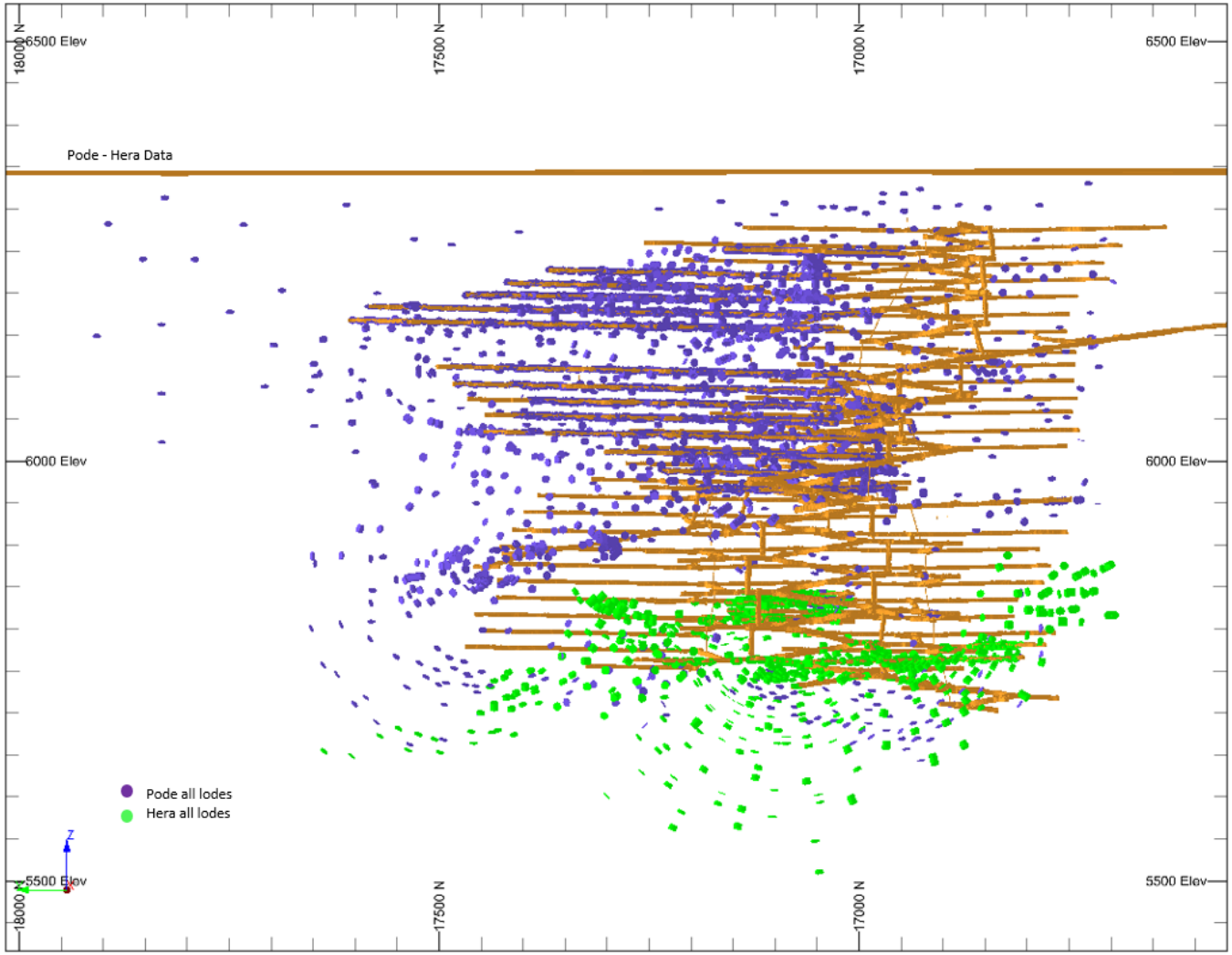


Figure 3. Long section view of Pode and Hera ore lodes and data used in resource estimations

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Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	Commentary
Database integrity	• Sampling and logging data are either recorded on paper and manually entered into a database system or is captured digitally via a logging laptop and directly loaded into the database system. There are checks in place to avoid duplicate holes and sample numbers. Where possible, raw data is loaded directly into the database from laboratory and survey-tool derived files.
	• The complete exported database (including drill and face samples) is imported into Datamine and checked visually for any apparent errors i.e. holes or faces sitting between levels or not on surface DTM's. Multiple checks are then made on numerical data. These include: • Empty table checks to ensure all relevant fields are populated. • Unique collar location check. • Distances between consecutive surveys is no more than 60m for drill-holes. • Differences in azimuth and dip between consecutive surveys of no more than 0.3 degrees. • The end of hole extrapolation from the last surveyed shot is no more than 30 m. • Underground face sample lines are not greater than +\- 5 degrees from horizontal. • Errors are corrected where possible. When not possible the data is resource flagged as "No" in the database and the database is re-exported. This data will not be used in the estimation process. • Several drilling programs completed between 2014 and 2016 had erroneous meter depths recorded therefore these drill holes have been omitted from the ore wireframe interpretations and flagged as invalid. However, where there were no QAQC issue with the assays, the correct intervals have been recorded, the translation in the easting direction required for them to be in the 'correct' location (based on development above and below) applied and these intervals were appended to the data set before compositing. • In addition to being Resource Flagged as "Yes" or "No", drill holes are assigned a Data Class, which provides a secondary level of confidence in the data quality. Data Class (DC) values range from 0 to 3, with criteria summarised below: • DC 3 = Recent data; all data high quality, validated and all original data available. • DC 2 = Historic data; may or may not have all data in AcQuire or hard copy available but has proximity to recent drilling which confirms the dip, width and tenor. Used to assist in classification. • DC 1 = Historic data; same criteria as DC 2 but cannot be verified with recent drilling, i.e., too far away, or dissimilar dip, width and/or tenor to recent drilling. Not used in Resource estimate. • DC 0 = Historic data; no original information or new drilling in proximity to verify. Not used in Resource estimate.
Site visits	• The geological interpretations underpinning these resource models were prepared by geologists working in the mine who were in direct, daily contact with the ore body. The estimation of grades was undertaken by personnel familiar with the ore body and the general style of mineralisation encountered. The Senior Resource Geologist, a Competent Person for reviewing and signing off on the Pode estimate maintained a site presence throughout the process.
	• Not applicable

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Criteria	Commentary
Geological interpretation	• The interpretation of the Pode deposits were carried out using a systematic approach to ensure continuity of the geology and estimated mineral resource. The confidence in the geological interpretation is high and is supported with information acquired during ore development as well as from underground and surface diamond drilling. The interpretation of all Pode mineralised wireframes was conducted using the sectional interpretation method in Datamine RM software. Most Pode lodes have been interpreted in plan-view section (with the remainder in cross-section view). Where development levels were present, sectional interpretation was completed at approximately 5 m spacing. Where only drilling data was present, sectional interpretation was completed at approximately 10 m- 20 m spacing. Checks were made to ensure that the wireframed volume agreed with the true ore widths of drillhole intersections. As a rule, wireframe extrapolation was limited to one half of the average drill spacing.
	• All available geological data was used in the interpretation including surface mapping, DD and RC drill holes, underground face channel data, 3D photogrammetry and regional and local structural models.
	• No alternative interpretations have been proposed.
	• The interpretation of the Pode mineralisation is based on the presence of mineralised structure (veining and shear), ore-bearing mineralogy (gold and associated sulphides), assayed samples and continuity between sections.
	• Individual Pode mineralised envelopes are reasonably continuous at the current drill spacing, as similar mineralisation styles, structures and grade tenor exists between adjacent drill holes. • Offsetting structures are not known to be present in Pode although significant undulations exist which may have some impact on continuity of the mineralised trends and metal estimated within. • Mineralised envelopes for Pode are confined to the Victorious (porphyritic) and Bent Tree (fine-grained) basalt lithological units.
Dimensions	• The strike length of the different ore systems varies from ~200 m to ~1,200 m. The individual ore bodies occur in a major regional Zuleika shear system extending over tens of kilometres. • Ore body widths are typically in the range of 0.4 m - 2 m. The widest orebody is Hera Halo at approximately 2 m. The narrowest is Zeus at approximately 0.4 m. The PodN structure has an average thickness of 1.5 m. • Mineralisation is known to occur from the base of cover to ~800 m below surface and is open in all directions.
Estimation and modelling techniques	• Pode mineralised zones used direct grade estimation by Ordinary Kriging (unless otherwise stated) supported by composited sample data. Composite lengths of 1 m were used for most lodes (except Maia and Athena lodes, which used 0.5m composite lengths), determined from statistical analysis of all sample lengths in the estimation dataset. • In smaller mineralised zones where construction of a coherent variogram was not possible, Inverse Distance has been used. All estimation was completed using Datamine RM software. • Details of estimation by Pode ore lode is summarised below: • PodN (Pode) – Divided into two subdomains based on data density. Data was top cut to 190 g/t using the influence limitation approach. In addition to this a hard topcut of 400 g/t was used to limit the impact of genuinely anomalous data points. Variography was completed on the composited data file with searches completed in three passes. For the high data-density estimate, search ranges of 50 m in direction 1 (dir1), 30 m in direction 2 (dir2) and 25 m in direction 3 (dir3) were used. For the low data-density estimate, search ranges of 100 m in dir1, 80 m in dir2 and 50 m in dir3 were used. Dynamic anisotropy has been used for the estimate, with the plunge component hard coded to 40° based on the variogram-derived search orientation. • PodH (Pode) – Divided into two subdomains based on data density. A hard topcut of 25 g/t was used to limit the impact of anomalous data points. Variography was completed on the composited data file with searches completed in three passes. For the high data-density estimate, search ranges of 15 m in dir1, 15 m in dir2 and 10 m in dir3 were used. For the low data-density estimate, search ranges of 80 m

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Criteria	Commentary
	in dir1, 70 m in dir2 and 20 m in dir3 were used. Dynamic anisotropy has been used for the estimate, with the plunge component hard coded to 40° based on the variogram-derived search orientation. • PodF (Pode) – Divided into two subdomains based on data density. A hard topcut of 20 g/t was used to limit the impact of anomalous data points. Variography was completed on the composited data file with searches were completed in three passes. For the high data-density estimate, search ranges of 15 m in dir1/dir2 and 10 m in dir3 were used. For the low data-density estimate, search ranges of 80 m in dir1, 70 m in dir2 and 20 m in dir3 were used. Dynamic anisotropy has been used for the estimate, with the plunge component hard coded to 40° based on the variogram-derived search orientation. • Splay2B (Pode) – Estimated as a single domain. A hard topcut of 30 g/t was used to limit the impact of anomalous data points. No variography completed due to lack of data pairs in domain. Searches were completed in three passes. Search ranges of 30 m in dir1, 30 m in dir2 and 30 m in dir3 were used. • K2B (Pode and Hera) – Divided into two subdomains based on grade. Top cutting was completed separately on the high-grade and low-grade subdomains (60 g/t and 15 g/t respectively). Variography was completed on the composited data files separately with searches completed in three passes. For the high-grade estimate, search ranges of 90 m in dir1, 50 m in dir2 and 30 m in dir3 were used. For the low-grade estimate, search ranges of 50 m in dir1/2/3 (isotropic) were used. ID was used for both subdomains. • Hestia (Pode) – Estimated as a single domain. Data was top cut to 30 g/t using the influence limitation approach. Variography was completed on the composited data file with searches completed in three passes. Search ranges of 50 m in dir1, 30 m in dir2 and 15 m in dir3 were used. • Ceto (Pode) – Estimated as a single domain. Data was top cut to 10 g/t using the influence limitation approach. Variography was completed on the composited data file with searches completed in three passes. Search ranges of 60 m in dir1, 40 m in dir2 and 30 m in dir3 were used. • Eris (Pode) – Estimated as a single domain. Data was top cut to 8 g/t using the influence limitation approach. No variography completed due to lack of data pairs in domain. Continuity fans analysed to ascertain search orientation and anisotropy. Searches were completed in three passes. Search ranges of 75 m in dir1, 35 m in dir2 and 15 m in dir3 were used. • Clio (Pode) – Estimated as a single domain. Data was top cut to 12 g/t using the influence limitation approach. No variography completed due to lack of data pairs in domain. Continuity fans analysed to ascertain search orientation and anisotropy. Searches were completed in three passes. Search ranges of 80 m in dir1, 50 m in dir2 and 30 m in dir3 were used. • Notus (Pode) – Estimated as a single domain, no top-cut applied as no anomalous samples present and coefficient of variance within acceptable range. No variography completed due to lack of data pairs in domain. Searches were completed in three passes. Search ranges of 70 m in dir1, 40 m in dir2 and 15 m in dir3 were used. • Kratos (Pode) – Estimated as a single domain. Data was top cut to 10 g/t using the influence limitation approach. No variography completed due to lack of data pairs in domain. Continuity fans analysed to ascertain search orientation and anisotropy. Searches were completed in three passes. Search ranges of 80 m in dir1, 50 m in dir2 and 30 m in dir3 were used. • Ares (Pode) – Estimated as a single domain. No top-cut applied as no anomalous samples present and coefficient of variance within acceptable range. No variography completed due to lack of data pairs in domain. Continuity fans analysed to ascertain search orientation and anisotropy. Searches were completed in three passes. Search ranges of 60 m in dir1/3 and 3 were used. • Athena (Pode) – Estimated as a single domain. Data was top cut to 28 g/t using the influence limitation approach. No variography completed due to lack of data pairs in domain. Continuity fans analysed to ascertain search orientation and isotropy. Searches were completed in three passes. Search ranges of 30 m in dir1, 30 m in dir2 and 30 m in dir3 were used.

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Criteria	Commentary
	• Apollo (Pode) – Estimated as a single domain. Data was top cut to 8 g/t using the influence limitation approach. Variography was completed on the composited data file, indicating grade continuity plunging moderately to the north. Searches were completed in three passes. Search ranges of 40 m in dir1, 20 m in dir2 and 20 m in dir3 were used. • PodS (Pode) – Estimated as a single domain. No top cutting required. No variography completed due to lack of data pairs in domain. Continuity fans analysed to ascertain search orientation and anisotropy. Searches were completed in three passes. Search ranges of 40 m in dir1, 40 m in dir2 and 40 m in dir3 were used. • Typhon (Pode) – Estimated as a single domain. Data was top cut to 12 g/t using the influence limitation approach. No variography completed due to lack of data pairs in domain. Continuity fans analysed to ascertain search orientation and anisotropy. Searches were completed in three passes. Search ranges of 60 m in dir1, 40 m in dir2 and 30 m in dir3 were used. • Hera (Hera) – Divided into two subdomains based on data density. Data was top cut to 400 g/t for the high-grade subdomain and 35 g/t for the low-grade subdomain using the influence limitation approach. Variography was completed on the composited data file with searches were completed in three passes. For the high data-density estimate, search ranges of 20 m in dir1/dir2 and 15 m in dir3 were used. For the low data-density estimate, search ranges of 35 m in dir1, 25 m in dir2 and 15 m in dir3 were used. Categorical Indicated Kriging has been used for the estimate using dynamic anisotropy with the plunge component hard coded to 40° based on the variogram-derived search orientation. • Hera Footwall Halo (Hera) – Divided into two subdomains based on data density. Hard top cuts were applied to the data of 25 g/t for the high-grade subdomain and 8 g/t for the low-grade subdomain. Search ranges of 30 m in dir1/dir2 and 15 m in dir3 were used. • Hera Hangingwall Halo (Hera) – Divided into two subdomains based on data density. Hard top cuts were applied to the data of 30 g/t for the high-grade subdomain and 6 g/t for the low-grade subdomain. For the high data-density estimate, search ranges of 30 m in dir1, 20 m in dir2 and 10 m in dir3 were used. For the low data-density estimate, search ranges of 30 m in dir1, 20 m in dir2 and 15 m in dir3 were used. • Hera Breccia lode (Hera) – Estimated as a single domain. A hard top cut of 7 g/t has been applied to the data. Searches were completed in three passes. Search ranges of 30 m in dir1, 15 m in dir2 and 10 m in dir3 were used. • Rhea (Hera) – Divided into two subdomains based on data density. Data was top cut to 6 g/t for the low-grade subdomain using the influence limitation approach. No top cut was required for the high-grade subdomain. No variography completed due to lack of data pairs in domain. Continuity fans analysed to ascertain search orientation and anisotropy. Searches were completed in three passes. Search ranges of 60 m in dir1, 40 m in dir2 and 30 m in dir3 were used. • Styx (Hera) – Estimated as a single domain. Data was top cut to 16 g/t using the influence limitation approach. No variography completed due to lack of data pairs in domain. Continuity fans analysed to ascertain search orientation and anisotropy. Searches were completed in three passes. Search ranges of 60 m in dir1, 40 m in dir2 and 30 m in dir3 were used. • Brizo (Hera) – Estimated as a single domain. Data was top cut to 6 g/t using the influence limitation approach. No variography completed due to lack of data pairs in domain. Continuity fans analysed to ascertain search orientation and anisotropy. Searches were completed in three passes. Search ranges of 60 m in dir1, 40 m in dir2 and 30 m in dir3 were used. • Maia (Hera) – Estimated as a single domain. No top cutting required. No variography completed due to lack of data pairs in domain. Continuity fans analysed to ascertain search orientation and anisotropy. Searches were completed in three passes. Search ranges of 40 m in dir1, 30 m in dir2 and 15 m in dir3 were used. • Thalia (Hera) – Estimated as a single domain. Data was top cut to 5 g/t using the influence limitation approach. No variography completed due to lack of data pairs in domain. Continuity fans analysed to ascertain search orientation and anisotropy. Searches were completed in three passes. Search ranges of 30 m in dir1, 20 m in dir2 and 10 m in dir3 were used.

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Criteria	Commentary
	• Selene (Hera) – Estimated as a single domain. Data was top cut to 25 g/t using the influence limitation approach. No variography completed due to lack of data pairs in domain. Continuity fans analysed to ascertain search orientation and anisotropy. Searches were completed in three passes. Search ranges of 60 m in dir1, 40 m in dir2 and 30 m in dir3 were used. • Zeus (Hera) – Estimated as a single domain. Data was top cut to 80 g/t using the influence limitation approach. No variography completed due to lack of data pairs in domain. Continuity fans analysed to ascertain search orientation and anisotropy. Searches were completed in three passes. Search ranges of 75 m in dir1, 35 m in dir2 and 15 m in dir3 were used.
	• Check estimates have been completed for all lodes. These include Inverse Distance (ID) and Nearest Neighbour (NN) estimates. Isotropic searches have also been tested to corroborate chosen variogram angles.
	• No assumptions have been made
	• No deleterious elements were estimated in these models.
	• Block sizes varied depending on sample density. In areas of high data-density (underground face samples with average spacing of 3 m – 4 m) a 5 m x 5 m x 5 m block size was chosen. Low density drill spacing is defined as approximately 30 m or greater and a 10 m x 10 m x 10 m block size was chosen. • Estimates were completed with soft boundaries between varying block size estimates (unless a geological feature and contact analysis indicated a hard boundary was required) and added together following individual estimation for final validations. • Search ellipse dimensions were derived from the variogram model ranges, or isotropic ranges based on data density where insufficient data was present for variographic analysis.
	• Selective mining units were not used during the estimation process.
	• All variables were estimated independently of each other. Density has used estimation parameters based on the equivalent gold estimation for that domain.
	• Hanging-wall and foot-wall wireframe surfaces were created using sectional interpretation. These were used to define the Pode/Hera mineralised zones based on the geology (usually a quartz vein) and gold grade. Pode/Hera mineralised zones are predominantly low angled dilatational fault zones with quartz veining evident from drilling (all lodes) and development (PodN, PodF, PodH, Hera and Hera Halo only). • For mine planning purposes a waste model is created by projecting the hanging wall and footwall surfaces 15 m either side. A default grade of 0.1 g/t is assigned and the same resource classification as the adjacent ore lode is applied.
	• Topcuts were applied to the composited sample data with the intention of reducing the impact of outlier values on the average grade. Top cuts were selected based on a statistical analysis of the data with a general aim of not impacting the mean by more than 5% and reducing the coefficient of variation to around 1.2. Topcuts vary by domain and range from 8 to 400 g/t. • The top cut values are applied in several steps, using a technique called influence limitation top cutting. A top cut (AU) and non-top cut (*_NC) variable is created, as well as a spatial variable (*_IL) which only has values where the top cut values appear. For example, where gold requires a top cut, the following variables will be created and estimated: • AU (top cut gold). • AU_NC (non- top-cut gold). • AU_IL (spatial variable; values present where AU data is top cut). • The top-cut and non-top cut values are estimated using search ranges based on the modelled gold variogram, and the *_IL values estimated using very small ranges (e.g., 5 m x 5 m x 5m). Where the *_IL values produce estimated blocks within these restricted ranges, the *_NC estimated values replace the original top cut estimated values (AU).

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<table>
<tr><th>Criteria</th><th>Commentary</th></tr>
<tr><td></td><td>

Statistical measures of Kriging error, such as Kriging Efficiency and Slope of Regression, are used to assess the quality of the estimation for each domain.
Differences in the global grade of the declustered, top-cut composite data set and the average model grade were within 10%, or justification for a difference outside 10% was explicable.
Swath plots comparing declustered, top-cut composites to block model grades are created and visual plots are prepared summarising the critical model parameters.
Visually, block grades are assessed against drill hole and face data.

</td></tr>
<tr><td>Moisture</td><td>

Tonnages are estimated on a dry basis.

</td></tr>
<tr><td>Cut-off parameters</td><td>

The cut-off grades were estimated using projected site mining costs, processing costs and site general administration costs.
a gold price of A$2,200/oz was utilised.
The cut-off grades applied to the deposit areas are listed below:

<table>
<tr><th>Deposit</th><th>COG (g/t Au) (m)</th></tr>
<tr><td>Open Pits (excl Boundary)</td><td>0.40 g/t Au</td></tr>
<tr><td>Raleigh & Raleigh North UG</td><td>2.44 g/t Au</td></tr>
<tr><td>East Kundana JV UG</td><td>2.44 g/t Au</td></tr>
</table>
</td></tr>
<tr><td>Mining factors or assumptions</td><td>

The Mineral Resource estimations for open pit resource have been reported within pit optimisation shells generated in Whittle software. Mining costs are based on regolith type and depth below surface. For Mineral Resources, no dilution or recovery factors have been applied. Mining selectivity of 10m (x) by 10m (y) by 5m (z) has been applied.
The Mineral Resource estimations for underground have been reported within Mining Shape Optimiser objects (MSOs) generated in Datamine or Deswik software. These shapes assume a minimum mining width of 2.5 m with a minimum footwall and hanging-wall slope of 50 to 80 degrees. The minimum strike of the panels is 10.0m and a vertical extent of 5.0m. No external dilution has been applied to the shapes however internal dilution has been applied where required (no estimated grade or sub Inferred Mineral Resource blocks) at 0.0 g/t.
All Mineral Resources have been depleted by prior mining. The prior mining is represented by detailed surveys completed over the life of the project. These surveys are represented by 3D models which have been used to flag blocks as mined or not. MSO’s are also validated and removed if they are considered to be sterilised (low likelihood of being mined) by current mine development.

</td></tr>
<tr><td>Metallurgical factors or assumptions</td><td>

Reasonable assumptions for metallurgical extraction factored into the resource estimate are based on previous processing of the ore from the nearby deposits at Kundana, Kunanalling and Carbine through the various historic and operational CIP/CIL processing facilities within the district (including the Mungari Mill)
Where a deposit has not been previously mined or processed, preliminary deportment and geo-metallurgical studies are completed on ore types to generate metallurgical factors and assumptions to be included in the resource estimate.
Target gold recoveries range from 86% to 95% recovery.

</td></tr>
<tr><td>Environmental factors or assumptions</td><td>

No significant environmental factors are expected to be encountered regarding the disposal of waste or tailing material. This expectation is based on previous mining and milling history of existing open pit operations with the project area.
Mungari Gold Operations has in place regulatory permits and approvals to continue operations.
A site Environmental team monitors ongoing compliance with approvals and maintains the site in good standing with regulators

</td></tr>
</table>

Criteria	Commentary
Bulk density	• A thorough investigation into average density values for the various lithological units at Pode was completed and the mean densities by lithology were coded into the database. Where there were no measurements for a specific lithology and default of 2.8 t/m3 was applied. Density was then estimated by Ordinary Kriging using the associated gold estimation parameters for that domain. Post estimation, default density values for the oxide and transition zones were applied, based on regional averages.
	• Bulk density measurements adequately account for any voids within the measured material.
	• Assumptions on the average bulk density of individual lithologies, based on 14,613 bulk density measurements at Pode and RHP. Assumptions were also made based on regional averages, on the default densities applied to oxide (1.80 t/m3) and transitional (2.30 t/m3) material, due to a lack of data in these zones.
Classification	• Classification is based on a series of factors including: • Geologic grade continuity. • Density of available drilling. • Statistical evaluation of the quality of the kriging estimate. • Confidence in historical data, based on the new Data Class system.
	• All relevant factors have been given due weighting during the classification process.
	• The resource estimation methodology is considered appropriate and reflects the Competent Persons view of the deposit.
Audits or reviews	• All resource models have been subjected to internal peer review.
Discussion of relative accuracy/ confidence	• These mineral resource estimates are considered as robust and representative of the Pode style of mineralisation. The relative accuracy of the Mineral Resource estimate is reflected in the reporting of the Mineral Resource as per the guidelines of the 2012 JORC Code.
	• The statement relates to global estimates of tonnes and grade.
	• No reconciliation factors are applied to the resource post-modelling.

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1.4 Raleigh-Sadler: Mineral Resource – 31 December 2022

Section 1: Sampling Techniques and Data

Criteria	Commentary
Sampling techniques	• A combination of sample types was used to collect material for analysis, including surface and underground diamond drilling (DD), surface reverse circulation drilling (RC) and face channel (FC) sampling. RAB holes were excluded from the estimate. Where sufficient diamond drill holes were present, RC holes were also excluded.

	Raleigh - Sadler		
Type	No.of Holes	Total Metres	No. of Samples
DD	1,009	194,249	69,411
FS	8,784	34,251	50,746
RC	231	22,896	19,185
RCDD	46	13,619	4,002
TOTAL	10,070	265,015	143,344

	• DD drilling is sampled within geological boundaries with a minimum (0.3 m) and maximum (1.0 m) sample length. Face channel sampling is constrained within geological and mineralised boundaries with a minimum (0.2 m) and maximum (1.0 m) channel sample length. In some cases, smaller samples (0.1 m – 0.2 m) have been taken to account for narrower structures in the face.
	• DD drill core is either half core or full core sampled. Half core samples were cut using an automated core saw. The mass of material collected was dependent on the drill hole diameter and sampling interval selected. • A sample size of at least 3 kg of material was targeted for each face sample interval. • All samples were delivered to a commercial laboratory where they were dried and crushed to 90% of material ≤3 mm. At this point, samples greater than 3 kg were split using a rotary splitter, then pulverised to 90% ≤75 µm. • A 40 g charge was selected for fire assay for all recent samples. Historically, charge weights of 50 g have also been used.
Drilling techniques	• Both RC and DD techniques were used to drill the Raleigh deposit. • Surface diamond drill holes were completed using HQ2 (63.5 mm) core whilst underground diamond drill holes were completed using both NQ2 (50.5 mm) and NQ3 (43 mm) core. • Historically, core was oriented using the Reflex ACT Core orientation system. Currently, core is oriented using the Boart Longyear Trucore Core Orientation system. • RC Drilling was completed using a 5.75” drill bit, downsized to 5.25” at depth. • In many cases, RC pre-collars were drilled, followed by diamond tails. Pre-collar depth was determined in the drill design phase.
Drill sample recovery	• Any core loss in diamond drilling is recorded on the core block by the driller. This is then captured by the logging geologist and entered as an interval into the hole log.
	• For diamond drilling, the contractors adjust their rate of drilling and method if recovery issues arise. All recovery is recorded by the drillers on core blocks. This is checked and compared to the measurements of the core by the geological team. Any issues are communicated back to the drilling contractor.
	• Sample recovery of the ore is challenging at Raleigh with the brittle quartz vein RMV lode adjacent to the much softer RMS lode. Triple tubing has been employed by the drilling contractor in order to minimise core loss. Samples which have logged core loss through the ore zone are excluded. No relationship between sample recovery and grade has been discerned.

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Criteria	Commentary
Logging	• All diamond core is logged for lithology, veining, alteration, mineralisation, and structural data. Structural measurements of specific features are also taken through oriented zones. • Logging is entered in AcQuire using a series of drop-down menus which contain the appropriate codes for description of the rock. • All underground faces are logged for lithology and mineralisation. Logging is captured on a face sample sheet underground which is then transferred to AcQuire. Faces are then entered into AcQuire using a series of drop-down menus which contain appropriate codes for description of the rock.
	• All core logging is qualitative with mineralised zones assayed for quantitative measurements. Every core tray is photographed wet. • All underground faces are logged and sampled to provide both qualitative and quantitative data. All faces are washed down and photographed before sampling is completed.
	• For all drill holes, the entire length of the hole was logged.
Sub-sampling techniques and sample preparation	• Diamond core is cut using an automated core saw. Sampling and cutting methodology are dependent on the type of drilling completed. Half core is generally utilised for exploration drilling. Some exploration and all Grade Control drilling (GC) is whole core sampled.
	• RC samples are split using a rig-mounted cone splitter to collect a sample 3-4 kg in size from each 1m interval. These samples were utilised for any zones approaching known mineralization and from any areas identified as having anomalous gold. Outside known mineralised zones spear samples were taken over a 4 m interval for composite sampling.
	• Preparation of samples was conducted at Bureau Veritas' Kalgoorlie facilities commencing with sorting, checking and drying at less than 110°C to prevent sulphide breakdown. Samples are jaw crushed to a nominal -6 mm particle size. If the sample is greater than 3 kg a Boyd crusher with rotary splitter is used to reduce the sample size to less than 3 kg (typically 1.5 kg) at a nominal <3 mm particle size. • The entire crushed sample (if less than 3 kg) or sub-sample is then pulverized to 90% ≤75 µm, using a Labtechnics LM5 bowl pulveriser. 400 g Pulp subsamples are then taken with an aluminium scoop and stored in labelled pulp packets. • The sample preparation is considered appropriate for the deposit.
	• Procedures are utilised to guide the selection of sample material in the field. Standard procedures are used for all processes within the laboratory. Grind checks are performed at both the crushing stage (3 mm) and pulverising stage (75 µm), requiring 90% of material to pass through the relevant size.
	• Umpire sampling is performed monthly, where 3% of the samples are sent to the umpire lab for processing. • Umpire samples of faces were analysed using a 40g charge weight.
	• The sample sizes are considered appropriate for the material being sampled.
Quality of assay data and laboratory tests	• A 40 g fire assay charge for diamond drill holes and a 40 g charge for face samples is used with a lead flux in the furnace. The prill is totally digested by HCl and HNO3 acids before Atomic Absorption Spectroscopy (AAS) determination for gold analysis.
	• No geophysical tools were used to determine any element concentrations.

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Criteria	Commentary
	• Certified reference materials (CRMs) are inserted into the sample sequence at a rate of 1 per 20 samples to ensure correct calibration. Any values outside of 3 standard deviations are re-assayed with a new CRM. • Blanks are inserted into the sample sequence at a rate of 1 per 20 samples. The insertion points are selected at random, except where high grade mineralisation is expected. In these cases, a Blank is inserted after the high-grade sample to test for contamination. Results greater than 0.2 g/t if received are investigated, and re-assayed if appropriate. New pulps are prepared if anomalous results cannot be resolved. • Barren flushes are regularly inserted after anticipated high gold grades at the pulverising stage. • No field duplicates were submitted for diamond core. • Pulp duplicates are requested after any ore zone. These are indicated on the sample sheet and the submission sheet. • When visible gold is observed in core, a quartz flush is requested after the sample. • Laboratory performance was monitored using the results from the QA samples mentioned above. This was supplemented by the internal QA samples used by the laboratories, which included pulp duplicates and CRMs. • The QA studies indicate that accuracy and precision are within industry accepted limits.
Verification of sampling and assaying	• All significant intersections are verified by another geologist during the drill hole validation process, and later by a Competent person to be signed off.
	• No twinned holes were drilled for Raleigh. Re-drilling of some drill holes has occurred due to issues downhole (e.g., bogged rods). These have been captured in the database with an 'A' suffix. Re-drilled holes are sampled whilst the original drill hole is logged but not sampled.
	• Geological logging and sampling are directly recorded into AcQuire. Assay files are received in csv format and loaded directly into the database using an Acquire importer object. Assays are then processed through a form in AcQuire for QAQC checks. Hardcopy and non-editable electronic copies of these are stored.
	• No adjustments are made to this assay data.
Location of data points	• Planned holes are marked up by the mine survey department using a total station survey instrument in mine grid (Kundana 10). The actual hole position is then located by the mine survey department once drilling is completed. In some cases, drill hole collar points are measured off survey stations if a mark-up cannot be completed. • Holes are lined up on the collar point using the DHS Azimuth Aligner. Planned azimuths and dips of the holes are downloaded to the aligner which is then placed on the rod string to align the hole for drilling. • During drilling, single shot surveys are conducted every 30 m to track the deviation of the hole and to ensure it stays close to design. This is performed using the DeviShot camera which measures the gravitational dip and magnetic azimuth. Results are uploaded from the Devishot software into a csv format which is then imported into the Acquire database. At the completion of the hole, a Multishot (using the Deviflex non-magnetic strain gauge instrument) survey is completed, taking measurements every 3 m to ensure accuracy of the hole. This is converted to .csv format and imported into the Acquire database.
	• Collar coordinates are recorded in mine grid (Kundana 10) and transformed into MGA94_51.
	• Quality topographic control has been achieved through Lidar data and survey pickups of holes over the last 15 years.
Data spacing and distribution	• Drill hole spacing varies across the deposit. For resource targeting drill spacing was typically 60 m x 60 m. This allowed for infill drilling at 30 m x 30 m spacing known as resource definition. Grade control drilling was drilled on a level-by-level basis with drill spacing between 10 m to 15 m.
	• The data spacing and distribution is considered sufficient to support the Resource and Reserve estimates
	• No sample compositing has been applied.

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Criteria	Commentary
Orientation of data in relation to geological structure	• The major Raleigh structures dip steeply (80°) to the west (local grid). Diamond drilling was designed to target the ore bodies as close to perpendicular as possible, allowing for a favourable intersection angle. In instances where this was not achievable (mostly due to drill platform location), drilling was not completed or re-designed once a suitable platform became available. • Drill holes with low intersection angles are excluded from resource estimation where more suitable data is available. • Robust data validation has been completed to ensure no sample bias is introduced by including these holes. • Where drill holes have been particularly oblique, they have been flagged as unsuitable for resource estimation.
Sample security	• Prior to laboratory submission samples are stored in a secure yard. Once submitted to the laboratories they are stored in a secure fenced compound, tracked through their chain of custody and via audit trails.
Audits or reviews	• No audits have been undertaken of the data and sampling practices at this stage.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	Commentary
Mineral tenement and land tenure status	• All holes mentioned in this report are located within either the M15/993 or M16/157 Mining leases. M15/993 which is held by the East Kundana Joint Venture (EKJV). The EKJV is majority owned (51%) and managed by Evolution Mining. The minority holding in the EKJV is held by Tribune Resources Ltd and Rand Mining Ltd. M16/157 is fully owned by Evolution Mining. • The tenements on which the Raleigh and Sadler deposit is hosted is subject to three royalty agreements. The agreements are the Kundana- Hornet Central Royalty, the Lake Grace Royalty and the Kundana Pope John Agreement No. 2602-13. • No known impediments exist, and the tenements are in good standing.
Exploration done by other parties	• No other parties performed exploration work at Raleigh during the reporting period. All previous exploration by other parties is summarised in open file annual reports which are available from the DMIRS.
Geology	• The Kundana gold camp is situated within the Norseman-Wiluna Greenstone Belt, in an area dominated by the Zuleika shear zone, which separates the Coolgardie domain from the Ora Banda domain. • Raleigh ore lodes are located along the Strzelecki structure, with mining commencing in 2000. The Raleigh mineralisation consists of narrow, laminated quartz veining on the contact between volcanogenic sedimentary rock unit and andesite/gabbro (RMV). Sadler is the southern extent of Raleigh with no clear geological boundary distinguishing them. Underground mining began in Sadler in FY19.
Drill hole Information	• No new information released in this report. • The collar locations are presented in plots contained in the December 2022 resource report. • Drill holes vary in survey dip from +48 to -83, with hole depths ranging from 15 m to 950 m, and having an average depth of 180 m. The assay data acquired from these holes are described in the December 2022 resource report. • All the drill hole data were used directly or indirectly for the preparation of the resource estimates described in the resource report. • No new information released in this report. Excluded information is not thought material to this release.

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Criteria	Commentary
Data aggregation methods	• No new information released in this report. All reported assay results have been length weighted to provide an intersection width. A maximum of 2 m of low-grade material (considered < 2.0 g/t) between mineralised samples has been permitted in the calculation of these widths. Typically grades over 2.0 g/t are considered significant, however, where wide zones of low grade are intersected in areas of known mineralisation these will be reported. No top-cutting is applied when reporting intersection results.
	• Where an intersection incorporates short lengths of high grade results these intersections will be reported in addition to the aggregate value. These will typically take the form of ##.#m @ ##.##g/t including ##.#m @ ##.##g/t.
	• No metal equivalent values have been used for the reporting of these exploration results.
Relationship between mineralisation widths and intercept lengths	• True widths have been calculated for intersections of the known ore zones, based on existing knowledge of the nature of these structures.
	• Both the downhole width and true width have been clearly specified when used.
	• Generally estimated true width is reported. Down hole lengths are noted where used.
Diagrams	• Appropriate plans and section have been included at the end of this Table.
Balanced reporting	• Both high and low grades have been reported accurately, clearly identified with the drill hole attributes and 'From' and 'To' depths.
Other substantive exploration data	• No other material exploration data has been collected for this area.
Further work	• Further work will include mining studies appropriate to EVNs current open-cut and underground mining methods. If mining studies yield a positive result, infill resource definition is planned to convert Inferred Mineral Resource category to Indicated Mineral Resource category and to test for extensions to mineralisation along strike and down-dip that would likely impact the economic outcome. • A feasibility study is progressing to determine the economics of reducing the Mungai Processing facility unit cost by increasing throughput from 2.0Mpta to 4.2Mtpa. This will likely reduce COGs for the MGO Mineral Resource Statement.
	• Appropriate diagrams accompany this release.

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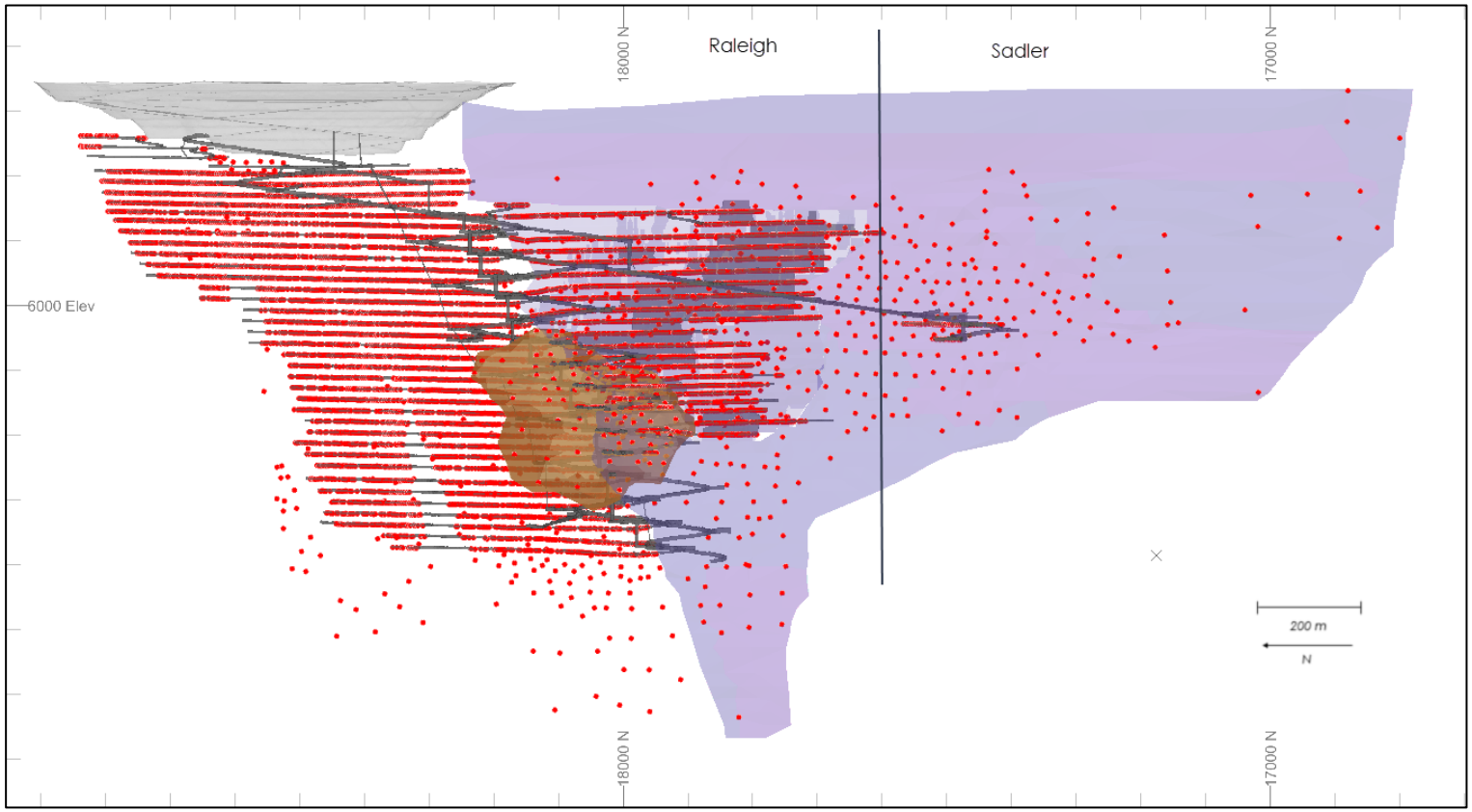


Figure 1. Long section view of the Raleigh and Sadler deposits and data used for estimation

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Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	Commentary
Database integrity	• Sampling and logging data is either recorded on paper and manually entered into a database system or is captured digitally via a logging laptop and directly loaded into the database system. There are checks in place to avoid duplicate holes and sample numbers. Where possible, raw data is loaded directly into the database from laboratory and survey derived files.
	• The database has further checks performed prior to estimation to confirm data validity. The complete exported database (including drill and face samples) is imported into Datamine and checked visually for any apparent errors i.e., holes or faces sitting between levels or not on surface DTM's. Multiple checks are then made on numerical data. These include: • Empty table checks to ensure all relevant fields are populated. • Unique collar location check. • Distances between consecutive surveys is no more than 60m for drill-holes. • Differences in azimuth and dip between consecutive surveys of no more than 0.3 degrees. • The end of hole extrapolation from the last surveyed shot is no more than 30 m. • Underground face sample lines are not greater than +\- 5 degrees from horizontal. • Errors are corrected where possible. When not possible the data is resource flagged as "No" in the database and the database is re-exported. This data will not be used in the estimation process. • Several drilling programs completed between 2015 and 2016 had erroneous meter depths recorded therefore these drill-holes have been omitted from the ore wireframe interpretations and flagged as invalid. However, where there were no QAQC issue with the assays, the correct intervals have been recorded, the translation in the easting direction required for them to be in the 'correct' location (based on development above and below) applied, and these intervals were appended to the data set before compositing. • In addition to being Resource Flagged as "Yes" or "No", drill holes are assigned a Data Class, which provides a secondary level of confidence in the data quality. Data Class (DC) values range from 0 to 3, with criteria summarised below: • DC 3 = Recent data; all data high quality, validated and all original data available. • DC 2 = Historic data; may or may not have all data in AcQuire or hard copy available but has proximity to recent drilling which confirms the dip, width and tenor OR recent data with minor issues but away from the ore zone. • DC 1 = Historic data; same criteria as DC 2 but cannot be verified with recent drilling, i.e., too far away, or dissimilar dip, width and/or tenor to recent drilling. Not to be used in Resource estimate. • DC 0 = Historic data; no original information or new drilling in proximity to verify. Not to be used in Resource estimate.
Site visits	• The geological interpretations underpinning these resource models were prepared by geologists working in the mine and in direct, daily contact with the ore body. The estimation of grades was undertaken by personnel familiar with the ore body and the general style of mineralisation encountered. The Senior Resource Geologist, a competent person for reviewing and signing off the Raleigh estimate maintained a site presence throughout the process.
	• Site visits undertaken.
Geological interpretation	• The interpretation of the Raleigh and Sadler deposit was carried out using a systematic approach to ensure continuity of the geology and estimated mineral resource. The confidence in the geological interpretation is high and is supported with information acquired during ore development as well as from drilling.

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Criteria	Commentary
	• All available geological data was used in the interpretation including mapping, drill holes, underground face channel data, 3D photogrammetry and structural models.
	• No alternative interpretations have been proposed.
	• The interpretation of Raleigh and Sadler mineralisation is based on the presence of mineralised structure (veining and shear), ore-bearing mineralogy (gold and associated sulphides), assayed samples and continuity between sections. • The Raleigh Main Vein (RMV) is based on a high-grade laminated quartz vein. Pinch-outs are common and significant time has been invested into ensuring a wireframe model is created that best represents the variable width of the lode. Volume considerations are of importance for the RMV as the average ore width is < 0.3 m. • The Raleigh Main Shear (RMS) is located adjacent to the RMV and migrates between the hangingwall and footwall along the contact between the quartz arenite (SAQ) and intermediate andesite (IA). It presents as a zone of increased shearing and, on rare occasions, some minor veining can also be present. • A halo lode has been used to estimate grade between the RMV and RMS. • Skinners Lode (SKV) is in the hanging wall of the RMV and presents as a chalky-white vein (as opposed to the laminated grey-white RMV). Pinch-outs are less common and width is more consistent than the RMV. Skinners Lode truncates against the RMV at its southern extent. • The ZZ and ZZ2 are hanging wall lodes comprised of stockwork-style vein arrays which dips shallowly to the west. They are truncated at the east by the RMV and at the west by the SKV. • The RMVS lode includes both the Raleigh vein and shear structures where data density is not sufficient to confidently separate the two mineralisation types. This has been extended from Raleigh to Sadler and constitutes much of the Sadler ore body where the RMV has not been delineated from ore development.
	• Grade continuity is affected when the percentage of quartz decreases within the main Raleigh structure and only a sheared structure remains. This results in lower grade in areas where only shear is present and higher grade where quartz is evident.
Dimensions	• The strike length of the different ore systems varies from ~100 m to 600 m, the Raleigh Main Vein and Shear (RMVS) being the most extensive. The individual ore bodies occur in a major regional Zuleika shear system extending over 10's of kilometres. • Ore body widths are typically in the range of 0.1 - 1.1 m. RMV records the narrowest at 0.1 m and SKV the widest at 1.1 m. RMV has an average width of 0.3 m • Mineralisation is known to occur from the base of cover to around 900 m below surface.
Estimation and modelling techniques	• Raleigh mineralisation zones, except for the Raleigh Main Shear (RMS), used direct grade estimation by Ordinary Kriging. The RMS was estimated using Categorical Indicator Kriging. Typically, full length composites were used, determined from statistical analysis of all sample lengths in the domain dataset. All estimation was completed using Datamine RM software. Details on the estimation by ore lode is summarised below: • RMV – Estimated as a single domain. Data was top cut to 1,000 g/t using the influence limitation approach. Variography was completed on the composited data file, indicating grade continuity plunging moderately to the north. Searches were completed in three passes. Search ranges of 100 m in direction 1 (dir1), 75 m in direction 2 (dir2) and 50 m in direction 3 (dir3) were used. • RMS – divided into two grade subdomains. Binary estimate completed on composited data set with indicators (0 or 1) applied based on grade cut-off (> 2.5 g/t) and quartz vein presence (vein logged in LITH1 field). Estimate returns result between 0 and 1. Cut-off of 0.45 chosen to ascertain two grade subdomains (high grade and low grade) for final gold estimate. Data sets top cut to 150 g/t (high grade subdomain) or 50 g/t (low grade subdomain) using the influence limitation approach. Same variogram and search parameters used for both high- and low-grade subdomains. Variograms indicate grade continuity plunging moderately to the north. Searches were completed in three passes. Search ranges of 100 m in dir1, 80 m in dir2 and 40 m in dir3 were used.

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Criteria	Commentary
	• RMVN – Divided into two subdomains based on data density. Data was top cut to 500 g/t and 100 g/t (for high-density and low-density subdomains respectively) using the influence limitation approach. Variography was completed on the composited data file, indicating grade continuity plunging steeply to the north. Searches were completed in three passes. For the high data-density estimate, search ranges of 100 m in dir1, 50 m in dir2 and 100 m in dir3 were used. For the low data-density estimate, search ranges of 190 m in dir1, 140 m in dir2 and 70 m in dir3 were used. Estimation was completed using a soft boundary between the high and low-density subdomains and between adjacent Raleigh domains (RMV, RMS and RMVS). • RMVS – Divided into two subdomains based on grade. Data was top cut to 200 g/t and 10 g/t (for high-grade and low-grade subdomains respectively) using the influence limitation approach. Variography was completed on the composited data file, indicating grade continuity plunging moderately to the south. Searches were completed in three passes. For the high-grade estimate, search ranges of 150 m in dir1, 80 m in dir2 and 50 m in dir3 were used. For the low-grade estimate, search ranges of 250 m in dir1, 150 m in dir2 and 100 m in dir3 were used. Estimation was completed using a soft boundary between the high and low-density subdomains and between adjacent Raleigh domains (RMV, RMS and RMVN). • RMV/RMS Halo (halo) - Estimated as a single domain. Data was top cut to 10 g/t using the influence limitation approach. Variography borrowed from the RMV estimate, as not enough sample pairs were available to construct a coherent variogram. Searches were completed in three passes. Search ranges of 100 m in dir1, 75 m in dir2 and 50 m in dir3 were used. • SKV – Divided into two subdomains based on grade. Data was top cut to 600 g/t and 30 g/t (for high-grade and low-grade subdomains respectively) using the influence limitation approach. Variography was completed on the composited data file, indicating grade continuity plunging moderately to the north. Searches were completed in three passes. For the high-grade estimate, search ranges of 100 m in dir1, 60 m in dir2 and 40 m in dir3 were used. For the low-grade estimate, search ranges of 100 m in dir1, 50 m in dir2 and 30 m in dir3 were used. • ZZ - Estimated as a single domain. Data was top cut to 60 g/t using the influence limitation approach. Variography was completed on the composited data file, indicating grade continuity plunging shallowly to the south. Searches were completed in three passes. Search ranges of 30 m in dir1, 15 m in dir2 and 10 m in dir3 were used. • ZZ2 - Estimated as a single domain. Data was top cut to 40 g/t using the influence limitation approach. Variography was completed on the composited data file, indicating grade continuity plunging moderately to the north. Searches were completed in three passes. Search ranges of 25 m in dir1, 15 m in dir2 and 10 m in dir3 were used.
	• Check estimates have been completed for all lodes. These include Inverse Distance (ID3) and Nearest Neighbour (NN) estimates.
	• No assumptions are made, and gold is the only metal defined for estimation.
	• No deleterious elements were estimated in the model.
	• Block sizes varied depending on sample density. In areas of high data-density (underground face samples with average spacing of 3 – 4 m) a 5 x 5 x 5 m block size was chosen. Low density drill spacing is defined as approximately 30 m or greater and a 10 x 10 x 10 m block size was chosen. • Estimates were completed with soft boundaries between varying block size estimates (unless a geological feature and contact analysis indicated a hard boundary was required) and added together following individual estimation for final validations. • Search ellipse dimensions were derived from the variogram model ranges, or isotropic ranges based on data density where insufficient data was present for variography analysis.
	• Selective mining units were not used during the estimation process.
	• All variables were estimated independently of each other. Density has used estimation parameters based on gold.

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Criteria	Commentary
	• Hangingwall and footwall wireframe surfaces were created using sectional interpretation. These were used to define the Raleigh mineralised zones based on the geology and gold grade. • Raleigh Main Vein (RMV) - Steeply dipping structure with smoky quartz veining evident from drilling and development. • Raleigh Main Vein South (RMVS) - Steeply dipping structure with smoky quartz veining and shearing evident from drilling and development. • Raleigh Main Vein North (RMVN) - Steeply dipping structure with smoky quartz veining evident from drilling and development. • Raleigh Main Shear (RMS) - Steeply dipping shear structure sitting in the footwall of the RMV with occasional quartz vein strings, evident from development. • Skinners Vein (SKV) - Steeply dipping structure with chalky-white quartz veining sitting in the hanging wall of the RMV. • ZZ/ZZ2 - Low angled narrow stacked quartz veining, sitting between the RMV and SKV, evident from drilling and development in the 5880 level. • For mine planning purposes a waste model is created by projecting the hanging wall and footwall surfaces 15 m either side. A default grade of 0.1 g/t is assigned and the same resource classification as the adjacent ore lode is applied.
	• Top cuts were applied to the composited sample data. Top cuts were selected based on a statistical analysis of the data. Top cuts vary by domain and range from 10 g/t to 1,000 g/t. • The top cut values are applied using technique called influence limitation top cutting. A top cut (AU) and non-top cut (*_NC) variable is created, as well as a spatial variable (*_BC) which only has values where the top cut values appear. For example, where gold requires a top cut, the following variables will be created and estimated: • AU (top cut gold). • AU_NC (non- top-cut gold). • AU_BC (spatial variable; values present where AU data is top cut). • The top-cut and non-top cut values are estimated using search ranges based on the modelled gold variogram, and the *_BC values estimated using very small ranges (e.g.,5 m x 5 m x 5m). Where the *_BC values produce estimated blocks within these restricted ranges, the *_NC estimated values replace the original top cut estimated values (AU). • A hard top cut is applied instead of/as well in the following situations: • If there are extreme outliers within an ore domain. • If the area has a history of poor reconciliation (i.e., overcalling).
	• Statistical measures of Kriging error, such as Kriging Efficiency and Slope of Regression, are used to assess the quality of the estimation for each domain. • Differences in the global grade of the top-cut, declustered composite data set and the average model grade were within 10%, or justification for a difference outside 10% was explicable. • Swath plots comparing top-cut, declustered composites to block model grades are created and visual plots are prepared summarising the critical model parameters. • Visually, block grades are assessed against drill hole and face data.
Moisture	• Tonnages are estimated on a dry basis.
Cut-off parameters	• The cut-off grades were estimated using projected site mining costs, processing costs and site general administration costs. • a gold price of A$2,200/oz was utilised. • The cut-off grades applied to the deposit areas are listed below:

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Criteria	Commentary
	• <table><tr><th>Deposit</th><th>COG (g/t Au) (m)</th></tr><tr><td>Open Pits (excl Boundary)</td><td>0.40 g/t Au</td></tr><tr><td>Raleigh & Raleigh North UG</td><td>2.44 g/t Au</td></tr><tr><td>East Kundana JV UG</td><td>2.44 g/t Au</td></tr></table>
Mining factors or assumptions	• The Mineral Resource estimations for open pit resource have been reported within pit optimisation shells generated in Whittle software. Mining costs are based on regolith type and depth below surface. For Mineral Resources, no dilution or recovery factors have been applied. Mining selectivity of 10m (x) by 10m (y) by 5m (z) has been applied. • The Mineral Resource estimations for underground have been reported within Mining Shape Optimiser objects (MSOs) generated in Datamine or Deswik software. These shapes assume a minimum mining width of 2.5 m with a minimum footwall and hanging-wall slope of 50 to 80 degrees. The minimum strike of the panels is 10.0m and a vertical extent of 5.0m. No external dilution has been applied to the shapes however internal dilution has been applied where required (no estimated grade or sub Inferred Mineral Resource blocks) at 0.0 g/t. • All Mineral Resources have been depleted by prior mining. The prior mining is represented by detailed surveys completed over the life of the project. These surveys are represented by 3D models which have been used to flag blocks as mined or not. MSO's are also validated and removed if they are considered to be sterilised (low likelihood of being mined) by current mine development.
Metallurgical factors or assumptions	• Reasonable assumptions for metallurgical extraction factored into the resource estimate are based on previous processing of the ore from the nearby deposits at Kundana, Kunanalling and Carbine through the various historic and operational CIP/CIL processing facilities within the district (including the Mungari Mill). • Where a deposit has not been previously mined or processed, preliminary deportment and geo-metallurgical studies are completed on ore types to generate metallurgical factors and assumptions to be included in the resource estimate. • Target gold recoveries range from 86% to 95% recovery.
Environmental factors or assumptions	• No significant environmental factors are expected to be encountered regarding the disposal of waste or tailing material. This expectation is based on previous mining and milling history of existing open pit operations with the project area. • Mungari Gold Operations has in place regulatory permits and approvals to continue operations. • A site Environmental team monitors ongoing compliance with approvals and maintains the site in good standing with regulators.
Bulk density	• A thorough investigation into average density values for the various lithological units at Raleigh-Sadler was completed and the mean densities by lithology were coded into the database. Where there were no measurements for a specific lithology and default of 2.7 t/m3 was applied. Density was then estimated by Ordinary Kriging using the associated gold estimation parameters for that domain. Post estimation, default density values for the oxide and transition zones were applied, based on regional averages. • No/minimal voids are encountered in the ore zones and underground environment. • Assumptions on the average bulk density of individual lithologies, based on 2,920 bulk density measurements at Raleigh. Assumptions were also made based on regional averages, on the default densities applied to oxide (1.8 t/m³) and transitional (2.3 t/m³) material, due to lack of measurements in these zones.
Classification	• Classification is based on a series of factors including: • Geologic grade continuity. • Density of available drilling. • Statistical evaluation of the quality of the kriging estimate.

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Criteria	Commentary
	• Confidence in historical data, based on the new Data Class system.
	• All relevant factors have been given due weighting during the classification process.
	• The resource model methodology is appropriate, and the estimated grades reflect the Competent Persons' view of the deposit.
Audits or reviews	• All resource models have been subjected to internal peer reviews.
Discussion of relative accuracy/ confidence	• These mineral resource estimates are considered as robust and representative of the Strzelecki style of mineralisation. The relative accuracy of the Mineral Resource estimate is reflected in the reporting of the Mineral Resource as per the guidelines of the 2012 JORC Code.
	• The statement relates to global estimates of tonnes and grade.
	• No reconciliation factors are applied to the resource post-modelling.

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1.5 Falcon: Mineral Resource – 31 December 2022

Section 1: Sampling Techniques and Data

Criteria	Commentary
Sampling techniques	• Underground and surface diamond drilling (DD) and surface reverse circulation drilling (RC) sampling were used to inform the gold estimation at Falcon. No issues have been reported regarding poor quality of sampling for any drill type. A review of core photography indicates good sample quality with occasional broken zones of core. Rotary air blast (RAB) and Air core (AC) holes were excluded from the estimation process. In total, 551 drillholes are drilled in and around the Falcon mineralisation dating from 2015 to the present day. Some of the holes were also targeting adjacent orebodies including Pode, Hera, Pegasus, Drake and Raleigh. All drilling was completed by Northern Star (NSR) on behalf of the East Kundana Joint Venture (EKJV).

FALCON Deposit - Drilling Statistics

Company	Period	Hole Prefix	Drill Type	Number of Drillholes	Total Metres	Number of Samples	% of Holes	% of Metres	% of Samples
Northern Star (EKJV)	2019-20	FALDT	DD	25	11,466.6	12,562	4.5%	7.0%	9.1%
Northern Star (EKJV)	2019	FALGC	DD	23	4,181.6	4,397	4.2%	2.6%	3.2%
Northern Star (EKJV)	2019-20	FALRSD	DD	196	43,504.3	34,849	35.6%	26.7%	25.4%
Northern Star (EKJV)	2019-20	FALRT	DD	126	49,348.0	39,457	22.9%	30.3%	28.7%
Northern Star (EKJV)	2015-2018	FLDD	DD	11	3,796.1	4,324	2.0%	2.3%	3.1%
Northern Star (EKJV)	2015	FLRC	RC	7	1,479.0	1,478	1.3%	0.9%	1.1%
Northern Star (EKJV)	2021	HERRSD	DD	9	2,321.6	1,471	1.6%	1.4%	1.1%
Northern Star (EKJV)	2017	PEGGC	DD	18	3,929.3	3,383	3.3%	2.4%	2.5%
Northern Star (EKJV)	2018	PEGRSD	DD	51	13,840.8	14,680	9.3%	8.5%	10.7%
Northern Star (EKJV)	2018	PEGRT	DD	23	8,357.6	6,666	4.2%	5.1%	4.9%
Northern Star (EKJV)	2015	PGDD	DD	5	3,433.3	2,598	0.9%	2.1%	1.9%
Northern Star (EKJV)	2020-21	PODRSD	DD	28	5,605.7	3,929	5.1%	3.4%	2.9%
Northern Star (EKJV)	2020	PODRT	DD	26	10,032.7	6,132	4.7%	6.2%	4.5%
Northern Star (EKJV)	2017	RALRT	DD	3	1,553.0	1,462	0.5%	1.0%	1.1%
				551	162,849.5	137,388.0	100.0%	100.0%	100.0%

	• Diamond core drilling is sampled to geological boundaries with a minimum (0.5 m) and maximum (1.49 m) sample length. • RC sampling is sampled at 1m intervals through mineralised zones with some primary composite samples still included in the dataset. RC sampling provides a larger sample size than drill core but is less representative of geology, particularly around geological contacts and narrow ore zones.
	• DD drill core was nominated for either half core or full core sampling. • Core designated for half core was cut using an automated core saw. The mass of material collected was dependent on the drillhole diameter and sampling interval selected. Core designated for full core was broken with a rock hammer at sample intervals and if sample segments were too large to fit into sample bags. • Recent RC samples are collected via a rig mounted riffle or cone splitter at 1m intervals to produce approximately 3kg of sample. Previously samples may have been split via a free-standing riffle splitter, particularly if they were a 1m re-sample of a primary composited sample that was anomalous for gold. • All samples were delivered to a commercial laboratory where they were dried and crushed, generally to 90% of material ≤3 mm. At this point large samples were split using a rotary splitter, then pulverised to 90% ≤75 µm. • A 40 g charge was selected for fire assay for all recent samples. Historically, charge weights between 30g and 50g have also been used.
Drilling techniques	• Both Reverse Circulation and Diamond Drilling techniques were used to drill the Falcon deposit. • Surface diamond drillholes were completed using HQ2 (63.5 mm) coring, whilst underground diamond drillholes were completed using NQ2 (50.5 mm) coring. • Historically, core was orientated using the Reflex ACT Core orientation system. Currently, core is orientated using the Boart Longyear Trucore Core Orientation system. • RC Drilling was completed using a 5.75” drill bit, downsized to 5.25” at depth. • In several cases, RC pre-collars were drilled, followed by diamond tails. Pre-collar depth was determined in the drill design phase.
Drill sample recovery	• For DD drilling, any core loss is recorded on the core block by the driller. This is captured by the logging geologist and entered as an interval into the hole log. • For RC sampling, sample weights may be recorded to give an indication of areas of poor sample return. Geology personnel at the drill site would give feedback to the driller in regard to sample recovery that may not have been satisfactory.
	• Contractors adjust the rate and method of drilling if recovery issues arise. All recovery is recorded by the drillers on core blocks. This is checked and compared to the measurements of the core by the geological team. Any issues are communicated back to the drilling contractor.
	• Recovery was generally very good for diamond core and no relationship between grade and recovery is observed or commented on in historical reporting.

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Logging	• All diamond core is logged for lithology, veining, alteration, mineralisation, and structural data. Structural measurements of specific features are also taken through oriented zones. RC chips are logged every metre and include the same except for structural data. • Historically, geological logging was initially on paper logs and then manually entered into a database, recent logging is by electronic methods and then uploaded to the site databases by various database import objects. • Logging is stored in the Mungari site geological database (acQuire) using a series of drop-down menus which contain the appropriate codes for description of the rock or regolith.
	• All core logging is qualitative with mineralised zones assayed for quantitative measurements. Core is photographed wet and or dry and most photography is available on the Mungari servers. • Photos of RC chip trays have not been located but it was a common practice for this to be done.
	• For all drill holes, the entire length of the hole is logged.
Sub-sampling techniques and sample preparation	• Diamond core is cut using an automated core saw. Sampling and cutting methodology is dependent on the type of drilling completed. Half core is utilised for exploration drilling. Some drill holes have been whole core sampled.
	• RC samples are split using a rig-mounted riffle or cone splitter to collect a sample 2 - 4 kg in size from each 1 m interval. Many of the earlier RC samples were composite sampled by spear or scoop with anomalous intervals re-sampled by a free-standing riffle splitter.
	• Preparation of drill samples was conducted at external laboratories commencing with sorting, checking, and drying at less than 110°C to prevent sulphide breakdown. Samples were jaw crushed to a nominal -6 mm particle size. If the sample is greater than 3 kg a Boyd crusher with rotary splitter is used to reduce the sample size to less than 3 kg (typically 1.5 kg) at a nominal <3 mm particle size. • The entire crushed sample (if less than 3 kg) or sub-sample is then pulverized to 90% ≤75 µm, using a LM5 bowl pulveriser. Pulp sub-samples of about 400g are then taken with an aluminium scoop and stored in labelled pulp packets. • The sample preparation is considered appropriate for the mineralisation type.
	• Standard procedures are used for all processes within the laboratory. Grind checks are performed at both the crushing stage (3 mm) and pulverising stage (75 µm), requiring 90% of material to pass through a sieve of relevant size.
	• Umpire sampling is performed frequently, where 3% of the samples are sent to the umpire laboratory for processing. • Umpire samples of faces were analysed using a 40 g charge weight.
	• The sample sizes are considered appropriate for the material being sampled.
Quality of assay data and laboratory tests	• A 30- 50 g fire assay charge is used with a lead flux in the furnace. The resultant prill is totally digested by HCl and HNO_3 acids before Atomic Absorption Spectroscopy (AAS) determination for gold analysis.
	• No geophysical tools were used to determine any element concentrations.

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	• For most drilling certified reference materials (CRMs) are inserted into the sample sequence at a rate of 1 per 20 samples to ensure correct calibration. Any values outside of 3 standard deviations are re-assayed with a new CRM. • Blanks are inserted into the sample sequence at a rate of 1 per 20 samples. The insertion points are selected at random, except where high grade mineralisation is expected. In these cases, a Blank is inserted after the high-grade sample to test for contamination. Results greater than 0.2 g/t if received are investigated, and re-assayed if appropriate. New pulps are prepared if anomalous results cannot be resolved. • Barren flushes are regularly inserted after anticipated high gold grades at the pulverising stage. • No field duplicates are submitted for diamond core. • Pulp duplicates are requested after any ore zone. These are indicated on the sample sheet and the submission sheet. • When visible gold is observed in core, a quartz flush would be requested after the sample. • Laboratory performance was monitored using the results from the QA samples mentioned above. This was supplemented by the internal QA samples used by the laboratories, which included pulp duplicates and CRMs. Laboratory visits and audits are conducted on a regular basis. • The QA studies indicate that accuracy and precision are within EKJV accepted limits.
Verification of sampling and assaying	• All significant intersections are verified by another geologist during the drill hole validation process, and later by a competent person to be signed off.
	• No specific twinned holes were drilled. Re-drilling of some drillholes has occurred due to issues downhole (e.g., bogged rods). These have been captured in the database with an 'A' suffix. Re-drilled holes are sampled, whilst the original drillhole is logged but not sampled.
	• Geological logging and sampling are directly recorded into acQuire. Assay files are received in .csv format and loaded directly into the database using an acQuire importer object. Assays are then processed through a form in acQuire for QAQC checks. Hardcopy and non-editable electronic copies of these are stored.
	• No adjustments have been made to this assay data.
Location of data points	• For all drilling, planned holes are marked up by the mine survey department using a total station survey instrument in mine grid (Kundana 10). The actual hole position is then located by the mine survey department once drilling is completed. • Surface drillholes are set up for azimuth by surveyed sighter pegs and tape line. Underground diamond core drillholes are lined up on the collar point using the DHS Minnovare Azimuth Aligner. Planned azimuths and dips of the holes are downloaded to the aligner which is then placed on the rod string to align the hole for drilling. • During drilling, single shot surveys are conducted every 30 m to track the deviation of the hole and to ensure it stays close to design. This is performed using the DeviShot camera which measures the gravitational dip and magnetic azimuth. Results are uploaded from the Devishot software into a csv format which is then imported into acQuire. At the completion of the hole, a Multishot (using the DeviFlex non-magnetic strain gauge instrument) survey is completed, taking measurements every 3 m to ensure accuracy of the hole. This is converted to csv format and imported into acQuire.
	• Collar coordinates are recorded in mine grid (Kundana 10 or K10) and transformed into MGA94_51.

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	KUNDANA 10		
	X	Y	Z
Point 1	10000.000	20000.000	6343.658
Point 2	10000.267	18668.600	6343.967

Dip	0
Azimuth	179.989

	MGA94-51		
	X	Y	Z
Point 1	331726.160	6600882.149	343.658
Point 2	332376.768	6599720.746	343.967

Dip	0
Azimuth	150.743

Rotation
29.246

	• Quality topographic control has been achieved through Lidar data and survey pickups of holes over the last 15 years.
Data spacing and distribution	• Drillhole spacing varies across the deposit, with most of the drilling between 120 x 120 m and 40 x 40 m spacing. Some areas proximal to development have been drilled at a 20 x 20 m drill spacing.
	• The data spacing and distribution is considered sufficient to support the Resource and Reserve estimates.
	• No sample compositing has been applied.
Orientation of data in relation to geological structure	• The geology and geometry of the Falcon mineralisation is complex and the ideal drill orientation cannot always be achieved with the Falcon mineralisation. • Diamond drilling was designed to target the ore bodies to as perpendicular as possible to allow for a favourable intersection angle.
	• Despite the complex mineralisation style much of the drilling has intersected Falcon mineralisation at an angle that does not introduce significant bias. From a resource estimation perspective, the Falcon mineralisation is known to have a high variability and subsequent nugget value and estimations are designed to account for this.
Sample security	• Prior to laboratory submission samples are stored at the secure Millennium core yard. Once submitted to the laboratories they are stored in a secure fenced compound, tracked through their chain of custody and via audit trails. Previous companies would have had a similar process of sample security.
Audits or reviews	• No audits have been undertaken of the data and sampling practices.

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Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	Commentary
Mineral tenement and land tenure status	• All holes mentioned in this report are collared on either M16/309 or M16/993 held by the East Kundana Joint Venture (EKJV). The EKJV is majority owned and managed by Evolution Mining Limited with the minority holding held by Tribune Resources Ltd and Rand Mining Ltd. • The tenement on which the Falcon Deposit is mostly hosted (M16/309) is subject to three royalty agreements. The agreements that are on M16/309 are the Kundana- Hornet Central Royalty, the Lake Grace Royalty and the Kundana Pope John Agreement No. 2602-13.
	• No known impediments exist, and the tenements are in good standing.
Exploration done by other parties	• The first reference to the mineralisation style encountered at the Kundana project was the Mines Department report on the area produced by Dr. I. Martin (1987). He reviewed work completed in 1983 – 1984 by a company called Southern Resources, who identified two geochemical anomalies, creatively named Kundana #1 and Kundana #2. The Kundana #2 prospect was subdivided into a further two prospects, dubbed K2 and K2A. • Between 1987 and 1997, limited work was completed. • Between 1997 and 2006, Tern Resources (subsequently Rand Mining and Tribune Resources) and Gilt-edged Mining focused on shallow open pit potential with production from the Rubicon open pit commenced in 2002. During this period the Star Trek mineralisation was identified and advanced with some deeper RC drilling. • Underground Mining commenced in 2011 at the Rubicon – Hornet prospects with the underground portal in the completed Rubicon Open Pit. • Northern Star took over the RHP project in March 2014 and drilled over 520 mostly resource development diamond core drill holes at Falcon during their ownership of the project however some of these holes were also targeting adjacent deposits within the EKJV.
Geology	• The Kundana camp is situated within the Norseman-Wiluna Greenstone Belt, in an area dominated by the Zuleika shear zone, which separates the Coolgardie domain from the Ora Banda domain. • The Falcon deposit is interpreted as a series of mineralised splays off low angle structures that persist through lithological contacts from the K2B (Victorious Basalt - Bent Tree Basalt contact) across the K2A (Bent Tree Basalt- upper felsic and volcaniclastic/sedimentary rocks of the Black Flag Group). The Falcon lodes sit in the hangingwall of the regional 'K2' structure, west of the Pode deposit. The Pode lodes have been used as a proxy when interpreting the Falcon structures as similar trends are present. • Falcon lodes are typically flat to south plunging at about 30° and are comprised of laminated to brecciated quartz veining internal to a sheared biotite-sericite-ankerite altered siltstone/sandstone unit and an intermediate volcaniclastic unit.

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		Mineralisation is present within veins, on vein selvedges, and within the altered host rock, with coarse gold often observed. There is a strong visual correlation between arsenopyrite and gold mineralisation. Vein orientation appears erratic and this is supported by structural measurements taken from lodes.
Drill hole Information	•	A summary of the data present in the Falcon deposit can be found above. Collar data is presented in the local Kundana (K10) mine grid. • The collar locations are presented at the end of this table. • Drillholes vary in survey dip from +30 to -72 degrees, with hole depths ranging from 42 m to 951 m, with an average depth of 379 m. • All validated drill hole data was used directly or indirectly for the preparation of the resource estimation.
	•	The exclusion of any drill hole data is not material to this report.
Data aggregation methods	•	All reported assay results have been length weighted to provide an intersection width. A maximum of 2 m of barren material (considered < 2 g/t) between mineralized samples has been permitted in the calculation of these widths. Typically grades over 2.0 g/t are considered significant, however, where low grades are intersected in areas of known mineralisation these will be reported. No top-cutting is applied when reporting intersection results.
	•	Where an intersection incorporates short lengths of high grade results these intersections will be reported in addition to the aggregate value. These will typically take the form of ##.#m @ ##.##g/t including ##.#m @ ##.##g/t.
	•	No metal equivalent values have been used for the reporting of Falcon exploration results.
Relationship between mineralisation widths and intercept lengths	•	Not applicable
	•	Not applicable
	•	Not applicable
Diagrams	•	Not applicable
Balanced reporting	•	Petrology samples were selected for key lithologies and sent for thin section preparation and petrographic investigation.
Other substantive exploration data	•	Resource definition drilling will continue in various parts of RHP with the intention of extending areas of known mineralisation. Further drilling would likely be resource definition scaled drill spacing to improve on resource confidence and with no plan to advance to mining grade control drilling at the present moment
Further work	•	Appropriate diagrams have been created for monthly and annual reporting.
	•	Not applicable

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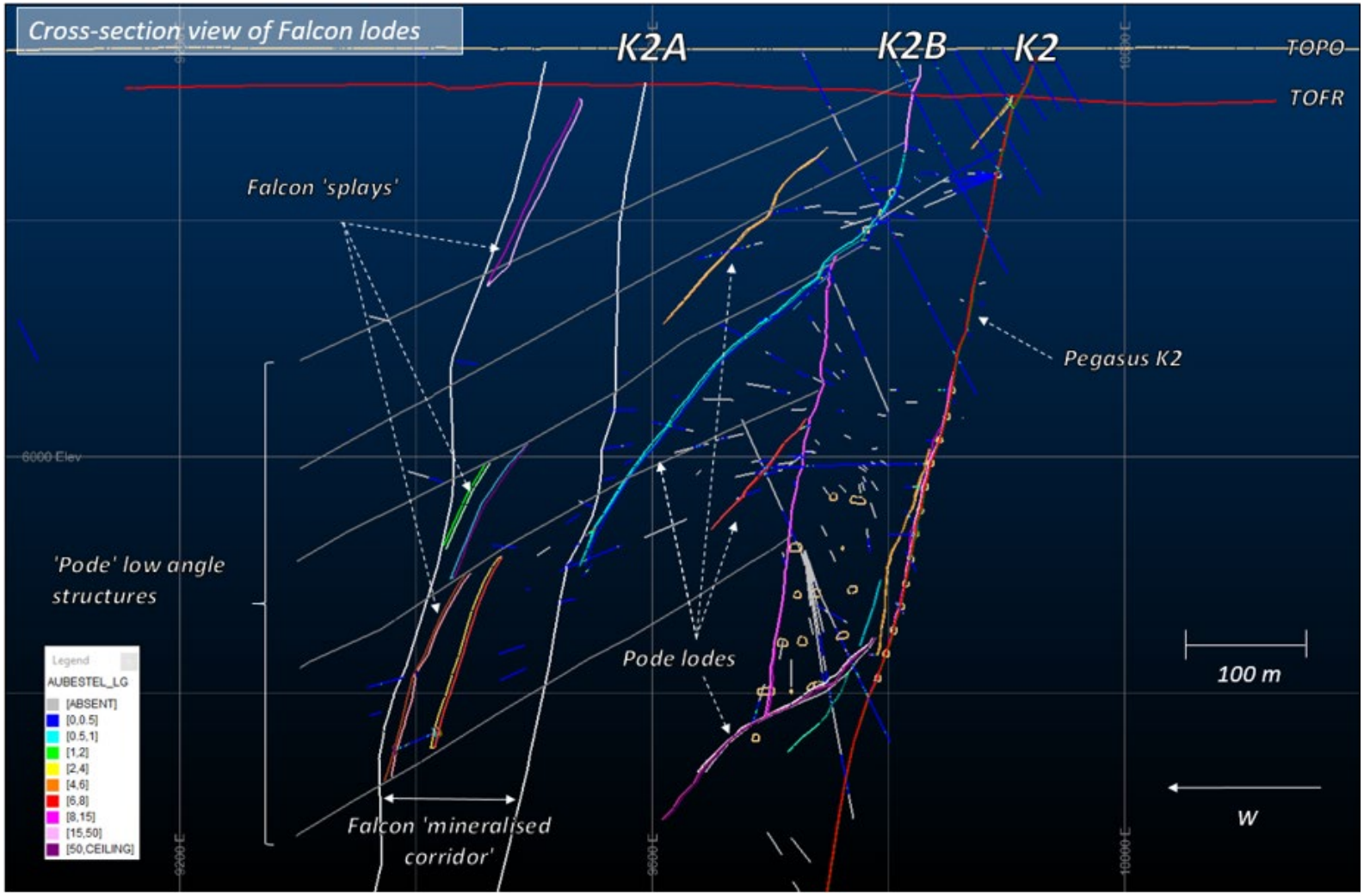


Figure 1. Cross section views of Falcon ore lodes (McKie, 2019)

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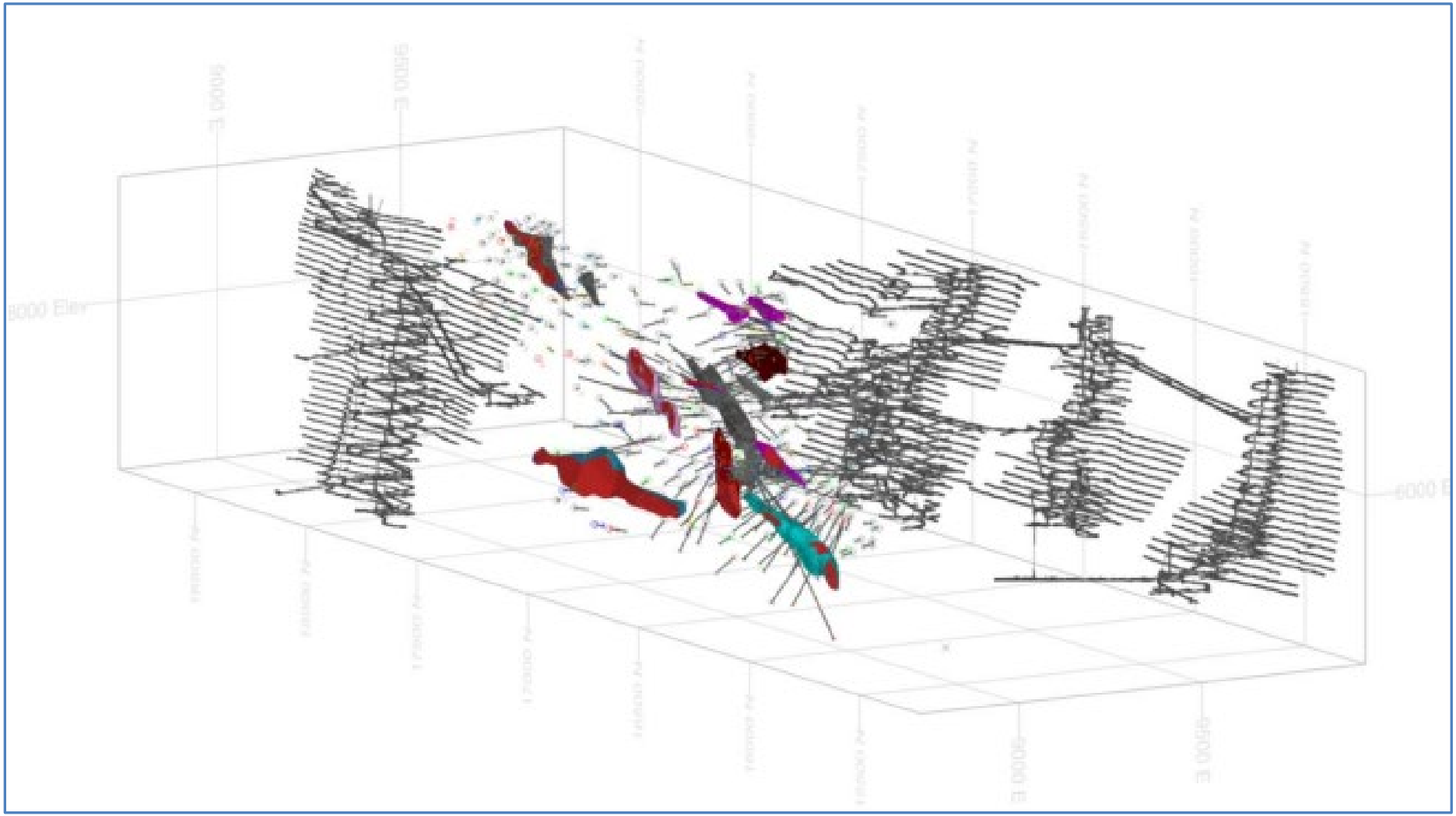


Figure 2. Oblique view of Falcon looking northeast, showing location relative to current underground development, the interpreted mineralisation pods and the current drilling (Gordon, 2022).

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Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Database integrity	• Sampling and logging data are either recorded on paper and manually entered into a database system or is captured digitally via a logging laptop and directly loaded into the database system. There are checks in place to avoid duplicate holes and sample numbers. Where possible, raw data is loaded directly into the database from laboratory and survey-tool derived files.
	• The complete exported database (including drill and face samples) is imported into Datamine and checked visually for any apparent errors i.e. holes or faces sitting between levels or not on surface DTM's. Multiple checks are then made on numerical data. These include: • Empty table checks to ensure all relevant fields are populated. • Unique collar location check. • Distances between consecutive surveys is no more than 60m for drill-holes. • Differences in azimuth and dip between consecutive surveys of no more than 0.3 degrees. • The end of hole extrapolation from the last surveyed shot is no more than 30 m. • Underground face sample lines are not greater than +\- 5 degrees from horizontal. • Errors are corrected where possible. When not possible the data is resource flagged as "No" in the database and the database is re-exported. This data will not be used in the estimation process. • Several drilling programs completed between 2014 and 2016 had erroneous meter depths recorded therefore these drill holes have been omitted from the ore wireframe interpretations and flagged as invalid. However, where there were no QAQC issue with the assays, the correct intervals have been recorded, the translation in the easting direction required for them to be in the 'correct' location (based on development above and below) applied and these intervals were appended to the data set before compositing. • In addition to being Resource Flagged as "Yes" or "No", drill holes are assigned a Data Class, which provides a secondary level of confidence in the data quality. Data Class (DC) values range from 0 to 3, with criteria summarised below: • DC 3 = Recent data; all data high quality, validated and all original data available. • DC 2 = Historic data; may or may not have all data in acQuire or hard copy available but has proximity to recent drilling which confirms the dip, width and tenor. Used to assist in classification. • DC 1 = Historic data; same criteria as DC 2 but cannot be verified with recent drilling, i.e., too far away, or dissimilar dip, width and/or tenor to recent drilling. Not used in Resource estimate. • DC 0 = Historic data; no original information or new drilling in proximity to verify. Not used in Resource estimate.

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Site visits	• The geological interpretations underpinning these resource models were prepared by geologists working in RHP. The estimation of grades was undertaken by personnel familiar with the ore body and the general style of mineralisation encountered. The Senior Resource Geologist and the Principal Resource Geologist, a Competent Person for reviewing and signing off on the Falcon estimations, maintained a site presence throughout the process.
	• The Competent Person has maintained a presence onsite.
Geological interpretation	• The geological interpretations underpinning these resource models have been prepared by geologists working in adjacent mines and in direct, daily contact with similar ore bodies. The estimation of grades was undertaken by personnel familiar with the orebody and the general style of mineralisation encountered. The Senior Resource Geologist, a competent person for reviewing and signing off on estimations of the Falcon lode maintained a presence throughout the process.
	• All available geological data was used in the interpretation including drill holes and previous geological modelling.
	• Alternative interpretations are not available for consideration. The mineralisation is interpreted based on the drilling as well as understanding from geologists who have a reasonable understanding of the Kundana geology.
	• The interpretation of the Star Trek mineralisation is based on the presence of mineralised structure (veining and shear), ore-bearing mineralogy (gold and associated sulphides), assayed samples and continuity between sections. Estimation is contained or controlled within hard boundaries for each ore domain.
	• Individual Star Trek mineralised structures are thought to be reasonably continuous at the current drill spacing, as similar mineralisation styles, structures and grade tenor exists between adjacent drillholes. • Post-mineralisation dextral offsetting faults (locally called D4 structures) affect the continuity of the Star Trek structure. These structures are steep-dipping, and the general trend is NNW-SSE. The largest is the Mary fault with a ~600 m offset. The White Foil and Poseidon faults form the bounding structures between the Hornet/Rubicon and Rubicon/Pegasus mine areas, respectively. Offset on these structures varies between 1 and 10 m. Many smaller scale faults exist within the mining areas (especially at the southern end of Hornet) although none have a material impact on the Resource model.
Dimensions	• The strike length of the different ore domains at Falcon vary but the extent of the mineralised trend at Falcon is in the order of 1.5km with individual ore domains having lengths more in the order of tens of metres. • Ore body widths are typically in the range of 0.5 – 5m. • Mineralisation is known to occur from the base of cover to 500 m below surface. The structure is open at depth.
Estimation and modelling techniques	• Multiple estimation methodologies have been tested to ascertain the sensitivity of the estimates to various input parameters, including top-cut, influence limitation model block size and kriging neighbourhood. This test work was completed on the Falc4 lode, which has the highest density of data present. The variability between estimates was

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~50%, which suggests the requirement for greater data density to improve geological confidence before an Indicated Resource can be released.

- In order to combat the variability in dip and dip direction a two-dimensional approach has been used for sample selection. Samples and blocks are transformed into two-dimensional space (a single plane in the Y-Z orientation), the estimate is completed in this space, then samples and blocks are back-transformed to their original position. This back-transformation is checked to ensure it agrees with the original position of the wireframe. This methodology negates the requirement for dynamic anisotropy and allows the variogram to be used to estimate grade in the major (down plunge) and semi-major (down dip) orientations.

- The downside of the two-dimensional approach is the inability of the estimate to reflect variability across the lode. To combat this, a proportional estimate has been used for final grade calculation.

- Firstly, a 'categorical estimate' is completed on a grade cut-off of 0.30 g/t (0.75 g/t for the Falc4 lode). This cut-off grade has been determined by looking for a break in the grade distribution. There is low variability in this grade between Falcon lodes, so the 0.30 g/t cut-off has been used across all lodes (except Falc4).

- Blocks above 0.30 g/t are coded with '1' and blocks below with '0'. An estimate is completed on the binary values to ascertain the probability of the block being above the grade cut-off. For instance, if the block estimate returned 0.65, the assumption would be that 65% of that block volume would be above the 0.30 g/t cut-off grade.

- Following this, two separate data sets are created. One contains all samples above 0.30 g/t and the other all samples below 0.30 g/t. These two data sets are used individually to estimate a high-grade and low-grade model. For lodes with few sample points, or lodes where it was not possible to create a coherent variogram model, Inverse Distance was used for both the proportional and grade estimates. For all other lodes, Ordinary Kriging was used.

- The final model is created by summing the products of the block proportion estimate and high- and low-grade estimates.

- FINAL_AU = (PROPORTION*HG _ESTIMATE) + (PROPORTION*LG_ESTIMATE)

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	• Note this final estimate is a weighted combination of these two models, which returns a single gold grade for the original block. All estimation use a three-pass search strategy and have been completed in Datamine RM v 1.4 software. As all estimates use data transformed into two-dimensional space, the direction 3 search has been manipulated to equal the direction 1 search. • Estimation was completed using Datamine Studio RM software.
	• Check estimates have been completed for all lodes. These include conventional Ordinary Kriging (OK) in three-dimensional space with search from variography (with and without dynamic anisotropy applied), conventional Ordinary Kriging (OK) with data and model transformed into two-dimensional space, OK with a generic variogram and isotropic search, Inverse Distance (ID) and Nearest Neighbour (NN) estimates.
	• No assumptions have been made.
	• No deleterious elements were estimated in these models.
	• For all lodes, a block size of 5 x 5 x 5 m has been chosen based on some Kriging Neighbourhood Analysis (KNA) work completed. • • Search ellipse dimensions were derived from the variogram model ranges (generally the distance corresponding to 80% of the total semivariance is used for pass 1, and the range of the variogram used for pass 2), or isotropic ranges based on data density where insufficient data was present for variographic analysis.
	• Selective mining units were not used during the estimation process.
	• All variables were estimated independently of each other. • Density has used estimation parameters based on the equivalent gold estimation for that domain.
	• The modelled Leapfrog shapes were used to define the Falcon mineralised zones which are based on the geology and gold grade. • For mine planning purposes a waste model is created by projecting the hanging wall and footwall surfaces 15 m either side. A default grade of 0.1 g/t is assigned and the same resource classification as the adjacent ore lode is applied.
	• Top cuts were applied to the composited sample data with the intention of reducing the impact of outlier values on the average grade. Top cuts were selected based on a statistical analysis of the data with a general aim of not impacting the mean by more than 5% and reducing the coefficient of variation to around 1.2; these vary by domain (ranging from 5 to 50 g/t for individual domains).

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	• The top cut values are applied in several steps, using a technique called influence limitation top cutting. A top cut (AU) and non-top cut (*_NC) variable is created, as well as a spatial variable (*_BC) which only has values where the top cut values appear. For example, where gold requires a top-cut, the following variables will be created and estimated: • AU (top cut gold) • AU_NC (non- top-cut gold) • AU_BC (spatial variable; values present where AU data is top cut) • The top-cut and non-top cut values are estimated using search ranges based on the variogram, and the *_BC values estimated using very small ranges (e.g. 5 m x 5 m x 5 m). Where the *_BC values produce estimated blocks within these restricted ranges, the *_NC estimated values replace the original top cut estimated values (AU). • The application of the top-cuts has not resulted in a significant decrease in the mean grade from the un-cut to top-cut data. Hard top cuts were applied to the Falc4 lode while the remainder of the lodes used influence limitation top cuts.
	• Statistical measures of Kriging error, such as Kriging Efficiency and Slope of Regression, are used to assess the quality of the estimation for each domain. • Differences between the declustered, top-cut composite data set and the average model grade must be within 10%. • Swath plots comparing declustered, top-cut composites to block model grades are created and visual plots are prepared summarising the critical model parameters. • Visually, block grades are assessed against drill hole data.
Moisture	• Tonnages are estimated on a dry basis.
Cut-off parameters	• Falcon is comprised of an underground resource but with potential for an open pit resource to be modelled in the future. The underground component has been reported at a 2.44 g/t cut off within 2.5 m minimum mining width MSOs.
Mining factors or assumptions	• No mining assumptions have been made during the resource wireframing or estimation process.
Metallurgical factors or assumptions	• No metallurgical assumptions have been made during the resource wireframing or estimation process.
Environmental factors or assumptions	• A “Licence to Operate” is held by the operation which is issued under the requirement of the “Environmental Protection Act 1986”, administered by the Department of Environment (DoE). The licence stipulates environmental conditions for the control of air quality, solid waste management, water quality, and general conditions for operation. Groundwater licenses are held for water abstraction, including production bore field water use for mineral processing, and mine dewatering, in accordance with the Rights in Water and Irrigation Act 1914. These licenses are also regulated by DoE and are renewable on a regular basis. Kanowna Operations conduct extensive environmental monitoring and management programs to ensure compliance with the requirements of the licences and lease conditions. An

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	Environmental Management System is in place to ensure that Evolution employees and contractors meet or exceed environmental compliance requirements. • The Mungari operations are fully permitted including groundwater extraction and dewatering, removal of vegetation, mineral processing, and open pits. • The Mungari Operations have been compliant with the International Cyanide Management Code since milling operations began.
Bulk density	• A thorough investigation into average density values for the various lithological units at Falcon was completed and the mean densities by lithology were coded into the database. Where there were no measurements for a specific lithology a default of 2.8 t/m^3 was applied. • Density was assigned to the model as average values for the various weathering and lithology types. • Post estimation, default density values for the oxide and transitional zones were applied, based on regional averages.
	• Mill tonnage reconciliation data validates the bulk density values being applied and natural voids or porosity are not a significant factor in estimating tonnages of material at the adjacent RHP operations.
	• Assumptions on the average bulk density of individual lithologies from the regional data set. 21,549 bulk density samples have been used. Results are in line with regional expectations. Default densities have been applied to oxide (1.9 t/m3) and transitional (2.3 t/m3) material, due to lack of data in this area. These values are in line with regional averages.
Classification	• Classification is based on a series of factors including: • Geologic grade continuity • Density of available drilling • Statistical evaluation of the quality of the kriged estimate • Confidence in historical data, based on the Data Class system applied
	• All relevant factors have been given due weighting during the classification process.
	• The resource estimation methodology is considered appropriate, and the estimated grades reflect the Competent Persons view of the deposit.
Audits or reviews	• All resource models have been subjected to internal peer review. Cube Consulting have undertaken some review during 2022 of EVN resource estimation methodologies and estimation validations.
Discussion of relative accuracy/ confidence	• These mineral resource estimates are considered as robust and representative of the Falcon styles of mineralisation. The relative accuracy of the Mineral Resource estimate is reflected in the reporting of the Mineral Resource as per the guidelines of the 2012 JORC Code.
	• The statement relates to global estimates of tonnes and grade.

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	• These mineral resource estimates are considered as robust and representative of the Falcon styles of mineralisation. The relative accuracy of the Mineral Resource estimate is reflected in the reporting of the Mineral Resource as per the guidelines of the 2012 JORC Code.

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1.6 Star Trek: Mineral Resource – 31 December 2022

Section 1: Sampling Techniques and Data

Criteria	Commentary
Sampling techniques	• Underground and surface diamond drilling (DD) and surface reverse circulation drilling (RC) sampling were used to inform the gold estimation at Star Trek. No issues have been reported regarding poor quality of sampling for any drill type. A review of core photography indicates good sample quality with occasional broken zones of core.Rotary air blast (RAB) and Air core (AC) holes were excluded from the estimation process. In total, 339 drillholes are drilled in and around the Star Trek mineralisation dating from 1996 to the present day.

Star Trek Deposit - Drilling Statistics

Company	Period	Hole Prefix	Drill Type	Number of Drillholes	Total Metres	Number of Samples	% of Holes	% of Metres	% of Samples
Tribune Resources	1996	TRC	RC	68	3,688.7	1,459	20.1%	6.8%	2.9%
EKJV	1999-2001	EKR	RC	35	3,117.0	1,133	10.3%	5.8%	2.2%
EKJV	1999-2001	EKD	DD	2	363.0	213	0.6%	0.7%	0.4%
Goldfields Exploration	2001	UR	RC	61	5,220.0	2,725	18.0%	9.7%	5.3%
Goldfields Exploration	2001	URD	DD	3	406.3	381	0.9%	0.8%	0.7%
Placer Dome	2003	SSTR	RC	50	4,436.0	2,749	14.7%	8.2%	5.4%
Barrick Gold	2009	STC09	RC	6	414.0	414	1.8%	0.8%	0.8%
Northern Star (EKJV)	2017	STDD	DD	3	745.8	909	0.9%	1.4%	1.8%
Northern Star (EKJV)	2017	STDT	DD	4	2,182.2	2,034	1.2%	4.0%	4.0%
Northern Star (EKJV)	2017-18	STRC	RC	7	1,314.0	1,313	2.1%	2.4%	2.6%
Northern Star (EKJV)	2020-21	STKRT	DD	70	24,035.3	32,853	20.6%	44.5%	64.3%
Evolution Mining (EKJV)	2021	STKRT	DD	12	3,571.2	1,611	3.5%	6.6%	3.2%
Evolution Mining (EKJV)	2021-22	STKDT	DD	18	4,493.5	3,318	5.3%	8.3%	6.5%
				339	**53,987.0**	**51,112**	100.0%	100.0%	100.0%

	• Diamond core drilling is sampled to geological boundaries with a minimum (0.5 m) and maximum (1.49 m) sample length. • RC sampling is sampled at 1m intervals through mineralised zones with some primary composite samples still included in the dataset. RC sampling provides a larger sample size than drill core but is less representative of geology, particularly around geological contacts and narrow ore zones.
	• DD drill core was nominated for either half core or full core sampling.

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	• Core designated for half core was cut using an automated core saw. The mass of material collected was dependent on the drillhole diameter and sampling interval selected. Core designated for full core was broken with a rock hammer at sample intervals and if sample segments were too large to fit into sample bags. • Recent RC samples are collected via a rig mounted riffle or cone splitter at 1m intervals to produce approximately 3kg of sample. Previously samples may have been split via a free-standing riffle splitter, particularly if they were a 1m re-sample of a primary composited sample that was anomalous for gold. • All samples were delivered to a commercial laboratory where they were dried and crushed, generally to 90% of material ≤3 mm. At this point large samples were split using a rotary splitter, then pulverised to 90% ≤75 µm. • A 40 g charge was selected for fire assay for all recent samples. Historically, charge weights between 30g and 50g have also been used.
Drilling techniques	• Both Reverse Circulation and Diamond Drilling techniques were used to drill the Star Trek deposit. • Surface diamond drillholes were completed using HQ2 (63.5 mm) coring, whilst underground diamond drillholes were completed using NQ2 (50.5 mm) coring. • Core was orientated where possible and a bottom of hole orientation line marked on the core. • RC Drilling was completed mostly using a 5.5” drill bit.
Drill sample recovery	• For DD drilling, any core loss is recorded on the core block by the driller. This is captured by the logging geologist and entered as an interval into the hole log. • For RC sampling, sample weights may be recorded to give an indication of areas of poor sample return. Geology personnel at the drill site would give feedback to the driller in regard to sample recovery that may not have been satisfactory.
	• Contractors adjust the rate and method of drilling if recovery issues arise. All recovery is recorded by the drillers on core blocks. This is checked and compared to the measurements of the core by the geological team. Any issues are communicated back to the drilling contractor.
	• Recovery was generally very good for diamond core and no relationship between grade and recovery is observed or commented on in historical reporting.
Logging	• All diamond core is logged for lithology, veining, alteration, mineralisation, and structural data. Structural measurements of specific features are also taken through oriented zones. RC chips are logged every metre and include the same except for structural data. • Historically, geological logging was initially on paper logs and then manually entered into a database, recent logging is by electronic methods and then uploaded to the site databases by various database import objects. • Logging is stored in the Mungari site geological database (acQuire) using a series of drop-down menus which contain the appropriate codes for description of the rock or regolith.
	• All core logging is qualitative with mineralised zones assayed for quantitative measurements. Core is photographed wet and or dry and most photography is available on the Mungari servers.

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	• Photos of RC chip trays have not been located but it was a common practice for this to be done.
	• For all drill holes, the entire length of the hole is logged.
Sub-sampling techniques and sample preparation	• Diamond core is cut using an automated core saw. Sampling and cutting methodology is dependent on the type of drilling completed. Half core is utilised for exploration drilling. Some drill holes have been whole core sampled.
	• RC samples are split using a rig-mounted riffle or cone splitter to collect a sample 2 - 4 kg in size from each 1 m interval. Many of the earlier RC samples were composite sampled by spear or scoop with anomalous intervals re-sampled by a free-standing riffle splitter.
	• Preparation of drill samples was conducted at external laboratories commencing with sorting, checking, and drying at less than 110°C to prevent sulphide breakdown. Samples were jaw crushed to a nominal -6 mm particle size. If the sample is greater than 3 kg a Boyd crusher with rotary splitter is used to reduce the sample size to less than 3 kg (typically 1.5 kg) at a nominal <3 mm particle size. • The entire crushed sample (if less than 3 kg) or sub-sample is then pulverized to 90% ≤75 µm, using a LM5 bowl pulveriser. Pulp sub-samples of about 400g are then taken with an aluminium scoop and stored in labelled pulp packets. • The sample preparation is considered appropriate for the mineralisation type.
	• Standard procedures are used for all processes within the laboratory. Grind checks are performed at both the crushing stage (3 mm) and pulverising stage (75 µm), requiring 90% of material to pass through a sieve of relevant size.
	• Umpire sampling is performed frequently, where 3% of the samples are sent to the umpire laboratory for processing. • Umpire samples of faces were analysed using a 40 g charge weight.
	• The sample sizes are considered appropriate for the material being sampled.
Quality of assay data and laboratory tests	• A 30- 50 g fire assay charge is used with a lead flux in the furnace. The resultant prill is totally digested by HCl and HNO_3 acids before Atomic Absorption Spectroscopy (AAS) determination for gold analysis.
	• No geophysical tools were used to determine any element concentrations.
	• For most drilling certified reference materials (CRMs) are inserted into the sample sequence at a rate of 1 per 20 samples to ensure correct calibration. Any values outside of 3 standard deviations are re-assayed with a new CRM. • Blanks are inserted into the sample sequence at a rate of 1 per 20 samples. The insertion points are selected at random, except where high grade mineralisation is expected. In these cases, a Blank is inserted after the high-grade sample to test for contamination. Results greater than 0.2 g/t if received are investigated, and re-assayed if appropriate. New pulps are prepared if anomalous results cannot be resolved. • Barren flushes are regularly inserted after anticipated high gold grades at the pulverising stage. • No field duplicates are submitted for diamond core.

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	• Pulp duplicates are requested after any ore zone. These are indicated on the sample sheet and the submission sheet. • When visible gold is observed in core, a quartz flush would be requested after the sample. • Laboratory performance was monitored using the results from the QA samples mentioned above. This was supplemented by the internal QA samples used by the laboratories, which included pulp duplicates and CRMs. Laboratory visits and audits are conducted on a regular basis. • The QA studies indicate that accuracy and precision are within EKJV accepted limits.
Verification of sampling and assaying	• All significant intersections are verified by another geologist during the drill hole validation process, and later by a competent person to be signed off.
	• No specific twinned holes were drilled. Re-drilling of some drillholes has occurred due to issues downhole (e.g., bogged rods). These have been captured in the database with an 'A' suffix. Re-drilled holes are sampled, whilst the original drillhole is logged but not sampled.
	• Geological logging and sampling are directly recorded into acQuire. Assay files are received in .csv format and loaded directly into the database using an acQuire importer object. Assays are then processed through a form in acQuire for QAQC checks. Hardcopy and non-editable electronic copies of these are stored.
	• No adjustments have been made to this assay data.
Location of data points	• For all drilling, planned holes are marked up by the mine survey department using a total station survey instrument in mine grid (Kundana 10). The actual hole position is then located by the mine survey department once drilling is completed. • Surface drillholes are set up for azimuth by surveyed sighter pegs and tape line. Underground diamond core drillholes are lined up on the collar point using the DHS Minnovare Azimuth Aligner. Planned azimuths and dips of the holes are downloaded to the aligner which is then placed on the rod string to align the hole for drilling. • During drilling, single shot surveys are conducted every 30 m to track the deviation of the hole and to ensure it stays close to design. This is performed using the DeviShot camera which measures the gravitational dip and magnetic azimuth. Results are uploaded from the Devishot software into a csv format which is then imported into acQuire. At the completion of the hole, a Multishot (using the DeviFlex non-magnetic strain gauge instrument) survey is completed, taking measurements every 3 m to ensure accuracy of the hole. This is converted to csv format and imported into acQuire.
	• Collar coordinates are recorded in mine grid (Kundana 10 or K10) and transformed into MGA94_51.

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	KUNDANA 10		
	X	Y	Z
Point 1	10000.000	20000.000	6343.658
Point 2	10000.267	18668.600	6343.967

Dip	0
Azimuth	179.989

	MGA94-51		
	X	Y	Z
Point 1	331726.160	6600882.149	343.658
Point 2	332376.768	6599720.746	343.967

Dip	0
Azimuth	150.743

Rotation
29.246

	• Quality topographic control has been achieved through Lidar data and survey pickups of holes over the last 15 years.
Data spacing and distribution	• Drillhole spacing varies across the deposit, with most of the drilling between 120 x 120 m and 40 x 40 m spacing. Some areas proximal to development have been drilled at a 20 x 20 m drill spacing.
	• The data spacing and distribution is considered sufficient to support the Resource and Reserve estimates.
	• No sample compositing has been applied.
Orientation of data in relation to geological structure	• Most of the structures in the Kundana area dip steeply (80°) to the west (local grid) with some other known more-shallow dipping (30-60°) lodes. Diamond drilling was designed to target the ore bodies perpendicular to this orientation to allow for a favourable intersection angle. Instances where this was not achievable (primarily due to drill platform location), drilling was not completed, or re-designed once a more suitable platform became available. • Drill holes with low intersection angles are excluded from resource estimation where more suitable data is available.
	• No sampling bias is considered to have been introduced by the drilling orientation. Where drillholes have been particularly oblique, they have been flagged as unsuitable for resource estimation.
Sample security	• Prior to laboratory submission samples are stored at the secure Millennium core yard. Once submitted to the laboratories they are stored in a secure fenced compound, tracked through their chain of custody and via audit trails. Previous companies would have had a similar process of sample security.
Audits or reviews	• No audits have been undertaken of the data and sampling practices.

Section 2 Reporting of Exploration Results

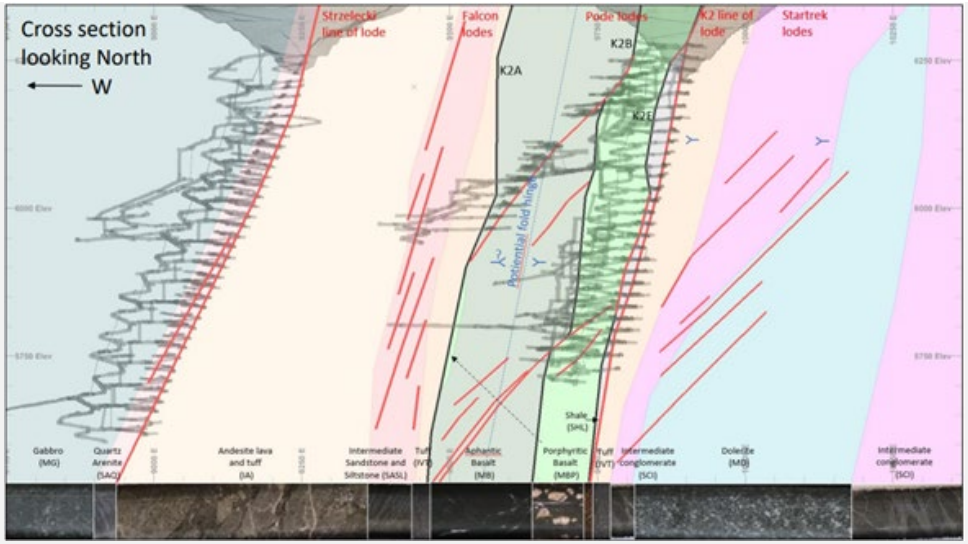
(Criteria listed in the preceding section also apply to this section.)

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Criteria	Commentary
Mineral tenement and land tenure status	• All holes mentioned in this report are collared on either M16/309 or M16/993 held by the East Kundana Joint Venture (EKJV). The EKJV is majority owned and managed by Evolution Mining Limited with the minority holding held by Tribune Resources Ltd and Rand Mining Ltd. • The tenement on which the Star Trek Deposit is mostly hosted (M16/309) is subject to three royalty agreements. The agreements that are on M16/309 are the Kundana- Hornet Central Royalty, the Lake Grace Royalty and the Kundana Pope John Agreement No. 2602-13.
	• No known impediments exist, and the tenements are in good standing.
Exploration done by other parties	• The first reference to the mineralisation style encountered at the Kundana project was the Mines Department report on the area produced by Dr. I. Martin (1987). He reviewed work completed in 1983 – 1984 by a company called Southern Resources, who identified two geochemical anomalies, creatively named Kundana #1 and Kundana #2. The Kundana #2 prospect was subdivided into a further two prospects, dubbed K2 and K2A. • Between 1987 and 1997, limited work was completed. • Between 1997 and 2006, Tern Resources (subsequently Rand Mining and Tribune Resources) and Gilt-edged Mining focused on shallow open pit potential with production from the Rubicon open pit commenced in 2002. During this period the Star Trek mineralisation was identified and advanced with some deeper RC drilling. • Underground Mining commenced in 2011 at the Rubicon – Hornet prospects with the underground portal in the completed Rubicon Open Pit. • Northern Star took over the RHP project in March 2014 and drilled over 80 mostly resource development diamond core drill holes at Star Trek during their ownership of the project.
Geology	• The Kundana camp is situated within the Norseman-Wiluna Greenstone Belt, in an area dominated by the Zuleika shear zone, which separates the Coolgardie domain from the Ora Banda domain. • K2-style mineralisation (Pegasus, Rubicon, Hornet, Drake) consists of narrow vein deposits hosted by shear zones located along steeply dipping overturned lithological contacts. The K2 structure is present along the contact between a black shale unit (Centenary Shale) and intermediate volcaniclastics (Black Flag Group). • Minor mineralisation, termed K2B, also occurs further west, on the contact between the Victorious basalt and Bent Tree Basalt (both part of the regional upper Basalt Sequence). Additional mineralised structures include the K2E and K2A veins, Polaris/Rubicon Breccia (Silicified and mineralised Shale) and several other HW lodes adjacent to the main K2 structure. • Star Trek lodes are typically 60° W dipping vein hosted mineralisation in the Footwall of the K2E lodes on an Intermediate Volcanic – Dolerite contact.

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	 ***Figure 1 Cross Section Schematic showing position of Star Trek Lodes***
Drill hole Information	• A summary of the data present in the Star Trek deposit can be found above. Collar data is presented in the local Kundana (K10) mine grid. • Drillholes vary in survey dip from +26 to -72 degrees, with hole depths ranging from 9 m to 615 m, with an average depth of 268 m. • All validated drill hole data was used directly or indirectly for the preparation of the resource estimation.
	• The exclusion of any drill hole data is not material to this report.
Data aggregation methods	• Not applicable
	• Not applicable
	• Not applicable

Relationship between mineralisation widths and intercept lengths	• Not applicable
	• Not applicable
	• No interval lengths are reported for the resource estimation
Diagrams	• Not applicable
Balanced reporting	• Not applicable
Other substantive exploration data	• Resource definition drilling will continue in various parts of RHP with the intention of extending areas of known mineralisation. Further drilling would likely be resource definition scaled drill spacing to improve on resource confidence and with no plan to advance to mining grade control drilling at the present moment
Further work	• Resource definition drilling will continue in various parts of RHP with the intention of extending areas of known mineralisation. Further drilling would likely be resource definition scaled drill spacing to improve on resource confidence and with no plan to advance to mining grade control drilling at the present moment. • Appropriate diagrams have been created for monthly and annual reporting.
	• Not applicable

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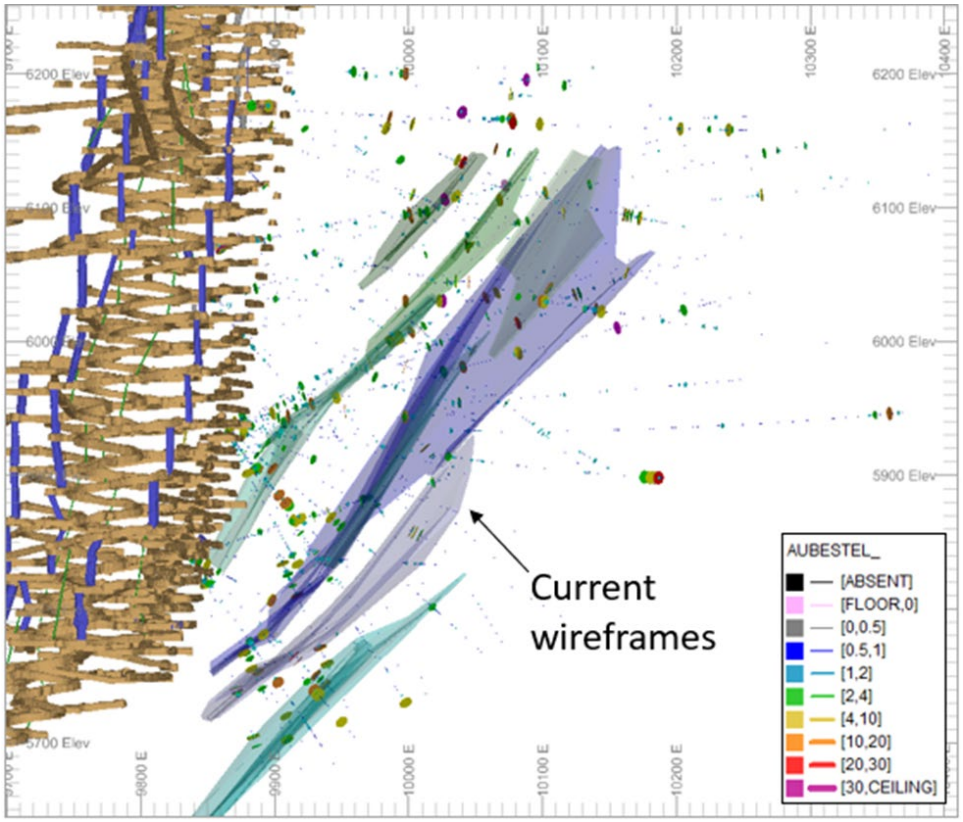


Figure 2. Cross section view (looking North) of Star Trek lodes

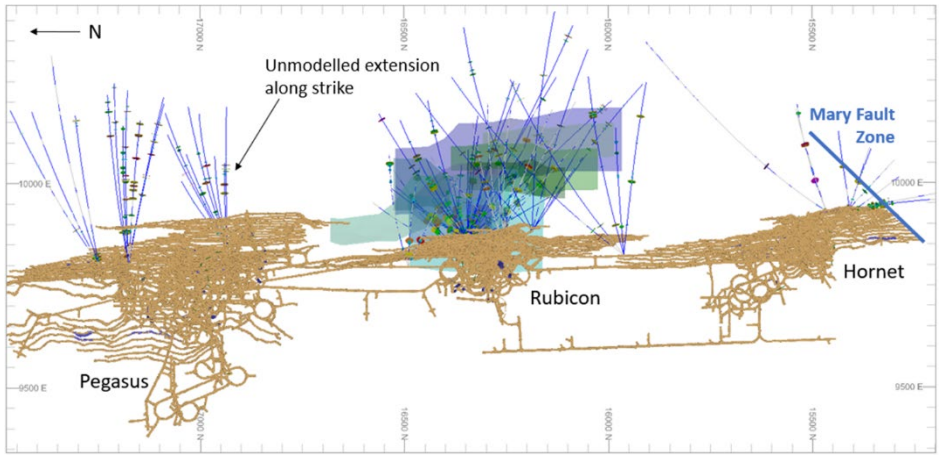


Figure 3. Plan view of Star Trek Lodes and Location in Relation to RHP Trend with Underground Drill Traces Displayed

Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Database integrity	• Data analysis and estimation was undertaken using Snowden Supervisor and Datamine Studio RM Pro software. Wireframing was undertaken using Leapfrog Geo 3D software. • Gold (Au) ppm block grades were estimated using ordinary kriging (OK). Snowden Optiro considers OK to be an appropriate estimation technique for this type of mineralisation. • Drilling is generally on a 80 m x 40 m spacing, there are areas of closer spaced drilling from the underground workings and this is drilled at around 40 m x 20 m spacing. • A maximum extrapolation distance of 50 m was applied along strike and 50 m down dip. • Over 42% of the assay data within the mineralisation is from samples of 1 m intervals, 53% is from intervals of less than 1 m and 5% is from intervals of over 1 m (to a maximum of 5 m). The data was composited to 1 m intervals. • Variogram analysis was undertaken to determine the kriging estimation parameters used for OK estimation of gold.

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	• Gold mineralisation continuity was interpreted from variogram analysis to have an along strike range of between 100 and 170 m and a down-dip range of 65 m. • Kriging neighbourhood analysis was performed to determine the block size, sample numbers and discretisation levels. • Three estimation passes were used; the first search was based upon the variogram ranges; the second search was 1.5 times the range of the variograms and the third search was double the first search; the second and third searches had reduced sample numbers required for estimation. The majority of gold block grades (almost 84%) were estimated in the first two search passes, 16% in the third pass and the remaining 1% an average was estimated by nearest neighbour approach. The gold estimated block model grades were visually validated against the input drillhole data and comparisons were carried out against the de-clustered drillhole data and by northing, easting and elevation slices.
	• The complete exported data base including drill and face samples is brought into Datamine and checked visually for any apparent errors i.e., holes or faces sitting between levels or not on surface DTM's. Multiple checks are then made on numerical data. This includes: • Empty table checks to ensure all relevant fields are populated • Unique collar location check • Distances between consecutive surveys is no more than 60m for drill-holes • Differences in azimuth and dip between consecutive surveys of no more than 0.3 degrees • The end of hole extrapolation from the last surveyed shot is no more than 30 m • Underground face sample lines are not greater than +\- 5 degrees from horizontal • Errors are corrected where possible. When not possible the data is resource flagged as "No" in the database and the database is re-exported. This data will not be used in the estimation process. • Several drilling programs completed between 2014 and 2016 had erroneous metre depths recorded by the drillers, therefore these drill holes have been omitted from the ore wireframe interpretations and flagged as invalid. However, where there were no QAQC issue with the assays, the correct intervals have been recorded, the translation in the easting direction required for them to be in the 'correct' location (based on development above and below) applied and these intervals were appended to the data set before compositing. • The sample translation method has been applied to surface drilling in between development levels which are deemed to cause an unrealistic kink in the wireframe interpretation. This is only done after a thorough investigation of the surrounding data to ensure that no secondary veining is present in the footwall or hanging wall and that no separate lodes are missed. • In addition to being Resource Flagged as "Yes" or "No", drill holes are assigned a Data Class, which provides a secondary level of confidence in the data quality. Data Class (DC) values range from 0 to 3, with criteria summarised below: • DC 3 = Recent data - all data high quality, validated and all original data available. • DC 2 = Historic data - may or may not have all data in acQuire or hard copy available but has proximity to recent drilling which confirms the dip, width and tenor which is used to assist in classification Or Recent data - minor issues with data but away from the ore zone.

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	• DC 1 = Historic data - same criteria as DC 2 but cannot be verified with recent drilling, i.e., too far away, or dissimilar dip, width and/or tenor to recent drilling. Not used in Resource estimate. • DC 0 = Historic data - no original information or new drilling in proximity to verify. Not used in Resource estimate.
Site visits	• The geological interpretations underpinning these resource models were prepared by geologists working in RHP. The estimation of grades was undertaken by personnel familiar with the ore body and the general style of mineralisation encountered. The Senior Resource Geologist and the Principal Resource Geologist, a Competent Person for reviewing and signing off on the Star Trek estimations, maintained a site presence throughout the process.
	• The Star Trek orebody is not exposed underground so has not been routinely visited by the competent person. The competent person has visited core processing facilities whilst Star Trek core is being processed.
Geological interpretation	• The geological interpretation of the Star Trek deposit has been carried out using a systematic approach to ensure continuity of the geology and estimated mineral resource. The confidence in the geological interpretation is high and is supported with information acquired during ore development as well as from underground and surface diamond drilling. • The interpretation of all Star Trek ore domain wireframes was conducted using the sectional interpretation method in Datamine RM software. All lodes have been interpreted in plan-view section. Where development levels were present, sectional interpretation was completed at approximately 5 m spacing. Where only drilling data was present, sectional interpretation was completed at approximately 10 m - 20 m spacing. Checks were made to ensure that the wireframed volume agreed with the true ore widths of drill hole intersections. As a rule, wireframe extrapolation was limited to one half of the average drill spacing.
	• All available geological data was used in the interpretation including drill holes and previous geological modelling.
	• Alternative interpretations are not available for consideration. The mineralisation is interpreted based on the drilling as well as understanding from geologists who have a reasonable understanding of the Kundana geology.
	• The interpretation of the Star Trek mineralisation is based on the presence of mineralised structure (veining and shear), ore-bearing mineralogy (gold and associated sulphides), assayed samples and continuity between sections. Estimation is contained or controlled within hard boundaries for each ore domain.
	• Individual Star Trek mineralised structures are thought to be reasonably continuous at the current drill spacing, as similar mineralisation styles, structures and grade tenor exists between adjacent drillholes. • Post-mineralisation dextral offsetting faults (locally called D4 structures) affect the continuity of the Star Trek structure. These structures are steep-dipping, and the general trend is NNW-SSE. The largest is the Mary fault with a ~600 m offset. The White Foil and Poseidon faults form the bounding structures between the Hornet/Rubicon and Rubicon/Pegasus mine areas, respectively. Offset on these structures varies between 1 and 10 m. Many smaller scale

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	faults exist within the mining areas (especially at the southern end of Hornet) although none have a material impact on the Resource model.
Dimensions	• The strike length of the different ore domains at Star Trek vary but the extent of the mineralised trend at Star Trek is in the order of 3.5km. The individual ore bodies occur in a major regional Zuleika shear system extending over tens of kilometres. • Ore body widths are typically in the range of 0.2 – 3.0 m. • Mineralisation is known to occur from the base of cover to 500 m below surface. The structure is open at depth.
Estimation and modelling techniques	• The Ordinary Kriged estimation method is appropriate for the Star Trek style of mineralisation. The Mineral Resource remains in the Inferred Resource category until there is more confidence that the estimation parameters are appropriate for the distribution of gold throughout the Star Trek trend. • Currently variogram analysis suggests grade continuity in excess of 150m along strike and 65m up and down dip which may be excessive for first pass estimation. • Estimation was completed using Datamine Studio RM software.
	• No check estimates have been completed. • There is no previous published Mineral Resource model to run comparisons against.
	• No assumptions have been made.
	• No deleterious elements were estimated in these models.
	• Parent cell sizes selected by KNA were 40m (N) x 20m (E) and 5m (RL) with sub-celling to 2.5m (N) x 1.25m (E) and 2.5m (RL). KNA also determined the minimum and maximum number of samples selected for each pass of estimation. • Search ellipse dimensions were derived from the variogram model ranges and increased by various factors for second and third passes. Three estimation passes were used; the first search was based upon the variogram ranges; the second search was 1.5 times the range of the variograms and the third search was double the first search; the second and third searches had reduced sample numbers required for estimation. The majority of gold block grades (almost 84%) were estimated in the first two search passes, 16% in the third pass and the remaining 1% an average was estimated by nearest neighbour approach. The gold estimated block model grades were visually validated against the input drillhole data and comparisons were carried out against the de-clustered drillhole data and by northing, easting and elevation slices.
	• Selective mining units were not used during the estimation process.
	• All variables were estimated independently of each other. • Density has used estimation parameters based on the equivalent gold estimation for that domain.

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	• The modelled Leapfrog shapes were used to define the Star Trek mineralised zones which are based on the geology and a selected cut-off gold grade. • For mine planning purposes a waste model is created by expanding the ore shapes a selected distance (generally 10-20m) in all directions. A default grade of 0.1 g/t is assigned to the waste and the same resource classification as the adjacent ore lode is applied.
	• Top cuts were applied to the composited sample data with the intention of reducing the impact of outlier values on the average grade. Top cuts vary by domain (ranging from 15 g/t to 40 g/t for individual domains).
	• Statistical measures of Kriging error, such as Kriging Efficiency and Slope of Regression, are used to assess the quality of the estimation for each domain. • Differences between the declustered, top-cut composite data set and the average model grade must be within 10%. • Swath plots comparing declustered, top-cut composites to block model grades are created and visual plots are prepared summarising the critical model parameters. • Visually, block grades are assessed against drill hole data.
Moisture	• Tonnages are estimated on a dry basis.
Cut-off parameters	• Star Trek is comprised of an underground resource but with potential for an open pit resource to be modelled in the future. The underground component has been reported at a 2.44 g/t cut off within 2.5 m minimum mining width MSOs.
Mining factors or assumptions	• No mining assumptions have been made during the resource wireframing or estimation process.
Metallurgical factors or assumptions	• No metallurgical assumptions have been made during the resource wireframing or estimation process.
Environmental factors or assumptions	• A “Licence to Operate” is held by the operation which is issued under the requirement of the “Environmental Protection Act 1986”, administered by the Department of Environment (DoE). The licence stipulates environmental conditions for the control of air quality, solid waste management, water quality, and general conditions for operation. Groundwater licenses are held for water abstraction, including production bore field water use for mineral processing, and mine dewatering, in accordance with the Rights in Water and Irrigation Act 1914. These licenses are also regulated by DoE and are renewable on a regular basis. Kanowna Operations conduct extensive environmental monitoring and management programs to ensure compliance with the requirements of the licences and lease conditions. An Environmental Management System is in place to ensure that Evolution employees and contractors meet or exceed environmental compliance requirements. • The Mungari operations are fully permitted including groundwater extraction and dewatering, removal of vegetation, mineral processing, and open pits. • The Mungari Operations have been compliant with the International Cyanide Management Code since milling operations began.

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Bulk density	• A thorough investigation into average density values for the various lithological units at Star Trek was completed and the mean densities by lithology were coded into the database. Where there were no measurements for a specific lithology a default of 2.8 t/m^3 was applied. • Density was assigned to the model as average values for the various weathering and lithology types. • Post estimation, default density values for the oxide and transitional zones were applied, based on regional averages.
	• Mill tonnage reconciliation data validates the bulk density values being applied and natural voids or porosity are not a significant factor in estimating tonnages of material at the adjacent RHP operations.
	• Assumptions on the average bulk density of individual lithologies, based on 252 bulk density measurements at Star Trek. Assumptions were also made based on regional averages, on the default densities applied to oxide (1.8 t/m³) and transitional (2.3 t/m³) material, due to a lack of data in these zones.
Classification	• Classification is based on a series of factors including: • Geologic grade continuity • Density of available drilling • Statistical evaluation of the quality of the kriged estimate • Confidence in historical data, based on the Data Class system applied
	• All relevant factors have been given due weighting during the classification process.
	• The resource estimation methodology is considered appropriate, and the estimated grades reflect the Competent Persons view of the deposit.
Audits or reviews	• All resource models have been subjected to internal peer review. Cube Consulting have undertaken some review during 2022 of EVN resource estimation methodologies and estimation validations.
Discussion of relative accuracy/ confidence	• These mineral resource estimates are considered as robust and representative of the Star Trek styles of mineralisation. The relative accuracy of the Mineral Resource estimate is reflected in the reporting of the Mineral Resource as per the guidelines of the 2012 JORC Code.
	• The statement relates to global estimates of tonnes and grade.
	• These mineral resource estimates are considered as robust and representative of the Star Trek styles of mineralisation. The relative accuracy of the Mineral Resource estimate is reflected in the reporting of the Mineral Resource as per the guidelines of the 2012 JORC Code.

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1.7 Section 4: Estimation and Reporting of Ore Reserves

Criteria	Commentary
Mineral Resource estimate for conversion to Ore Reserves	• The Ore Reserve estimates are based on the current Mineral Resource estimates as described in Section 3. • The Mineral Resources are reported inclusive of the Ore Reserve.
Site visits	• Competent persons are both Mungari Employees and based at the Mungari Operations (Blake Callinan)
Study status	All assets included in the CY2022 Reserves Statement have been completed to a Pre-Feasibility Study level or better with the following assets currently actively mining: • RHP (Rubicon/Hornet/Pegasus) Underground • Raleigh Underground (currently on care-of-maintenance)

Cut-off parameters	The Evolution Mining's Strategic Planning Standards (EVN-COR-STD-002) were used to determine the cut-off grades for the Ore Reserve with the following costs included:
	• Incremental Mining Costs
	  ○ for Open Pit Reserves these were incremental cost of mining ore
	  ○ for Underground Reserves these were stoping costs
	• Processing costs
	  ○ Current costs for EKJV prior to the mill upgrade
	• General and Administration costs
	  ○ Current costs for assets prior to the mill upgrade
	• Surface rehandle (or haulage) costs.
	  ○ Based on current contracted cost structure
	• Mill recoveries for operating assets were based on historical recoveries from the Mungari Process Plant at:
	  ○ RHP and Raleigh (East Kundana Operations) = 93.5%
	A gold price of A$1,600/ounce was used to calculate all cut-off grades.

Mining factors or assumptions	The methodology for converting a Mineral Resource to reserve at Evolution Mining is as follows: • Derivation of cut-off grades as determined from the cut-off parameters. • Definition of optimisation parameters from either empirical data (operating mines) or previous project work undertaken. • Optimisation of mining resource based on parameters using recognised software. • Open Pit optimisations were completed using GEOVIA Whittle™ • Underground Optimisations were completed using Deswik.SO (built around the AMS Mineable Shape Optimizer) • Evaluation and selection of optimal mining pits/shapes • Complete minable design (Open Pit – Pit Design, Underground – final stopes and required development) • Apply modifying factors, review Resource classification, and technical requirements to be defined as a Proven or Probable Reserve are met. • Complete a full costing evaluation at a range of gold prices (A$1,600, A$1,900, and A$2,200/oz) to determine economics and sensitivity
	Geotechnical considerations have been considered during the Ore Reserve process including: • Open Pit mining: geotechnical studies provide detailed pit slope angle for consideration during the design process. • Underground mining: the mines are exposed to some degree to seismic risk. Multiple studies have been conducted with regular internal and external geotechnical reviews to ensure the most effective design, support, and extraction sequence are employed. These are captured in the individual Ground Control Management for each underground mine and were adhered to during the mine design and sequencing of the Reserves

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Criteria	Commentary
	• All OP resource models have been converted to regularised block model where required to enable the use of OP optimisation software. • UG resource models have been developed for UG mine planning and have been used during the reserve process.

	Dilution
	• For Open Pit Reserves a dilution factor of 10% was used
	• For Underground Reserves both paste dilution (for mines where stoping with paste exposures) and waste dilution (to represent expected blast overbreak on stope shapes) have been used. These have been derived from stope reconciliation data for each of the Underground mines. The following dilution factors were used in the Underground Reserve calculations:
	  • RHP: Dilution = 15% to 21%, Paste Dilution = 2% to 9% (based on ore zones)
	  • Raleigh: Dilution = 23% to 33% (based on relative level), Paste Dilution = 4%
	• All dilution is considered as zero grade

	Mining Recovery • A mining recovery factor of 95% was used for all OP reserve calculations. • For underground mines the mining recovery factors were derived from stope reconciliations for each of the deposits and modified where required to reflect mining, the following factors have been used for UG mines • RHP = 70% to 85% based on ore zone and mining method • Raleigh = 96%
	Minimum Mining Width • The minimum mining widths for the Open Pit Reserves were defined by the planned mining fleet and vary between 2.5 to 10m. The block model was regularised to a defined SMU based on the Resource. • UG minimum mining widths reflect the narrow ore zones targeted with 2.5m to 3m used for all stope optimisation depending on the deposit
	Material Classification for inclusion • Inferred material outside of the main ore zone is treated as waste while small amounts of Inferred material within the ore zone may be included in the Design Pit (this accounts for less than 1% of the total Reserve) • All optimised stope shapes are tested for resource classification and any stopes containing more than 49% of Inferred material were removed from the reserve along with any associated development. All development with greater than 49% Inferred material is treated as waste.
	Capital Costs and Infrastructure • Both RHP and Raleigh have the required infrastructure to ensure ongoing operations and where necessary capital has been included for any extensions to existing infrastructure, including, access/materials handling/services (power, water management and vent)/safety systems and emergency egress) • Capital required to bring the pit reserves “on-line” as per the defined project work have been used during the reserves process.
Metallurgical factors or assumptions	• All ore deposits included in the MGO CY2022 Ore Reserves are conventional free-milling ores which are amenable to processing through a carbon-in-leach (CIL) gold processing plant. • All reserves declared in this statement are assumed to be treated at the Mungari Process Plant (commissioned 2014) • All assets mined after the commissioning date for the Mungari Plant expansion (schedule for Jan 2026 in the assumptions for the Ore Reserve) are assumed to be treated at the expanded process plant (with lower unit costs, higher throughputs, and changed metallurgical recoveries). • The following metallurgical recoveries have been used in the development of the Ore Reserve estimates:

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Criteria	Commentary
	○ RHP = 93.5% ○ Raleigh = 93.5% ○ New project open pits = between 91% to 94% (dependent on completed asset metallurgical test work)
	• Mungari Gold Process Plant is a conventional CIL process plant with inline gravity circuit and is a well-tested technology for free-milling type ores.
	• Current mining operations confirm the amenability of these ore zones with varying degrees of metallurgical test work completed for each of the projects included in the reserves.
	• All current operations have proven metallurgical characteristics shown by the consistent recoveries through the process plant. • Project work conducted by both Evolution and Northern Star have been used to confirm the ore from other projects will be amenable to this process.
	• No evidence of deleterious elements in any ores within the reserves.
	• No bulk sampling has been conducted through the Mungari Mill outside of normal operating process.
Environmental	• Current mining operations are fully compliant with legal and regulatory requirements with all government permits and licenses and statutory approvals granted. • Legal and regulatory commitments for other reserve projects are well understood and a schedule for applications and future work is currently in place
Infrastructure	• Current operations are well serviced by the required service infrastructure as follows: ○ Mungari Gold Process plant and office complex services the administration while individual office/workshop/magazine etc. complexes are available for operational purposes. ○ Current Life of Mine (LOM) planning includes the expansion of the current Mungari Mill from ~2 mtpa to 4.2 mtpa from January 2026 with final approval for the Expansion being sought in H2 FY2023 ○ Mine is connected to the main highway between Kalgoorlie and Coolgardie ○ Current operations are connected to grid power with the Kundana Diesel Power Station providing back up power as required. ○ Water supplied and discharge reticulation is in place. ○ Kalgoorlie is a major regional centre for supplies and labour while the airport connects the area to Perth for FIFO of labour not based in Kalgoorlie. • Projects away from the current mining areas have been assessed for infrastructure requirements and capital and been included in the project evaluation for: ○ Site set-up ○ Haul Roads ○ Water Supply & Dewatering ○ Communication, Offices & Ablutions ○ Workshops & Fuel Storage ○ Magazines etc.
Costs	• For operating mines current LOM capital forecast has been included where relevant. • For projects the project capital schedule has been reviewed and added to the financial evaluation.
	• Current first principal costings have been used to derive the operating costs for the Ore Reserve estimates. • Operating costs are based on current wages, materials, consumables and equipment prices, and LOM costs combined with actual or budget results for year-to-date CY22. • Costs are all expressed and calculated in Australian dollars.

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Criteria	Commentary
	• No cost impact is expected from deleterious elements and no costs have been included in the Ore Reserve estimate for these. • All State Government and third-party royalties are built into the cost model
Revenue factors	• All financial assumptions are in Australian dollars. • A gold price of A$2,200 per ounce has been used to generate revenue for the reported Ore Reserve estimate. Evolution uses an internal gold price assumption of A$2,400 per ounce for Life of Mine (LOM) planning. • This gold price is assumed to be constant for the mine plan associated with the Ore Reserve estimate. • Sensitivity is conducted at a range of different gold prices (A$1,600, A$1,900, and A$2,200/oz)
Market assessment	• All product is sold direct to refinery at spot market prices
	• A customer and competitor analysis were deemed unnecessary
Economic	• Financial modelling has been completed using reconciled cost models as previously described with outlined revenue factors. With significant historical precedent the confidence of the forecast economic outcomes is high • The Ore Reserve has been evaluated using a financial model, with sensitivity to internal and external factors being included in the evaluation.
Social	• Evolution's Mungari Gold Operations operate in the Goldfields region of Western Australia, which is a well-established, supportive jurisdiction for mineral operations from both a statutory and community perspective. There are no outstanding material stakeholder agreements required. • The practicalities of the Aboriginal Cultural Heritage Act 2021 are still being developed. Cultural heritage could be considered as a material risk to the Ore Reserve estimations for projects that are not yet in production. • The Sustainability Manager liaises regularly with Native Title claimant groups to inform and strategise a plan to conduct heritage surveys where required to assess for areas of cultural significance. These are either approved by claimant groups to proceed, or a cultural heritage management plan negotiated between the parties is developed to allow mining to commence in a sustainable manner protecting any sites of significance to the traditional owners. • In the opinion of the Competent Person there is no known grounds that additional required Cultural Heritage approvals will not be granted in the timeframes used for the schedule
Other	• No major issues have been identified that will materially affect the estimation or classification of the Ore Reserves
	• No material risks with the potential to prevent the commencement and operation of any projects in the Ore Reserve have been identified.
	• No outstanding legal issues exist that could compromise the Ore Reserve.
	• All mining tenements and government approvals are in place for current mining operations while project schedules exist for applications and approvals required for exiting projects. • In the opinion of the Competent Person there is no reasonable grounds that statutory approvals will not be granted in the timeframes used for the schedule

Classification	• Only Measured and Indicated Resources have been included in the Ore Reserves estimation (expect for secondary Inferred material as outlined for the Underground Ore Reserves) with:
	  ○ Measured converting into Proven Reserves and
	  ○ Indicated converting to Probable Reserves
	• Stockpiles have been classified as Probable Reserves
	• It is the Competent Person's view that the classifications used for the Ore Reserves are appropriate

	• For the CY2022 Underground Ore Reserve estimates all stopes that contain less than 49% Measured Resource (and less than 49% Inferred Resource) are classified as Probable Reserves

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Criteria	Commentary
Audits or reviews	• Evolution Mining's corporate based Transformation and Effectiveness Department conduct in-house Ore Reserve peer review annually with periodic internal and external audits. The last external audit was completed by Cube Consulting Pty Ltd in 2022. All material actions were completed for the CY2022 Ore Reserve estimate. • The last internal audit was completed in 2022. All material actions were completed for the CY2022 Ore Reserve estimate
Discussion of relative accuracy/ confidence	• Established Mineral Resource and Ore Reserves processes developed at Mungari Operations, combined with a detailed peer review corporate process provide confidence in the generated December 31, 2022, Reserves.
	• Ore Reserves are generally developed on global estimates however some local estimates are used in current operational areas which are generally reflected as Measure Resources (or Proven Reserves).
	• Confidence in the reserves for operating mines is generally higher reflecting the greater amount of data available to develop modifying factors. Project estimations for modifying factors will be based on reduce data volumes.
	• Producing mines include reconciliation process which are used for the forward-looking forecasts and reserves.

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