

ANNEXURE C

Technical Assessment Report

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Mineral Assets of the Kudz Ze Kayah Project, Yukon, Canada

Technical Assessment Report

Prepared for

BMC MINERALS

BMC Minerals Limited

Date
7th November 2025

Report No.
R220.2025

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BMCITA01 (0591951)



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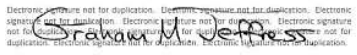
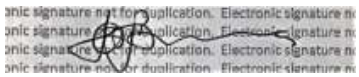
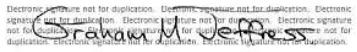
Cover Image: ABM deposit massive sulfide core on geological map of ABM area.

AUTHOR DETAILS AND SIGNATURE PAGE

Mineral Assets of the Kudz Ze Kayah Project, Yukon, Canada

Technical Assessment Report

BMCITA01 (0591951)

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This Report has been subject to multiple rounds of peer review and client fact checking. The Competent Person's have reviewed their content as part of their consent process, and an independent third party engaged by the client has also completed a peer review.

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EXECUTIVE SUMMARY

BMC Minerals Limited ("BMC" or the "Company") is engaged in the assessment, acquisition, and development of base metals projects with significant precious metal credits.

BMC through its various entities is the owner of the Kudz Ze Kayah Project (the "Project") in southeast Yukon, Canada. The Project is in the northern Pelly Mountains, 115 km south of Ross River in south-central Yukon.

The Project comprises eight separate tenure packages of contiguous mineral claims in the Finlayson district:

- The KZK Property (BMC 100%), covering the ABM Deposit (containing the ABM and Krakatoa Zones), and the GP4F Prospect. The KZK Property is the focus of a proposed mine development outlined in this report.
- The Pelly Property (BMC 100%), which is adjacent to the Wolverine Mine owned by Yukon Zinc Corp (Receivership discharged February 2024).
- The Kona Property (BMC 100%), which is centred on the Kona Deposit, comprising the Fyre Lake claims and the contiguous Tsa Da Glisza claims.
- The Wolf Property (BMC 100%), which is centred on the Wolf Deposit.
- The 1st BASE, MER, Rivier, and RB properties (BMC 100%), which comprise regional exploration tenure.

The most advanced asset is the ABM Mine Project on the KZK Property, which has been the subject of Feasibility Study-level investigations reported in 2025.

BMC's mineral claims currently cover approximately 372 km^2 surrounding the ABM, Kona (Fyre Lake) and Wolf volcanic-hosted massive sulfide (VHMS) deposits within the Finlayson Lake district.

This area is host to at least six known volcanogenic massive sulfide (VHMS) deposits that include the Kona, Kudz Ze Kayah, and GP4F deposits, owned by BMC; as well as the Wolverine, Ice and R15 deposits that are not owned by BMC.

BMC acquired the Kudz Ze Kayah and Pelly Property in January 2015. BMC subsequently acquired the Wolf Property in 2016, the Tsa Da Glisza claims in 2018, the 1st BASE, MER and RB Properties in 2020, the Fyre Lake claims in 2023, and the Rivier Property in 2024.

BMC regards these additional claims and prospects with known mineralisation as assets for potential future exploration.

Feasibility Studies to assess the economic viability of mining and processing the ABM Deposit have been completed and updated several times by BMC. The current Feasibility Study-level work, with key inputs having been reviewed and updated as required, is summarised in the Technical Report completed in accordance with NI 43-101 requirements with an Effective Date of 3rd January 2025 that was lodged on SEDAR on 3rd April 2025 (the "2025 Technical Report").

The Feasibility Study-level investigations, Mineral Resource Estimates and Mineral (Ore) Reserve Estimate in this Technical Report were completed in accordance with (Canadian Institute of Mining, Metallurgy and Petroleum) CIM Definition Standards for Mineral Resources and Mineral Reserves (CIM 2014). These Mineral Resource, Mineral Reserve, and mining study definitions are incorporated, by reference, into National Instrument 43-101 – *Standards of Disclosure for Mineral Projects* (NI 43-101). As a CRIRSCO family code, these definitions are equivalent to the JORC Code definitions.

The Mineral Resources and Mineral Reserves were generated in conformity with generally accepted CIM "Estimation of Mineral Resource and Mineral Reserves Best Practice Guidelines" (CIM Council, 2003) and CIM "Definition Standards for Mineral Resources and Mineral Reserves" (CIM Council, 2014).

The operating and capital cost estimates reported in the 2025 Technical Report are considered accurate to within the normal limits expected for a Feasibility Study as defined in the CIM Standards, and the costs (real terms) remain valid.



Figure 1-1: Kudz Ze Kayah Project location
Source: ERM

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Mining is proposed via both open pit and underground mining methods, with ore processed into separate copper, high precious metal (HPM), and zinc concentrates, via sequential flotation through a nominal 2.0 Mtpa processing plant. Tailings will be deposited in a dry stack tailings facility, while waste rock will be stored according to acid generating and metal leaching potential.

The ABM Mine Project is yet to be developed.

The proposed ABM mine has annual production targets of approximately 200 kt of dry zinc concentrate, 60 kt of dry copper concentrate, and 50 kt of dry HPM concentrate. Zinc and HPM concentrates will be transported to Canada's most northerly ice-free port, the Port of Stewart, British Columbia (BC), for shipment to smelters, while provision has been made for copper concentrates to be transported to a potential rail head in British Columbia for subsequent loading and transportation on the Canadian rail network to domestic customers, if required.

The production targets and forecast financial information in this Report are underpinned solely by Probable Ore Reserves estimated for the ABM Mine, reported in accordance with the JORC Code, and are based on the material assumptions outlined in this Report and are subject to various risk factors, such as those outlined in this Report and elsewhere in the Prospectus.

No Inferred Mineral Resources have been included in the Ore Reserves nor in production targets in this Report. Inferred Mineral Resources have not been included when determining the forecast financial information detailed in this Report.

In ERM's professional opinion, the project feasibility, as demonstrated by the 2025 Technical Report summary of the Feasibility Study-level investigations and all the underlying technical work completed on the project, constitute a reasonable basis to support the production targets and forecast financial metrics reported in this Report, and that BMC has reasonable grounds for expecting that the requisite additional funding can be raised, based on the Ore Reserves defined at the Project, and the level of confidence for various inputs to that Ore Reserve.

ERM notes that the work completed in the Feasibility Study-level investigations, and the Mineral Resources and Mineral Reserves were completed to the required standards to be reportable under either the JORC Code or NI 43-101 (CIM Standards), and the outputs are equivalent. The Mineral Resource estimate and Mineral Reserve estimate summarised in the 2025 Technical Report and presented in this Technical Assessment Report are equivalent and are reported in accordance with the JORC Code.

Geology and Mineral Resource Estimates

The KZK Property contains the ABM Deposit (the subject of the feasibility studies and current permitting processes), a polymetallic VHMS deposit containing economic concentrations of copper, lead, zinc, gold, and silver.

The ABM Deposit comprises the ABM and Krakatoa Zones, separated by faulting. Massive sulfides in the ABM Zone are up to 39 m thick, extending ≈700 m along strike and ≈500 m down dip. It dips to the north-northeast at ≈35° near surface, transitioning to a dip of ≈15° at around 200 m below the valley floor. The up-dip extent of the deposit is truncated by erosion and covered by ≈2–20 m of overburden.

Massive sulfide mineralisation in the Krakatoa Zone is fault-bounded to both the east and west, is covered by 20–30 m of overburden, and dips at ≈35° to the north-northeast. The massive sulfides are up to 22 m thick, extending over ≈200 m of strike and over at least 500 m down dip. The zone remains open at depth.

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BMC commissioned several independent Mineral Resource Estimates (MRE) for the ABM and Kona Deposits during the period 2016 to 2019 using historical datasets and, in the case of the ABM Deposit, extensive core drilling completed by BMC.

The MRE for the ABM Deposit was updated in 2024 with a review of reasonable prospects for eventual economic extraction, and released as part of the 2025 Technical Report with an effective date of 3rd January 2025, and the MRE for the Kona Deposit was updated in 2025, with a review of the reasonable prospects for eventual economic extraction, with an effective date of 30th June 2025.

These re-assessments were undertaken to provide an up-to-date demonstration of reasonable prospects for eventual economic extraction (RPEEE) given changes in costs, metal prices, and exchange rates since the last estimates were completed.

The ABM Mineral Resource has been reported above net smelter return (NSR) cut-offs of US$40/t (C$53/t) for "shallow" mineralisation and above US$150/t (C$200/t) for "deep" mineralisation based on the results of new RPEEE assessment in mid-2024 that was reported in the 2025 Technical Report.

Table 1-1: ABM Deposit Mineral Resource Estimate

Zone	Category	Tonnes (Mt)	Cu (%)	Pb (%)	Zn (%)	Au (g/t)	Ag (g/t)	Cu (kt)	Pb (kt)	Zn (kt)	Au (koz)	Ag (Moz)
ABM (shallow)	Indicated	14.6	1.0	1.6	6.1	1.3	132	141	229	887	614	62
	Inferred	0.3	1.5	1.6	4.5	1.1	117	5	5	14	11	1
Krakatoa (shallow)	Indicated	3.5	0.6	3.2	7.2	1.8	213	21	113	256	204	24
	Inferred	0.1	0.6	2.3	6.3	1.3	143	0.1	2	6	4	0.4
Krakatoa (deep)	Indicated	0.2	1.0	2.1	6.1	1.7	173	2	3	11	9	1
	Inferred	0.4	0.8	1.6	9.4	1.2	165	3	6	38	15	2
Total	Indicated	18.3	0.9	1.9	6.3	1.4	148	164	346	1,153	827	87
	Inferred	0.8	1.0	1.7	7.2	1.2	143	8	13	58	30	4
Grand Total	**Ind & Inf**	**19.1**	**0.9**	**1.9**	**6.3**	**1.4**	**148**	**172**	**359**	**1,211**	**857**	**91**

- BMC's interest in the ABM Deposit is 100%.
- The Mineral Resources are reported in accordance with the JORC Code by Aaron Green, Competent Person, FAIG.
- The Effective Date of this MRE is 3rd January 2025.
- Numbers have been rounded to reflect the precision of an Indicated and Inferred MRE (noting that MRE are, by nature, approximate, and with a degree of uncertainty).
- The ABM Deposit Mineral Resources are inclusive of the Probable Ore Reserves.
- Shallow Zone cut-off at NSR cut-off grade of US$40/t.
- Deep Zone cut-off at NSR cut-off grade of US$150/t.
- NSR formula: NSR US$/t =((69.17*Cu_cut) + (6.85*Pb_cut) + (19.53*Zn_cut) + (30.13*Au_cut) + (0.49*Ag_cut)).
- An exchange rate of 0.75 CAD:USD.
- The optimal transition from open pit to underground has not been considered when reporting the Mineral Resource. Key Modifying Factors in determining this transition have been factored into reporting of the Ore Reserve.

ERM is of the opinion the drilling, surveying, sampling and analytical methods, and quality assurance processes implemented by BMC during the exploration and resource drilling campaigns are suitable, adequate and reasonable for the style of deposit under consideration in this Report.

ERM further believes that ordinary kriging is an appropriate grade interpolation mechanism for the ABM Deposit given the current level of project development and available data. The Kriging

Neighbourhood Analysis undertaken confirmed that reliable block estimates were achieved to enable the resources to be classified as Indicated and Inferred Mineral Resources.

Geological interpretation is considered by ERM to be a risk factor where the revision of mineralisation models, modelling of internal waste domains, modelling of dykes and structural offsets such as faults and shear zones must be completed as new data and geological understanding is obtained.

ERM further suggests that infill drilling is required to define the mineralisation and improve the level of confidence in the current Mineral Resource classification.

Based on the results of the feasibility studies as summarised in the 2025 Technical Report, the ABM Deposit is of sufficient grade, quantity, and continuity to have reasonable prospects for eventual economic extraction.

ERM notes that although past work on the ABM Deposit has been reported according to NI 43-101 and CIM standards, the underlying work is of a high standard, and equivalence of between CIM and JORC Code allows reporting of the Mineral Resource estimate under either code with confidence.

The Kona Deposit MRE is reported in Table 1-2. A total of 114 core drill holes (22,700 m) define the Kona Deposit, and 73 assayed drill holes intersect the interpreted mineralisation zones with holes spaced 25–200 m apart along a 1,500 m plunge extent.

Table 1-2: Kona Deposit Mineral Resource Estimate

Classification	Tonnes (Mt)	Cu (%)	Au (g/t)	Ag (g/t)	Cu (kt)	Au (koz)	Ag (koz)
Indicated	2.1	1.6	0.8	4	33	53	294
Inferred	6.7	1.7	0.6	4	117	138	762
Total	**8.8**	**1.7**	**0.7**	**4**	**150**	**191**	**1,056**

Notes:

- BMC's interest in the Kona Deposit is 100% through its wholly owned subsidiary, Finlayson Copper Ltd.
- Mineral Resources are reported in accordance with the JORC Code by Aaron Green, Competent Person, FAIG.
- The Effective Date of this MRE is 30th June 2025.
- Numbers have been rounded to reflect the precision of an Indicated and Inferred MRE (noting that MRE are, by nature, approximate, and with a degree of uncertainty).
- The Kona MRE has been reported above an NSR cut-off of C$113/t.
- Silver was concluded not to be economic and thus is not included in the NSR calculation.
- NSR formula: NSR US$/t =((68.31*Cu_cut) + (60.26*Au_cut)).
- An exchange rate of 0.75 CAD:USD.
- Preliminary underground optimisation studies support the reporting of the Mineral Resource above the C$113/t cut-off particularly as a satellite mining operation to a central processing facility at the Kudz Ze Kayah Project.
- The Kona MRE is not included in the feasibility studies completed since 2015.

ERM is of the opinion that the historical 1996 and 1997 exploration and resource drilling data (validated by BMC), including drill hole spacing, surveying, sampling and analytical methods, and quality assurance processes, was suitable, adequate, and reasonable for the style of deposit under consideration in this Report. The Kona Deposit remains open, and infill and extension drilling are required to fully define the mineralisation extents and improve the level of confidence in the current Mineral Resource classification

Exploration Potential

The Kudz Ze Kayah Project contains economically significant polymetallic VHMS deposits, with additional prospects and deposits located in the surrounding district. The VHMS deposits that have been identified to date either outcrop or lie under relatively thin surficial cover.

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The district is relatively under-explored in terms of effective modern exploration coverage. There are deficiencies with historical selections of geochemical sample media, QA/QC, and high analytical detection limits for the past geochemical work (in particular, the regional soil geochemistry). There is also a lack of good resolution geophysical coverage in the district (CSA Global 2017b,c).

ERM considers the Project holds considerable potential for the discovery of further VHMS deposits and extensions to known mineralisation based on the prospective geological setting and the available of improved exploration methods and improved scientific understanding of the controls on VHMS mineralisation.

To quantify the potential, BMC has completed considerable surface exploration (comprising mapping, soil and rock chip sampling, aeromagnetics, airborne electromagnetics (EM), and petrology), supported by historical drilling to estimate Exploration Targets for the GP4F Prospect (Table 1-3), the Kona (Table 1-4) and Wolf (Table 1-5) Deposits, and the Jackman Prospect (Table 1-6). All Exploration Targets are separate from any Mineral Resource estimates.

Table 1-3: GP4F Exploration Target

Tonnes Lower Mt	Tonnes Higher Mt	Cu Lower %	Cu Higher %	Pb Lower %	Pb Higher %	Zn Lower %	Zn Higher %	Au Lower g/t	Au Higher g/t	Ag Lower g/t	Ag Higher g/t
1.7	2.6	0.18	0.24	2.3	3.1	4.8	6.4	1.3	1.7	66	88

Table 1-4: Kona Exploration Target

Tonnes Lower Mt	Tonnes Higher Mt	Cu Lower %	Cu Higher %	Au Lower g/t	Au Higher g/t	Ag Lower g/t	Ag Higher g/t
3.0	5.0	1.5	1.8	0.5	0.8	3	5

Table 1-5: Wolf Exploration Target

Tonnes Lower Mt	Tonnes Higher Mt	Zn Lower %	Zn Higher %	Pb Lower g/t	Pb Higher g/t	Ag Lower g/t	Ag Higher g/t
2.7	3.3	4.4	5.4	1.3	1.5	38	46

Table 1-6: Jackman Exploration Target

Tonnes Lower Mt	Tonnes Higher Mt	Zn Lower %	Zn Higher %	Cu Lower %	Cu Higher %	Pb Lower g/t	Pb Higher g/t	Au Higher g/t	Au Lower g/t	Ag Lower g/t	Ag Higher g/t
2.5	5.0	10.0	12.0	1.0	1.2	1.3	1.6	1.4	1.7	240	360

The potential quantity and grade ranges of the Kudz Ze Kayah Project Exploration Targets are conceptual in nature. There has been insufficient exploration to estimate a Mineral Resource, and it is uncertain whether future exploration will result in an estimation of a Mineral Resource.

Testwork and studies on "Modifying Factors", such as metallurgy, to determine whether additional mineralisation may have potential feasibility.

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BMC proposes the following actions to advance the exploration of the Kudz Ze Kayah, Kona, Wolf, and Pelly Properties:

- Core drilling to follow-up previous significant intersections at existing prospects, including ABM Down Plunge, the Kuril, Fuego, GP4F and Rhyolite Peak prospects, Kona extensions, and Wolverine extensions (Jackman)[1].
- Implement geophysical surveys (EM, IP, and magnetics) over prospective formations with coincident geochemical anomalies and/or geological attributes. Follow with core drill testing of geophysically-defined targets.
- Detailed structural and geochemical analysis to understand the timing of mineralisation, stratigraphy, and geological controls. Improved understanding of the deposit controls will aid in more regional exploration efforts across the Project.
- Implement broad-based geological mapping, geochemical sampling, and geophysical surveys over the remainder of the Project tenure to target subtle signs of VHMS mineralisation.

BMC proposes to undertake these activities over the next 2–3 years.

Mining, Feasibility Study-level investigations, and Ore Reserve Estimates

A Feasibility Study to assess the economic viability of mining and processing the ABM Deposit has been completed and updated several times. The most recent Feasibility Study-level investigations, with key metrics having been recently reviewed and updated, is summarised in a NI 43-101 report with an Effective Date of 3rd January 2025 and lodged on SEDAR on 3rd April 2025 (the "2025 Technical Report").

ERM notes that whilst the Feasibility Study-level investigations, Mineral Resource Estimate and Mineral (Ore) Reserve Estimate were completed in accordance with Canadian Institute of Mining, Metallurgy and Petroleum Standards (CIM 2014), and reported in accordance with NI 43-101, the Canadian standards are functionally equivalent to Australian JORC Code standards and definitions, and as such are able to be reported in accordance with the JORC Code in this report.

Extraction of the ABM Deposit is planned by open pit (89% of ore) and underground (11% of ore) mining methods.

Four separate phases of open pit mining are proposed for the ABM Zone to manage overall waste stripping requirements, while the adjoining Krakatoa Zone will be mined as a single phase.

The underground operations will start in Year 3, extracting the lower Krakatoa Zone. An in-pit portal will be developed once the ABM open pit is deep enough. The underground mining of the Krakatoa Zone beneath the open pit will be predominantly via longhole open stoping with paste fill securing the voids produced.

Approximately 14.0 Mt of ore will be mined from the open pit and 1.7 Mt of ore from underground.

138.4 Mt of waste will be mined by open pit mining methods, for an expected average life-of-mine (LOM) strip ratio of 9.9:1. The initial ABM Zone pit has an expected strip ratio of 6:1, to optimise payback of pre-production capital.

Waste material mined from the open pit and underground would be stored permanently on surface. Wherever possible suitable waste material will be used for the infrastructure construction.

[1] Note that the drilling at Kona and Jackman is likely to occur after the 2-year post-IPO period envisaged in the Use of Funds.

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Open pit mining will take approximately nine years, including pre-production mining requirements.

All Ore Reserves are classified as Probable Ore Reserves, since no Measured Mineral Resources were declared for the ABM Deposit.

The Ore Reserve includes external dilution that will be mined in conjunction with the Ore Reserve shapes and delivered to the process plant.

No Inferred Mineral Resources are included in the Ore Reserve estimate.

The Ore Reserve estimate includes material extracted from open pit and underground and is sourced from Indicated Mineral Resources only where the block value is greater than the NSR cut-off for the relevant mining method.

An Ore Reserve estimate was prepared for the ABM Deposit (for mining both the ABM Zone and the Krakatoa Zone) following the completion of the original 2019 Feasibility Study. The Feasibility Study was updated and re-stated in 2020 with revised financial estimates. The Ore Reserve estimate was subsequently re-reported in the 2025 Technical Report using June 2023 quarter economic data. The metal prices used (Table 1-8) in the revised economic modelling were higher than those of the 2020 Re-stated Feasibility Study.

The Ore Reserve estimate was formally reviewed under the revised metal price and exchange rate scenarios and no adjustments to the calculated Ore Reserve estimate were considered necessary. The modelling considered all capital, operating, and realisation costs as outlined in the 2025 Technical Report.

The 2019 ore schedule was evaluated using the economic parameters from the June 2023 quarter estimates. This showed a substantial positive economic outcome, demonstrating that the updated commodity prices and exchange rates offset the escalation in and changes to the project operating costs.

In the 2025 Technical Report, using the June 2023 quarter cost estimates (NB. these costs are still considered valid), the Ore Reserve estimate remains unchanged, with the Ore Reserve estimate reported in accordance with the JORC Code (Table 1-7).

Table 1-7: ABM Deposit (ABM and Krakatoa Zones) Ore Reserve Estimate

Mine	Category	Tonnes (Mt)	Cu (%)	Pb (%)	Zn (%)	Au (g/t)	Ag (g/t)	Cu (kt)	Pb (kt)	Zn (kt)	Au (koz)	Ag (Moz)
Open pit	Probable	14.0	0.9	1.6	5.9	1.3	136	128	226	828	596	61
Underground	Probable	1.7	0.4	2.3	5.0	1.3	147	7	40	87	70	8
Total	**Probable**	**15.7**	**0.9**	**1.7**	**5.8**	**1.3**	**138**	**136**	**266**	**915**	**666**	**70**

Notes:

- BMC's interest in the ABM Deposit is 100%.
- Ore Reserves in this report are reported in accordance with the JORC Code by Karl van Olden as Competent Person.
- The effective date of this Ore Reserve is 30th October 2023.
- Numbers have been rounded to reflect the precision of the estimates.
- Open pit Ore Reserves are reported within a practical design for an open pit using an NSR cut-off.
- Practical open pit designs were informed by economic mining envelopes determined using Whittle pit optimisation software.
- Overall slope angles for the designed open pit range from 27° to 47°.
- Underground Ore Reserves are based on an underhand longhole stoping with cemented paste fill mining method and reported to a NSR cut-off.
- Ore Reserves incorporate estimates of mining dilution and mining recovery.
- Processing recoveries have been calculated for each of the defined metallurgical domains. Average processing recoveries are 73.8% for copper, 73.5% for lead, 85.9% for zinc, 64.9% for gold and 86.0% for silver.
- NSR calculations represent the net revenue to Mine Gate after accounting for concentrate treatment and refining charges, concentrate penalties, concentrate transport costs, government royalties, and payments to First Nations.

In ERM's opinion the operating and capital cost estimates informing the Ore Reserve estimate are considered accurate to within the normal limits expected for a Feasibility Study as defined in the JORC Code, and the costs remain valid.

Table 1-8: Consensus Metal Prices and Exchange Rate (June 2023 quarter, 2025 Technical Report)

Parameter	Unit	2023	2024	2025	2026	2027 / Long-term
Zinc	US$/lb Zn	1.21	1.21	1.23	1.24	1.20
Silver	US$/lb Ag	23.55	23.75	23.61	23.36	22.60
Copper	US$/lb Cu	3.90	3.91	4.13	4.27	3.80
Gold	US$/oz Au	1,922	1,915	1,853	1,808	1,700
Lead	US$/lb Pb	0.95	0.94	0.93	0.94	0.95
Exchange Rate	USD:CAD	1.342	1.327	1.320	1.315	1.297

Source: 2025 Technical Report

Metallurgy and Processing

The ABM Mine concentrator (processing plant) and associated service facilities are designed to process run-of-mine (ROM) ore at an average rate of 2.0 Mtpa to produce separate copper, high precious metals (HPM), and zinc concentrates, as well as tailings; with both the copper and HPM concentrates having high levels of gold and silver credits.

The processing plant is initially planned to operate for about nine years and is expected to produce around 200 kt zinc, 60 kt copper, and 50 kt of HPM concentrates annually. Concentrates will be transported by road to port for sale to market.

BMC has executed concentrate offtake agreements with buyers for all of the copper and HPM concentrate and 95% of the zinc concentrate produced during the first five years of operations.

Concentrate treatment and refining charges are based on the various offtake agreements that have been executed by BMC. Concentrate treatment charges in all of the offtake agreements are referenced to benchmark treatment charges, with BMC's concentrate marketing consultant advising that appropriate long term benchmark treatment charges are US$85/dmt, US$180/dmt and US$217/dmt for copper, HPM and zinc concentrates, respectively.

Several changes to project infrastructure were introduced from the execution of several concentrate offtake agreements:

- minor modifications to the zinc concentrate thickening circuit have been adopted to allow for the optional flexibility of production of different qualities of zinc concentrate (prefloat and recleaner concentrates) if the market provides the opportunity and if the Company so desires;
- allowing for the costs of creating future optionality for delivery of copper concentrate to a rail head, for transport to domestic customers if required; and
- corresponding right sizing of the bulk concentrate storage shed at Stewart World Port to reflect current (more accurate) scheduling and shipping expectations through the facility.

A large volume of metallurgical testwork has been undertaken on the ABM Deposit, initially by Cominco in the 1990s, then by ALS Metallurgy (in Perth and Adelaide, Australia, for BMC's Pre-Feasibility Study (PFS) and subsequent feasibility studies.

Five metallurgical domains based on texture and mineralogy have been defined for the ABM Deposit. The metallurgical testwork programme investigated comminution and flotation performance for all five domains using domain composite samples together with five variability samples for each domain.

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Variability samples were primarily selected to assess variability in flotation performance over a range of head grades within each metallurgical domain.

Comminution properties established from testwork for design purposes indicate that the mineralisation can be considered "soft" in terms of the impact breakage parameter and of medium hardness in terms of Bond Ball Mill Work Index.

Flotation testwork data was used to derive relationships for the recovery of economic metals and deleterious elements into concentrates for each domain and the LOM recoveries determined for the 2025 Technical Report are summarised in Table 1-9. Concentrate grades are predicted to be 25.0% copper, 52.0% lead and 52.0% zinc for the copper, HPM, and zinc concentrates, respectively.

Table 1-9: LOM Processing Recoveries of Revenue Elements

Concentrate	Copper (%)	Lead (%)	Zinc (%)	Gold (%)	Silver (%)
Copper	73.8	n/a	n/a	27.3	36.8
HPM	n/a	73.5	n/a	29.4	38.2
Zinc	n/a	n/a	85.9	8.1	11.0

Source: 2025 Technical Report

Settling and filtration testwork was completed and pressure filtration has been selected for the dewatering of all concentrates and tailings.

The processing plant and associated facilities have been designed to process mine production at an average rate of 2.0 Mtpa to produce separate copper, HPM, and zinc concentrates. The plant will be capable of processing at a higher throughput rate of 270 tph and this allows the process rate to be varied depending on the grade of the ore presented to the plant.

A sequential flotation circuit is planned to recover copper, lead, and zinc, in that order. Each of the three flotation stages includes a pre-float circuit as part of the rougher cells. A three-stage cleaning circuit will be used for copper and zinc flotation, while the lead circuit will operate two-stage cleaning. All three circuits include regrinding to a P_{80} of 30 µm, 30 µm and 35 µm for copper, lead, and zinc, respectively.

The total process flowsheet consists of following key stages:

- Primary crushing using a jaw crusher to produce a crushed product size of nominally 80% passing (P_{80}) 130 mm.
- Stacking of ore onto a conical, covered stockpile with a nominal 12-hour live capacity.
- Semi-autogenous grinding ("SAG") mill/ball mill configuration comminution circuit including open circuit SAG mill and closed-circuit ball mill grinding with potential for recycle of some of the cyclone underflow to the SAG mill, to produce a P_{80} grind size of 70 µm.
- Sequential flotation of copper, lead, and zinc using conventional pre-float, rougher, and cleaner flotation cells. Regrinding of copper, lead, and zinc rougher concentrate with fine grinding mills.
- Thickening, filtration, and stockpiling on site of copper, HPM, and zinc flotation concentrates.
- Copper and zinc concentrates will be loaded in bulk onto trucks for transport off site, while HPM concentrate will be loaded into sealable containers before transport by truck off site.
- Dewatering of flotation tailings by thickening and pressure filtration with the residual filter cake either transported to the dry stack tailings storage facility or combined with cement to produce underground paste backfill.
- Transportation of filtered flotation tailings to the Class A Waste Storage Facility for disposal.

The expected LOM saleable concentrates details are provided in Table 1-10.

Table 1-10: LOM metallurgical recoveries and concentrate grades

	Cu (%)	Pb (%)	Zn (%)	Au (g/t)	Ag (g/t)
Cu Con. grade	25.0			14.1	1,984
Pb Con. grade		51.8		16.2	2,190
Zn con. Grade			51.9	1.1	157
% Recovery	73.8	73.5	85.9	64.9	86.0

Source: 2025 Technical Report

A minor modification to the zinc concentrate thickening circuit has been adopted to allow production of two different qualities of zinc concentrate (pre-float and recleaner concentrates).

No changes were required nor have been made to the underlying engineering designs and project schedules from earlier iterations of the Feasibility Study since the flotation circuit has always included a pre-float stage for all three concentrates to recover the faster floating minerals prior to passing through to classification and concentrate regrind.

These pre-float concentrates have typically had a cleaner quality than those produced from the subsequent classification and regrind part of the circuit, by having higher base metal grades, lower precious metals grades, and lower concentrations of impurities. The flowsheet combines the pre-float and recleaner concentrate streams before feeding into the concentrate thickeners for thickening and subsequent filtration.

Minimal additional infrastructure is required to produce separate concentrate qualities and a second smaller thickener and associated pumping infrastructure only will be required. A second filter feed stock tank is required to produce separate copper and HPM pre-float and recleaner concentrates, while the zinc circuit already has two filter feed stock tanks available. Sufficient filtration capacity and stockpiling of filtered concentrates is available.

Certain offtake parties elected to take up separate pre-float and recleaner zinc concentrates given the difference in concentrate qualities between pre-float, and recleaner concentrates while copper and HPM concentrates will each continue to be sold as single, combined concentrate products in line with buyer preferences.

Non-Process Infrastructure and Logistics

The Project is serviced by existing infrastructure that includes highways and airstrips. The towns of Watson Lake at 268 km from the Project site and Whitehorse (517 km) provide light industrial support, while Ross River (115 km) provides KZK camp supplies and hosts the local fuel depot. Labour is currently sourced from all these locations.

The Kudz Ze Kayah Project is currently accessed by an existing 24 km gated Tote Road that extends from the Robert Campbell Highway south to the Project site. The Highway provides part of the 905 km direct route to the Port of Stewart which has year-round access to deep water bulk export facilities.

Management of tailings, waste rock, and water has been an integral component of the design of the proposed mine. Tailings from ore processing are to be produced as a filtered tailing product that is designed to be deposited in a purpose designed facility on the western slope of the Geona valley. BMC believes that this method of tailings storage presents a better long-term solution than

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conventional wet tailings disposal, which would require construction of a permanent facility within Geona Creek. Waste rock is to be classified based on its potential to be acid generating and metal leaching, with Class A having strong potential for acid generation or metal leaching, Class B having weak potential for acid generation or metal leaching and Class C being potentially acid consuming. Tailings are also expected to be classified as Class A material and will be co-disposed with Class A waste rock. Class A and B storage facilities are designed to encapsulate the stored waste products to minimise contact with oxygen and water.

A low permeability seepage barrier comprising layers of glacial till, high-density polyethylene (HDPE) geomembrane and crushed sand and gravel is planned for construction at both the base and cover of the Class A and B storage facilities. Progressive reclamation is planned on both facilities to control the amount of material exposed to the environment. A buttress is also planned for construction for waste confinement at the downstream slope of the Class A Storage Facility. The Class C Storage Facility is not expected to require specific encapsulation methods and has been designed for long-term physical stability. Progressive reclamation will also be adopted for this facility.

Overburden comprising glacial till and glaciolacustrine sediments, and topsoil will both be stockpiled temporarily on surface for later reuse during reclamation of the site.

All Project infrastructure has been designed to be contained within a single catchment to minimise effects on the broader environment.

The Feasibility Study-level investigations provides the framework for a comprehensive approach to water management, addressing water management objectives for construction, operations, decommissioning, and post closure. The water management plan involves collecting and managing site runoff from disturbed areas and maximising the recycling of process water.

A water treatment plant (WTP) will be constructed to treat water to meet site discharge quality requirements. As the WTP treats several different water source streams with variable chemistry, the system is designed to keep the different sources of water segregated. By doing this, treatment can be applied selectively and allow for staged deployment of the treatment system.

Reuse of water within the mining and processing facilities has also been planned to limit the amount of raw water required for project operations and therefore limit water requiring treatment prior to discharge from site.

The Company has studied the surface water and the groundwater environments since 2015, building on nearly 20 years of data collection by the previous owner.

The water management will be designed to limit the impacts of mining on the natural environment throughout all stages of development and enable the reclamation of Geona Creek to a fully functioning aquatic and biophysical environment.

The existing 24 km Tote Road will be upgraded to an all-weather, single-lane road with sufficient passing bays to safely facilitate two-way traffic. The Tote Road will be the main access to the site for all traffic including personnel transport, supply trucks, and concentrate transport trucks. In and around the site, approximately 25 km of roads will be either upgraded or constructed new to service the needs of the operation. This will include the construction of both light vehicle access roads and mine haul roads.

A permanent accommodation camp will be constructed adjacent to the existing exploration camp. Ninety-eight rooms of the permanent camp are installed on site with 60 of these fully integrated into the site services. The remaining rooms will be integrated into the camp services during 2026 and 2027 on an as-needed basis.

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The camp will ultimately be expanded to 348 dormitory rooms, including temporary double-bunks to cater for the peak construction phase. The existing Finlayson airstrip is located approximately 40 km from the site and will be the main facility used to fly all project personnel to and from Whitehorse. It is a gravel strip capable of handling up to 14-seat capacity aircraft. Project personnel will be bussed between the site and airstrip.

Power is planned to be generated onsite by five dual fuel (diesel/natural gas) generators that allow the fuel mix to be varied to take advantage of differences in fuel prices and availability. Installed power generation capacity is designed for 27.5 MW, with up to four of the five generators expected to be in operation at one time. Full heat recovery from the generators has been planned to provide heat to the process plant facilities during winter. The incorporation of this system is designed to minimise greenhouse gas emissions from this facility

Zinc and HPM concentrates will be hauled to the Port of Stewart along a 905 km southerly route utilising a combination of gravel and sealed secondary highways and paved primary highways. Provision has been made for copper concentrate to be hauled to a potential rail head for subsequent loading and transportation on the Canadian rail network to domestic customers, if required.

The preferred port facility for export of the zinc and HPM concentrates is the Stewart World Port (SWP) at the Port of Stewart on the northwest coast of Canada, at the head of the Portland Waterway about 80 nautical miles from the open sea.

Concentrates from the mine will be stored at a purpose-built storage facility where zinc concentrates will be bulk stored until a ship arrives prior to being conveyor fed to a ship loader for vessel loading. HPM concentrate will be transported from site to SWP via purpose-built half height containers that will be stored in an outdoor hardstand area until vessel loading via a container rotating system and ships crane.

Project Economics

Detailed Feasibility-level studies were first completed on the Kudz Ze Kayah Project in 2019 and demonstrated a robust positive financial outcome. An updated economic assessment of the project was completed in November 2020 – and was solely a cost and revenue update to the Project, with engineering designs, and schedules remaining unchanged from that of the 2019 Feasibility Study.

In October 2023, a full economic update was completed to reflect a June 2023 quarter cost base to the past studies. This update of the Project economics was completed as the Project continued to advance through the regulatory phase of the licensing process and the Company commences preparations for financing the project development.

On 3rd April 2025, the Company published its latest NI 43-101 Technical Report on SEDAR with the effective date of 3rd January 2025. The NI 43-101 Technical Report included the Mineral Resource estimate (2024) and Ore Reserve estimate (2023) used as the basis for the financial metrics reported in the same document and supported by Feasibility Study-level investigations.

Physical aspects of the Project and supporting engineering work remained largely unchanged from that detailed in previous iterations of Feasibility Study work since the designs were to the requisite level of detail and confidence. Changes introduced predominantly resulted from the concentrate offtake agreements that BMC has executed with various offtake customers since 2021.

All capital and operating costs were reviewed and updated by the consultants that contributed to the Feasibility Study-level investigations and the Company reviewed and updated all other cost elements. Updates were achieved through a combination of updated quotations for equipment and

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consumables, consultant in-house cost databases, and escalation of the previous cost estimate to bring to a June 2023 quarter cost base.

All revenues and costs presented below are in United States dollars (USD, US$) and in real dollar terms unless otherwise noted. All costs discussed below are sourced from the 2025 Technical Report.

Capital Costs

An estimated US$492 million will be required in pre-production capital to bring the mine into production, while an additional US$200 million of sustaining capital will be required during operations and closure (Table 1-11). Total capital over the LOM has been estimated to be US$692 million.

The capital cost estimate is considered accurate to within the normal limits expected for a Feasibility Study (as defined by CIM and JORC Code) and the costs as reported in the 2025 Technical Report remain valid.

Table 1-11: LOM Capital Cost Summary

Capital Cost Area	Pre-production (US$M)	Sustaining (US$M)	Total (US$M)
Process plant	190	13	202
Open pit mine development and infrastructure	51	5	56
Underground mine	0	72	72
Non-process infrastructure	30	10	40
Waste storage facilities	20	35	55
Water storage and management facilities	17	11	28
Water treatment plant	21	4	25
Port and rail facilities	17	0	17
Other infrastructure	7	5	12
Subtotal Direct Costs	351	155	506
Closure	0	45	45
Total Direct Costs	351	200	552
Owner's costs	18	Incl	18
Indirect costs	67	Incl	67
Contingency	55	Incl	55
Total Capital Cost	**492**	**200**	**692**

- Source: 2025 Technical Report
- Costs are rounded to nearest $1M. Totals may not sum precisely.
- Costs exclude amounts for equipment assumed leased. Refer to Section 13.3.6 for more information.
- 100% equity financing assumed.
- Excludes project finance interest, offtake agreement financing, reclamation bonding, and other financing arrangements and costs, working capital, exchange rate fluctuations, and all licence fees.
- Mining of open pit waste is treated as an operating expense, except for pre-production mining activity which is capitalised as a pre-production expense.

The capital cost estimate is considered accurate to within the normal limits expected for a Feasibility Study and the June 2023 costs reported in the 2025 Technical Report remain valid. The inputs and assumptions of the Feasibility Study-level investigations reported in this Report (and the reports informing it) remain applicable and appropriate for the disclosed information

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Operating Costs

The estimated operating costs over the life of the Project are expected to be approximately US$2,679 million.

Over the LOM, unit operating costs are expected to be US$170/t of ore processed, with operating costs ranging between approximately US$144/t and US$195/t.

Table 1-12: LOM Operating Cost Summary, US$ million

Operating cost summary	LOM total (US$M)	Unit cost (US$/t processed)
Open Pit Mining	$528	$33.60
Underground Mining	$157	$10.00
Processing	$318	$22.20
Water Treatment	$20	$1.30
Site G&A	$164	$10.40
Equipment Leases	$72	$4.60
First Nations	$37	$2.40
Road Transport	$305	$19.40
Sea / Rail Transport and Loading Operations	$220	$14.00
Government Royalties	$218	$13.80
PM PA	$112	$7.10
Cone. Marketing (Offsite G&A)	$11	$0.70
TC/RC's& Penalties	$516	$32.80
Total	**$2,679**	**$170.40**

Source: June 2023 costs as per 2025 Technical Report

Base Case Parameters

Economic analysis of the project as presented in this Technical Assessment Report shows that the ABM Mine Project is commercially viable given the Base Case economic results, with key indicators shown in (Table 1-13) on a before-tax basis.

All metrics are derived using a 7% discount rate to remain consistent with that used in the 2020 Re-stated Feasibility Study.

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Table 1-13: Base Case Economic Results[2]

Parameter	USD
Before tax cashflow	$1,426M
Before tax NPV7	$835M
Before Tax IRR	42.1%
Payback period	2.2 years
EBITDA (LOM)	$2,090M
EBITDA (steady state[1] average per year)	$288.0M

Note:
1. Excludes Year 1 and final year of production.
Source: 2025 Technical Report

Unit Costs

Annual C1 and All-in Sustaining Costs (AISC) are shown below (Table 1-14) and as >75% of the net revenue for the project is generated from zinc, copper, and silver in concentrate, the C1 costs, and AISC have been prepared for all three metals for comparative purposes. All other metals are considered by-product credits in calculations.

Table 1-14: Annual C1 and All-In-Sustaining Unit Costs in $US[3]

Cost	Unit	LOM	Y1	Y2	Y3	Y4	Y5	Y6	Y7	Y8
Zinc C1 Unit Cost	US$/lb Zn	-0.44	-0.29	-0.35	-0.30	-0.63	-0.55	-0.18	-0.50	-0.90
Silver C1 Unit Cost	US$/oz Ag	-23.77	-17.28	-22.69	-25.57	-30.47	-26.92	-22.88	-23.14	-20.04
Copper C1 Unit Cost	US$/lb Cu	-7.52	-14.68	-9.38	-6.28	-2.95	-7.75	-7.88	-10.44	-9.87
Zinc AISC Unit Cost	US$/lb Zn	-0.12	-0.01	-0.12	0.07	-0.18	-0.14	0.05	-0.28	-0.51
Silver AISC Unit Cost	US$/oz Ag	-14.77	-9.73	-16.09	-13.62	-17.44	-15.21	-15.21	-17.36	-12.17
Copper AISC Unit Cost	US$/lb Cu	-5.32	-11.18	-7.45	-3.78	-1.29	-5.02	-5.91	-8.64	-7.34

Source: 2025 Technical Report
Note: each metal unit costs includes credits from the other metals

[2] Non-IFRS measures – defined in glossary.
[3] Non-IFRS measures – defined in glossary.

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The annual LOM cashflows for the Base Case are shown in Figure 1-2.

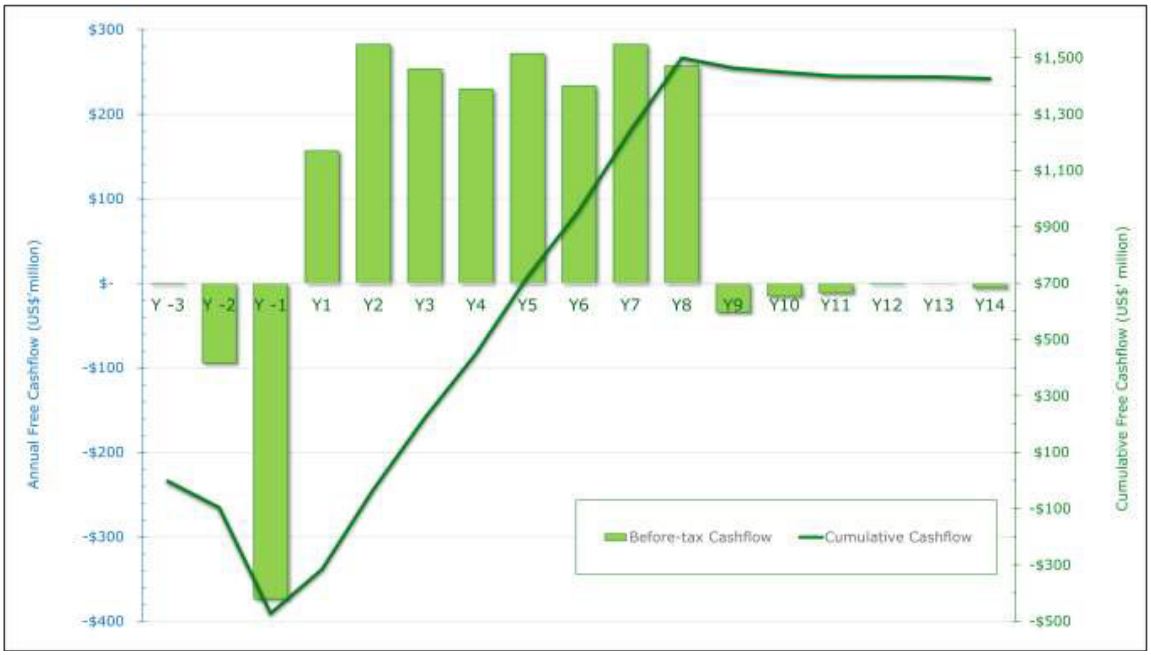


Figure 1-2: Base Cash Project Before-Tax Cashflow in US$ million

Several additional scenarios were modelled by BMC as variations from the Base Case where an Upside and Downside Case considered flexing of key revenue and cost inputs.

Sensitivities

The Project is most sensitive to changes in exchange rate, followed by discount rate, OpEx, metals prices and grades and then CapEx. The sensitivity of changes in key variables on the before-tax net present value (NPV) has been determined through a simple factoring of each element. The relative sensitivity of the before-tax NPV, for the most sensitive variables, is shown below (Figure 1-3).

Most variables were assessed on a standard ±10% proportional change while the remaining variables are percentage driven (e.g. metal recovery) and were assessed based on flexing the variable by ±2 units to better represent the expected variability range.

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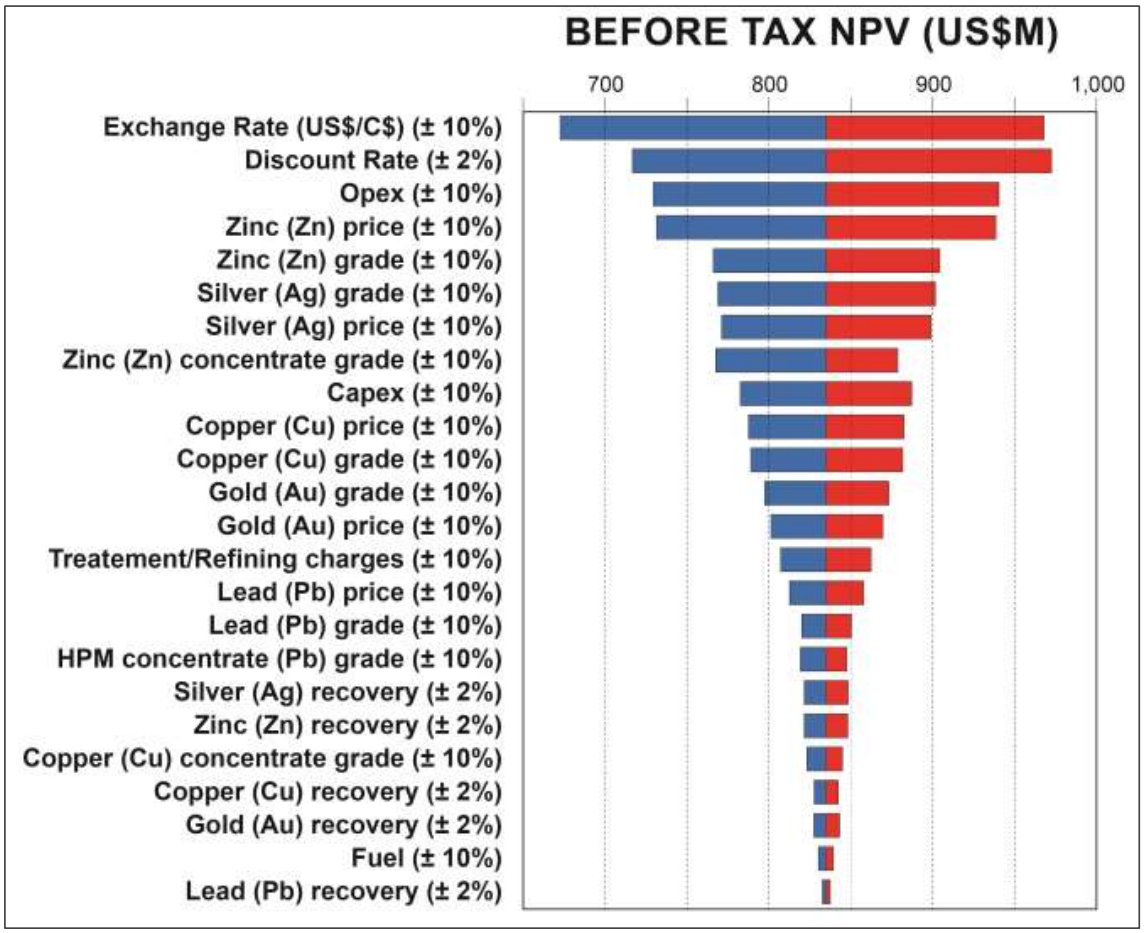


Figure 1-3: Tornado analysis showing before-tax NPV sensitivity results.
Source: 2025 Technical Report

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Reasonable Basis Discussion

A considerable volume of work on the ABM Mine Project has been completed, including a comprehensive range of studies, and updates to those studies (for aspects that are subject to changes over time, such as costs and commodity prices), have been completed.

The technical studies completed by the Company demonstrate that it is reasonable to expect that the project will be economically viable and that the forecasts are achievable. The technical work has been completed by senior and experienced individuals across the full range of the inputs.

The Feasibility Study-level investigations described in this Report support a Production Target and forecast financial information for the ABM Mine Project and are based on updated Feasibility Study-level investigations for the ABM Mine Project.

The Ore Reserve and Mineral Resources underpinning the production target and forecast financial metrics have been prepared by Competent Persons in accordance with the requirements of the JORC Code. Modifying Factors informing the Ore Reserve estimate are based on extensive and detailed studies.

All material inputs to the production schedule forecasts and forecast financial metrics summarised in this Report are at the level of confidence expected for a Feasibility Study and provide a reasonable basis for the disclosed information.

ERM considers that the inputs and assumptions of the Feasibility Study-level investigations reported in this Report (and the reports informing it) remain applicable and appropriate for the disclosed information.

The Life of Mine Plan (LOM Plan) and subsequent production target and forecast financial metrics are based on Probable Ore Reserves derived from Indicated Mineral Resources; no Inferred Resources have been included in the LOM Plan.

The Production Target is based on BMC's current expectations of future results or events.

Important Note: The financial forecasts in this Report are Non-IFRS Financial Measures.

ERM considers these measures provide useful information about the financial outcomes derived from the Feasibility Study, however, they should not be considered in isolation or as a substitute for measures of performance or cash flow prepared in accordance with IFRS.

Since the financial forecasts and economic discussion in this Report are not based on IFRS, they do not have standardised definitions and the way these measures have been derived may not be comparable to similarly titled measures used by other companies. Investors should therefore not place undue reliance on these Non-IFRS Financial Measures.

Community, Environment, and Permitting and Approvals

Environment

Following the acquisition of the Project in 2015, the Company initiated a full suite of environmental baseline studies to support the environmental assessment of the Project as part of the Yukon Environmental and Socio-economic Assessment Board (YESAB) review process. A range of these studies are ongoing. This is in addition to environmental baseline studies commenced in the 1990s, some of which were ongoing until after the acquisition of the project by BMC.

Environmental studies and monitoring will be required throughout the life of the proposed mine, including post closure. The Company is committed to undertaking all requisite environmental monitoring and mitigation measures that are expected to arise from the environmental assessment and licensing processes in Yukon.

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BMC currently operates in accordance with a site-specific Exploration Environmental Management Plan (EMP), which includes all relevant environmental conditions that are stipulated in the various existing permits and licences.

When permits are amended or renewed, they are assessed, and any additional or modified conditions are added to the EMP, along with operating strategies to meet required permit conditions as a minimum standard.

The Project has been designed to minimise energy consumption and to thereby minimise greenhouse gas emissions. The use of dual fuel (natural gas / diesel) power generation, the use of sophisticated electronic control systems in the concentrator and powerhouse, centralised controls for water pumping systems, the use of modern heat recovery systems, the use of solar panels where possible, the use of gravity in the flotation circuit design and the use of "in-line" process controls and water recycling will all contribute to minimising energy use and thereby minimising greenhouse gas and other emissions.

Recent Developments

The Company submitted a proposal to YESAB in March 2017 for the development of the ABM Mine Project.

The application has been subjected to an environmental and socio-economic assessment under the Yukon Environmental and Socio-Economic Assessment Act (YESAA), administered by the Yukon Environmental and Socio-Economic Assessment Board (YESAB).

In April 2025, the Yukon government wrote to BMC advising that they were satisfied that the ABM Mine Project was economically feasible, and that they were consulting with Kaska on the matter. BMC has been advised that consultation between the Yukon, Canadian and Kaska governments is ongoing.

Once the current government to government consultation is completed BMC will receive a new Decision Document.

BMC has submitted applications to the Yukon Water Board for a Water Licence under the Waters Act (Yukon), an application for a Quartz Mining Licence under the Quartz Mining Act (Yukon) and applications for other authorisations required to develop and operate the proposed ABM Mine.

These applications have been reviewed by the Yukon government but are currently on hold until a new Decision Document is issued.

Community Engagement

BMC's employees include local community members, and current community issues are routinely raised and discussed at internal management meetings.

In addition to meetings with First Nation Elders, Chiefs, and Councils, key community engagement with local First Nations communities, general stakeholders, and interested parties occurs through open houses, public meetings, and individual meetings, held in the local Yukon towns of Ross River, Faro, Whitehorse, and Watson Lake.

First Nations

The Company has a goal of creating a positive long-term legacy for those communities within whose traditional territory it operates. To this end, BMC has been involved in a range of projects dedicated to increasing long-term capacity building in Kaska First Nations communities.

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BMC and the Ross River Dena Council, on behalf of the Kaska Nation, are party to a Socio-Economic Participation Agreement (SEPA), in accordance with which BMC has been operating since 2015. The Company has processes and procedures that aim to increase local business participation and prosperity, these include supplier, and service provider contracts, request for proposal criteria, and procurement guidelines, some which are requirements under the existing SEPA.

ERM believes that all appropriate baseline investigations and monitoring programmes have been completed and the mitigation measures considered are appropriate for this type of project development. There can be no doubt the delays in financing and project commencement have benefited the environmental planning and design activities, and also provided time for the Company to build additional and wider-reaching relationships in the immediate area and country.

Conclusions

Prospectivity

The Kudz Ze Kayah Project contains economically significant polymetallic VHMS deposits, with additional deposits known in the surrounding district. ERM considers that the Project holds good potential for the discovery of additional VHMS mineralisation and extensions to known mineralisation.

Numerous targets have been identified that are worthy of drill testing. Geochemical and geophysical anomalies have been identified across the project tenements which are worthy of further exploration work to define drilling targets.

BMC has assembled an exploration team which has developed a strong understanding of the VHMS mineralising systems drilled to date and is showing considerable success at applying this knowledge to the discovery of additional mineralisation.

The Kudz Ze Kayah Project comprises a wide range of base metal targets for exploration from near grassroots geochemical anomalies, conceptual geological and geophysical targets to drill ready targets (Fuego, Wolverine extensions, Kona stacked lens, Krakatoa extensions, and Wolverine (Jackman)) and advanced stage deposits consisting of Ore Reserves (ABM), Mineral Resources (Kona) and formally defined JORC Code Exploration Targets (GP4F, Wolf, Kona and Jackman).

In addition to this, large sections of ground within the Kudz Ze Kayah Project remain under-explored. BMC's flagship ABM Deposit remains open beyond the existing Ore Reserves and additional drilling is required to fully define the extents of the mineralisation.

Use of Funds

In the two-year period after listing on the ASX, the Company plans activities aiming to discover and define additional Mineral Resources and Ore Reserves that can be treated at the ABM Mine. Exploration will focus on increasing Mineral Resources and Ore Reserves at the Kudz Ze Kayah Property. BMC has identified a pipeline of targets for exploration ranging from early-stage exploration targets through to advanced prospects. By prioritising exploration near the proposed ABM Mine, the Company hopes to extend the potential mine life beyond what is currently outlined in its studies. In the medium term, the Company plans to add mineral assets in the Finlayson District around the Kudz Ze Kayah Project by acquiring or partnering on promising mineral properties.

Project advancement will include continuing to obtain all required permits and licences, and on starting front end engineering design (FEED studies) for the ABM Mine and its infrastructure.

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Based on the Company's past exploration success and on the outcomes of the advanced technical studies (at a Feasibility Study level of confidence) completed at the Kudz Ze Kayah Project, the Company has developed an 18–24 month work programme comprising:

- Exploration and evaluation activities aiming to expand and improve the Kudz Ze Kayah Project's resource base.
- Permitting and approvals.
- Feasibility Study optimisation and engineering.
- Detailed Engineering.
- Continuation of community engagement and environmental works.

The use of funds for the project are summarised in Table 1-15.

Table 1-15: BMC's 24-month Proposed Use of Funds

Indicative Allocation of Funds	US$ million	% of use of funds
Exploration and Evaluation	24.6	36
Permitting	7.5	11
Feasibility Optimisation and engineering	4.3	6
Detailed engineering	11.9	17
Community	3.0	4
Camp costs	1.5	2
Corporate and administration	7.7	11
Working Capital	4.5	6
Estimated Costs of the Offer	4.9	7
Total Indicative Allocation of Funds	**69.9**	**100**

Source: BMC; Rounded to nearest 100k. Totals may not sum correctly due to rounding.

The proposed budgets are considered consistent with the exploration potential of the Company's projects and considered adequate to cover the costs of the proposed programmes.

The Company has prepared staged exploration, development and production programmes and budgets, specific to the potential of the project, and which are consistent with the budget allocations. ERM considers that the relevant areas have sufficient technical merit to justify the proposed programmes.

The proposed exploration budget also exceeds the anticipated minimum statutory annual expenditure commitments on the various project tenements

The Company provided ERM with a copy of their exploration strategy, proposed work programmes and planned expenditure for the Kudz Ze Kayah Project for an initial two-year period following listing on the ASX.

The mineral properties held by the Company are considered to be advanced exploration and pre-development that are intrinsically speculative in nature. ERM considers, however, that the projects identification and acquisition has been based on sound technical merit.

The projects are also considered to be sufficiently prospective, subject to varying degrees of exploration risk, to warrant further exploration and assessment of their economic potential, consistent with the proposed programmes.

ERM concludes that the Company's portfolio of projects offers prospects for additional discoveries in an environment that has been relatively under explored using modern methods. The exploration activities will also provide insights that may enable further discoveries.

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Significant hiatuses in the exploration and mineral development history of the region suggests that application of modern geophysical and geochemical methods, coupled with a relatively well understood mineral system may see new discoveries being made.

The presence of existing and historical mines in the region support the proposed VHMS mineral system model currently underpinning BMC's approach.

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1. INTRODUCTION

1.1 Context, Scope, and Terms of Reference

ERM Australia Consultants Pty Ltd ("ERM"), was retained by BMC Minerals Ltd (BMC or "the Company") to prepare a Technical Assessment Report (the "Report") for consolidating, summarising and updating technical information relating to the various mineral assets that comprise the Kudz Ze Kayah Project ("the Project") in a format suitable for public release and in accordance with the JORC and VALMIN Codes.

This Report discusses BMC's mineral assets in the Project, comprising eight groups of tenure (claim blocks, claims or properties):

1) KZK Property (BMC 100%), covering the ABM Deposit (containing the ABM and Krakatoa Zones), and the GP4F Prospect. The KZK Property is the focus of the proposed mine development outlined in this Report.
2) Pelly Property (BMC 100%), which is adjacent to the Wolverine Mine owned by Yukon Zinc Corp (Receivership discharged February 2024).
3) Kona Property (BMC 100%), that is centred on the Kona Deposit, comprising the Fyre Lake claims and the contiguous Tsa Da Glisza claims.
4) Wolf Property (BMC 100%), that is centred on the Wolf Deposit.
5) 1st BASE Property (BMC 100%), prospective area for exploration.
6) RB Property (BMC 100%), prospective area for exploration.
7) MER Property (BMC 100%), prospective area for exploration.
8) Rivier Property (BMC 100%), prospective area for exploration.

The most advanced asset is the KZK Property that contains the ABM Mine Project.

The ABM Mine Project has been the subject of a series of completed Feasibility Studies and Feasibility Study-level work starting in 2017, with the first such report delivered in 2019, to assess the economic viability of mining and processing the ABM Deposit.

The current Feasibility Study-level investigations, with key inputs having been reviewed and updated as required, is summarised in the Technical Report completed in accordance with NI 43-101 requirements with an Effective Date of 3rd January 2025 that was lodged on SEDAR on 3rd April 2025 (ERM 2025b, the "2025 Technical Report").

1.2 About this Report

This Report describes the base metal mineral assets of BMC in Canada, primarily the Kudz Ze Kayah Project.

This Report is an attempt to summarise, simplify and update various NI 43-101 Technical Reports describing the ABM Mine Feasibility Study-level investigations, together with other technical reports on the various deposits and properties that comprise the Kudz Ze Kayah Project.

The geology and mineralisation for the Project area is discussed, as well as the current Mineral Resources and Ore Reserve, the metallurgical activity involved in developing a processing flowsheet for a staged processing operation, the Feasibility Study-level work for an open pit and underground mining operation at Kudz Ze Kayah, ESG considerations, and other material information associated with the development of the project.

A significant amount of historical data pertains to past work completed on the Kudz Ze Kayah Project and other nearby projects and an effort was made to summarise this to contain the length and readability of the Report.

The quality of information, conclusions, and estimates contained in this Report are consistent with the level of the work carried out by ERM to date on the assignment, in accordance with the assignment specification agreed between ERM and the Client.

This Report has been prepared by ERM for consolidating and updating technical information relating to the various mineral properties that comprise the Kudz Ze Kayah Project in a format suitable for public release, and reportable in accordance with the JORC Code.

The statements and opinions contained in this Report are given in good faith and in the belief that they are not false or misleading. The conclusions are based on information available up to 30th September 2025, which could alter over time depending on exploration results, mineral prices, and other relevant market factors.

The interpretations and conclusions reached in this Report are based on current scientific understanding and the best evidence available to the authors at the time of writing. It is the nature of all scientific conclusions that they are founded on an assessment of probabilities and, however high they might be, make no claim for absolute certainty.

The ability of any person to achieve forward-looking production and economic targets depends on numerous factors beyond ERM's control and that ERM cannot anticipate. These factors include, but are not limited to, site-specific mining, and geological conditions, management, and personnel capabilities, availability of funding to properly operate and capitalise the operation, variations in cost elements, and market conditions, developing and operating the mine efficiently, unforeseen changes in legislation, and new industry developments. Any of these factors may substantially alter the performance of any mining operation.

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1.3 Terminology and Naming Conventions

BMC's project in Yukon has evolved a series of names and particular usages to capture the nomenclature of their projects, as presented in Table 1-1.

In keeping with Canadian practice, the discrete tenement packages of contiguous claims are referred to as properties in this report.

Table 1-1: BMC's Yukon Projects Nomenclature

Name	Usage
Kudz Ze Kayah Project (or the Project)	The overall project name, comprising: all the claim blocks (or properties[4]) held or controlled by BMC in the Finlayson District; and, the ABM Mine Project.
KZK Property or KZK Claim Block	The collective Mineral Claims comprising the KZK Claim Block as set out in Schedule A of the Solicitor's Tenement Report (which includes the ABM Deposit and the GP4F Exploration Target).
ABM Deposit	An accumulation of base and precious metal-rich VHMS mineralisation located within the KZK Property.
ABM Zone	The western part of the ABM Deposit, separated from the Krakatoa Zone by the East Fault.
Krakatoa Zone	The eastern part of the ABM Deposit, separated from the ABM Zone by the East Fault.
ABM Mine	The open pit and underground mining (*sensu stricto*) development associated with the ABM Deposit, comprising both ABM Zone, and Krakatoa Zone.
ABM Mine Project	The proposed ABM Mine **and** supporting infrastructure development. This term is being used in licence documentation and will be used for the proposed construction project.
Kona Deposit	An accumulation of base and precious metal-rich VHMS mineralisation located within the Kona Property.
Kona Property	Those Mineral Claims (formerly known as "Fyre Lake") centred 20 km south of BMC's KZK Property

1.4 Reporting Standard and Compliance with JORC and VALMIN Codes

The Report has been prepared in accordance with the VALMIN Code 2015[5], which is binding upon Members of the Australian Institute of Geoscientists ("AIG") and the Australasian Institute of Mining and Metallurgy ("AusIMM"), the JORC Code[6] and the rules and guidelines issued by such bodies as the Australian Securities and Investments Commission ("ASIC") and Australian Securities Exchange ("ASX") that pertain to Independent Experts' Reports.

The Report has been prepared to the standard of, and is considered by ERM to be, a Technical Assessment Report as defined in VALMIN Code (2015).

[4] In Canada, the term property is generally used for specific parcels of land with mineral rights – i.e. tenure. In Australia, the term project is more commonly used to refer to entire areas of related mineral assets, which may comprise one or more tenements.

[5] Australasian Code for Public Reporting of Technical Assessments and Valuations of Mineral Assets. The VALMIN Code, 2015 Edition. Prepared by the VALMIN Committee, a joint committee of the Australasian Institute of Mining and Metallurgy and the Australian Institute of Geoscientists.

[6] Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves. The JORC Code, 2012 Edition. Prepared by the Joint Ore Reserves Committee of The Australasian Institute of Mining and Metallurgy, Australian Institute of Geoscientists and Minerals Council of Australia (JORC).

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For the avoidance of doubt, this Report has been prepared according to:

- the 2015 edition of the Australasian Code for the Public Reporting of Technical Assessments and Valuations of Mineral Assets (the "VALMIN Code")
- the 2012 edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources, and Ore Reserves (the "JORC Code").

The authors have taken due note of the rules and guidelines issued by such bodies as ASIC and ASX, including ASIC Regulatory Guide 111 – Content of Expert Reports, and ASIC Regulatory Guide 112 – Independence of Experts.

In preparing this Report, ERM has relied on the accuracy and completeness of the data provided to it by BMC, and that the Company has made ERM fully aware of all material information in relation to the projects.

ERM has not been engaged to comment on any legal matters and notes that it is not qualified to make legal representations regarding the ownership and legal standing of the tenement licences. ERM has not attempted to independently confirm the legal status of the tenure associated with the projects and has relied on information provided by BMC and the Company's representation that it will hold adequate security of tenure for exploration, mining, and assessment of the projects to proceed.

1.5 Project Classification

Following the technical assessment comprising this Report, ERM has classified the Mineral Assets of BMC in accordance with the categories listed in the VALMIN code.

The Kudz Ze Kayah Project comprises:

a. Early-stage Exploration Projects – Tenure holdings where mineralisation may or may not have been identified, but where Mineral Resources have not been identified;

b. Advanced Exploration Projects – Tenure holdings where considerable exploration has been undertaken and specific targets identified that warrant further detailed evaluation, usually by drill testing, trenching or some other form of detailed geological sampling. A Mineral Resource estimate may or may not have been made, but sufficient work will have been undertaken on at least one prospect to provide both a good understanding of the type of mineralisation present and encouragement that further work will elevate one or more of the prospects to the Mineral Resources category;

c. Pre-Development Projects – Tenure holdings where Mineral Resources have been identified and their extent estimated (possibly incompletely), but where a decision to proceed with development has not been made.

The ABM Mine Project is a pre-development project, whereas the other mineral assets of the overarching Kudz Ze Kayah Project are early-stage and advanced exploration projects.

1.6 Principal Sources of Information and Reliance on Other Experts

ERM has based its review of the Projects on information made available to the authors by BMC, along with technical reports prepared by the Company's consultants, government agencies and previous tenement holders, and other relevant published and unpublished data.

ERM has also relied upon discussions with BMC's management for information contained within this assessment.

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ERM has endeavoured, by making all reasonable enquiries (including sense checking inputs and assumptions), to confirm the authenticity, accuracy, and completeness of the technical data upon which this Report is based. Unless otherwise stated, information and data contained in this technical report, or used in its preparation, has been provided by BMC in the form of documentation and digital data.

BMC was provided a final draft of this Report and requested to identify any material errors or omissions prior to its use.

ERM has not independently verified the legal status or ownership of the properties or any of the underlying agreements; however, all the information appears to be of sound quality.

BMC has warranted to ERM that the information provided for the preparation of this Report correctly represents all material information relevant to the Projects.

1.7 Site Visit

The VALMIN Code (Clause 11.1) notes that where an inspection of a Mineral Asset is likely to reveal information or data that are material to a public report, the Specialist should inspect it.

ERM concluded that a specific site visit for the purposes of this Report was not required.

This is due to the stage of the project, the availability of high-quality satellite imagery of the project areas and the access to them, the lack of outcrops and features of interest requiring inspection, the availability of drill core/cuttings elsewhere, and the familiarity of the authors and Competent Persons with the project through past work on the project/in the project area.

In ERM's professional opinion, undertaking a site inspection solely for the purposes of this report would not provide any additional information that would likely change ERM's opinions or conclusions contained in this Report.

ERM notes that the Mineral Resource estimate and Ore Reserve estimate Competent Persons have both made several visits to the site. Mr Green having done so in June 2024.

1.8 Declarations

This Report has been prepared by ERM at the request of, and for the sole benefit of, the Company. Its purpose is to provide an independent technical assessment of the Company's Minerals Assets.

The Report is to be included in its entirety within a prospectus to be prepared by the Company in connection with an initial public offering (IPO) for a listing on the ASX. It is not intended to serve any purpose beyond that stated and should not be relied upon for any other purpose.

ERM has consented to the inclusion of this Report in the Prospectus in the form and context in which it is included. At the date of this Report this consent has not been withdrawn. ERM has not authorised the issue of the Prospectus. Accordingly, ERM makes no representation regarding, and takes no responsibility for, any other statements in, or material omissions from, the Prospectus.

The opinions expressed in this Report have been based on the information supplied to ERM by BMC. The opinions in this Report are provided in response to a specific request from the Company to do so.

ERM has prepared this Report as part of the Company's listing documentation and asserts that it has exercised all reasonable diligence to ensure that the information within this report is, to the best of its knowledge, accurate and free from material omissions. To the extent that ERM has been able to determine, the information supplied by the Company was thorough and not misleading or incorrect in any significant respect.

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ERM does not accept responsibility for any errors or omissions in the supplied information and does not accept any consequential liability arising from commercial decisions or actions resulting from them.

Opinions presented in this Report apply to the site conditions and features as they existed at the time of ERM's or the Competent Persons' investigations, and those reasonably foreseeable. These opinions do not necessarily apply to conditions and features that may arise after the date of this Report, about which ERM had no prior knowledge nor had the opportunity to evaluate.

The interpretations and conclusions reached in this Report are based on current scientific understanding and the best evidence available to the authors at the time of writing. It is the nature of all scientific conclusions that they are founded on an assessment of probabilities and, however high these probabilities might be, they make no claim for absolute certainty.

The statements and opinions contained in this Report are given in good faith and in the belief that they are not false or misleading. The conclusions are based on the reference date of 30th September 2025 and could alter over time depending on exploration results, mineral prices and other relevant market factors.

This Report concerns a technical assessment in accordance with the VALMIN Code and is not financial advice. In preparing this Report, ERM is not relying on an Australian Financial Services Licence.

This Report contains technical details that have been condensed and organised into tables, showcasing subtotals, totals, and other derived figures. The computation of these summary data may involve some rounding. When rounding is applied, it is intended to represent the relative accuracy and confidence level of the data, and the subtotals and totals may not correspond precisely to the individual components.

1.8.1 Prior Association and Independence

The authors of this Report have had no prior association with the mineral assets of BMC. Neither ERM, nor the authors of this Report, have or have had previously, any other material present or contingent interest in BMC or the mineral properties in which BMC has an interest.

ERM's relationship with BMC is solely one of professional association between client and independent consultant.

No member or employee of ERM is, or is intended to be, a director, officer, or other direct employee of BMC. No member or employee of ERM has, or has had, any material shareholding in BMC.

There is no formal agreement between ERM and BMC in relation to ERM conducting further work for BMC.

ERM, and the authors of this Report, has no beneficial interest in the outcome of this Report, nor any pecuniary or other interest that could reasonably be regarded as capable of influencing its independence.

1.8.2 Indemnities

As recommended by the VALMIN Code (2015), the Company has provided ERM with an indemnity under which ERM is to be compensated for any liability and/or any additional work or expenditure resulting from any additional work required:

- that results from ERM's reliance on information provided by BMC or from BMC not providing material information; or
- that relates to any consequential extension workload through queries, questions or public hearings arising from the Report.

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1.9 Authors of the Report – Qualifications, Experience, and Competence

The Report has been prepared by the Technical Mining Services (TMS) team at ERM, a privately owned consulting company, which has been operating for over 50 years. ERM's headquarters are in London, United Kingdom.

ERM provides multidisciplinary services to a broad spectrum of clients across the global mining industry. Services are provided across all stages of the mining cycle from project generation to exploration, and encompass resource estimation, project evaluation, development studies, operations assistance, and corporate advice, such as valuations, and independent technical documentation.

More details on ERM's Technical Mining Services are provided at the end of this report.

This Report has been prepared by consultants sourced principally from ERM's office in Perth, Western Australia. The individuals who have provided input to the Report have extensive experience in the mining industry and are members in good standing of appropriate professional institutions. The consultants preparing this Report are specialists in the field of geology and exploration, mining, and project development in base metals.

The Report was prepared by ERM Principal Geologist and Partner (Technical Mining Services), Graham Jeffress BSc(Hons1) *Applied Geology*, FAIG RPGeo (*Mineral Exploration*), FAusIMM, FSEG, FGSAust, and by ERM Associate Principal Mining Engineer and Geologist, Mr Terry Burns, BAppSc (Geology), GDipEd (Secondary), PGDipGeosci (Mineral Economics), GDipEng (Mining), FAusIMM (CP Man).

The report was compiled from the work of the technical Competent Person's listed below.

1.10 Competent Persons' and Practitioners' Statements

1.10.1 This Report

Exploration Results, Exploration Targets, Mineral Resource and Ore Reserve estimates in this report have been prepared and reported in accordance with the JORC Code (2012).

The information in this Report that relates to Technical Assessment of Mineral Assets reflects information compiled and conclusions reached by Mr Graham Jeffress and by Mr Terry Burns, as well as on the work of the Competent Person's listed below.

Mr Jeffress is a Fellow of the AusIMM, the AIG, the Society of Economic Geologists, and the Geological Society of Australia.

Mr Jeffress is a full-time Principal Geologist and Partner (Technical Mining Services) of ERM and has no conflict of interest in relation to this Report. Mr Jeffress has sufficient experience that is relevant to the Technical Assessment of the Mineral Assets under consideration, the style of mineralisation and types of deposit under consideration and to the activity being undertaken to qualify as a Practitioner as defined in the 2015 Edition of the "Australasian Code for Public Reporting of Technical Assessments and Valuations of Mineral Assets", and as a Competent Person as defined in the 2012 Edition of the "Australasian Code for Reporting of Exploration Results, Mineral Resources, and Ore Reserves". Mr Jeffress consents to the inclusion in the Report of the matters and the supporting information based on his information in the form and context in which it appears.

Mr Terry Burns is a Fellow and Chartered Professional of the AusIMM.

Mr Burns has sufficient experience that is relevant to the technical assessment of the Mineral Assets under consideration, the style of mineralisation and types of deposit under consideration and to the activity being undertaken to qualify as a Practitioner as defined in the 2015 Edition of the

"Australasian Code for the public reporting of technical assessments and Valuations of Mineral Assets" (2015 VALMIN Code), and as a Competent Person as defined in the 2012 Edition of the "Australasian Code for Reporting of Exploration Results, Mineral Resources, and Ore Reserves" (2012 JORC Code).

Mr Burns consents to the inclusion in the Report of the matters based on his information in the form and context in which it appears.

1.10.2 Exploration Targets and Mineral Resource Estimates

The information in this Report that relates to Exploration Targets and Mineral Resources is based on and fairly represents information and supporting documentation compiled and conclusions derived by Mr Aaron Green, a Competent Person who is a Fellow of the AIG. Mr Green is currently employed by Cube Consulting Pty Ltd.

Mr Green has no conflict of interest in relation to this Report.

Mr Green has sufficient experience that is relevant to the Technical Assessment of the Mineral Assets under consideration, the style of mineralisation and types of deposit under consideration and to the activity being undertaken to qualify as a Practitioner as defined in the 2015 Edition of the "Australasian Code for the public reporting of technical assessments and Valuations of Mineral Assets", and as a Competent Person as defined in the 2012 Edition of the "Australasian Code for Reporting of Exploration Results, Mineral Resources, and Ore Reserves".

Mr Green has previously consented to the inclusion in the Report of the matters and the supporting information based on his information in the form and context in which it appears.

1.10.3 Ore Reserve Estimates

The information in this Report related to Ore Reserves is based on and fairly represents information and supporting documentation compiled and conclusions derived by Mr Karl van Olden, a Competent Person who is a Fellow of the AusIMM. Mr van Olden is currently employed by AMC Consultants Pty Ltd.

He has no conflict of interest in relation to this Report.

Mr van Olden has sufficient experience that is relevant to the Technical Assessment of the Mineral Assets under consideration, the style of mineralisation and types of deposit under consideration and to the activity being undertaken to qualify as a Practitioner as defined in the 2015 Edition of the "Australasian Code for the public reporting of technical assessments and Valuations of Mineral Assets", and as a Competent Person as defined in the 2012 Edition of the "Australasian Code for Reporting of Exploration Results, Mineral Resources, and Ore Reserves".

Mr van Olden has previously consented to the inclusion in the Report of the matters and the supporting information based on his information in the form and context in which it appears.

1.10.4 Metallurgy and Processing

The information in this Report that relates to the metallurgy and mineral processing of Mineral Assets is based on and fairly represents information and supporting documentation compiled and conclusions derived by Mr John Riordan, a Competent Person who is a Fellow of the AusIMM. He is currently employed by DRA Global Limited.

Mr Riordan has no conflict of interest in relation to this Report.

Mr Riordan has sufficient experience that is relevant to the mineral processing of the Mineral Assets under consideration, the style of mineralisation and types of deposit under consideration and to the

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activity being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the "Australasian Code for Reporting of Exploration Results, Mineral Resources, and Ore Reserves".

Mr Riordan has previously consented to the inclusion in the Report of the matters and the supporting information based on his information in the form and context in which it appears.

1.10.5 Reliance on other technical specialists

In preparing this report, ERM has extensively relied on information collated by other parties, as described above.

ERM has critically examined this information, made its own enquiries and applied general geological competence and industry experience to conclude that the information presented in this Report complies with the definitions and guidelines of the JORC and VALMIN Codes.

1.11 Fees

ERM is an independent consultancy. This Report is prepared in return for our normal professional fees based upon agreed commercial rates, plus reimbursement of incidental expenses, and the payment of these fees is in no way contingent on the results of this Report.

The agreed fee was based on the complexity of the assignment, ERM's knowledge of the assets, and data availability.

The fee for the preparation of this Report is approximately A$62,000.

1.12 Effective Report Date

The effective date of this Report is 30th September 2025. The technical information is presented as at this date.

At the release date of this Report, namely on or around 30th September 2025, ERM is not aware of any events or conditions that would necessitate material changes in the Report after the effective date. This includes among other things no material alterations to the technical information presented in this Report.

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2. LOCATION, CLIMATE, AND PHYSIOGRAPHY

The Kudz Ze Kayah Project is located on the northern flank of the Pelly Mountain Range, 260 km northwest of Watson Lake and 115 km southeast of Ross River (Figure 2-1). The tenements are within the Watson Lake Mining District and Finlayson Lake geographic districts.



Figure 2-1: Kudz Ze Kayah Project Location Map
Source: 2025 Technical Report

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All tenements lie within the traditional territory of the Kaska First Nations ("Kaska"), and a SEPA, signed by RRDC on behalf of the Kaska, covers much of the Kudz Ze Kayah Project.

2.1 ABM Deposit – Kudz Ze Kayah Property

The ABM Deposit lies within the KZK Property, approximately 23 km south of Finlayson Lake and 25 km west of the Wolverine Mine (Figure 2-2).

Road access to the ABM Deposit and BMC Exploration Camp is via a 24 km long, 4 m-wide, road (Tote Road, Figure 2-3, Figure 2-6, and Figure 12-1) connecting the deposit to the all-weather Robert Campbell Highway that links the towns of Watson Lake and Carmacks (Figure 2-1).

The highway is multi-surfaced with chip seal from Carmacks to Faro, gravel from Faro to the Nahanni Range Road turn-off, and chip seal the remainder of the way to Watson Lake. The GP4F Prospect is located approximately 5 km southeast of the ABM Deposit.

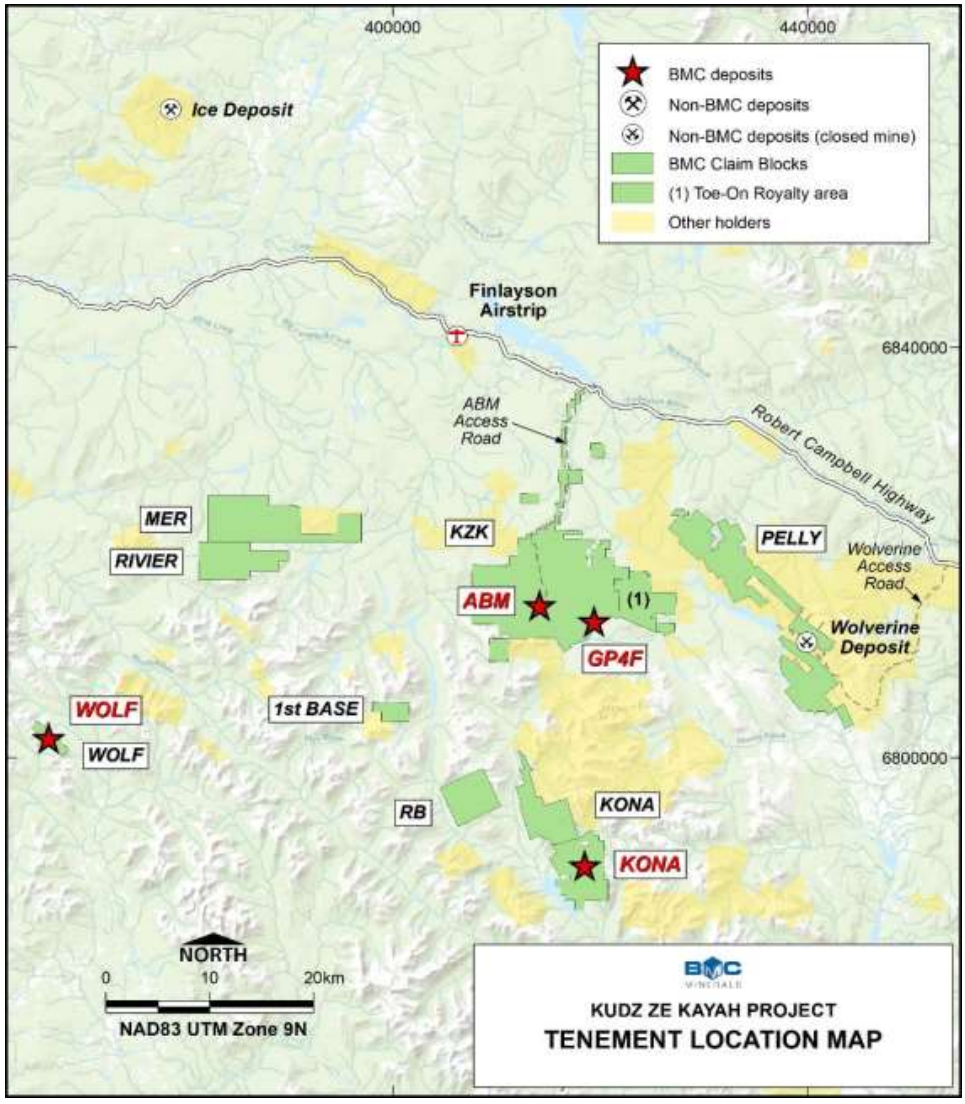


Figure 2-2: Kudz Ze Kayah Project Tenement Location Map.
Source: BMC



Figure 2-3: View of the Tote Road (looking south towards the Process Plant and Mining Area)
Source: BMC

The KZK Property occurs within the Pelly River and Pelly Mountain ecoregions and is specifically located within the northern foothills of the Pelly Mountains of the Yukon Plateau, on the east side of the divide between the Pelly River and the Liard River drainage basin.

The area's topography comprises high rolling hills, locally with ponds and lakes occupying valley bottoms (Figure 2-4), where the elevations range from 1,000 m near Finlayson Lake to over 2,000 m at the peaks of the mountains southwest of the ABM Deposit.



Figure 2-4: Landscape hosting the ABM Deposit (Looking NW – Geona Creek)
Source: BMC

The project area was glaciated, and bedrock exposures typically occur only in deep ravines or on steep slopes where post-glacial erosion has removed the overburden. Valley bottoms are covered with till and glaciofluvial sediments that are locally overlain by alluvial fan sediments. Colluvial apron sediments are also common. The project is located within the discontinuous but widespread permafrost zone, with permafrost typically within approximately 2 m of the surface.

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The ABM Deposit is located at approximately 1,400 m elevation in a broad, gently sloping, U-shaped valley covered by 2–30 m of residual glacial overburden. Geona Creek, a north-flowing tributary to Finlayson Creek, drains several small ponds, which partly overlie the deposit (Figure 2-5).

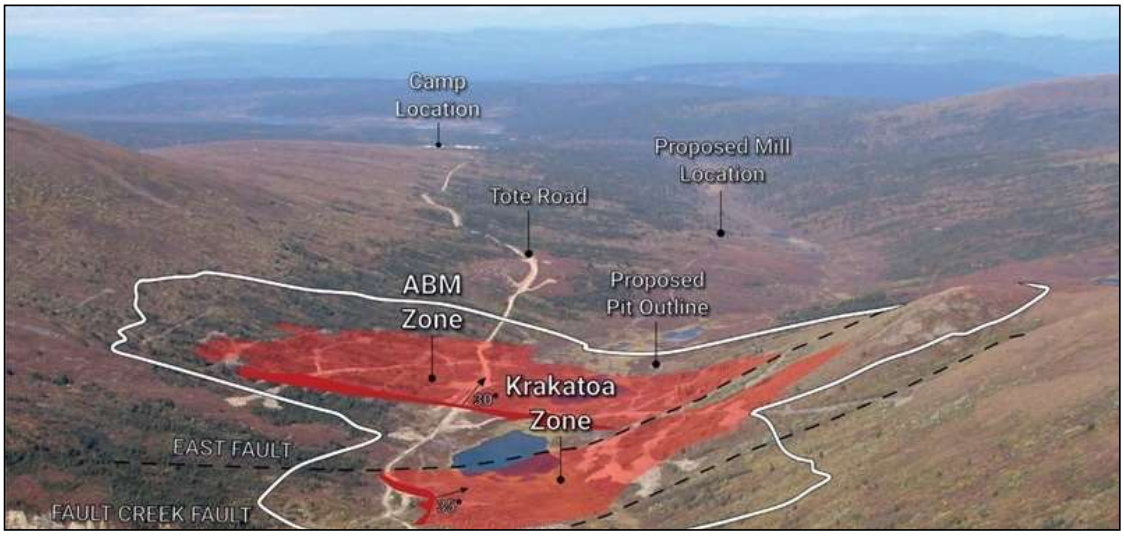


Figure 2-5: Aerial view of the ABM Deposit (mineralisation projected to surface).
Source: BMC

White and black spruce are the most common tree types below the tree line (1,350–1,500 m). Black spruce is usually dominant in wetter areas, whereas white spruce predominates where it is drier. Paper birch, aspen, balsam, and lodgepole pine are also present, and alpine fir grows near the tree line. Feather moss dominates the understory in dense coniferous stands, but willows and heath-like shrubs become prevalent in more open areas.

Sedge or sphagnum tussocks are common in wetlands and under black spruce. Shrub birch and willow occur in the subalpine and extend well above the tree line. The region has intermittent permafrost with moist depressions comprising peat plateaus, patterned fen, and bog complexes.

The climate in the area is typically sub-arctic and characterised by cold winter temperatures (minimum mean monthly temperature of –13°C) and low snowfall (Figure 2-6). Summer is generally mild, with a maximum mean monthly temperature of 10°C.The long-term mean annual temperature is estimated to be -2.8°C, with minimum and maximum mean monthly temperatures estimated to be -12.9°C and 9.9°C in December and July, respectively.

Precipitation falls reasonably evenly throughout the year, predominantly as rain from May through September, and snow for the rest of the year. The long-term mean annual precipitation is 520 mm for the site. Precipitation at the site is split between rain and snow, with approximately 37% of it estimated to fall as snow. The 24-hour 100-year, 200-year, and probable maximum precipitation values are estimated to be 89 mm, 95 mm, and 274 mm, respectively. The one-in-ten-year wet annual precipitation is estimated to be 646 mm, and the one-in-ten-year dry annual precipitation is estimated to be 394 mm.

Groundwork on the KZK Property is possible year-round; however, snow can impact activity and may cover parts of higher elevations quite late into the summer. Drilling can be conducted year-round using heated water during the colder months.

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The production operations will be conducted on a 24-hour, seven-day basis year-round, and all habitable buildings must be appropriately insulated and temperature-controlled to enable this operating regime.



Figure 2-6: ABM Deposit – Valley view along the Tote Road (looking north)
Source: CSA, 2015

2.2 Kona Property

The Kona Property (formerly known as "Fyre Lake") is centred 20 km south of BMC's KZK Property, approximately 140 km southeast of Ross River, and 250 km east of Whitehorse. There is no road access with access restricted to fixed wing aircraft or helicopter. A winter access trail historically provided temporary road access from the southern end of Cominco's camp to historical emerald workings on the Tsa Da Glisza Claim Block.

The Kona Property covers linear open valleys and high rolling to craggy ridges and mountains, and the topographic relief is moderate to locally high with elevations ranging from 1,100 m at Fire Lake to 1,900 m along the eastern ridge crests. To the northeast, there are two easterly trending hanging valleys and broad open cirques.

The drainage from the northern hanging valley, within which most of the known mineralisation is situated, is called "Kona Creek", and the central valley is drained by "Outfitters Creek".

Spruce forest covers the southern area, while to the north the vegetation becomes more open with buckbrush and eventually disappears to a caribou moss cover at elevation.

2.3 Wolf Property

The Wolf Property is located approximately 40 km west of the KZK Property, 85 km southeast of the town of Ross River and 205 km east-northeast of Whitehorse. The property lies in rugged terrain in the St Cyr Range of the Pelly Mountains with elevations ranging from 1,500 m to 1,882 m at the top of Mount Vermilion.

The area is accessible by helicopter only, with the nearest road-accessible point lying 42 km due north on the Robert Campbell Highway.

Most of the property lies near or above the tree line and the lower lying forest consists mostly of white and black spruce, with black spruce predominant in wetter areas and white spruce favouring drier ground. Paper birch, aspen, balsam, and lodgepole pine are also present. Alpine fir grows near the tree line.

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2.4 Pelly Property

The Pelly Property is located approximately 20 km east of the KZK Property and approximately 280 km east-northeast of Whitehorse.

The Pelly Property is accessed by the Robert Campbell Highway via two alternative routes. The Wolverine mine access road reaches to within 100 m of the Pelly Property, and a formerly active winter access trail traverses the northern 7 km of the Pelly Property starting on the Robert Campbell Highway 9 km north of the property.

The Pelly Property lies within the Liard River drainage basin 25 km east of the KZK Property and comprises three non-contiguous claim groups WOL, JACK, and GO. Topography is fairly rugged with elevations ranging from 1,100 m near Wolverine Lake to nearly 1,800 m on the peaks to the northeast.

The region has intermittent permafrost with moist depressions comprising peat plateaus, patterned fen, and bog complexes.

Creeks within the WOL claim group either drain northeast into the Finlayson River or southwest into Wolverine Lake, whereas creeks on the JACK and GO claim groups drain west into Wolverine Lake or southward towards Money Creek.

Below the tree line (1,350–1,500 m), white, and black spruce are the most common tree types. Black spruce is usually dominant in wetter areas whereas white spruce predominates in drier areas. Paper birch, aspen, balsam, and lodgepole pine are also present. Alpine fir grows near the tree line. In dense coniferous stands, feather moss dominates the understory, but in more open areas, willows, and heath-like shrubs become prevalent. Sedge or sphagnum tussocks are common in wetlands and under black spruce. Shrub birch and willow occur in the subalpine and extend well above the tree line.

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3. MINERAL TENURE AND SURFACE RIGHTS

The Kudz Ze Kayah Project comprises 2,013 mineral claims in Yukon, Canada, in eight properties covering a total of 372 km^2 all 100% held by BMC.

The claims are owned by BMC and granted under the *Quartz Mining Act* (Yukon) and are underlain by Crown Land.

The mineral claims are divided into eight claim blocks or properties. The KZK, Pelly, Kona, and Wolf claims cover the key mineral assets, while the 1st BASE, MER, Rivier and RB properties are exploration tenure.

The expiry dates for the Kudz Ze Kayah Project claims range between 19th October 2029 and 2nd April 2044.

Details on tenure are provided in Appendix F: Tenement Summary, and discussed in detail elsewhere in the Solicitor's Report elsewhere in the prospectus.

3.1 KZK Property

The KZK Property comprises 879 contiguous mineral claims, covering 161.3 km^2. BMC acquired the KZK Property from Teck Resources Limited (Teck) on 24th January 2015.

3.2 Kona Property

The Kona Property comprises two contiguous claim block subsets covering a total of 51 km^2. At the southern extent are 161 mineral claims covering 28.4 km^2, historically referred to as the Fyre Lake Claim Block and acquired in 2023 by Finlayson Copper Ltd, a wholly owned subsidiary of BMC.

Immediately adjoining to the north are an additional 121 mineral claims (BMC 100%) historically referred to as the Tsa Da Glisza Claim Block. The Tsa Da Glisza Claim Block covers 22.6 km^2 and was purchased from True North Gems in 2018. BMC does not hold metals rights over the Tsa Da Glisza claims, as those rights were retained by Yukon Zinc Corporation (Receivership discharged February 2024).

3.3 Wolf Property

The Wolf Property comprises 18 mineral claims (WOLF 1–18) covering 375 ha which is owned 100% by BMC following the purchase of the Property from Atna Resources Limited (Atna) in April 2016.

3.4 Pelly Property

The Pelly Property consists of 422 mineral claims that cover 70.6 km^2 which are owned 100% by BMC following their purchase from Teck in January 2015.

The Pelly Property comprises three separate claim groups: JACK – located northeast of Wolverine, GO – located southwest of Wolverine, and WOL – located northwest along Wolverine Lake. The JACK and GO claim groups flank the northeast and southwest sides of claims covering Yukon Zinc's Wolverine Deposit and historical mine.

3.5 Mineral Tenure

Mineral claims confer title to hard rock mineral tenure only. Surface rights are held by the Crown and administered by the Yukon government.

Trapping rights over the western portion of the KZK Property are held by the Ross River Dena Council (RRDC) under group Trapline #405, while trapping rights over the rest of the Project are held under

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Single Holder Trapline #250. The KZK Property overlaps with part of Outfitter Concession #20, held by Yukon Big Game Outfitters.

Staking of new mineral tenure is currently not permitted within RRDC or Liard First Nation (LFN) traditional territories surrounding the Kudz Ze Kayah Project due to government claim staking moratoriums currently set to expire on 30th April 2026 and they may be extended beyond that date.

The footprint of the proposed mine, processing facility and related infrastructure as outlined in this Report lie within a fully contiguous set of mineral claims except for a narrow strip of ground that underlies a small portion of the Class C waste facility that is not essential to the viability of the Project. To acquire surface rights over this area, BMC intends to apply for a surface lease under the *Territorial Lands (Yukon) Act*.

3.5.1 Royalties

A 0.75% NSR royalty is payable to Teck for future production from the Minerals Claims ON 21 85, ON 87-101, ON 104-113, ON 116-125 ON 162-173, and ON 197-198 (Figure 2 2). These claims do not encompass the current Ore Reserves, Mineral Resources, or Exploration Targets of the KZK Property

A precious metal purchase agreement (the PMPA) was acquired in 2021 by OMF Fund III (Bi) LP over the KZK Property (KZK Property claim block) only (Figure 2-2), and this was subsequently sold to Wheaton Precious Metals Corp in February 2024. The PMPA encompasses the current Ore Reserves and Mineral Resources of the ABM Deposit.

There is a 3% NSR royalty over the 1st BASE Property and a 1.0% gross royalty on gemstone production from the Tsa Da Glisza Claim Block (Figure 2-2).

3.6 Environment, Community, Approvals

3.6.1 Environmental Liabilities

There has been no previous mining activity on the Project[7]. ERM does not expect there to be environmental liabilities associated with the project attributable to previous exploration activities, and exploration undertaken by BMC.

3.6.2 First Nations

All the tenements of the Kudz Ze Kayah Project lie within the traditional territory of the Kaska First Nations, comprising RRDC, LFN, Dease River First Nation, and Kwadacha First Nation. The Wolf claims also overlap part of the traditional territory of the Teslin Tlingit Council.

Portions of the KZK Property, including the ABM Deposit and all proposed supporting infrastructure, are covered by a socio-economic participation Agreement (SEPA) established 1st April 2004, to which BMC and RRDC, on behalf of the Kaska Nations, are party. BMC releases annual, publicly available reports in accordance with the SEPA (BMC, 2025).

BMC is the 100% owner of Lease 105G07-001, granted under the *Territorial Lands (Yukon) Act* and associated regulations, and a security deposit has been lodged for the lease. The lease relates to a 47.24-ha parcel of land that covers the Kudz Ze Kayah access road (Tote Road) and Gatehouse. The Tote Road Lease was set to expire on 30th April 2025, but this has date since been extended as BMC submitted an application for a replacement lease under the *Resource Roads Regulations* that came into force on 27th January 2025 (as is discussed in more detail elsewhere in the prospectus).

[7] Other than a small-scale, historical, emerald mine on the Tsa Da Glisza claim block.

3.6.3 Permitting

Project Proposal

The Company submitted a proposal to YESAB in March 2017 for the development of the ABM Mine Project.

The application has been subjected to an environmental and socio-economic assessment under the Yukon Environmental and Socio-Economic Assessment Act (YESAA) administered by the Yukon Environmental and Socio-Economic Assessment Board (YESAB).

In October 2020, YESAB issued a final screening report which recommended that the proposed ABM Mine Project be allowed to proceed to permitting under s. 58(1)(b) of YESAA, subject to thirty recommendations and conditions.

The final screening report was provided to the relevant Decision Bodies for review and, following consultation with affected First Nations, the Decision Bodies issued a Decision Document in June 2022 that allowed the Project to be developed subject to certain conditions.

In July 2022, the Kaska First Nation applied for a judicial review of this document on the basis that the Government had failed to properly consult with Kaska.

In January 2024, the judicial review found that the government's consultation was incomplete, and the court ordered the Yukon government to carry out further consultation with Kaska. The review was completed in March 2024, after which the Government issued a new Decision Document allowing the ABM Mine Project development to proceed.

In February 2024, Kaska appealed the January 2024 judgement on the basis that the government should have specifically included consultation on the financial viability of the ABM Mine Project.

In December 2024, the Court of Appeal upheld the application, ordering the Government and Kaska to consult on the matter of financial viability and to issue a new Decision Document.

In April 2025, the Yukon government wrote to BMC advising that they were satisfied that the ABM Mine Project was economically feasible, and that they were consulting with Kaska on the matter. BMC has been advised that consultation between the Yukon, Canadian and Kaska governments is ongoing. Once the current government to government consultation is completed BMC will receive a new Decision Document.

BMC has submitted applications to the Yukon Water Board for a Water Licence under the Waters Act (Yukon), an application for a Quartz Mining Licence under the Quartz Mining Act (Yukon) and applications for other authorisations required to develop and operate the proposed ABM Mine.

These applications have been reviewed by the Yukon government but are currently on hold until a new Decision Document is issued.

Water Licence

A Type A Water Licence (QZ97-026-1) was granted to Cominco for 20 years on 17th September 1998 and assigned to BMC in January 2015. The Water Licence at the time of the grant allowed for the construction and operation of the mine as proposed by Cominco and was more recently sufficient for BMC's water use in support of exploration activities. This licence expired on 28th September 2018.

Before the Type A Water Licence expiry, BMC was granted a Type B Water Licence (QZ16-085) on 15th June 2017 to allow for continuity of exploration activities after the Type A licence expiry. This licence expires on 6th June 2027. BMC has submitted applications for Water Licences to the Yukon

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Water Board and an application for a Quartz Mining Licence to the Yukon Department of Energy, Mines, and Resources.

The Company anticipates that the Type A Water Licence and Quartz Mining Licence will be issued after a 12-month period following the receipt of the Decision Document.

Exploration Activities

A Class 3 Mining Land Use Approval (MLU) (LQ00424) for exploration activities was granted to BMC for a 5-year period from an effective date of 29th June 2015 and covered the contiguous claims over and adjacent to the ABM Deposit (the KZK Property). This permit was subsequently amended on 15th June 2017 to a 10-year period, resulting in an expiry of 28th June 2025 (MLU LQ00424b). A new Class 3 Mining Land Use permit application has been lodged. A YESAB recommendation to proceed has now been received for this MLU permit application. Next step is to receive a Decision Document from the Decision Body (Yukon Government).

Meanwhile, a Yukon Government Order in Council (OIC) has extended current Class 3 MLU permit to end of 2025 as an interim measure. If new Class 3 is granted the OIC and current Class 3 fall away (see solicitors report).

Class 1 Mining Land Use permit applications have been lodged with Yukon Government for the Pelly, and Kona properties. A Class 1 permit has been received for the Wolf and GP4F Properties.

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4. VHMS DEPOSITS

Volcano-sedimentary-hosted massive sulfide deposits (VHMS) – also known as volcanic-associated, volcanogenic, or volcanic-hosted massive sulfides – are an economically important class of base and precious metal mineral deposits. They are relatively common and are found in rocks spanning three-quarters of the age of the Earth.

As the name implies, VHMS deposits are accumulations of sulfide minerals, hosted by volcanic rocks, where the sulfides comprise more than 60% by volume of the rock. This definition is generally extended to include massive sulfate deposits and sulfide deposits dominated by disseminated to semi-massive mineralisation and to include deposits hosted by volcanic successions, i.e. volcaniclastic and sedimentary rocks deposited adjacent to volcanoes.

VHMS deposits are predominantly layered accumulations or lenses of polymetallic massive sulfide minerals that precipitate from hydrothermal fluids on or beneath the seafloor (Figure 4-2) as the result of mixing of upwelling hydrothermal fluid with seawater.

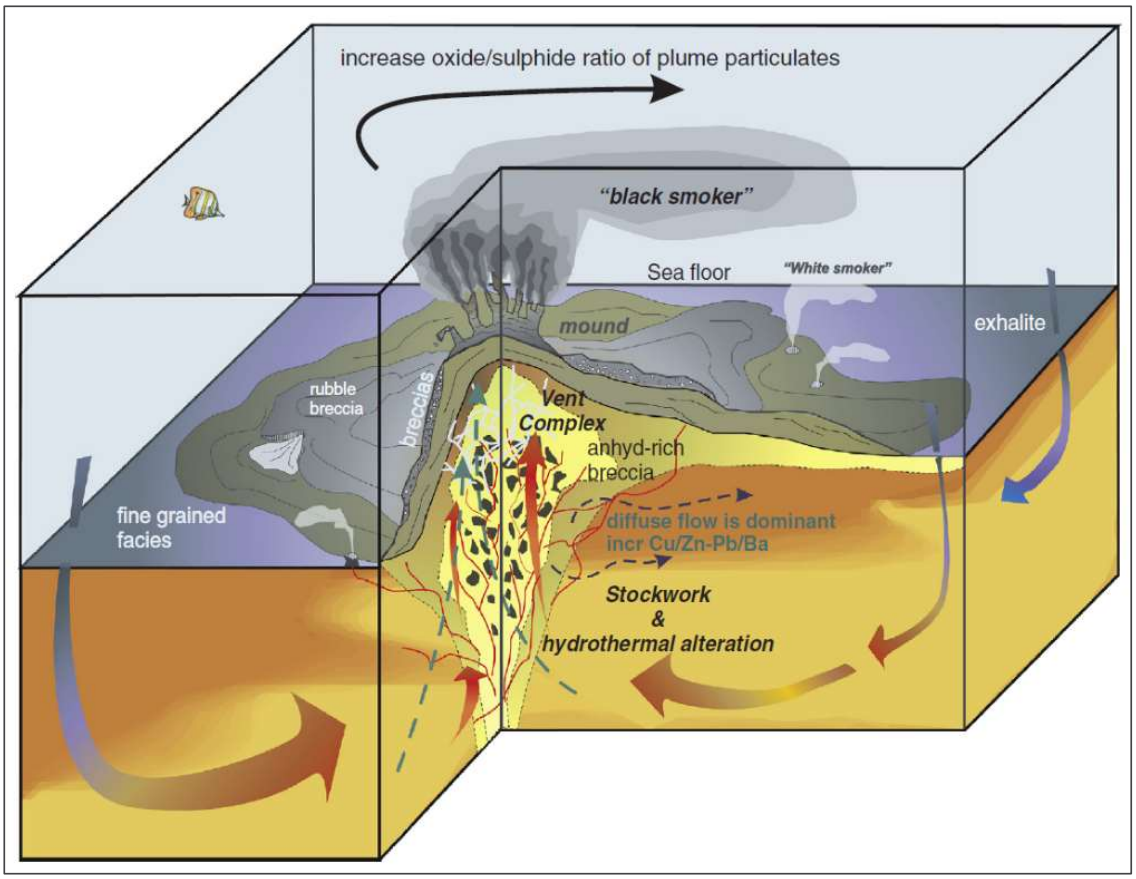


Figure 4-1: Schematic diagram of a "classic" VHMS deposit, with concordant semi-massive to massive sulfide lens underlain by a discordant stockwork vein system and pipe of alteration.
Source: from Tornos et al. (2015)[8]

[8] Noting that these authors have not consented to the use of their technical report in this Report, but it is included as per ASIC RG55 and Instrument 2016/72.

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They are associated with and created by volcanism-associated hydrothermal events that are still forming on the seafloor today (sulfurous plumes called "black smokers") around undersea volcanoes along many ocean ridges, and associated with subduction (within back-arc basins and forearc rifts) (see Figure 4-3).

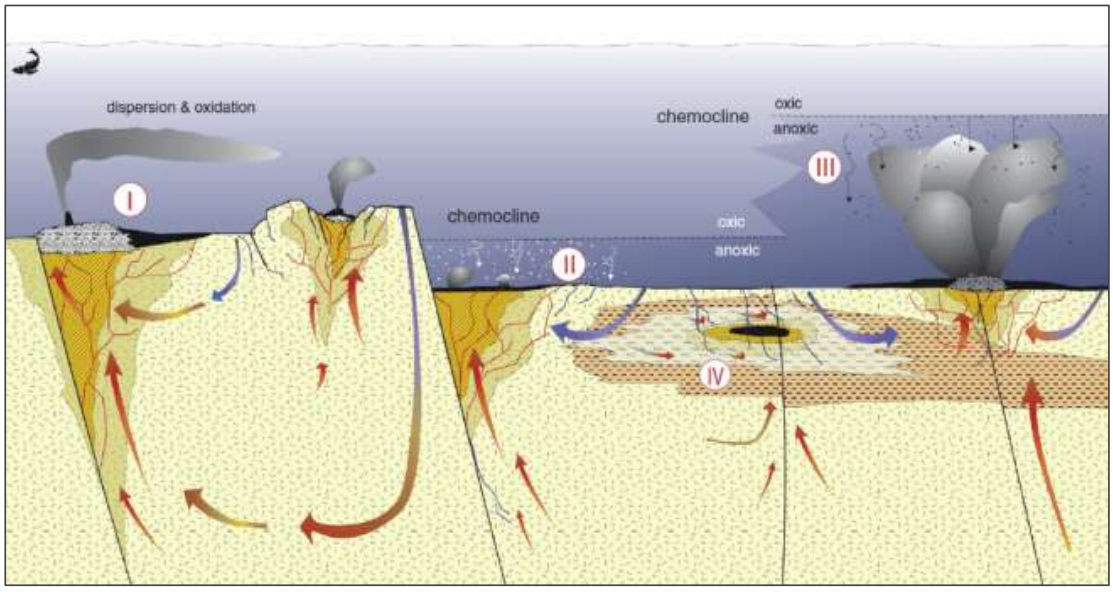


Figure 4-2: Schematic diagram showing the main features of the different styles of VHMS mineralisation.
(I) Mounds and black smoker chimneys in oxic environments; (II) brine pools; (III) mound and stratiform sulfides in regional anoxic environments; (IV) sub-seafloor replacement.
Source: Tornos et al. (2015)[9]

VHMS range in age from 3,400 million years to deposits still actively forming in modern seafloor environments. They are major sources of zinc, copper, lead, silver, and gold, and significant sources for cobalt, tin, selenium, manganese, cadmium, indium, bismuth, tellurium, gallium, and germanium.

Huston et al. (2010) note some key features of the deposit type.

VHMS are interpreted to have formed subaqueously, at or just below the sea floor, from moderate- to high-temperature (200℃–400℃) fluids driven by the high heat flow accompanying volcanism.

These deposits are considered syngenetic or nearly so, hence, in many cases these deposits form along district-scale stratigraphic positions (or marker horizons) that represent either quiescent periods of volcanism or changes in lithology or compositional characteristics of the host succession

The largest VHMS deposits are interpreted to form as replacements of unconsolidated volcanic, volcaniclastic, and sedimentary rocks beneath ancient seafloors at depths from 10–100 m. Infiltration and replacement processes below the seafloor can significantly improve the number of metals retained, compared with the dispersal that can occur when metals are precipitated in the overlying water column. Sulfide deposits formed beneath the seafloor also have a higher potential for preservation, as they are less impacted by erosion and oxidation.

[9] Noting that these authors have not consented to the use of their technical report in this Report, but it is included as per ASIC RG55 and Instrument 2016/72.

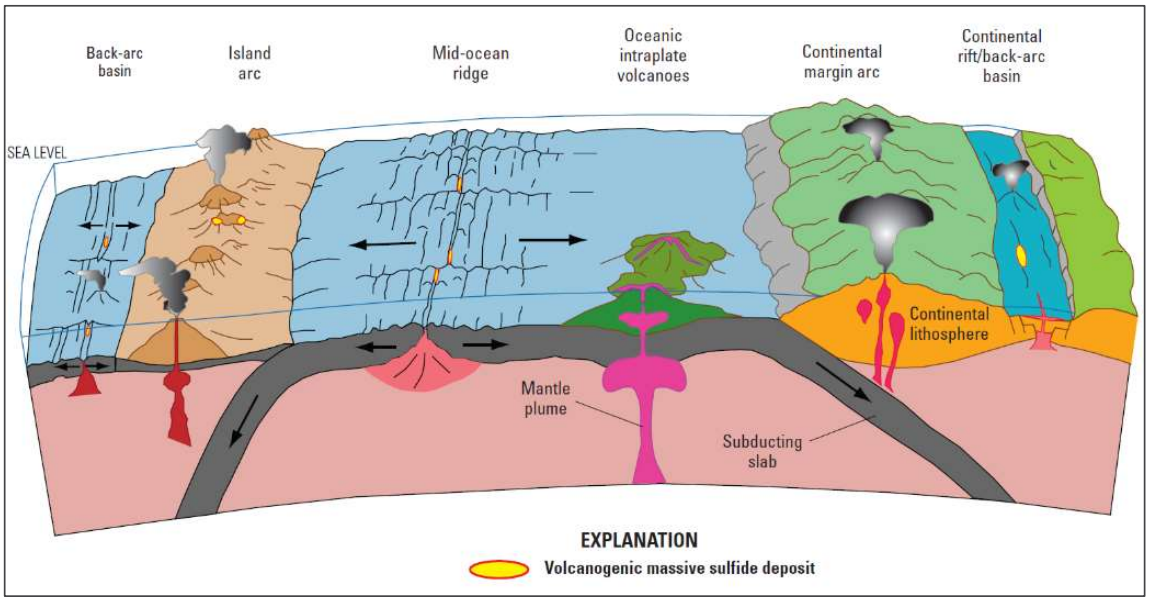


Figure 4-3: Schematic diagram showing volcanogenic massive sulfide deposits in divergent (mid-ocean ridge and back-arc basin) and convergent (subduction related island arc and continental margin arc) plate tectonic settings. Source: Shanks and Thurston (2012)[10]

Deposit-specific features can be found such as sulfide-rich sediments adjacent to the deposit, accumulations of sulfate minerals such as barite and anhydrite, or collapsed areas containing siliceous sinter cones.

Other distinct deposit features include widespread alteration in rocks adjacent and often contemporaneous to chloritisation, silicification and pyritisation.

The most common feature among all types of VHMS deposits is that they are formed in extensional tectonic settings, including both oceanic seafloor spreading and arc environments.

Most ancient VHMS deposits that are still preserved in the geological record formed mainly in oceanic and continental nascent-arc, rifted arc, and back-arc settings. Primitive bimodal mafic volcanic-dominated oceanic rifted arc and bimodal felsic-dominated siliciclastic continental back-arc terranes contain some of the world's most economically important VHMS districts.

Most significant VHMS mining districts are defined by deposit clusters formed within rifts or calderas. Their clustering is further attributed to a common heat source that triggers large-scale sub-seafloor fluid convection systems. These subvolcanic intrusions may also supply metals to the VHMS hydrothermal systems through magmatic devolatilisation.

VHMS mining districts are commonly characterised by extensive semi-conformable zones of hydrothermal alteration that intensifies into zones of discordant alteration in the immediate footwall and hangingwall of individual deposits because of large-scale fluid flow.

VHMS camps can often be further characterised by the presence of thin, but laterally extensive, units of ferruginous chemical sediment formed from exhalation of fluids and distribution of hydrothermal particulates.

[10] Noting that these authors have not consented to the use of their technical report in this Report, but it is included as per ASIC RG55 and Instrument 2016/72.

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Examples of large-scale subsea-floor replacement deposits hosted by felsic to intermediate volcanic successions include:

1. Australia:

- Rosebery, Hercules, Mount Lyell, Benambra, Liontown, Highway-Reward, Mount Morgan, Sulfur Springs and Golden Grove Deposits (including Gossan Hill), also see Figure 16-23.

2. Canada

- Mattabi (and other Sturgeon Lake Deposits), Horne H lenses, Ansil, Kidd Creek, Coniagas, and some lenses of the Myra Falls Deposits.

3. Sweden

- Renström, Kyrkvägen, Kankberg, Holmtjärn, Petiknäs North, Långdal, Långsele, Boliden and West, North and East Maurliden Deposits.

4. Portugal and Spain

- San Miguel, Salomon-Lago (Rio Tinto), San Platón, Concepción, Neves Corvo, Aguas Teñidas and Los Frailes-Aznalcóllar Deposits of the Iberian Pyrite Belt.

Understanding the different deposit models enables optimised approaches in exploration and provides improved understanding of the potential of known VHMS mineralisation. Siliciclastic-rich deposits are known to be the largest tonnage systems, but polymetallic bimodal systems are known for the highest grades.

Tornos et al (2015)[11] summarise key observations on VHMS deposits:

- VHMS deposits formed in a restricted number of geological settings that reflect the existence of different geochemical traps.
- The largest deposits formed as replacements of volcanic and sedimentary rocks below the seafloor and as stratiform accumulations deposited in regionally anoxic water bodies.
- Anoxic brine pools formed in only certain VHMS basins, whereas mounds and related chimney complexes are fairly uncommon in the ancient rock record. In clear contrast, most present-day deposits form mounds and, presumably, underlying replacement zones and stockworks. There are no exhalative deposits known in anoxic basins.
- The various styles of VHMS mineralisation can rarely be distinguished by a single criterion, and in most cases several criteria are required.
- Furthermore, most VHMS deposits comprise two or more styles of mineralisation, and a single district likely contains a range of deposits of different styles.
- In general, VHMS deposits formed by exhalative processes were initiated as mounds but may have evolved into a stratiform deposit if conditions were (or became) anoxic.
- Most exhalative deposits have underlying replacive mineralisation in the stockwork zone if the host rock characteristics were favourable.

In summary, there are three main controls on the depositional processes and depositional sites of volcanogenic massive sulfide mineralisation:

- the geology and facies architecture of the sub-seafloor stratigraphic succession control whether exhalative versus replacive style mineralisation predominates;

[11] Noting that these authors have not consented to the use of their technical report in this Report, but it is included as per ASIC RG55 and Instrument 2016/72.

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- the physicochemical composition of the hydrothermal fluids (which governs the redox state, the metal and sulfur contents and the temperature and salinity — and, thus, the buoyancy of the fluid); and
- the redox conditions and physiography of the depositional site within the basin.

Any exploration approach to be considered in the case of VHMS deposits is ultimately linked to the processes involved in their formation and the properties inherent in the resultant mineral deposit and variably altered host rocks. The scientific understanding of processes that produce VHMS deposits provide key exploration criteria.

The deposits are typically formed on the seafloor at or near volcanic or hydrothermal vents as a product of circulating hydrothermal fluids precipitating metals and trace elements leached from the underlying crust. This results in lithological, structural and geochemical fingerprints that are unique to the environment of formation.

Moreover, the physical properties of the resultant mineralisation relative to the host rocks provide unique geophysical signatures.

VHMS deposits form in extensional, rift, environments with high heat flow; evidence includes:

- Subvolcanic intrusions (often with strong hydrothermal alteration and evidence of shallow emplacement);
- Synvolcanic dyke swarms (correspond with vent corridors, and typically show evidence of intrusion into wet unconsolidated sediments);
- Rock types associated with volcanic vents; and
- Rock chemistry.
- Hydrothermal (alteration) systems showing lateral and vertical zonation in both alteration minerals and metals.
    - Semi-conformable alteration: lateral fluid flow – metal leaching – patchy.
        - In mafic-dominated substrates = epidote-quartz and silicificiation.
        - In felsic-dominated substrates = sericite-quartz and silicification.
        - Semi-conformable to stratigraphy (i.e., not discordant).
    - Pipe-like or proximal alteration: vertically and laterally zoned.
        - Chlorite-(quartz) – proximal.
        - Chlorite-sericite – medial.
        - Sericite-quartz – medial to distal.
        - Quartz – distal.
- Metal-rich sediments (exhalates) with mineralogical and chemical zonations pointing to vents; these marker horizons can extend for tens of kilometres away from deposits.

Field mapping and prospecting can be undertaken to identify rock sequences that may be amenable to hosting VHMS mineralisation, in conjunction with techniques such as whole rock, rare earth and trace element geochemical fingerprinting as a guide to the likely tectonic setting of the host stratigraphy. Additional, more detailed field mapping and scout drilling can be utilised to identify areas of interest, including altered volcanic rocks, syngenetic fault structures and proximal-to-vent volcanic facies.

The accumulation of metals and various trace elements in the mineral deposit, the enrichment and/or depletion of a range of major and trace elements in the surrounding host rocks, and in some cases the enrichment of metals and trace elements in associated exhalite units, all lend themselves to the use of geochemical exploration techniques.

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In the case of the Kudz Ze Kayah Project this has to date included geological mapping of alteration, and soil, silt and rock chip geochemical surveys. The mineralisation itself may, as in the case of the ABM deposit, which comprises a mix of heavy, and variably magnetic and conductive mineral accumulations, be amenable to gravity, magnetic and electrical geophysical (e.g. surface, airborne and down-hole EM, IP) techniques, all of which have been utilised at the Kudz Ze Kayah Project to date.

All of these techniques have been applied with an iterative approach to identify broader areas of prospectivity followed by subsequent surveys of increasing detail until there is a target defined by multiple encouraging features from several independent datasets.

Once targets are generated, they are drilled using core drilling methods to the point that the extents of the mineralisation are known and are then infill drilled to increase geological confidence.

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5. REGIONAL GEOLOGY

The Kudz Ze Kayah Project is located within the Finlayson Lake District, a crescent-shaped area that is approximately 300 km long and 50 km wide and extends from Ross River in the north to Watson Lake in the south (Figure 5-1).

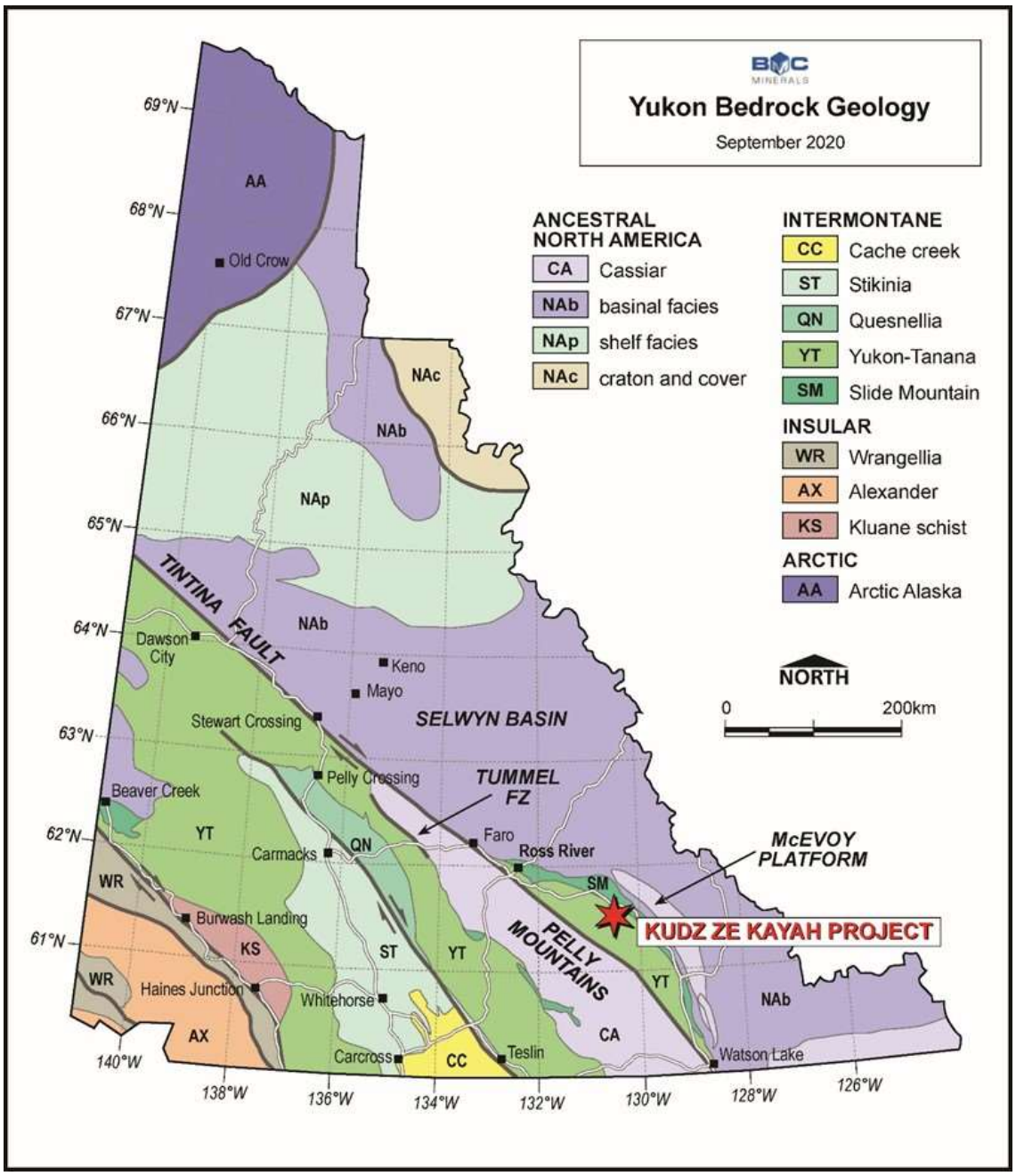


Figure 5-1: Yukon Bedrock Geology and Terrane Map
Source: BMC

The Finlayson Lake District predominantly comprises Devonian to Lower Carboniferous volcanic, intrusive, and sedimentary rocks bounded to the east by Proterozoic and Palaeozoic strata of the

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Selwyn Basin, representing the ancient North American continental margin, and to the southwest by the Tintina Fault. Rocks of the Finlayson Lake District comprise several fault- and unconformity-bound groups and formations of early Mississippian to Early Permian age. The Yukon-Tanana and Slide Mountain terranes, which together with minor allochthonous elements that make up the Finlayson Lake District, are separated from the ancient continental strata to the northeast by the Inconnu Thrust. A deposit and Finlayson Lake district geology plan is included as Figure 5-2.

The rocks of the Finlayson Lake District indicate formation and emplacement in a variety of tectonic settings, including rifted frontal arc, continental back-arc, and oceanic back-arc that range in age from 365 Ma to 275 Ma. The Finlayson Lake District is characterised by a central core of higher-grade metamorphic rocks (to lower amphibolite facies) surrounded by lower-grade, low greenschist facies rocks. This relatively simple metamorphic distribution is interpreted to be a consequence of Cretaceous dynamo-thermal events. Also occurring during the Cretaceous was the emplacement of late syn- to post-kinematic granite plutons that are regionally associated with tungsten-molybdenum-gold-bismuth occurrences and the Tsa Da Glisza emerald occurrence north of the Kona Deposit.

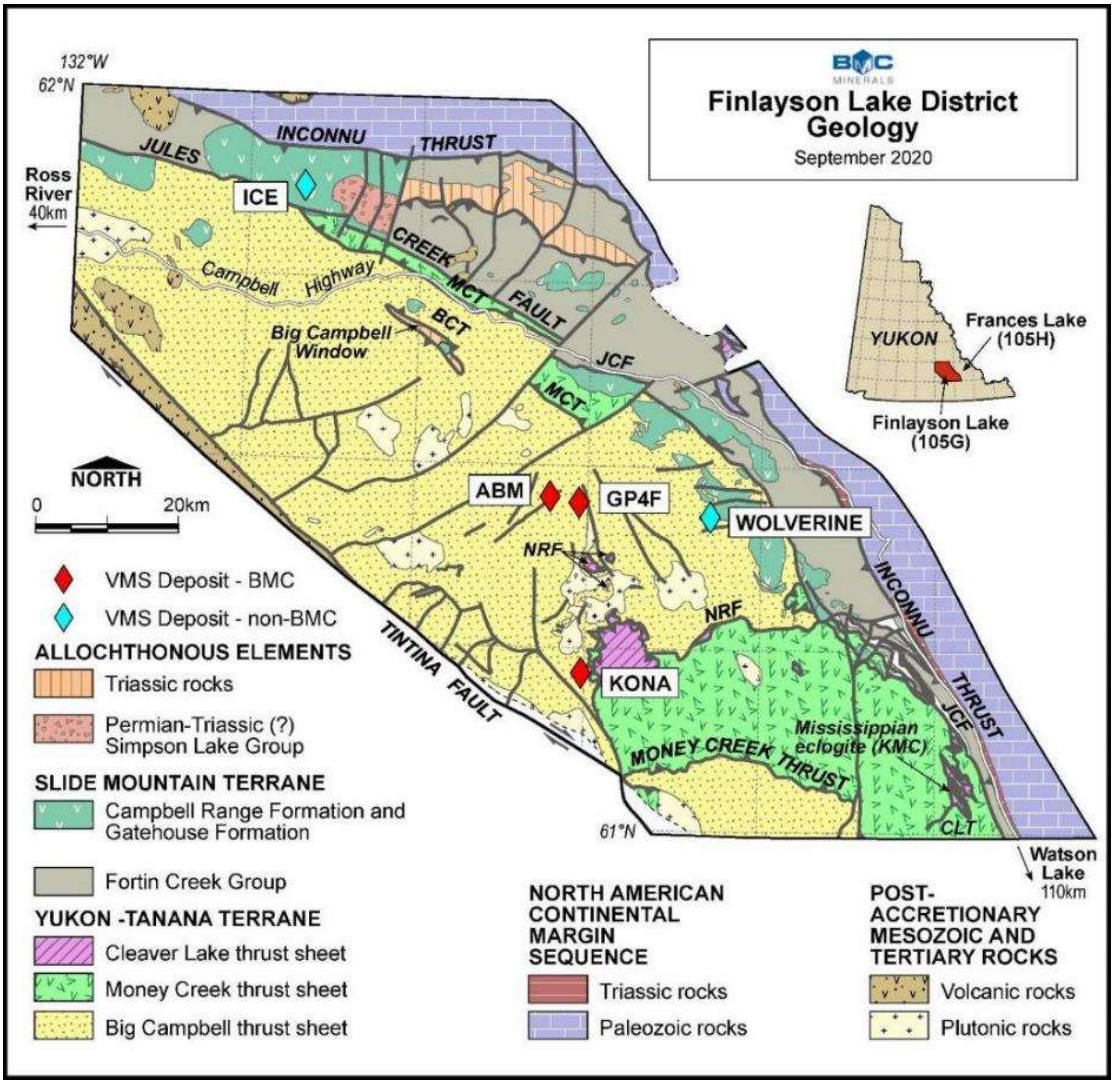


Figure 5-2: Geological map of the Finlayson Lake District
Source: BMC

5.1 Stratigraphy

Massive sulfide deposits of the Finlayson district are primarily hosted within stratigraphic components of the Big Campbell thrust sheet and within the adjacent Fire Lake thrust sheet. The exception is the Ice Deposit, which is hosted within the Campbell Range Formation, a stratigraphic component of the Slide Mountain terrane.

Rocks of the Big Campbell thrust sheet include Pre-Late Devonian quartz-rich sedimentary rocks of the North River formation; mafic and felsic volcanic, and carbonaceous clastic rocks of the Upper Devonian Grass Lakes group; Late Devonian to Early Mississippian granitic rocks of the Grass Lakes plutonic suite; carbonaceous clastic and mafic and felsic volcanic rocks of the Lower Mississippian Wolverine Lake group; and carbonaceous clastic rocks and chert of the Lower Permian Money Creek formation.

The Grass Lakes Group comprises strongly foliated and lineated layered sedimentary and volcanic rocks positioned in a roof setting above and between bodies of Early Mississippian granitic orthogneiss and weakly foliated mid-Cretaceous granite. The Grass Lakes Group has been subdivided into three formations which, from oldest to youngest, are the Fire Lake formation, Kudz Ze Kayah formation, and the Wind Lake formation. Each formation is described below:

- The Upper Devonian (≈365 Ma) Fire Lake formation is a mafic volcanic sequence comprising mainly chloritic phyllite with some carbonaceous phyllite and rare muscovite-quartz phyllite of probable felsic volcanic protolith. Intrusions and sills of mafic and serpentinised ultramafic plutonic rocks occur within the Fire Lake formation.
- Stratigraphically overlying the Fire Lake formation is the Late Devonian (≈360–356 Ma) Kudz Ze Kayah formation, a dominated by what is interpreted as sequence of felsic volcanic and volcaniclastic and sedimentary rocks. It predominantly comprises feldspar-muscovite-quartz phyllite and augen phyllite of probable felsic volcanic and volcaniclastic origin, and lesser fine-grained carbonaceous and siliciclastic sedimentary rocks.
- The Wind Lake formation forms the uppermost unit of the Grass Lakes Group and comprises carbonaceous phyllite, quartzite, and chloritic phyllite of probable alkalic mafic volcanic and intrusive protolith.

Coeval with the Kudz Ze Kayah and Wind Lake formations are peraluminous plutonic granitoids of the Grass Lakes Suite which are interpreted as the subvolcanic intrusive equivalents to the felsic volcanic host rocks of the ABM Deposit and are as old as 363 ± 3.3 Ma. These rocks are deformed and were intruded by younger, late-kinematic plutonic rocks prior to deposition of the Wolverine Lake Group. The Grass Lakes Group is unconformably overlain by rocks of the Wolverine Lake Group and comprises a basal unit of conglomerate, grit, sandstone, and carbonaceous argillite, a middle unit of quartz-feldspar phyric felsic volcanic rocks, rare chert and sandstone, and an upper unit of aphyric rhyolite, argillite, magnetite iron formation, and mafic volcanic and intrusive rocks. A second unconformity separates the Wolverine Lake Group from the overlying carbonaceous clastic rocks (carbonaceous phyllite, chert-pebble conglomerate, quartzofeldspathic sandstone to pebble conglomerate, and locally, matrix-supported diamictite) and dark grey to black chert of the Lower Permian Money Creek formation. Both the Grass Lakes Group and Wolverine Lake Group occur in the footwall of the Money Creek thrust and record two cycles in the evolution of a Late Devonian to early Mississippian ensialic back-arc. The unconformity separating these groups marks a period of deformation, uplift, and erosion. Uranium-lead geochronology places an upper age limit of 356.9 ± 0.5 Ma for the host rocks to the Wolverine deposit, and the immediate stratigraphic hangingwall is dated at 346 ± 2.2 Ma, indicating that Wolverine is younger than Kudz Ze Kayah. The Campbell Range formation is a mafic-dominated sequence comprising basalt, chert, and argillite which

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unconformably overlies rocks of the Wolverine Lake Group. Radiolarians and c. 273–274 Ma U-Pb ages on gabbros and plagiogranites indicate a Pennsylvanian to Permian age. The rocks of the Finlayson Lake District indicate formation and emplacement in a variety of tectonic settings, including rifted frontal arc, continental back-arc, and oceanic back-arc that range in age from 365 Ma to 275 Ma. The Finlayson Lake District is characterised by a central core of higher-grade metamorphic rocks (to lower amphibolite facies) surrounded by lower grade, low greenschist facies rocks. This relatively simple metamorphic distribution is interpreted to be a consequence of Cretaceous dynamothermal events. Also occurring during the Cretaceous was the emplacement of late syn- to post-kinematic granite plutons that are regionally associated with W-Mo-Au-Bi occurrences and the Tsa Da Glisza emerald occurrence north of the Kona Deposit.

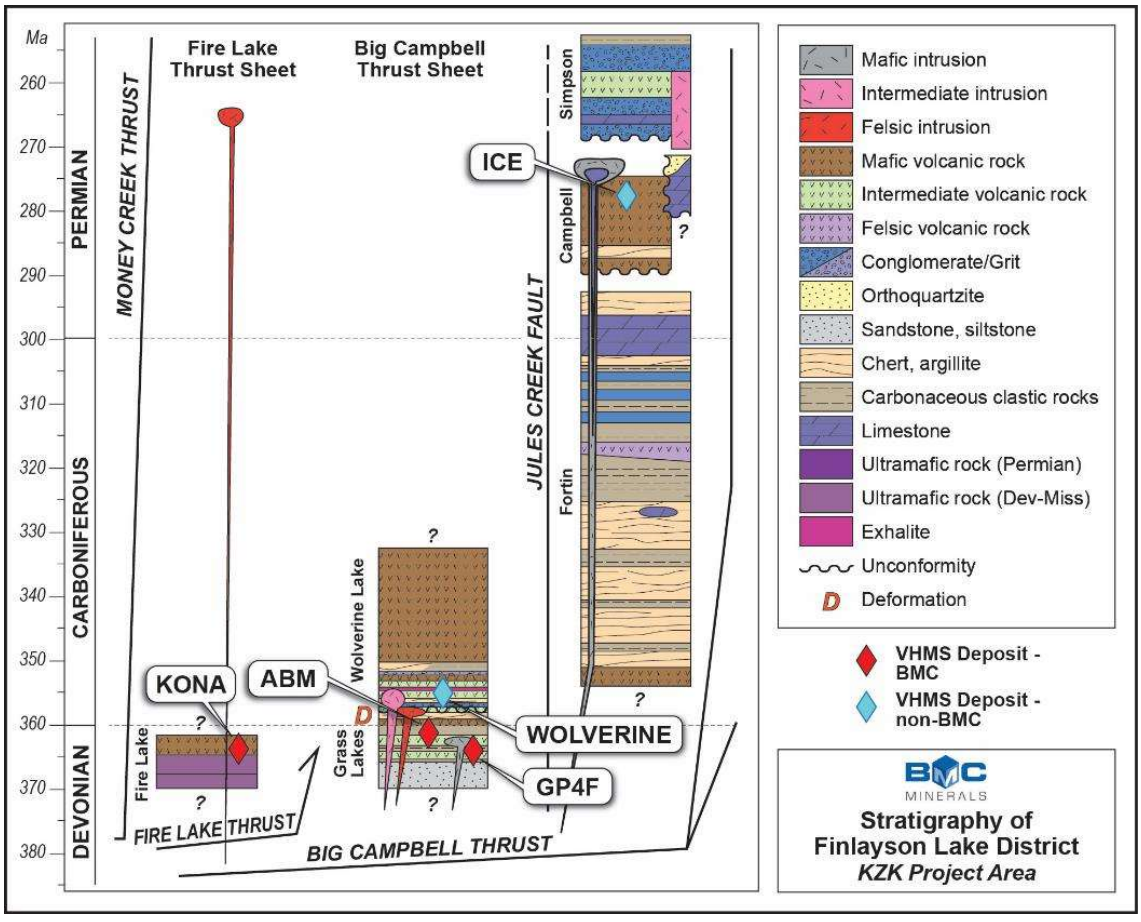


Figure 5-3: Stratigraphy of the Finlayson Lake District, showing location of VHMS deposits
Source: BMC

5.2 Mineralisation

Regionally, significant VHMS deposits have been discovered in the Finlayson Lake District from 1994 to 1998 and, to date, at least 41 VHMS occurrences and five deposits have been identified at different stratigraphic levels within the Finlayson Lake District. Figure 5-2 shows the location of the main base metal deposits of the district against the mapped tectonostratigraphic subdivisions.

Five deposits; ABM, GP4F, Kona, Ice and Wolverine, collectively contain more than 45 Mt of base metal-rich massive sulfide mineralisation. Within adjacent properties, the Wolverine and Ice deposits

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are the most significant of these and are considered material to the exploration potential of BMC's tenements.

Figure 5-4 is a schematic of the ancient Earth's crust that places these deposits into the tectonic setting in which they are interpreted to have formed. The four tectonic settings of interest and the associated deposits are summarised below:

- *Kuroko-type*: Represented by the ABM zinc-lead-copper-silver-gold rich massive sulfide deposit.

  ABM occurs within the predominantly felsic volcanic rocks that comprise the Kudz Ze Kayah formation.
- *Besshi-type*: Represented by the Kona copper-cobalt-gold rich massive sulfide deposit.

  Kona is interpreted as the stratigraphically oldest of the massive sulfide deposits, hosted within mafic volcanic rocks of the Fire Lake Formation. Kona is interpreted to be situated at the transition from mafic volcanic rocks to overlying turbiditic sedimentary rocks emplaced in a forearc setting.
- *Bathurst-type*: Represented by the Wolverine zinc-lead-copper-silver-gold rich massive sulfide deposit.

  It is hosted by rhyolitic volcanic rocks and carbonaceous argillite of the Wolverine Formation at a stratigraphic position above a regional unconformity and higher than both the ABM and GP4F deposits. As the Wolverine Deposit is hosted by graphitic shales and lesser felsic volcanic and volcaniclastic rocks, it may alternatively be classified as a volcanic-sediment-hosted massive sulfide (VSHMS) deposit.
- *Cyprus-type*: Represented by the Ice copper-gold rich massive sulfide deposit.

  Ice is not on BMC's tenure and is hosted within late Palaeozoic mafic volcanic and associated sedimentary rocks of the Campbell Range Formation.

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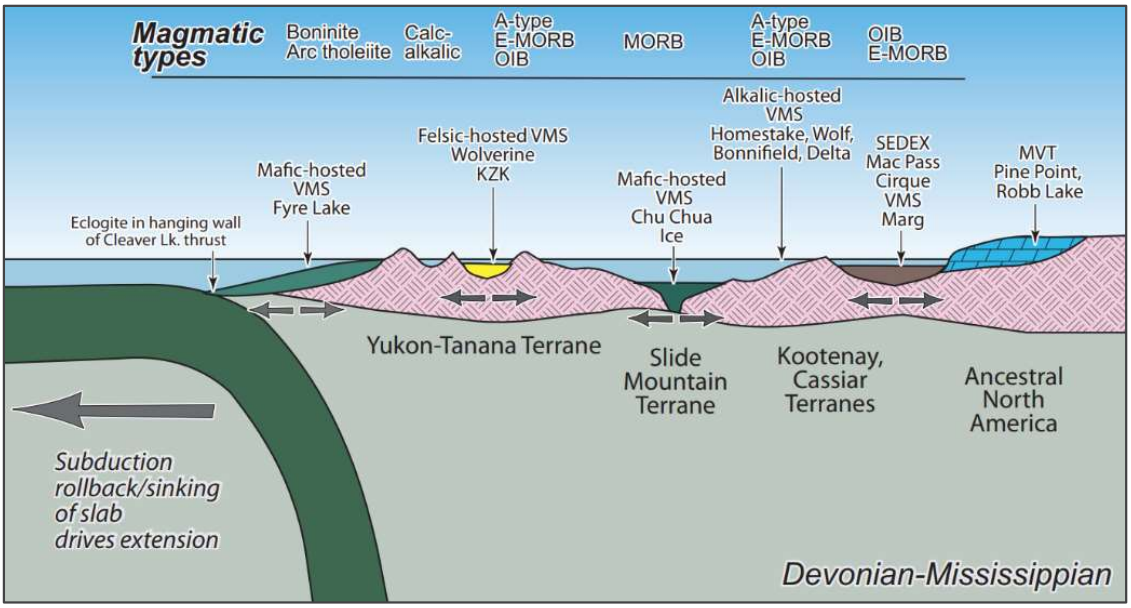


Figure 5-4: Interpreted Tectonic Setting of the Mineral Deposits
Source: Nelson and Colpron (2007)[12]

Although interpreted to have been deposited in similar tectonic environments, a range of recent studies undertaken on the mineralisation and host rocks of the Wolverine and ABM Deposits highlight key features, which clearly differentiate the two mineralisation events, as summarised in Table 5-1.

Table 5-1: Summary of key mineralisation event features.

Features	Wolverine deposit	ABM Deposit	Comments
Age	347–346 Ga (Piercey et al., 2008)	362.4–362.9 Ga (Manor and Piercey et al., 2018)	Approximately 16 Ma age difference and separated by mapped unconformity
Metal source (Pb isotopes)	1.7 Ga (Proterozoic) (Peter et al., 2007)	approximately 3.14 Ga (Archaean) (Peter et al., 2007)	Different basement metal sources
Host rocks	Carbonaceous shale dominant	Felsic volcanic and volcaniclastic dominant	Markedly different host rocks to mineralisation
Selenium source (Se isotopes)	Footwall and coeval carbonaceous shales (broad and strongly negative $\delta^{82}Se_{NIST}$) (Layton-Matthews et al, 2013)[13]	Magmatic (leaching or degassing) (narrow and mildly negative $\delta^{82}Se_{NIST}$) (Layton-Matthews et al, 2013)	Different host rock/basement source control on selenium content of mineralisation

Source: BMC

[12] Noting that these authors have not consented to the use of their technical report in this Report, but it is included as per ASIC RG55 and Instrument 2016/72.

[13] Noting that these authors have not consented to the use of their technical report in this Report, but it is included as per ASIC RG55 and Instrument 2016/72.

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6. LOCAL GEOLOGY AND MINERALISATION

The KZK Property within which the ABM Deposit is located, is dominated by outcrop of the Grass Lakes Group. The surface geology of the property was initially mapped by Cominco in 1996 and subsequently by BMC in 2017 (Figure 6-1).

The stratigraphy trends easterly, dips moderately to the north-northeast, and is interpreted as predominantly right way up except locally, where it may be overturned in tight, mesoscale F_2 folds.

The rocks are generally overprinted by greenschist facies metamorphism and a penetrative deformation fabric.

The property has been crosscut by north-to-northeast trending brittle faults (e.g. Fault Creek and East Fault), which cut across all stratigraphic units. These faults can be traced as trends in aeromagnetic data, and structures of similar timing and orientation can be readily identified in regional mapping datasets.

6.1 Stratigraphy

6.1.1 Surficial Geology and Overburden

Glacial sediments comprising ablation till have been mapped in the valley floor, locally to 30 m in thickness and progressively thinning up the valley slopes. Several small eskers and a glaciofluvial terrace have also been identified in the Kudz Ze Kayah Project area and may provide a source of construction aggregate. An active alluvial fan is present at the confluence of Geona and Fault creeks south of the ABM Deposit area. Outcrop is limited.

6.1.2 Bedrock Geology

The Wind Lake formation outcrops on topographic highs to the west, north and east of the ABM Deposit. It is encountered in holes collared above the Krakatoa Zone and eastern parts of the ABM Zone where the Wind Lake formation stratigraphy is juxtaposed against the Kudz Ze Kayah formation by late faulting.

The Wind Lake formation comprises undifferentiated carbonaceous and siliceous mudstone, siltstone and chert that is locally intercalated fine-grained mafic volcaniclastic units occurring as massive intervals up to 7 m in thickness.

The mafic volcaniclastic rocks are interpreted to be epiclastic in nature, derived from a distal mafic volcanic source and is typically rubbly in drill core. The contact with the underlying Kudz Ze Kayah formation is conformable.

The Kudz Ze Kayah formation underlies the Wind Lake formation in the vicinity of the ABM Deposit and is host to the massive sulfide mineralisation. The Kudz Ze Kayah formation is here informally separated into a lower sediment and mafic volcanic dominant unit (lower Kudz Ze Kayah formation) and an upper felsic volcanic dominant unit (upper Kudz Ze Kayah formation) (Figure 6-3).

The upper Kudz Ze Kayah formation comprises a thick sequence of felsic volcanic schist interbedded with variably carbonaceous metasedimentary and calcareous mafic schist units in the vicinity of ABM. Although in places recognisable, primary volcanic and sedimentary textures in these rocks have typically been poorly preserved due to the overprinting impact of hydrothermal alteration, metamorphism, and polyphase deformation. Primary textures that can be recognised in the felsic rocks hosting the ABM Deposit include fine to coarse volcaniclastic and autoclastic textures, peperitic textures, and massive coherent units with flow banding. Closer to the overlying Wind Lake formation the upper Kudz Ze Kayah formation is dominated by finer grained stratified volcaniclastic units.

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By way of contrast, the felsic volcanic stratigraphy immediately east of the Fault Creek Fault is markedly different to the host rocks of the ABM Deposit, comprising a sequence of stratified felsic volcaniclastic units. Utilising the base of the conformable Wind Lake formation as a marker unit, both the East Fault and Fault Creek Fault are interpreted have originated as faults that were broadly synchronous with mineralisation. The Fault Creek Fault is interpreted to mark the eastern side of a faulted basin, or graben, within which the host volcanics and sulfide mineralisation were emplaced. The syngenetic faults were then reactivated during subsequent deformation events.

Mafic intrusive rocks are also present within in the upper Kudz Ze Kayah formation, comprising numerous approximately 0.5–5 m thick dykes and sills, with a large (to 50 m thick) and more continuous mafic sill located in the footwall to massive sulfide mineralisation of both the ABM Zone and the shallower lenses of the Krakatoa Zone. This sill also hosts minor sulfide mineralisation beneath the ABM Zone and a significant component of the massive sulfide mineralisation that comprises the Krakatoa Zone.

The Grass Lakes plutonic suite is interpreted as a subvolcanic intrusive equivalent of the felsic volcanics of the Kudz Ze Kayah formation.

The stratigraphy trends easterly, dips moderately to the northeast and is interpreted as predominantly right way up except locally where it may in places be overturned in tight, mesoscale F2 folds. The rocks are generally overprinted by greenschist facies metamorphism and a penetrative deformation fabric, and north to northeast trending brittle faults cut across all stratigraphic units.

6.2 Mineralisation

The upper Kudz Ze Kayah formation is host to the ABM Deposit and Rhyolite Peak mineralisation and lower Kudz Ze Kayah formation is host to the GP4F Deposit (Figure 6-1). Mineralisation at ABM, Rhyolite Peak and GP4F is broadly conformable with the local stratigraphy, whereas mineralisation at Fuego and Kuril appears to transgress the local stratigraphy.

The ABM Deposit (comprising the ABM Zone and Krakatoa Zone) is interpreted to have formed through the mixing of heated metalliferous hydrothermal fluids with cold ambient seawater within a felsic pile at a depth of 10–100 m below the ancient seafloor.

6.2.1 ABM Zone

The massive sulfide of the ABM Zone is up to 39 m in true thickness, extending approximately 700 m along strike and approximately 500 m down dip. It dips to the north-northeast at approximately 35° near surface, transitioning to a dip of approximately 15° at around 200 m depth below the valley floor. The up-dip extent of the deposit is truncated by erosion and covered by approximately 2–20 m of glaciofluvial overburden.

Massive sulfide mineralisation occurs as several stacked massive sulfide lenses to the west, transitioning to a single massive horizon at around 415,025 mE and extending to approximately 415,250 mE, where it is then truncated by the East Fault, a re-activated syn-mineralisation fault.

Stockwork and disseminated mineralisation are present equally in both the hangingwall and the footwall to massive sulfides and, to a lesser degree, between the massive sulfide lenses.

The sulfide mineralisation is dominated by pyrite, sphalerite, pyrrhotite (±marcasite), galena and chalcopyrite, with minor arsenopyrite and a range of sulfosalts (predominantly comprising tennantite-tetrahedrite and freibergite). The up-dip part of the ABM Zone and most of the Krakatoa Zone have elevated sulfosalt content relative to the remainder of the deposit.

Illustrations of the nature of the sulfide mineralisation are presented in Figure 6-2.

6.2.2 Krakatoa Zone

Mineralisation at Krakatoa is broadly concordant with the stratigraphic layering of the host Kudz Ze Kayah formation rocks and dips at 35° to the north-northeast extends over approximately 200 m of strike, at least 500 m down dip, and up dip to the base of glacial overburden which is approximately 30 m thick.

Host rock types and alteration styles associated with Krakatoa Zone mineralisation are like those encountered in the ABM Zone. The key difference is the degree of mineralisation associated with a mafic sill, which below the ABM Zone is only poorly mineralised. Mineralisation is bound to the west by the East Fault, to the east by the Fault Creek Fault and currently remains open at depth beyond the down-dip extent of the mafic sill.

Massive sulfide mineralisation of the Krakatoa Zone occurs within three principal mineralised horizons:

- Upper Lens – broadly interpreted as the stratigraphic equivalent to the ABM Zone.
- Main Lens – the major component of the Krakatoa Zone with a true thickness of up to 22 m.
- Lower Lens – less pronounced and semi-continuous.

The Main lens comprises the bulk of mineralisation at Krakatoa, with massive sulfide occurring both within the felsic volcanics immediately beneath the mafic sill and within the mafic sill, after replacement of enclaves of felsic volcaniclastics and/or replacement of the mafic sill itself.

The surface projection of the ABM and Krakatoa Zones are shown in Figure 6-4.

The following extended and schematic cross-sections A-A’ (Figure 6-6), B-B’ (Figure 6-5) and C-C’ (Figure 6-7) show representative drill holes and intercepts for each of the deposits.

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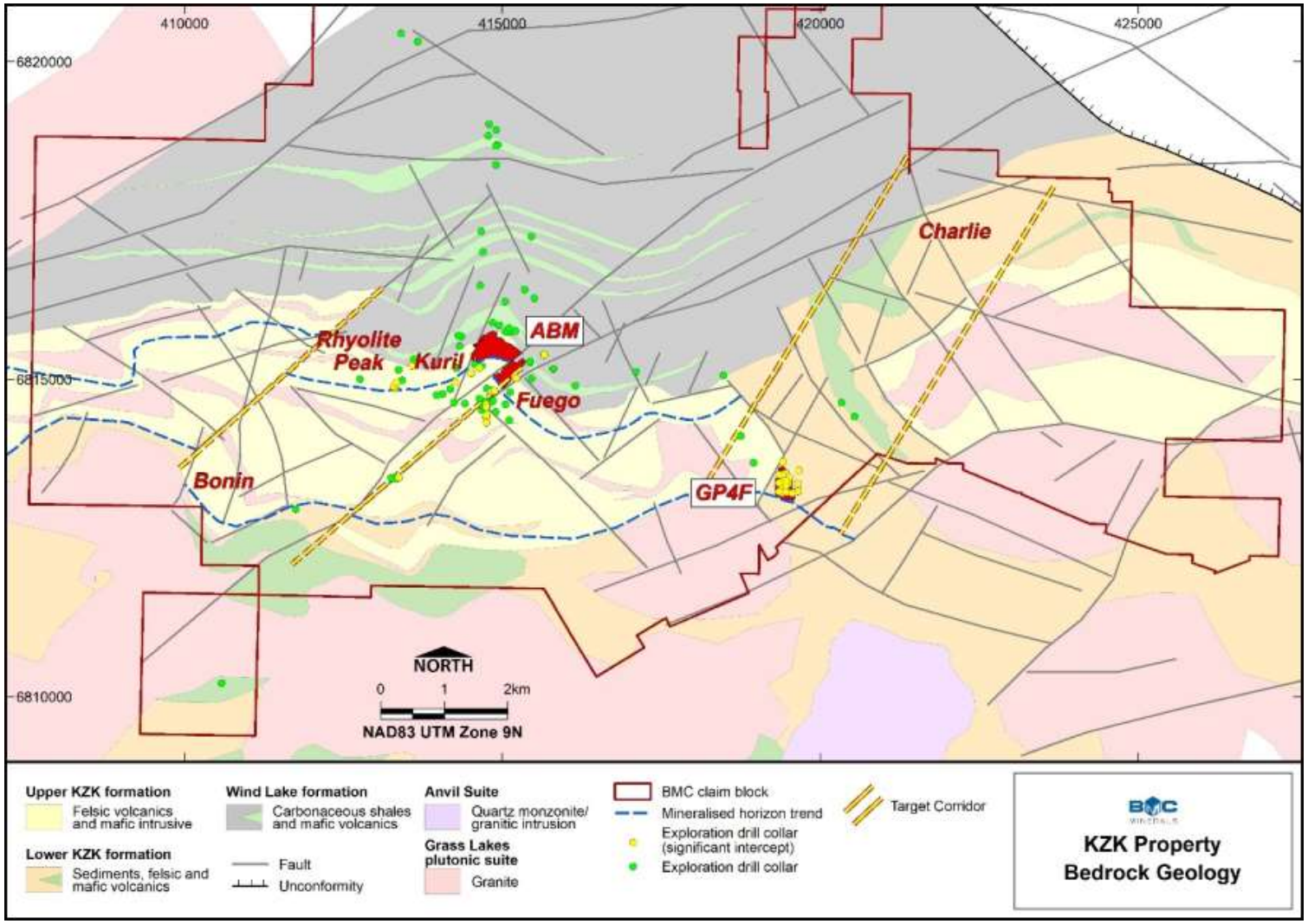


Figure 6-1: Interpreted bedrock geology of the KZK Property.

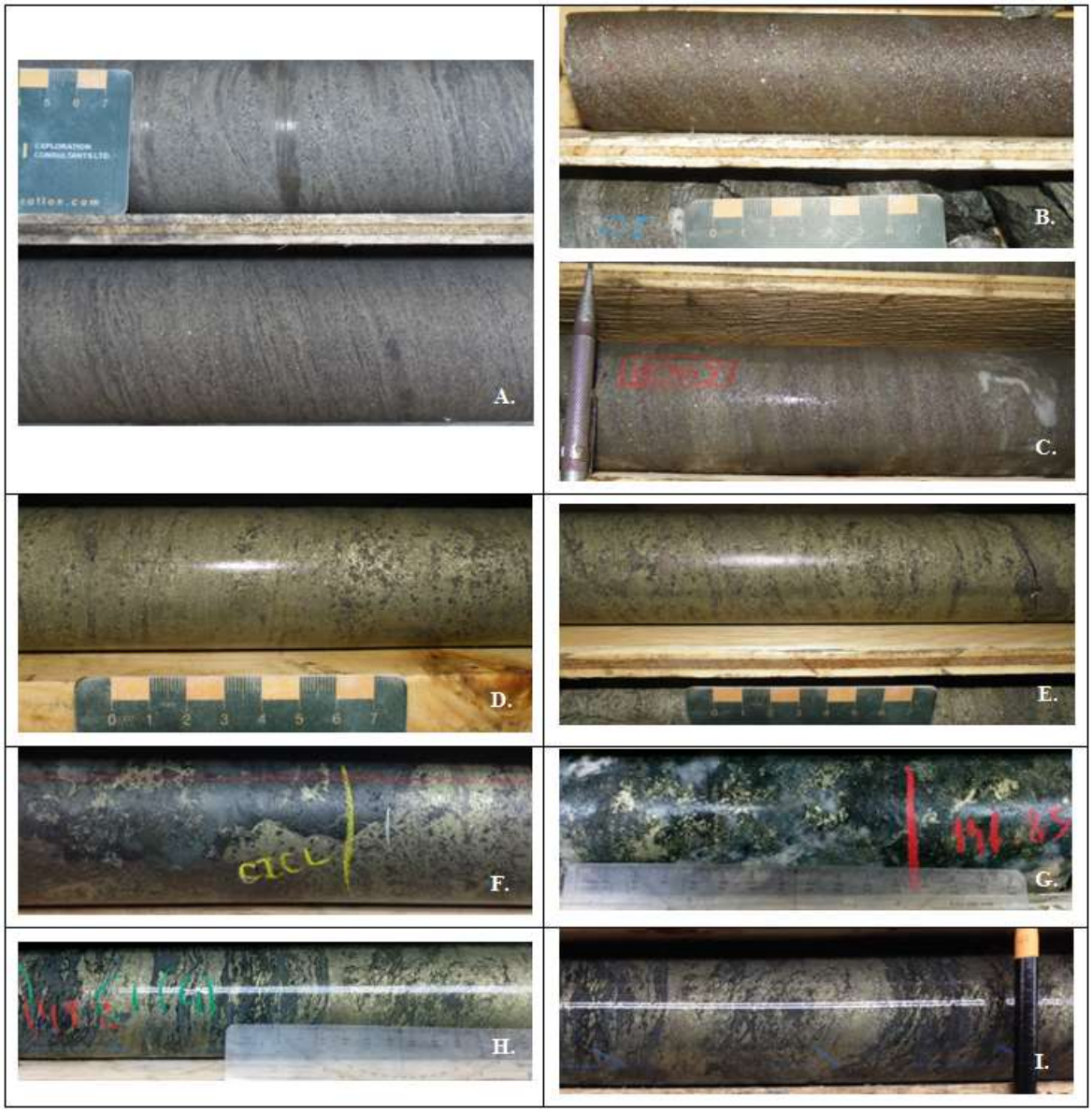


Figure 6-2: Photographs of ABM Deposit massive and disseminated sulfide types (Source: Hughes and Baknes, 2015)[14]

Photo A: medium-grained magnetite (10-20%) forming thin bands within massive pyrite (80-90%).

Photos B and C: disseminated red-brown sphalerite (20-40%) in medium- to coarse-grained pyrite (20-30%) and quartz-carbonate gangue.

Photos D and E: massive chalcopyrite (60-80%) intergrown with clots and narrow bands of pyrrhotite (10-30%).

Photos F and G: coarse-grained net-textured chalcopyrite (5-15%) and pyrrhotite (10-20%) associated with strong chlorite alteration and quartz-carbonate gangue.

Photos H and I: deformed stringer-style chalcopyrite-pyrrhotite mineralisation in intense chlorite-cordierite alteration (10-20% Cpy; 20-30% Po).

[14] Noting that these authors have not consented to the use of their technical report in this Report, but it is included as per ASIC RG55 and Instrument 2016/72.

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Table 6-1: Assays for core in Figure 6-2

Picture	Hole	From	To	Cu (%)	Pb (%)	Zn (%)	Ag (ppm)	Au (ppm)	SampleID	SampleType
A	K15-270	143.1	143.9	No assays					B00265760	Metallurgical Sample
B	K15-273	107.2	108	0.75	2.14	6.98	300	2.64	B00268866	Half Core
C	K15-266	76	77	No assays					B00268067	Metallurgical Sample
D	K15-273	92.2	93	10.7	0.09	2	265	2.52	B00268847	Half Core
E	K15-273	95	96	5.14	0.3	1.56	161	2.07	B00268852	Half Core
F	K15-281	180.16	180.84	5.58	0.02	0.52	47.8	0.953	B00268281	Half Core
G	K15-264	146.85	146.85	1.7	0.01	0.13	40.7	0.209	B00264951	Half Core
H	K15-264	149.2	149.9	9.3	0.05	0.6	190	3.41	B00264954	Half Core
I	K15-264	149.2	149.9	9.3	0.05	0.6	190	3.41	B00264954	Half Core

Source: BMC

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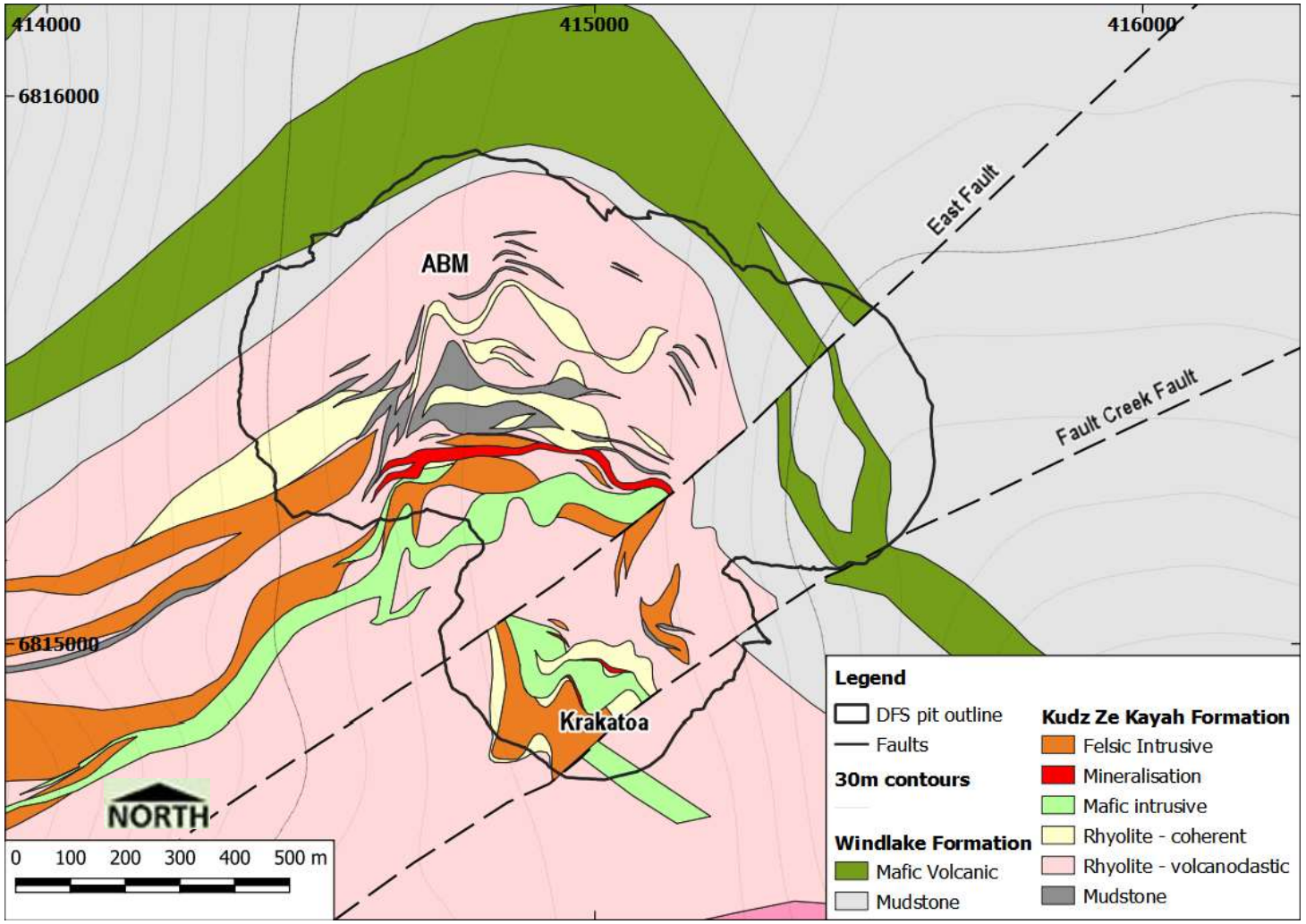


Figure 6-3: Simplified bedrock geology map of the ABM Deposit area, showing the ABM and Krakatoa Zones
Source: BMC

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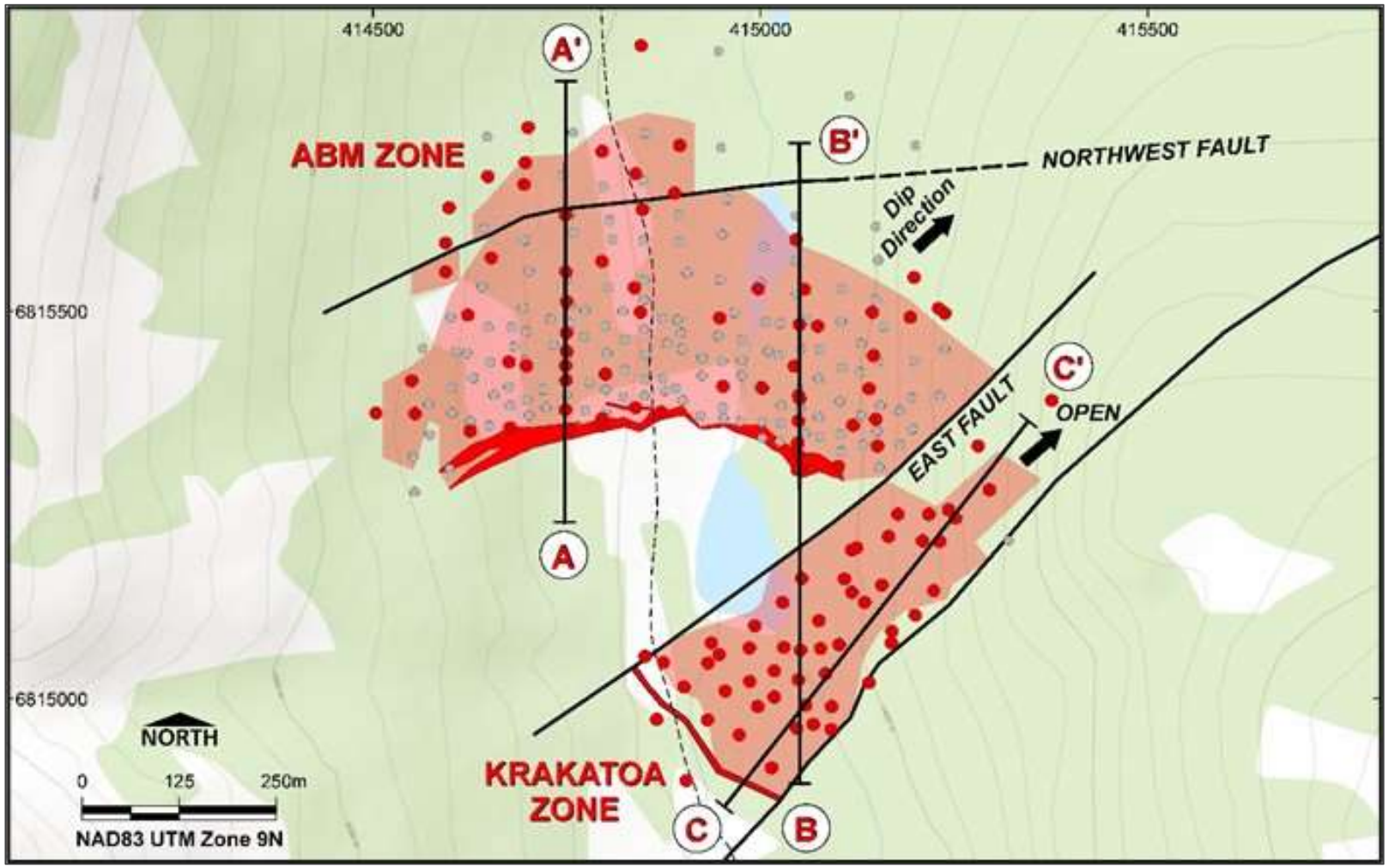


Figure 6-4: Plan view of ABM Deposit showing both ABM and Krakatoa zones.
Source: BMC

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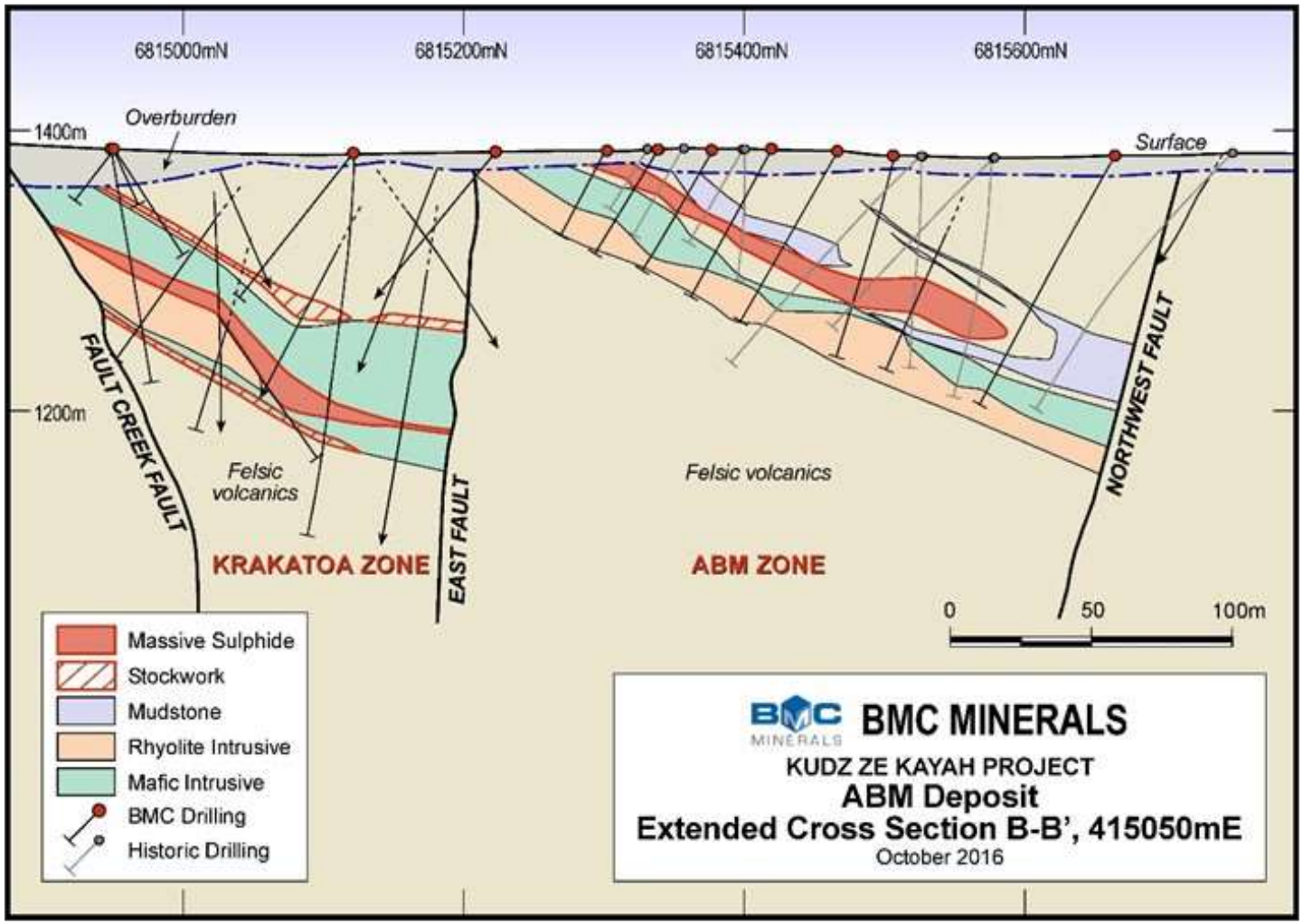
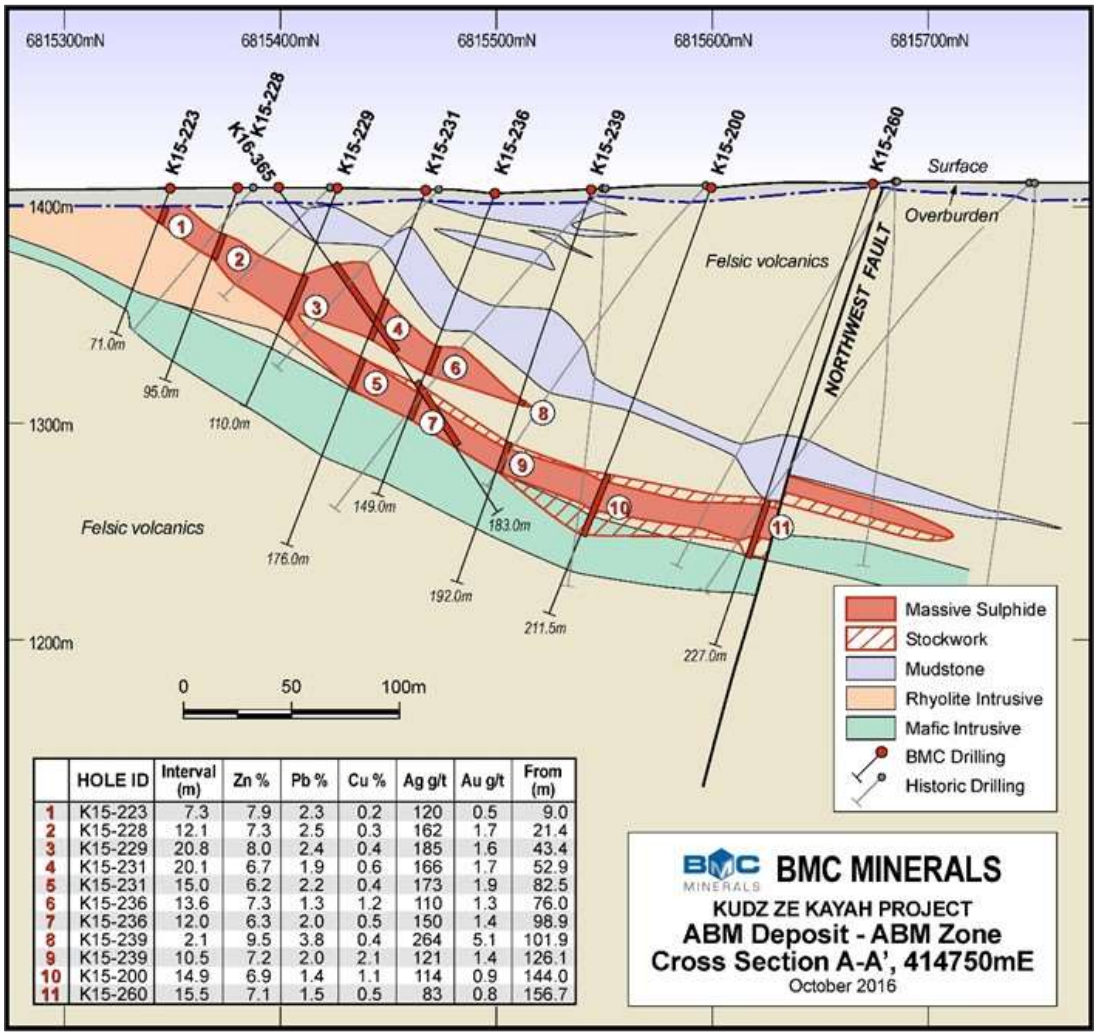


Figure 6-5: Schematic cross-section B-B' 415,050 mE showing ABM and Krakatoa zones.
Source: BMC

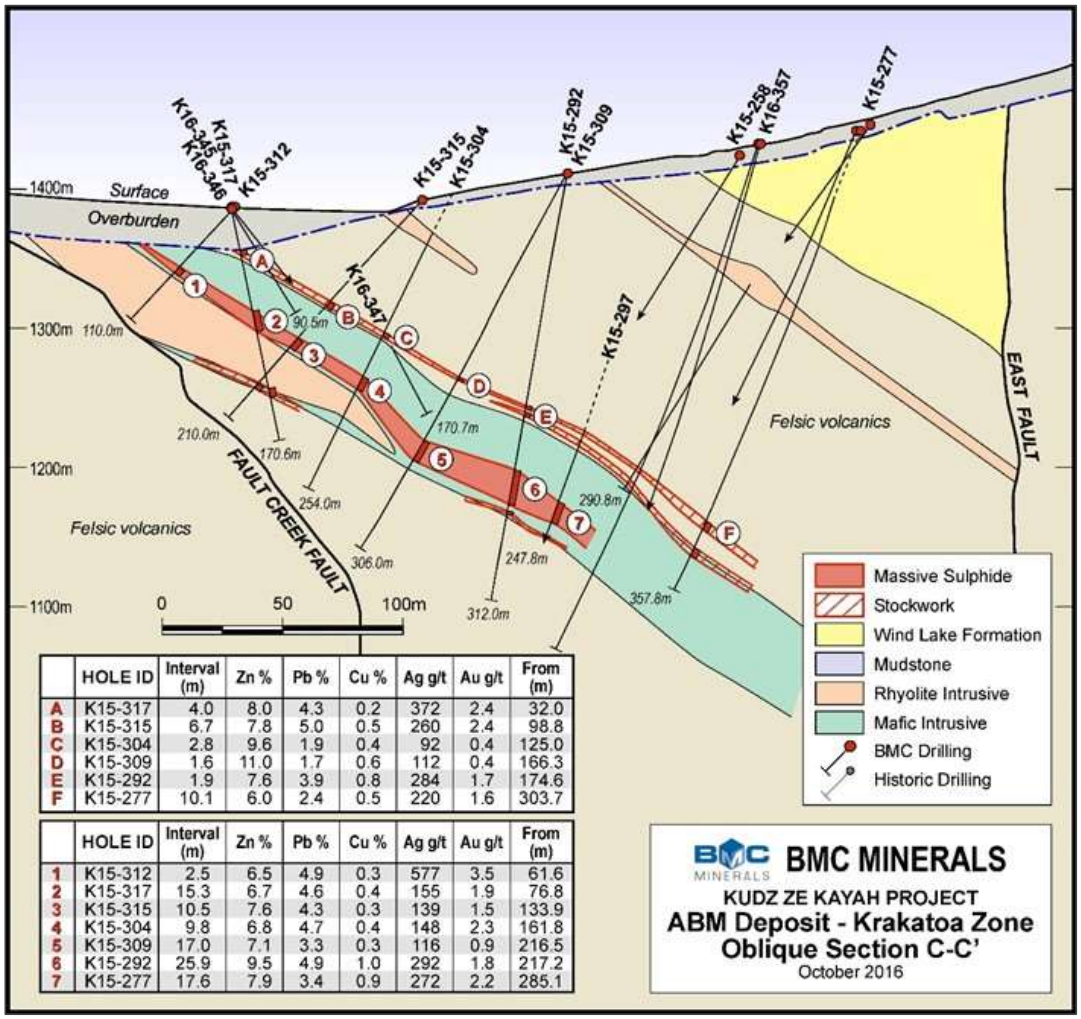
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	HOLE ID	Interval (m)	Zn %	Pb %	Cu %	Ag g/t	Au g/t	From (m)
1	K15-223	7.3	7.9	2.3	0.2	120	0.5	9.0
2	K15-228	12.1	7.3	2.5	0.3	162	1.7	21.4
3	K15-229	20.8	8.0	2.4	0.4	185	1.6	43.4
4	K15-231	20.1	6.7	1.9	0.6	166	1.7	52.9
5	K15-231	15.0	6.2	2.2	0.4	173	1.9	82.5
6	K15-236	13.6	7.3	1.3	1.2	110	1.3	76.0
7	K15-236	12.0	6.3	2.0	0.5	150	1.4	98.9
8	K15-239	2.1	9.5	3.8	0.4	264	5.1	101.9
9	K15-239	10.5	7.2	2.0	2.1	121	1.4	126.1
10	K15-200	14.9	6.9	1.4	1.1	114	0.9	144.0
11	K15-260	15.5	7.1	1.5	0.5	83	0.8	156.7

Figure 6-6: Schematic cross-section A-A' 414,750 mE looking west – ABM Zone/Source: BMC

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	HOLE ID	Interval (m)	Zn %	Pb %	Cu %	Ag g/t	Au g/t	From (m)
A	K15-317	4.0	8.0	4.3	0.2	372	2.4	32.0
B	K15-315	6.7	7.8	5.0	0.5	260	2.4	98.8
C	K15-304	2.8	9.6	1.9	0.4	92	0.4	125.0
D	K15-309	1.6	11.0	1.7	0.6	112	0.4	166.3
E	K15-292	1.9	7.6	3.9	0.8	284	1.7	174.6
F	K15-277	10.1	6.0	2.4	0.5	220	1.6	303.7

	HOLE ID	Interval (m)	Zn %	Pb %	Cu %	Ag g/t	Au g/t	From (m)
1	K15-312	2.5	6.5	4.9	0.3	577	3.5	61.6
2	K15-317	15.3	6.7	4.6	0.4	155	1.9	76.8
3	K15-315	10.5	7.6	4.3	0.3	139	1.5	133.9
4	K15-304	9.8	6.8	4.7	0.4	148	2.3	161.8
5	K15-309	17.0	7.1	3.3	0.3	116	0.9	216.5
6	K15-292	25.9	9.5	4.9	1.0	292	1.8	217.2
7	K15-277	17.6	7.9	3.4	0.9	272	2.2	285.1

Figure 6-7: Schematic oblique cross-section C-C' looking northwest - Krakatoa Zone/Source: BMC

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6.3 Alteration

At the deposit scale, massive sulfide mineralisation is surrounded by an alteration halo that changes in a broadly systematic fashion moving out from the mineralisation:

- Massive sulfide to stringer and disseminated sulfide to disseminated sulfide dominated pyrite with minor pyrrhotite.
- Ankerite/siderite to calcite.
- Albite/celsian/chlorite to sericite/muscovite.

Hydrothermal alteration extends into the footwall, hangingwall and down dip of massive sulfide. The alteration distribution and intensities vary to some degree with the underlying lithology (mafic vs felsic) and is locally variable (millimetre to tens of metre scale).

In addition to this pervasive alteration, restricted zones of cordierite alteration are present with cordierite spatially associated with proximal chlorite alteration as well as in more distal fine-grained carbonaceous and tuffaceous mudstones and ash tuffs with or without chlorite. The mafic intrusives, especially at Krakatoa, are locally characterised by elevated arsenic within calcite veining.

Syn- to post-deformation quartz ± calcite veining is observed throughout the drilling. Distal to the massive sulfide, where the syn-mineralisation alteration is subdued, these veins are variably associated with haloes of phyllosilicate (sericite, biotite), calcite and tourmaline. This veining is interpreted to be related to the emplacement of Cretaceous intrusions in the district.

6.4 Structure and Metamorphism

Host rocks to the ABM Deposit have been deformed and metamorphosed to upper greenschist to lower amphibolite facies and, almost without exception, display one or more of the following penetrative deformation fabrics:

- S_0 - most commonly recognised as bedding in mudstone and tuff units in the Wind Lake formation, and locally within units of the Kudz Ze Kayah formation
- S_1 - typically subparallel to the original bedding (S_0) with a mean dip direction of 007° and a dip of 24.3°. The S_1 foliation may represent a compaction fabric.
- S_2 - crenulation cleavage defined by fine folds of S_1 generally strikes similarly to S_1 but is more steeply dipping to the north or northeast. Development of S_2 crenulations is highly localised and varies from intense to broadly-spaced. More felsic and well foliated rocks with abundant sericite tend to exhibit the most intense and finely developed D_2. F_2 folds are typically mesoscale, south-verging, and appear to fold S_0 and S_1 only locally.
- S_3 kink bands - are rare and defined by cm-scale kinking of the main (S_1) schistosity. Although based on a small subset of data, S_3 planes have two dominant orientations, subvertical with a northwest-southeast strike and sub-horizontal and all their hinge lines plunge gently to moderately to the north suggesting conjugate sets of kink bands. Small, presumably parasitic, folds are observable in drill core, but no large-scale fold patterns have been identified in the field. The current interpretation is of a tilted stratigraphy with faulting the main deformation.

Several possible small-scale growth faults have been identified within the Krakatoa Zone, striking west-northwest and dipping steeply north-northeast. These structures have been identified based on apparent offsets and rapid changes in the thickness and extent of coherent mafic and felsic intrusive bodies, rapid changes in the thickness and extent of massive sulfide mineralisation, and localised zones of elevated copper-gold mineralisation and intense chlorite alteration. It is most likely that the interpreted growth faults predate mineralisation and were later conduits for hydrothermal fluids during emplacement of ABM sulfide mineralisation.

Host rocks, mineralisation and pervasive deformation fabrics are cut by two significant late faults; East Fault and Fault Creek Fault, both of which are filled with cataclasite (including sulfide clasts). These faults can be traced as trends in aeromagnetic data for kilometres to tens of kilometres.

The East Fault and Fault Creek Fault define a fault-block containing the massive sulfide-bearing volcanic and sedimentary package that comprises the Krakatoa Zone. This fault block is dissected by several smaller-scale late-stage faults that do not appear to extend beyond the larger bounding faults and have offsets of less than 20 m. These smaller-scale structures are characterised by up to several metres core length of cataclasite and gouge.

6.5 Metallurgical Domains

Sulfide mineralisation can be readily categorised based on texture, style, and significant mineral composition. Stringer vein, stockwork and disseminated sulfide style mineralisation (MET8) occurs in both the footwall and hangingwall to massive sulfide mineralisation. Massive sulfide mineralisation can be visually separated into pyrrhotite-magnetite-dominant (MET2-4) and pyrite-dominant (MET5-7) domains.

Examination of geochemical data from core drilling (Table 6-2) demonstrates a clear geochemical differentiation between the domains.

MET2-4:

- Elevated copper, iron, bismuth, selenium
- Moderate lead, zinc, antimony
- Reduced silver, gold, arsenic, barium, mercury.

MET5-7:

- Elevated silver, gold, arsenic, barium, mercury, antimony
- Moderate iron, lead, zinc, bismuth, selenium
- Reduced copper.

MET8:

- Elevated copper
- Low silver, gold, iron, lead, zinc, arsenic, barium, bismuth, mercury, antimony, and selenium.

When the geochemical data is normalised against the iron content, to consider the increased gangue component, sulfide mineralisation in the MET8 domain is also seen to be characterised by elevated copper, bismuth, selenium and moderate silver, gold, lead, zinc, arsenic, barium, mercury, antimony in a similar fashion to the pyrrhotite-magnetite-rich MET2-4 domain.

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Table 6-2: Geochemical data by metallurgical domain

Metallurgical Domain	Statistic	Ag ppm	Au ppm	Cu %	Fe %	Pb %	S %	Zn %	As ppm	Ba ppm	Bi ppm	Hg ppm	Sb ppm	Se ppm
Massive Sulfide	Number	1,823	1,812	1,823	1,823	1,823	866	1,823	1,807	1,725	1,807	1,043	1,806	1,447
	Minimum	-0.30	-0.07	-0.01	0.76	-0.01	-1.00	-0.01	-1	-1	-1.00	-1.00	-1	-1
	Maximum	1,181.50	19.16	18.00	49.50	14.90	49.20	29.60	39,740	256,805	608.00	248.00	9,927	1,290
	Mean	164.76	1.63	0.92	29.96	1.97	31.32	6.55	3,077	17,981	50.63	24.08	596	109
	SD	113.72	1.27	1.82	10.91	1.53	13.70	3.89	3,464	32,412	54.80	27.23	726	170
	CV	0.69	0.78	1.99	0.36	0.78	0.44	0.59	1.13	1.8	1.08	1.13	1.22	1.56
Stockwork	Number	449	438	450	449	450	139	450	416	343	416	205	416	250
	Minimum	-0.30	-0.07	-0.01	1.50	-0.01	-1.00	0.00	-1	-1	-1.00	-1.00	-1	-1
	Maximum	619.20	4.65	12.60	48.00	8.35	44.45	17.35	17,892	104,896	367.00	80.10	4,146	799
	Mean	68.48	0.63	1.08	16.45	0.63	9.65	2.59	1,025	5,600	45.08	6.13	164	87
	SD	79.39	0.72	1.41	10.42	1.04	10.59	3.22	2,194	10,376	44.33	11.47	422	144
	CV	1.16	1.14	1.3	0.63	1.64	1.1	1.24	2.14	1.85	0.98	1.87	2.57	1.66
Magnetite	Number	576	576	570	576	576	576	195	566	524	566	340	566	397
	Minimum	1.60	0.02	-0.01	1.90	-0.01	-1.00	0.04	-1	2	-1.00	-1.00	-1	-1
	Maximum	859.00	5.83	10.78	49.80	6.83	48.80	18.40	20,322	70,000	696.00	66.70	3,760	1,840
	Mean	89.41	0.95	1.09	38.83	1.11	33.81	6.43	1,508	2,864	79.67	6.54	203	149
	SD	70.65	0.78	1.17	7.20	1.13	11.23	3.70	2,500	7,718	55.60	6.86	361	223
	CV	0.79	0.82	1.08	0.19	1.02	0.33	0.57	1.66	2.69	0.7	1.05	1.78	1.5

- Source: 2025 Technical Report
- Geochemical data for MET2-4 (magnetite), MET5-7 (massive sulfide) and MET8 (stockwork) domains, including all ABM and Krakatoa Zone ores.
- Abbreviations: SD = standard deviation; CV = coefficient of variation.
- Negative values shown represent levels below the detection limit for the analysis undertaken. After removing the negative sign, the value of the numeric displayed is the analytical method detection limit.

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Data derived from petrographic studies, supplemented by scanning electron microscope (SEM) and Laser Ablation Inductively Coupled Plasma Mass Spectrometry (LA-ICP-MS) studies, revealed that, both the ABM Zone sulfide mineralisation above ≈1340 mRL and the Krakatoa Zone as a whole, comprise mineralisation with a significantly elevated silver-rich sulfosalt content. In both cases, the mineralisation is pyrite-rich. Utilising these observations, ABM mineralisation was divided into five principal metallurgical domains for the purpose of metallurgical testwork:

MET2-4 (below 1,340 mRL):

- Magnetite-pyrrhotite-rich massive sulfide (pyrrhotite often partially replaced by marcasite).
- Low galena, sulfosalt and arsenopyrite content.

MET5-7 (below 1,340 mRL):

- Pyrite-rich massive sulfide, often with barite.
- Elevated galena, sulfosalt and arsenopyrite content.
- Visible gold/electrum in thin section.

MET8 (below 1,340 mRL):

- Stringer/disseminated sulfide, typically with chlorite-rich gangue.
- Similar mineralogy to MET2-4.

+1,340RL (above 1,340 mRL):

- Elevated tetrahedrite, arsenopyrite and visible gold content.
- Predominantly pyrite-rich mineralisation with minor stringer and pyrrhotite-magnetite component, often with barite.

Krakatoa:

- Elevated freibergite content.
- Predominantly pyrite-rich mineralisation with minor stringer and pyrrhotite-magnetite component, often with barite.

A summary of the relative proportion of the metallurgical domains by tonnage derived from the current Mineral Resource Estimate is summarised in Table 6-3.

Table 6-3: Summary of metallurgical domains for the ABM Deposit.

Zone	MET2-4	MET5-7	MET8	Comment
ABM Zone (All)	20%	65%	15%	Comprises 100% of ABM Zone
ABM (above 1340 m RL)	18%	75%	7%	Comprises 26% of ABM Zone
ABM (below 1340 m RL)	20%	61%	19%	Comprises 74% of ABM Zone
Krakatoa Zone (All)	9%	80%	11%	Comprises 100% of Krakatoa Zone
ABM + Krakatoa (All)	**17%**	**69%**	**14%**	**100% of ABM + Krakatoa zones**
	The + 1,340RL domain comprises 16% of combined ABM + Krakatoa Zones			

Source: BMC

6.5.1 Oxidation

Visual evidence of oxidation (iron staining), due to weathering along fractures and faults in the host rocks, typically extends to a vertical depth of around 18 m below surface and in places can be as deep as 50 m below surface.

A total of 132 core samples from 12 drill holes along the full strike of the ABM Deposit were submitted for EDTA analysis. EDTA provides a quantitative measure of the degree of oxidation by forming water-

soluble complexes with the oxidation products of sulfide minerals (Bicak and Ekmekci, 2012). Samples were collected from the just below the base of the glaciofluvial overburden to a vertical depth of approximately 60 m.

No soluble copper or zinc was identified, but a modest level of soluble lead was found to be present (maximum 668 mg/l, median 140 mg/l). A further 26 samples were also taken from the deepest part of the ABM Zone, well below any visual sign of weathering, and analysed by the same method. The analysis also returned no evidence of soluble copper or zinc but indicated a similar level of soluble lead (maximum 534 mg/l, median 197 mg/l).

This result is interpreted to indicate that soluble lead evident in the mineralisation is not the result of weathering and oxidation but is instead related to the inherent solubility of lead-rich minerals in the sulfide mineralisation. On this basis, there is no evidence of near-surface oxidation which may impact on metallurgical recoveries.

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7. MINERAL RESOURCE ESTIMATES

7.1 ABM Deposit

7.1.1 Drill Hole Data

A total of 335 core drill holes defines the ABM Deposit (55,782 m) with 241 assayed drill holes intersecting the mineralised zones at a nominal 50 m spacing on 25 m spaced north-south oriented sections extending out to 100 m on the periphery of the deposit.

The Krakatoa Zone is sampled by pierce points of 25–60 m in the central portion of the deposit to 100 m on the periphery. Holes are broadly drilled perpendicular to the mineralisation.

The ABM resource model was prepared using all drilling data available as of 11th September 2016 and includes historical drilling results as well as results from the 2015 and 2016 exploration programme.

The JORC Code Table 1 data in Appendices A–D provide details of drilling, surveying, logging, sampling, sample preparation, analysis, security, quality assurance and quality control (QAQC), and data storage and discusses them in terms of the JORC Table 1, Sections 1 and 2 criteria.

A total of 32 holes were excluded from the ABM MRE dataset, predominantly comprising metallurgical holes and/or wedges. Two holes; K95-168 and K95-169, were excluded from the MRE as the collar locations and down-hole surveys appeared questionable.

A total of 69 holes for 11,322 m were drilled during the 2024 field season with results received subsequent to the MRE. The drilling was a mix of exploration, metallurgical and geotechnical holes with 28 holes drilled within the ABM Deposit footprint. Results from these holes are consistent with holes used in the MRE and therefore will not materially alter the previous estimate.

7.1.2 Drilling Techniques

Diamond core drilling was used across the KZK Property for all resource definition and exploration drilling. Core was used to obtain high-quality samples that were logged for lithological, structural, density, and other attributes.

The ABM Zone was sampled using core drill holes at nominal 50 m spacing on 25 m north-south oriented sections extending out to 100 m on the peripheries of the deposit. The Krakatoa Zone was sampled targeting pierce points of 25 m to 60 m in the central portion of the deposit to 100 m on the peripheries. Details are presented in Appendix A.

Drilling at the ABM Deposit was completed by Cominco from 1994 through 1998 (199 holes). Since 2015, BMC Minerals Ltd completed a further 165 holes for 31,036 m at the ABM Deposit. A total of 335 diamond core drill holes were used to define the ABM Deposit and for resource estimation for 55,782 m of drilling. A total of 241 assayed drill holes intersect the interpreted mineralisation zones.

All Cominco drilling at the deposit was NQ size diamond core and was not oriented.

Drilling completed by BMC used NQ3 and HQ3 size drill core. Larger diameter core was used where wedging from parent holes to retrieve core used for metallurgical studies was required.

For ABM, 109 holes were completed using HQ3 and 57 completed using NQ3 tools. Triple tube coring with inner split tubes were used to maximise recovery.

All core was oriented from 20 m above the mineralised zone to the end of hole using the Reflex ACTII RD core orientation system.

Based on an assessment of the past reports, historical drilling results, and review of the current procedures, ERM considers the entire dataset to be acceptable for use in Mineral Resource estimation.

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7.1.3 Sampling and Sub-sampling techniques

All sulfide intersections in 1994 intersected by Cominco were sawn with an open circulation rock saw and in 1995, all samples were split by hydraulic splitter, typically into 1.5 m long samples.

Samples were sent to Cominco Exploration Research Laboratory (CERL) in Vancouver for geochemical analysis.

Samples were subjected to a three-stage crushing procedure, pulverised, and screened to ≈150 µm.

Details of the post-1995 sampling and preparation procedures have not been located, but the Competent Person considers that it is reasonable to assume that similar procedures have been followed to those used previously and ERM concurs.

During BMC's management, all sulfide intersections were sawn using an open-circulation rock saw, typically into 1.0 m long samples. Samples were sent to SGS Vancouver for analysis.

Samples were weighed, dried and crushed to 75% passing 2 mm, with a 250 g split pulverised to 85% passing 75 µm.

Details are presented in Appendix A.

7.1.4 Sample Analysis

Historical work by Comino used aqua regia digestion (and solvent extraction in the case of gold) and assaying by AAS or ICP-AES. Details are presented in Appendix A.

Durning BMC's management, gold was analysed by 30 g fire assay with an atomic absorption spectrophotometry (AAS) finish and silver analysed by inductively coupled plasma (ICP) with an AAS finish on a 2 g two-acid digest aliquot. Gold and silver over limits were triggered at Au >5 g/t and Ag >150 g/t respectively, resulting in re-analysis using a 30 g fire assay with gravimetric finish. Assay results for copper, lead, zinc, barium, sulfur, and iron were completed using a sodium peroxide fusion and ICP-AES analysis. Select samples were analysed for trace elements including As, Bi, Hg, Sb and Se using aqua regia digest and ICP-MS finish.

Sulfide intersections from exploration holes drilled in 2024 were sent to ALS in Vancouver. for analysis. Analytical techniques for gold were the same as at SGS. A suite of 48 elements including Cu, Pb, Zn and Ag were analysed using a 4-acid digest and ICP-MS finish. Over limits were analysed using in ICP-AES finish.

Details are presented in Appendix A.

7.1.5 Quality Assurance

No documented QA procedures have been located for the Cominco drilling programmes complete prior to 2015. Detailed and systematic programmes do not appear to have been in place during the Cominco drilling; however, it may be that the documentation has not yet been located.

To check for assay accuracy, 1 in 10 samples from the 1995 drill programme were selected by Cominco for 'umpire' analysis by Chemex Laboratories using the same assay methods. The gold assays compared well up to 3 g/t, however 32 of 133 analyses above this threshold showed some scatter. Silver showed good correlation at all levels.

The 2015 field QA/QC programme entailed submission of coarse blank material every 20th sample and Certified Reference Material ("CRM") every 20th sample. CRMs were selected with the aim of covering a wide range of base and precious metal grades and with a matrix similar to the mineralogy of the ABM Deposit.

Approximately 3% of samples analysed in 2015 were submitted to ALS Minerals for umpire analyses via sodium peroxide fusion and ICP-OES finish.

Additional quartz wash was inserted in the pulverizing stage where high-grade mineralisation was suspected. Quartz wash residues were retained for possible later analyses. Wet screen analyses were completed every 50th sample to ensure consistent crush size.

In addition, as part of the re-logging programme, a total of 417 half-core samples drilled by Cominco within the resource area were re-sampled by BMC and sent for chemical analysis.

Blanks

Cross contamination of samples has been monitored using coarse garden stone ('blank') sourced from a garden supplies supplier in Ontario containing negligible base and precious metals.

Data from 149 coarse blanks have been evaluated using two threshold values — 3 times the lower limit of detection (3xDL) and 10 times the lower limit of detection (10xDL). The 3xDL threshold is appropriate for exploration programmes where low-level regional geochemical anomalies are sought. The higher threshold value of 10xDL has been employed in this review. There is only one clear case of probable cross contamination involving Zn, with a blank giving a value of 0.12%.

Overall, the percentage of samples potentially affected by cross contamination is less than 1% (CSA Global, 2015).

Certified Reference Materials

CRM selection was based on trying to get coverage over a range of base and precious metal grades reflected from historical assay datasets with a minimal number of CRMs. CRM selection was significantly hampered by what was commercially available through a range of international suppliers.

Details in this section below are taken from CSA Global (2015).

Data from a total of six CRMs inserted into the sample stream by BMC were reviewed. There is a clear positive bias in data from five of the CRMs certified for Zn and for four certified for Pb (Table 7-1). In contrast, data for Cu, Ag and Au show negative biases, although this is not consistent across all CRMs certified for these elements (Table 7-1). There is no relationship between grade and Pb or Zn bias.

The base metal CRMs used by BMC are largely derived from VHMS deposits and so are considered to be matrix appropriate for the Kudz Ze Kayah Project. Ag was analysed following a 2-acid digestion whereas CDN-ME-1311 and OREAS 113 are certified for Ag by a 4-acid digestion only, and the analytical method used from GBM310-16 is not described. This may in part explain the negative bias for Ag, which is particularly pronounced in these CRMs.

CDN-ME-1311 has a high SiO_2 content which would likely lend itself to having a component of the certified metals "locked up" as inclusions in the silicates that would not be accessible with a 2-acid digest. This may explain in part the negative bias for this standard. Petrographic work consistently shows that the ABM Deposit has a much lower silicate content and a significant carbonate content, which contrasts with the CRM.

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Table 7-1: Summary of average biases from CRMs for 2015 programme

CRM	CRM Recommended Values						Average Bias (%)					
Element	Ag (ppm)	Au (ppm)	Cu %	Pb %	Zn %	Fe %	Ag	Au	Cu	Pb	Zn	Fe
CDN-ME-1311	44.90	0.84	0.47	0.30	1.12	n/a	-1.89	-1.44	-2.44	0.89	1.88	n/a
OREAS 623	20.40	0.83	1.73	0.25	1.03	13.5	-1.23	-4.69	0.36	3.91	3.45	1.01
OREAS 621	68.00	1.25	0.37	1.33	5.22	3.71	1.28	0.25	-1.49	2.58	1.69	2.25
GBM310-16	314.30	n/a	0.35	11.26	17.02	n/a	-1.88	n/a	-2.37	0.42	4.49	n/a
OREAS 113	22.60	n/a	13.30	0.02	0.42	28	-6.57	n/a	1.07	n/a	2.38	-2.4
G312-4	n/a	5.30	n/a	n/a	n/a	n/a	n/a	-4.50	n/a	n/a	n/a	n/a
Overall bias							**-2.06**	**-2.60**	**-0.97**	**1.95**	**2.78**	**0.29**

*n/a not applicable
Source: CSA Global (2015)

Subsequently it was discovered that Pb was under-reporting by the sodium peroxide fusion method employed where the samples contained >1% Ba, as barite was precipitating out of the fusion and taking Pb with it. The difference was significant enough that these samples have been re-assayed using a reduced aliquot weight.

Umpire Laboratory Results

Details is this section are taken from CSA Global (2015).

Pulps from a total of 150 samples from the 2015 programme were submitted to ALS Canada Inc. (ALS), as a check laboratory in Vancouver, for check assay using the same analytical methods as those employed at SGS Canada Inc. (SGS), the original laboratory.

The data have been examined using a series of scatter plots with fits to the data obtained by ordinary least squares regression. The data are compared in Table 7-2 using the coefficient of variation (CV), the correlation coefficient and an estimate of relative bias derived from the percentage difference (i.e. (original assay-check assay)/original assay*100). Negative values in Table 7-2 indicates that the original SGS data have an average negative bias relative to the ALS check data from the check assays.

Table 7-2: Summary of check assay statistics for 2015 programme

Element	Coefficient of Variation	Correlation Coefficient	Bias Original lab Relative to check lab
Ag	7.18	0.99	+3.31
Au	21.3	0.93	-2.83*
Cu	2.79	0.99	-0.11
Pb	7.92	0.95	-0.44
Zn	2.56	0.99	-1.00

*Data are imprecise, and this bias estimate is not considered to be definitive.
Source: CSA Global (2015)

Overall, there is very good agreement between copper and zinc values from original SGS and ALS check lab, with original SGS values slightly lower than the check ALS data and little scatter between the two data sets. Both Pb and Ag show strong positive correlations between the original SGS and check ALS data, but with much more scatter than the Cu or Zn data (Figure 7-1). Ag is slightly lower in the check lab samples, on average, whereas Pb is slightly higher in the check lab samples compared to the original SGS data (Figure 7-1). Variability in the Ag data is due in part to the nuggetty distribution of some of the silver at ABM hosted in fine-grained electrum grains and sulfosalts, as well as slight differences in

the strength of aqua regia used at the two laboratories. Lower Pb in the original SGS samples probably reflects under-reporting due to the presence of barite, even though both labs used a sodium peroxide digestion for the base metals analyses.

As previously discussed, data for gold is the least precise and this imprecision is reflected in both the high coefficient of variation (CoV) and low correlation coefficient (R) values for the two data sets. LA-ICP-MS and petrography demonstrate that gold occurs as electrum grains and within minor arsenopyrite component of the ore, both of which display a heterogenous distribution. Overall, Au is slightly lower in the original SGS samples, although this conclusion must be moderated by the poor precision of the combined data.

A total of 15 QC samples were submitted with the check assays, including six blanks, three CDN-ME-1311, four OREAS 621 and three OREAS 623 CRMs. The CRM data all lie within 1 or 2 standard deviations of the recommended values and the blanks are all within acceptable limits. The quality of the check lab data is therefore considered to be acceptable, although it must be borne in mind that there are far fewer QC samples than were submitted to the original lab.

However, as was the case with the original lab data, there are clear positive biases in the lead and zinc data, as well as negative biases in the copper and gold data for some of the CRMs. These biases are generally similar to or slightly more extreme than those displayed by the original lab data for the BMC CRMs, albeit based on a much smaller dataset.

This observation is consistent with the relative biases for lead and zinc between the original lab and check lab assays described previously, as well as being consistent with a slight positive bias in the original lab data relative to the historical assays, as discussed in the following section.

The silver assays remain problematic. The check lab silver data for the BMC CRMs generally show a positive bias, and yet the check lab data are lower, on average, than the original lab data for the check assays. This contradiction may in part lie in the variable nature of the silver bias observed in original lab assays over time, particularly for CDN-ME-1311, as well as the small number of QC samples available for the check assays.

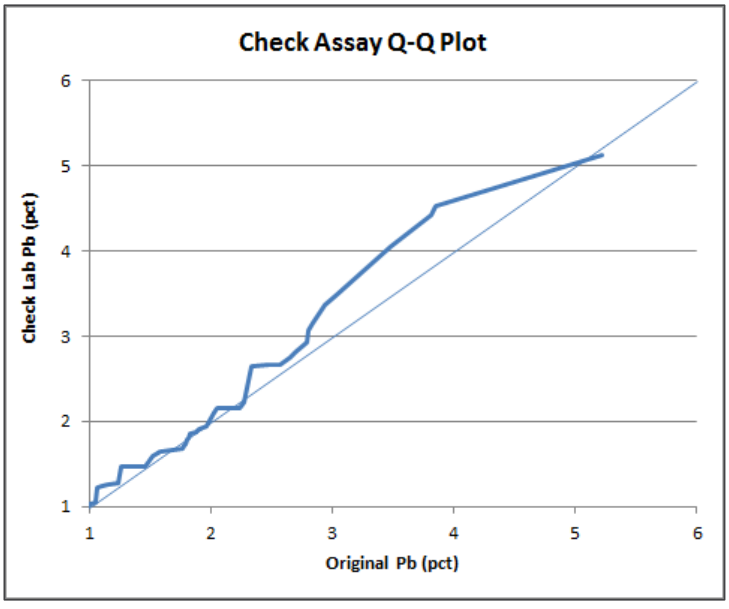


Figure 7-1: Q-Q plot using each data pair as a quantile and showing different distributions for Pb data from ALS check data and original SGS data

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(pct = per cent)

Historical Core Resampling

Details in this section are taken from CSA Global (2015).

Remaining half drill cores for 417 samples previously sampled by Cominco and analysed by Cominco Exploration Research Laboratory (CERL) were re-sampled during the 2015 field programme by BMC and analysed by SGS (Vancouver) using the same methods employed on the 2015 drill holes (sodium peroxide digestion with an ICP-OES finish). Historical drill core was stored on site under cover, and no significant oxidation of the core was noted.

The historical assays undertaken by CERL involved an aqua regia digestion followed by an AAS or ICP finish. Ore grade material is believed to have been analysed following dilution. Ag and Au were also analysed by fire assay and Ba was analysed by XRF.

Scatter and Q-Q plots were generated for each element and an example for Zinc is shown in Figure 7-2 and Figure 7-3.

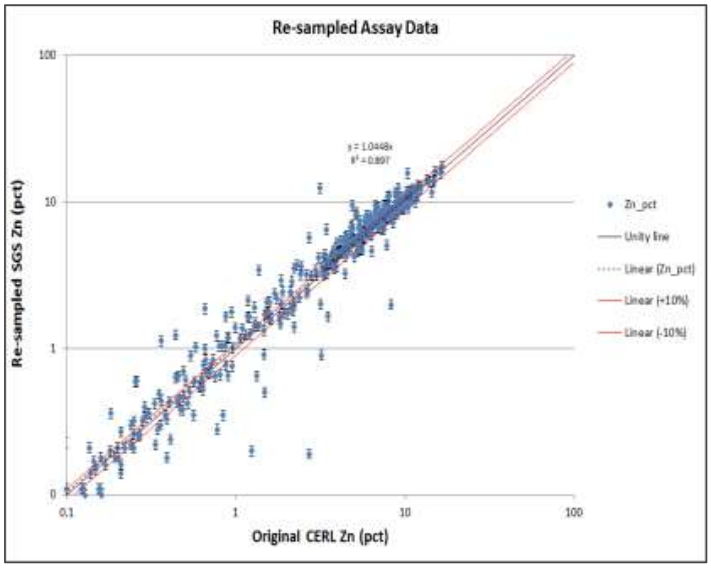


Figure 7-2: Scatter plot of historical and 2015 data for Zn Error bars for the SGS (original lab) data are estimates of precision from preparation duplicate pairs expressed at 2 standard deviations.
Source: CSA Global

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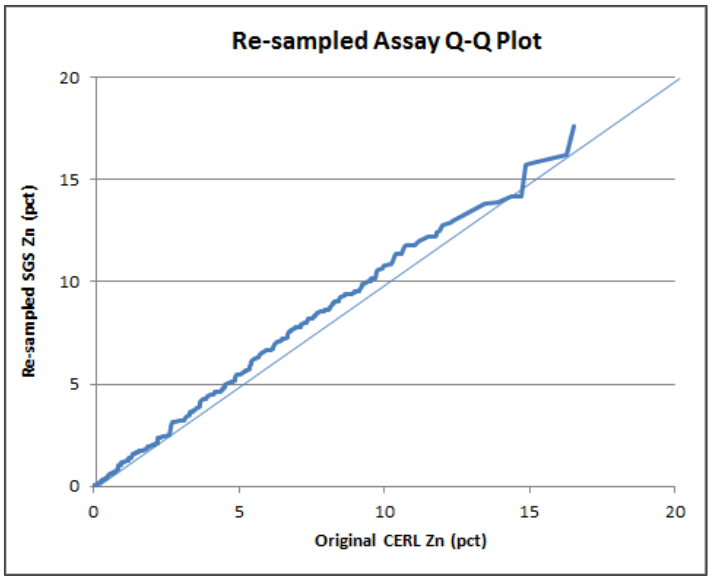


Figure 7-3: Q-Q plot for historical and 2015 data for Zn.
Source: CSA Global

The main conclusions of the comparison of the historical CERL data (1990s era) obtained using an aqua regia digestion for the base metals and the 2015 data obtained from original lab using a sodium peroxide fusion are summarised in point form below.

- Cu – good agreement up to 3%
- Pb – slight positive bias in original lab data, once samples with>1% Ba were re-assayed
- Zn – positive bias in original lab data >2.6 to 15%
- Ag – good agreement to 250 ppm
- Au – good to fair agreement to 3 ppm
- Fe – good agreement in the range 8-15%; positive bias in original lab data <8%; negative bias in original lab data between 15 and 20%.

The observed agreement in Cu data up to 3% supports the conclusions reached from a comparison of the original lab and check assays that the Cu data are generally reproducible between laboratories. Positive Zn biases in the original lab Pb and Zn data relative to the historical CERL data is consistent with positive biases seen in the original lab Pb and Zn data relative to a number of CRMs. The slight positive bias seen in the check Pb and Zn assays relative to the original lab data indicate that check lab would produce an even stronger positive biases relative to the historical Pb and Zn data. The Ag data are in good agreement to 250 ppm when both original lab and historical data were obtained using an aqua regia digestion. The agreement breaks down above 250 ppm Ag, close to the upper detection limit of 300 ppm for this method at original lab.

Given the particulate nature of gold observed at ABM, poor agreement between original lab and historical data above 3 ppm Au is not surprising, but the systematic positive bias observed above this value in the historical data, rather than random scatter, suggests a fundamental difference in the way the samples were prepared and analysed by fire assay.

Data Quality Assessment by Competent Person

Based on an assessment of the historical drilling results and the recent drilling by BMC, the Competent Person considers the entire dataset to be acceptable for resource estimation with assaying posing minimal risk to the overall confidence level of the Mineral Resource estimate.

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ERM recommends that commercial CRMs are located that more closely match the ABM-style mineralisation, or preferably, CRMs are prepared from existing ABM material and certified.

7.1.6 Wireframing

The drill hole traces on cross-sections were colour-coded according to logged lithology and sample grade values and separate strings were generated for the polymetallic massive sulfide, stockwork/disseminated sulfide mineralisation, mafic volcanic footwall unit, overburden surface, top of fresh rock surface and interpreted faults.

Interpretation techniques included the following:

- Each cross-section was displayed on screen with a clipping window equal to a half distance from the adjacent sections.
- All interpreted strings were snapped to either lithology and/or assay drill hole intervals.
- Internal waste within the mineralised envelopes was not interpreted and modelled (except for a small internal waste zone in the Krakatoa Zone). Instead, it was either included in the interpreted envelopes or split using bifurcation techniques, where supported by surrounding drill information.
- If a mineralised envelope did not extend to the adjacent drill hole section, it was projected halfway to the next section and terminated. The general direction and dip of the envelopes was maintained, although the lens thickness was reduced from the last known intersection.
- Where no drill hole was present down dip, the mineralisation was extended approximately half the drill spacing on section).
- If a mineralised lens extended to the overburden surface, it was extended, at the same width as the last drill hole, above the surface to ensure there would not be any gaps between the lens and the overburden when the block model was constructed.

Figure 7-4 shows an example of an interpreted cross-section with mineralisation and geological features wireframed.

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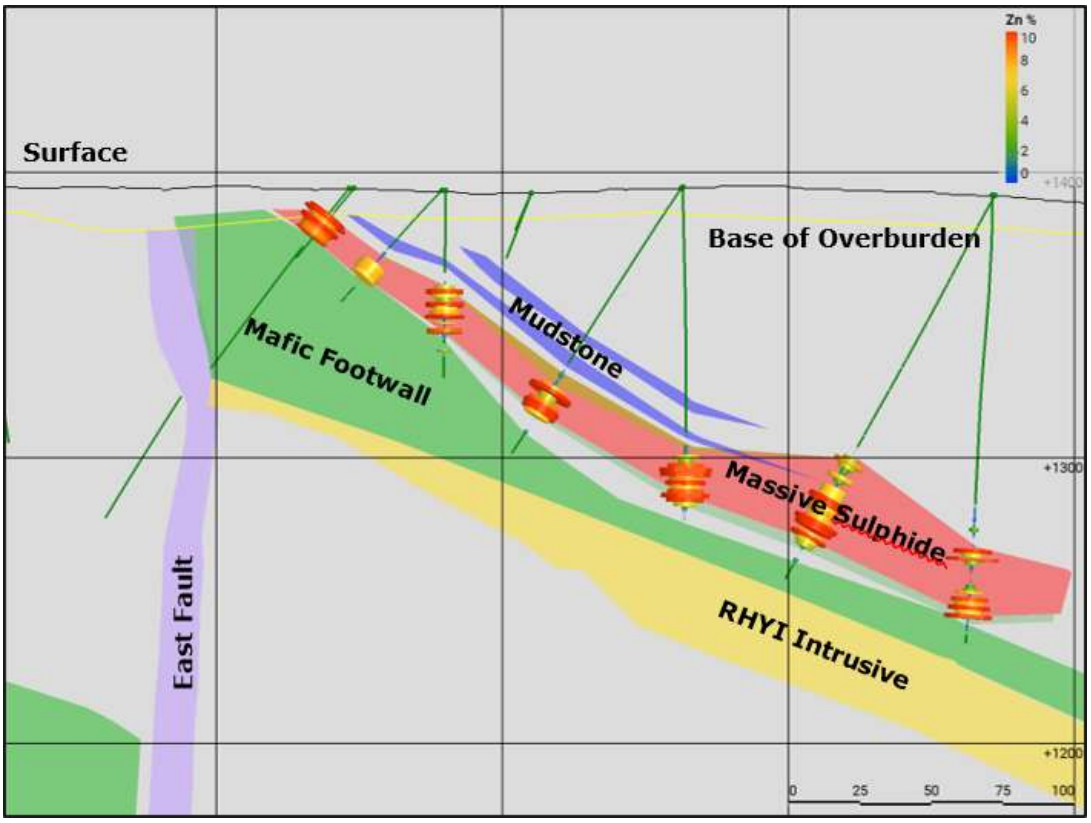


Figure 7-4: ABM geology interpretation (Section 415,100 mE looking west)

The interpreted strings were used to generate three-dimensional (3D) solid wireframes for the mineralised envelopes, and every section was displayed on screen along with the closest interpreted section. If the corresponding envelope did not appear on the next cross-section, the former was projected halfway to the next section, where it was terminated.

Separate mineralisation wireframes were generated for the ABM and Krakatoa Zones, respectively (Figure 7-5). The wireframes were also separated as either being massive sulfide or stockwork/disseminated mineralisation based on logged geology.

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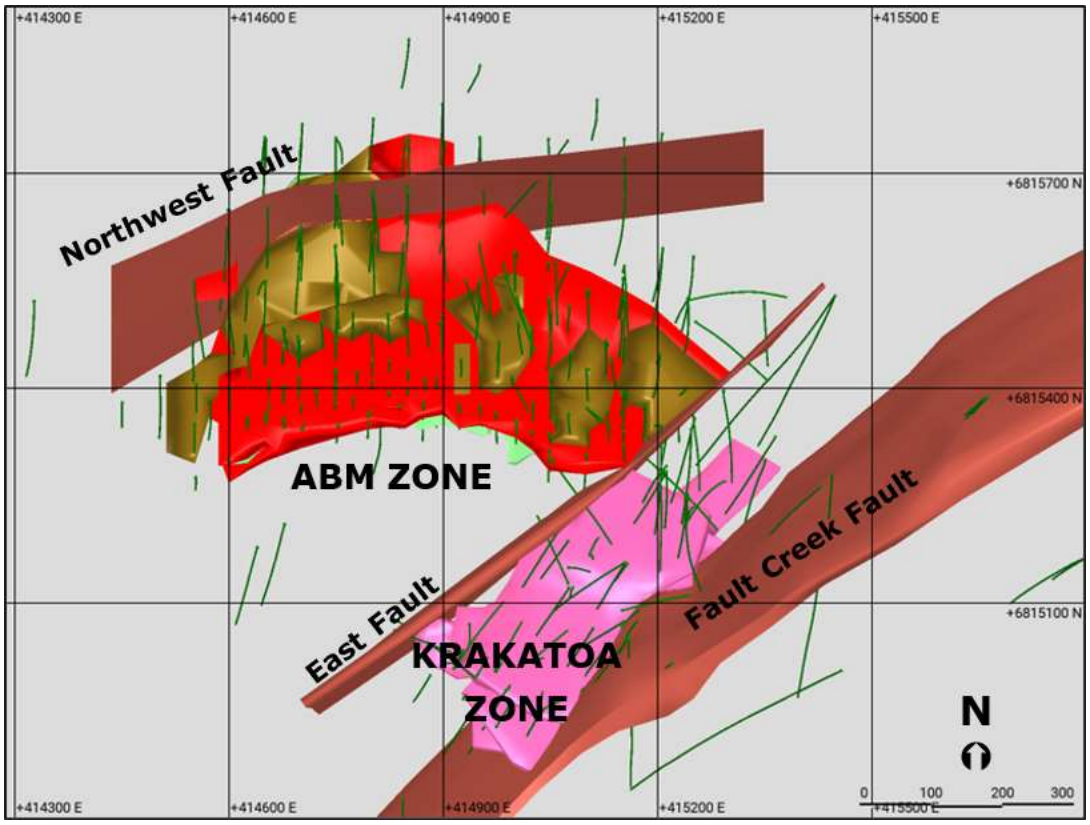


Figure 7-5: Plan view of the ABM and Krakatoa Zone mineralisation wireframes and drill hole traces

A dilution skin encompassing all the mineralisation wireframes was also created for mine planning purposes at each of the zones where a minimum 3 m down-hole intersection was used for wireframing the dilution skin.

Lithological and structural features were defined from logged and interpreted geology and Mafic intrusive, Rhyolite intrusive, Carbonaceous mudstones, Wind Lake formation, Northwest Fault, East Fault, Fault Creek Fault, Krakatoa Faults, and Overburden surfaces were wireframed.

Logging and re-logging of current and historical drill core, in conjunction with ethylene diamine tetra acetic acid (EDTA) analyses, determined there was no significant weathering profile for the ABM Deposit. However, geotechnical studies modelled a fractured zone below the base of overburden, and adjustments to the pit slope profile were made to account for this zone.

A detailed light detection and ranging (LiDAR) survey over the key sectors of the KZK Property was completed in 2015 to create an accurate and detailed digital terrain model of the surface and the survey specifically focused over the ABM Deposit area and potential infrastructure sites (horizontal accuracy of 35 cm and vertical accuracy of 15 cm).

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7.1.7 Statistics and Geostatistics

The data for lithological and mineralisation wireframes was assigned a code in the wireframe object number field and a summary of these codes used to distinguish the data during geostatistical analysis and estimation is shown in Table 7-3.

Table 7-3: Wireframe object field and description for the ABM Deposit

Wireframe object number	Zone	Description
2	ABM	Dilution
219	Krakatoa	Dilution
4, 13, 23, 33, 43, 53, 63, 73, 83, 93, 103, 113, 123, 133, 143, 153	ABM	Stockwork
202	Krakatoa	Stockwork
8, 17, 27, 37, 47, 57, 67	ABM	Massive sulfide
208, 209, 217, 218, 228, 238, 248, 258	Krakatoa	Massive sulfide

Source: 2025 Technical Report

Composite downhole lengths of 1.5 m and 1.0 m were selected for ABM and Krakatoa, respectively, given these lengths reflect majority of the sample intervals within each of the deposits and are a suitable scale for the width of the resource wireframes.

Statistical analysis was completed at each zone for the major elements (copper, lead, zinc, gold, silver, and iron) as well as arsenic, barium, bismuth, mercury, sulfur, antimony, and selenium. The interpreted mineralised massive sulfide and stockwork domains were grouped into global domains for the ABM and Krakatoa zones for the purpose of reporting statistical analyses.

Global statistics for the clustered, composited, and uncut major elements for the ABM and Krakatoa Zones are shown in Table 7-4 and Table 7-5, respectively. Global statistics for the clustered, composited, and uncut minor elements for the ABM and Krakatoa Zones are shown in Table 7-6 and Table 7-7, respectively. Cu % was characterised by a higher CV indicating increased dispersion of grade around the mean grade than the rest of the major elements.

Table 7-4: Major elements global statistics for ABM Zone

ABM	Cu (%)	Pb (%)	Zn (%)	Au (g/t)	Ag (g/t)	Fe (%)
Total samples	2,287	2,284	2,287	2,274	2,287	2,287
Minimum	0.002	0.01	0.01	0.01	0.30	1.31
Maximum	17.27	14.18	22.09	16.48	695.65	49.80
Mean	0.98	1.62	5.97	1.36	136.44	29.83
Median	0.48	1.33	6.16	1.13	114.90	32.37
Variance	2.40	1.91	13.54	1.19	10,195	124.02
Standard deviation	1.55	1.38	3.68	1.09	100.97	11.14
CV	1.58	0.86	0.62	0.80	0.74	0.37

Note: Clustered, composited, and uncut.
Source: 2025 Technical Report

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Table 7-5: Major elements global statistics for Krakatoa Zone

Krakatoa	Cu (%)	Pb (%)	Zn (%)	Au (g/t)	Ag (g/t)	Fe (%)
Total samples	769	769	769	769	769	769
Minimum	0.005	0.02	0.03	0.005	1.02	1.95
Maximum	8.08	8.21	21.53	26.86	3,347	48.41
Mean	0.61	3.06	7.18	1.75	210	0.61
Median	0.33	3.01	7.18	1.56	193	0.33
Variance	0.69	3.24	10.55	2.32	28,967	0.69
Standard deviation	0.83	1.80	3.25	1.52	170	0.83
CV	1.37	0.59	0.45	0.87	0.81	1.37

Note: Clustered, composited, and uncut.
Source: 2025 Technical Report

Table 7-6: Minor elements global statistics for ABM Zone

ABM	As (ppm)	Ba (ppm)	Bi (ppm)	Hg (ppm)	S (%)	Sb (ppm)	Se (ppm)
Total samples	2,253	2,147	2,253	1,118	862	2,253	1,607
Minimum	1.00	2.00	0.01	0.01	0.04	0.05	0.50
Maximum	39,740	255,085	608	182	48.70	7,112	1,425
Mean	2,458	13,450	56	18	28.72	460	114
Median	1,384	2,700	44	10	34.90	228	0.50
Variance	9,494,791	686,884,819	2,562	532	197.31	388,538	28,690
Standard deviation	3,081	26,208	51	23	14.05	623	169
CV	1.25	1.95	0.91	1.26	0.49	1.35	1.49

Note: Clustered, composited, and uncut.
Source: 2025 Technical Report

Table 7-7: Minor elements global statistics for Krakatoa Zone

Krakatoa	As (ppm)	Ba (ppm)	Bi (ppm)	Hg (ppm)	S (%)	Sb (ppm)	Se (ppm)
Total samples	763	662	761	751	759	760	751
Minimum	11.42	100	0.083	0.098	0.2	5	1.82
Maximum	46,000	358,560	477	110	48.6	33,200	1,900
Mean	4,512	24,486	39	20	30.195	620	198
Median	2,839	1,200	24	15	32.168	372	144
Variance	27,137,516	3.38E+09	2,138	305	87.012	2,117,514	46,596
Standard deviation	5,209	58,120	46	17	9.33	1,455	216
CV	1.155	2.37	1.18	0.87	0.31	2.35	1.09

Note: Clustered, composited, and uncut.
Source: 2025 Technical Report

Table 7-8 and Source: 2025 Technical Report

Table 7-9 show the correlation matrices.

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Table 7-8: Correlation matrix for the ABM Zone

Indep/ Dep	Cu %	Pb %	Zn %	Au g/t	Ag ppm	Fe %	As ppm	Ba ppm	Bi ppm	Hg ppm	S %	Sb ppm	Se ppm
Cu %	1	-0.27	-0.23	0.23	0.10	0.12	-0.17	-0.16	0.60	-0.20	-0.09	-0.16	0.23
Pb %	-0.27	1	0.70	0.44	0.70	0.13	0.42	0.30	-0.23	0.44	0.36	0.50	-0.16
Zn %	-0.23	0.70	1	0.25	0.45	0.38	0.31	0.11	-0.04	0.34	0.54	0.31	-0.07
Au g/t	0.23	0.44	0.25	1	0.78	0.16	0.54	0.27	0.06	0.41	0.21	0.67	-0.10
Ag ppm	0.10	0.70	0.45	0.78	1	0.12	0.46	0.36	-0.02	0.54	0.23	0.74	-0.13
Fe %	0.12	0.13	0.38	0.16	0.12	1	0.14	-0.16	0.37	0.04	0.83	0.00	0.15
As ppm	-0.17	0.42	0.31	0.54	0.46	0.14	1	0.13	-0.14	0.41	0.31	0.53	-0.15
Ba ppm	-0.16	0.30	0.11	0.27	0.36	-0.16	0.13	1	-0.23	0.40	0.08	0.34	-0.12
Bi ppm	0.60	-0.23	-0.04	0.06	-0.02	0.37	-0.14	-0.23	1	-0.21	0.15	-0.18	0.27
Hg ppm	-0.20	0.44	0.34	0.41	0.54	0.04	0.41	0.40	-0.21	1	0.28	0.61	-0.23
S %	-0.09	0.36	0.54	0.21	0.23	0.83	0.31	0.08	0.15	0.28	1	0.17	0.32
Sb ppm	-0.16	0.50	0.31	0.67	0.74	0.00	0.53	0.34	-0.18	0.61	0.17	1	-0.18
Se ppm	0.23	-0.16	-0.07	-0.10	-0.13	0.15	-0.15	-0.12	0.27	-0.23	0.32	-0.18	1

Source: 2025 Technical Report

Table 7-9: Correlation matrix for the Krakatoa Zone

Indep/ Dep	Cu %	Pb %	Zn %	Au g/t	Ag ppm	Fe %	As ppm	Ba ppm	Bi ppm	Hg ppm	S %	Sb ppm	Se ppm
Cu %	1	-0.03	0.25	0.36	0.31	0.05	-0.13	-0.17	0.52	-0.03	-0.07	0.25	0.13
Pb %	-0.03	1	0.57	0.14	0.26	0.32	0.21	0.05	-0.07	0.12	0.38	-0.01	-0.04
Zn %	0.25	0.57	1	0.03	0.12	0.50	0.03	-0.23	0.53	0.22	0.55	-0.11	0.32
Au g/t	0.36	0.14	0.03	1	0.90	-0.14	0.27	0.17	-0.08	0.24	-0.04	0.88	-0.13
Ag ppm	0.31	0.26	0.12	0.90	1	-0.13	0.11	0.16	-0.07	0.30	-0.02	0.88	-0.03
Fe %	0.05	0.32	0.50	-0.14	-0.13	1	0.12	-0.27	0.27	0.07	0.85	-0.22	0.34
As ppm	-0.13	0.21	0.03	0.27	0.11	0.12	1	0.18	-0.10	0.27	0.17	0.10	-0.01
Ba ppm	-0.17	0.05	-0.23	0.17	0.16	-0.27	0.18	1	-0.28	0.03	-0.07	0.10	-0.27
Bi ppm	0.52	-0.07	0.53	-0.08	-0.07	0.27	-0.10	-0.28	1	-0.05	0.19	-0.12	0.29
Hg ppm	-0.03	0.12	0.22	0.24	0.30	0.07	0.27	0.03	-0.05	1	0.21	0.11	0.14
S %	-0.07	0.38	0.55	-0.04	-0.02	0.85	0.17	-0.07	0.19	0.21	1	-0.18	0.31
Sb ppm	0.25	-0.01	-0.11	0.88	0.88	-0.22	0.10	0.10	-0.12	0.11	-0.18	1	-0.14
Se ppm	0.13	-0.04	0.32	-0.13	-0.03	0.34	-0.01	-0.27	0.29	0.14	0.31	-0.14	1

Source: 2025 Technical Report

Scatterplots were created for the global domains for the ABM Deposit by plotting the clustered, composited, and uncut variables against one another to assess relationships and possible correlations. Review of the scatterplots by ERM show strong correlations between silver and gold, silver and antimony, and iron and sulfur for the ABM Zone, and between silver and gold, gold and antimony, silver and antimony, and iron and sulfur for the Krakatoa Zone.

Cutting of gold (10 g/t), silver (1,500 g/t) and antimony (6,000 ppm) for the Krakatoa Zone results in a relative drop in correlations for gold:silver (0.86 to 0.74), gold:antimony (0.81 to 0.69) and silver:antimony (0.85 to 0.65).

A review of grade outliers was undertaken to ensure that extreme grades are treated appropriately during grade interpolation and although extreme grade outliers within the grade populations of variables

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are real, they are potentially not representative of the volume they inform during estimation. If these values are not cut, they have the potential to result in significant grade over-estimation on a local basis.

Top cuts were selected following statistical review of the sample population. The cutting strategy was applied following review of the following:

- Skewness of the data
- Probability plots
- Spatial position of extreme grades.

To determine the top cuts, histograms and probability plots were reviewed for the major elements (copper, lead, zinc, gold, silver, and iron) and minor elements (arsenic, barium, bismuth, mercury, sulfur, antimony, and selenium). The plots were compiled based on the 1.5 m and 1.0 m composites for each mineralised zone for the ABM and Krakatoa Zones, respectively.

Geostatistical Analysis

An assessment of spatial anisotropy within the input data was made for each of the main mineralised zones. Experimental semi-variograms were constructed in each of the three principal directions based on the anisotropic directions selected on a per-domain basis.

A semi-variogram model was then fitted to the experimental variograms. The variogram parameters were subsequently used in ordinary kriging estimation of block grades.

Kriging Neighbourhood Analysis (KNA) was completed and adopted the relevant variogram models for the estimation domains based on the combined massive sulfide dataset of the ABM Zone and the updated massive sulfide dataset of the Krakatoa Zone, respectively.

Variography was attempted on stockwork mineralisation, but the data was patchy and structures poor. As such, conceptual variogram parameters based on the massive sulfide results were modelled to best reflect stockwork geometry.

The KNA results show that the search parameters and block sizes selected are suitable for use in the MRE and adequately take drill spacing, geology and practicality into account. The number of composites used for the major and potential deleterious element grade estimations in the ABM and Krakatoa Zones were considered adequate. The modelled variogram parameters together with the selected estimation panel size and number of samples were used to determine the appropriate search ellipses for the primary search pass.

7.1.8 Block Modelling

A block model was created to encompass the full extent of the ABM Deposit and used a parent cell size of 10 m(E) by 10 m(N) by 5 m(RL) with standard sub-celling to 5 m(E) by 5 m(N) by 2.5 m(RL) to maintain the resolution of the mineralised lenses.

The northing parent cell size was selected based on approximately half of the average drill section spacing in better drilled areas of the deposit and the model cell dimensions in other directions were selected to provide sufficient resolution to the block model in the across-strike and down dip directions.

A list of block model parameters is displayed in Table 7-10.

Table 7-10: Block model parameters – ABM Deposit

Axis	Extent (m)		Block size (m)	Maximum sub-celling (m)
	Minimum	Maximum		
Easting	414,200	415,700	10	5
Northing	6,814,600	6,816,000	10	5
RL	1,000	1,700	5	2.5

Source: 2025 Technical Report

A comparison of the wireframe volumes to the block model volume for each of the resource zones was undertaken and the difference between the wireframe volumes and the block model volumes was within the margin of error in 29 of the 32 domains (approximately 98% of the total volume) and demonstrates that the resolution of the block model sub-celling is satisfactory.

7.1.9 Grade Interpolation and Estimation

The wireframe objects were used as hard boundaries in grade interpolation for all except five of the mineralised zones of the ABM Deposit and this process reflects and supports field observations around the mineralisation contacts. Semi-soft boundaries were introduced for the other five mineralised zones where samples from a neighbouring large domain were used in the estimation of the smaller domain. Such boundaries were required for these five zones due to lack of supporting data to reliably inform the estimate for each domain. All mineralised zones at the Krakatoa Deposit were estimated using hard boundaries.

Ordinary kriging (OK) was selected for grade interpolation in the mineralised zones and inverse distance cubed (ID3) was used in the estimation of the dilution skin. OK was selected to allow a degree of smoothing within the model based on the measured variability from the variograms. ID3 was chosen over ID2 for the dilution skin as it further restricted the influence of individual high-grade samples thereby approximating a nearest neighbour approach.

An oriented "ellipsoid" search was used to select data for interpolation and an "anisotropic in the plane" ellipse (different major and semi-major distances) was oriented according to the rotations derived from the variography.

Estimation parameters at ABM were calculated using all data, as the domains at ABM are deemed to be similar enough to be treated as a single domain for statistical purposes. However, in the Krakatoa Zone, this was thought not to be the case, and estimation parameters were calculated using the data from the largest domain only, which was subsequently applied to all other domains.

A three-pass estimation search was used to complete estimation for copper, lead, zinc, gold, silver, iron, arsenic, barium, bismuth, mercury, sulfur, antimony, and selenium. Approximately 99% of the blocks were informed in the first two estimation passes for the mineralisation estimate and the third expanded estimation pass was used to inform remaining "un-estimated" blocks.

7.1.10 Bulk Density

A combination of methods was utilised to assign bulk density for the mineralised material including that which falls within the dilution skin. A dataset of bulk density values for interpolation into the block model was constructed based on a hierarchy of confidence. The bulk density value for the ABM Zone was determined according to the following tiered priorities:

- Measured bulk density value was used where available.
- Pycnometer specific gravity was used where there was no measured bulk density.
- Bulk densities were calculated using multiple regression, using sulfur data where available, optimised for the highest coefficient of determination.

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Where sulfur data was absent, bulk densities were calculated using weighted iron-copper-lead-zinc data with the simple exponential regression

*(1.0*Cu%)+(1.81*Pb%)+(0.97*Zn%)+(1.20*Fe%).*

This was completed for the bulk densities for zone 8 and for samples having a bulk density <2.75 g/cm^3 in zones 5, 6 and 7.

Measured bulk densities were available for all samples within the mineralisation wireframes at Krakatoa. Bulk density was estimated into the block model using OK for the mineralised zones, and ID3 for the dilution skin.

Estimation parameters were duplicated from those used in the estimation of iron; this ensured that the relationship between bulk density and iron was maintained. Approximately 96% of the blocks were informed in the first two estimation passes for the bulk density estimate. The swath plots shown in Figure 7-6 and Figure 7-7 demonstrate that the estimated bulk densities in the model correspond well with the input samples for the main zone at ABM Zone and Krakatoa Zone, respectively.

The bulk density values used for the ABM MRE are displayed in Table 7-11.

Table 7-11: Bulk density values applied to the ABM MRE

Material type	Bulk density (t/m^3)	Description
Overburden	2.00	Topographic surface to base of overburden
Felsic volcanics	2.76	Assigned directly to host rock based on measured average
Mafic intrusive (MAFi)	2.80	Assigned directly to mafic wireframes and based on measured average
Rhyolite intrusive (RHYi)	2.68	Assigned directly to RHYi wireframes and based on measured average
Carbonaceous mudstone (MDS)	2.74	Assigned directly to mudstone wireframes and based on measured average
Wind Lake formation	2.74	Assigned directly to Wind Lake formation wireframes and based on measured average
ABM – Stockwork	3.44	Estimated, mean value
Krakatoa – Stockwork	3.86	Estimated, mean value
ABM – Massive Sulfide	4.19	Estimated, mean value
Krakatoa – Massive Sulfide	4.09	Estimated, mean value

Source: CSA Global, 2025 Technical Report

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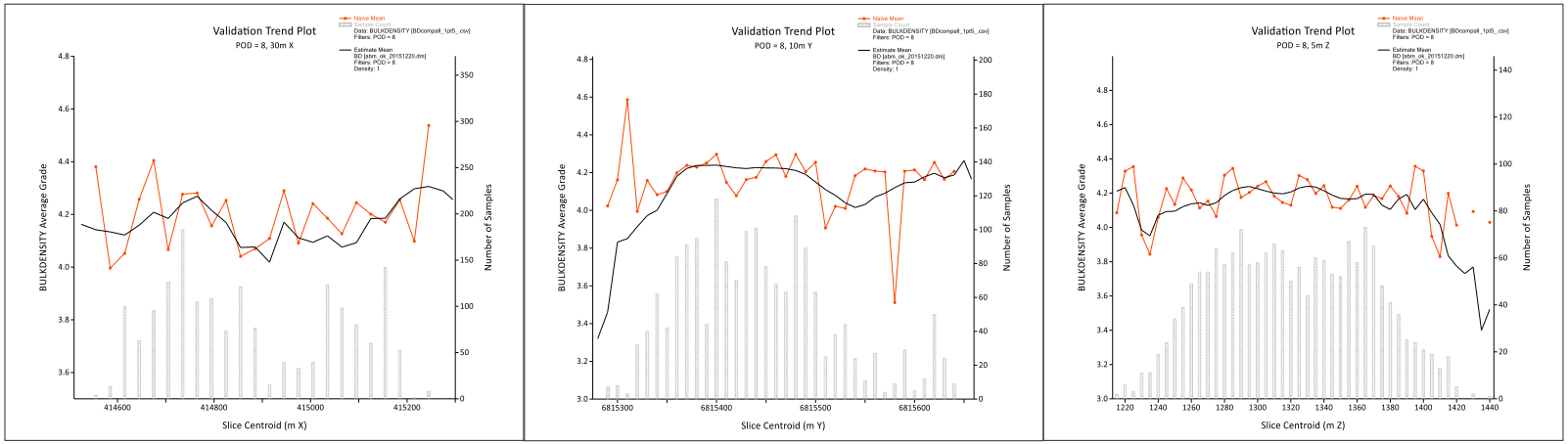


Figure 7-6: Swath plot of the ABM main zone bulk density (by 30 m easting, 10 m northing, and 5 m bench).
Native Mean in orange, Estimate Mewan in Black
The drop off in estimated bulk density in relation to sample values seen south of 6,815,350 mN and above 1,420 mRL is related to assigned bulk densities in the overburden portion of Pod 8, which do not have corresponding bulk density samples.

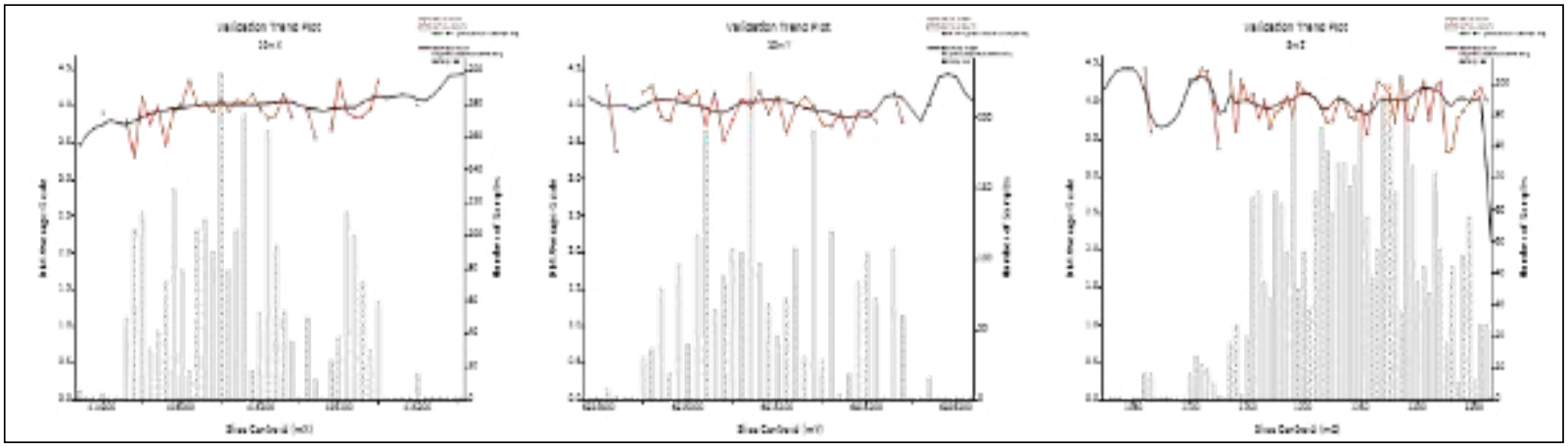


Figure 7-7: Swath plot of the Krakatoa Zone bulk density (by 30 m easting, 10 m northing, and 5 m bench).
Native Mean in orange, Estimate Mean in Black
Source: CSA Global

7.1.11 Mineral Resource Classification

The Mineral Resource estimates for the ABM Deposit (ABM and Krakatoa Zones) have been classified in accordance with the guidelines specified in the JORC Code (2012).

The Competent Person considers there are reasonable prospects for eventual economic extraction based on the results of the Feasibility Study-level work completed for the ABM Deposit (ERM 2025b) confirming that the ABM Deposit had demonstrated that extraction was reasonably justified and economically viable.

The Mineral Resource classification is based upon an assessment of geological understanding of the deposit, geological and grade continuity, drill hole spacing, quality control results, search and interpolation parameters, and an analysis of available density information.

The ABM Deposit shows excellent continuity of mineralisation within well-defined geological constraints. Drill holes are located at a nominal spacing of 50 m on 25 m north-south oriented sections extending out to 100 m on the peripheries of the deposit. The drill spacing is sufficient to allow the geology and mineralisation zones to be modelled into coherent wireframes for each domain. Reasonable consistency is evident in the orientations, thickness, and grades of the mineralised zones.

The 2015 BMC exploration programme included re-drilling of several sections within the ABM Zone, "twinning" historical holes, re-logging and resampling of historical core, and re-surveying historical drill collars. This work validated the historical work undertaken by Cominco and improved the confidence level in the historical data and, along with the additional infill drilling, has largely confirmed the continuity of the geology and known mineralisation.

The Mineral Resource is classified as Indicated where, in the Competent Person's opinion, sufficient data exists to assume geological and mineralisation continuity. For areas with more limited data density and limited along strike or down dip continuity, there is sufficient evidence to imply but not verify geological and grade continuity and these areas are classified as Inferred. The resource classification strategy is illustrated in Figure 7-8.

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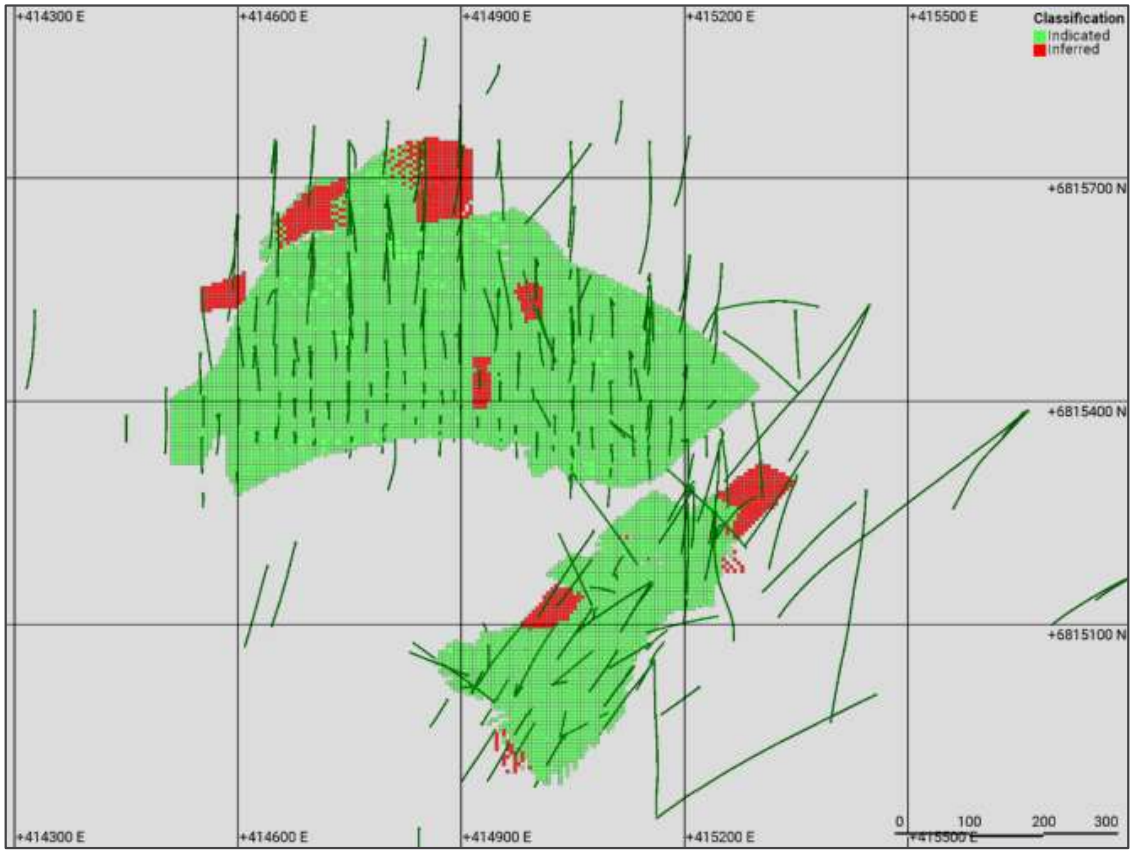


Figure 7-8: ABM Deposit Mineral Resource classification in plan view (red = Inferred, green = Indicated).
Source: CSA Global

7.1.12 NSR Cut-Off Grade and Grade-tonnage Curves

A net smelter return (NSR) calculation was used to create a composite metal cut-off value for a polymetallic deposit, as a single metal cut-off value is not appropriate in this instance. Such a calculated cut-off value is used primarily for reporting of the MRE as any mining feasibility studies are based on the Ore Reserve Estimate after consideration of all modifying factors.

The NSR values were calculated using assumed metal prices, metallurgical recoveries, smelter terms (including payable factors, concentrate costs and refining charges) and government royalties. No penalties were included. Metal price assumptions were: US$4.50/lb copper, US$1.65/lb zinc, US$0.9/lb lead, US$1,875/oz gold and US$22.5/oz silver, and an exchange rate of US$0.75 = C$1.00. Metal recovery assumptions 90% for copper, 90% for zinc, 80% for lead, 64% for gold (whereby 27% is recovered from copper concentrate, 29% is recovered from HPM concentrate and 8% is recovered from zinc concentrate) and 86% for silver (37% from copper concentrate, 38% from HPM concentrate and 11% from zinc concentrate). Based on these assumptions, the formula for the NSR for use was expressed as:

$$NSR\ US\$/t = (69.17*Cu_cut) + (6.85*Pb_cut) + (19.53*Zn_cut) + (30.13*Au_cut) + (0.49*Ag_cut)$$

Shallower resources were reported above a cut-off NSR of US$40/t and deeper resources reported above US$150/t to reflect an obvious increase in mining costs with depth.

A Lerchs-Grossman open pit optimisation was completed to aid in the determination of the reporting for the ABM Deposit Mineral Resources as either "shallow" or "deep". Parameters used for the

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optimisation included base case metal price assumptions and exchange rate used in the NSR calculation, a mining recovery of 97% and dilution of 10%, an overall pit wall slope angle of 50°, total processing costs (fresh) of US$33.02/t and plant throughput of 2 Mtpa.

Only material reporting inside the selected pit shell (Revenue Factor = 1.00) has been reported above the NSR cut-off of US$40/t for the ABM Zone. For the Krakatoa Zone, mineralised material inside the pit shell has been reported above the NSR cut-off of US$40/t, while the remainder has been designated as "deep" resource and reported above a cut-off NSR of US$150/t.

Grade-tonnage tables have been generated for copper, lead, zinc, gold, and silver and the global ABM Deposit grade-tonnage curves for copper, lead, and zinc are shown in Figure 7-9.

Figure 7-10 shows the block model for the ABM and Krakatoa Zones coloured according to zinc.

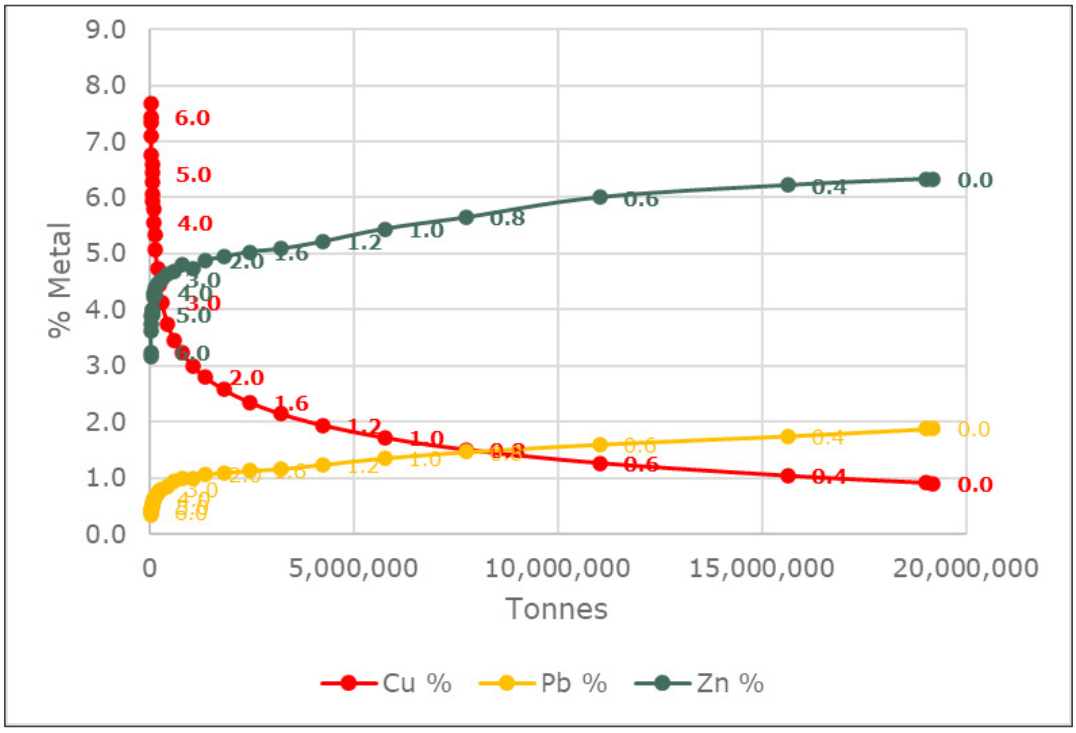


Figure 7-9: ABM Deposit global grade-tonnage curves for Cu%, Pb%, and Zn%.
Source: Cube

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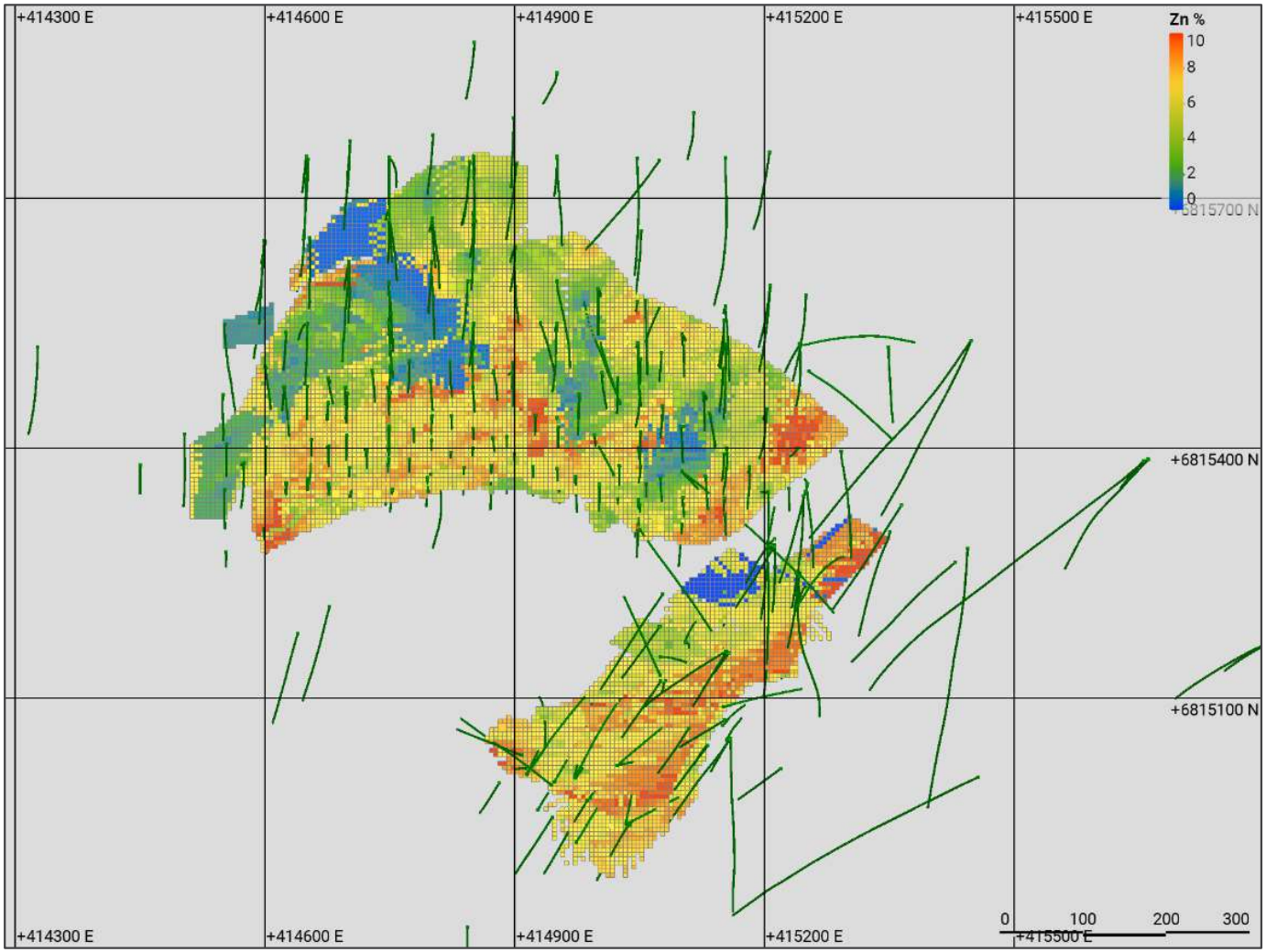


Figure 7-10: ABM-Krakatoa block model showing zinc grades (%) (plan view)./Source: Cube.

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7.1.13 Mining and Metallurgical Methods and Parameters

The ABM Deposit has been the subject of extensive technical studies to a Feasibility Study level. Discussion of Modifying Factors and other material considerations demonstrating a robust basis for the declaration of a Mineral Resource estimate are presented in subsequent sections of this Report.

7.1.14 Mineral Resource Reporting

The estimated Mineral Resources for the ABM Deposit are reported in Table 7-12.

Table 7-12: ABM Deposit Mineral Resource estimate

Zone	Category	Tonnes (Mt)	Cu (%)	Pb (%)	Zn (%)	Au (g/t)	Ag (g/t)	Cu (kt)	Pb (kt)	Zn (kt)	Au (koz)	Ag (Moz)
ABM (shallow)	Indicated	14.6	1.0	1.6	6.1	1.3	132	141	229	887	614	62
	Inferred	0.3	1.5	1.6	4.5	1.1	117	5	5	14	11	1
Krakatoa (shallow)	Indicated	3.5	0.6	3.2	7.2	1.8	213	21	113	256	204	24
	Inferred	0.1	0.6	2.3	6.3	1.3	143	0.1	2	6	4	0.4
Krakatoa (deep)	Indicated	0.2	1.0	2.1	6.1	1.7	173	2	3	11	9	1
	Inferred	0.4	0.8	1.6	9.4	1.2	165	3	6	38	15	2
Total	Indicated	18.3	0.9	1.9	6.3	1.4	148	164	346	1,153	827	87
	Inferred	0.8	1.0	1.7	7.2	1.2	143	8	13	58	30	4
Grand Total	**Ind & Inf**	**19.1**	**0.9**	**1.9**	**6.3**	**1.4**	**148**	**172**	**359**	**1,211**	**857**	**91**

Notes:

- BMC's interest in the ABM Deposit is 100%.
- The Mineral Resources are reported in accordance with the JORC Code by Aaron Green, Competent Person, FAIG.
- The Effective Date of this MRE is 3rd January 2025.
- Numbers have been rounded to reflect the precision of an Indicated and Inferred MRE (noting that MRE are, by nature, approximate and with a degree of uncertainty).
- The ABM Indicated Mineral Resources are inclusive of the Probable Ore Reserves estimated for ABM.
- Shallow Zone cut-off at NSR cut-off grade of US$40/t, assuming an open pit extraction.
- Deep Zone cut-off at NSR cut-off grade of US$150/t, assuming underground extraction.
- NSR formula: NSR US$/t =((69.17*Cu_cut) + (6.85*Pb_cut) + (19.53*Zn_cut) + (30.13*Au_cut) + (0.49*Ag_cut)).
- Metal recovery assumptions 90% for copper, 90% for zinc, 80% for lead, 64% for gold (whereby 27% is recovered from copper concentrate, 29% is recovered from HPM concentrate and 8% is recovered from zinc concentrate) and 86% for silver (37% from copper concentrate, 38% from HPM concentrate and 11% from zinc concentrate)
- An exchange rate of 0.75 CAD:USD.
- The optimal transition from open pit to underground have not been considered when reporting the Mineral Resource. Key modifying factors in determining this transition have been factored into reporting of the Ore Reserve.

7.2 Kona Deposit

The MRE for the Kona Deposit is based on historical datasets and more recent interpretations BMC have undertaken since acquiring the Fyre Lake Claim Block, the southern part of the Kona Property.

7.2.1 Drill Hole Data

BMC has not conducted any drilling activities on the Kona Property, with all holes drilled by previous owners or related parties. A total of 114 core drill holes (22,700 m) define the Kona Deposit where a total of 73 assayed drill holes intersected the interpreted mineralised zones, with holes spaced 25–200 m apart along a 1,500 m plunge extent. Holes were drilled in various orientations due to physical access restrictions at surface.

A drill plan and typical cross-section are shown in Figure 7-11.

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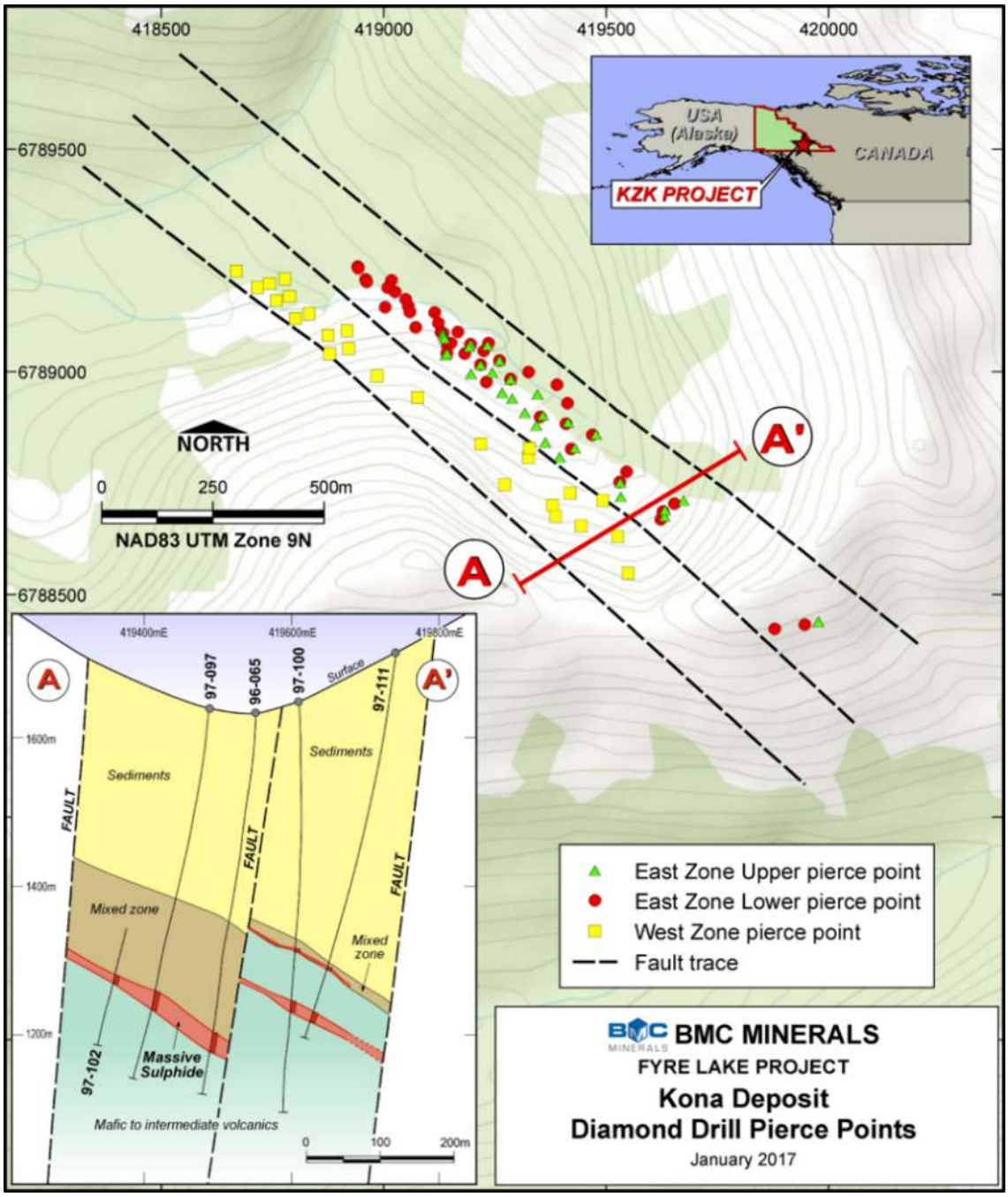
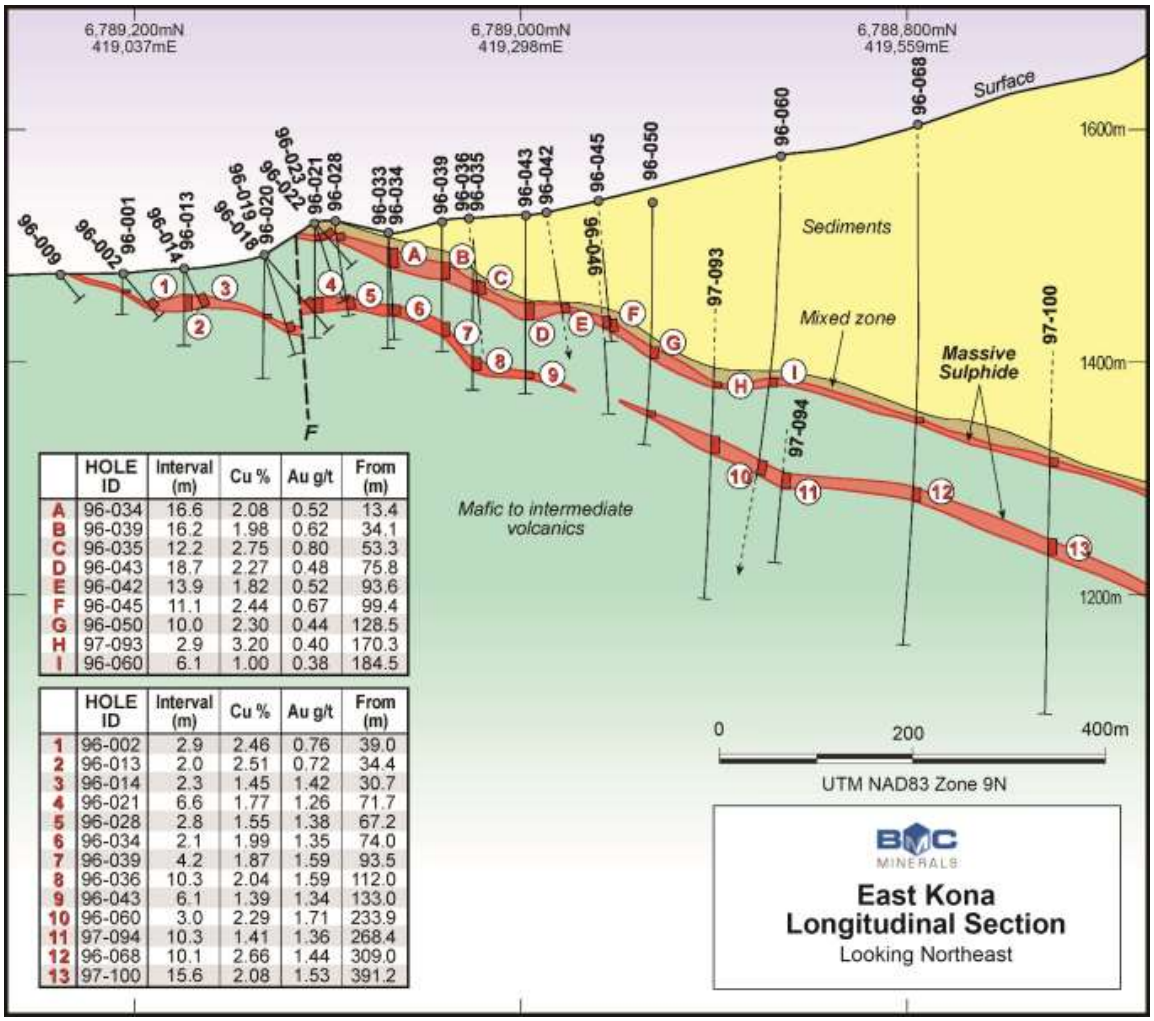


Figure 7-11: Plan and Cross-Section View of the Kona Deposit
Source: BMC

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	HOLE ID	Interval (m)	Cu %	Au g/t	From (m)
A	96-034	16.6	2.08	0.52	13.4
B	96-039	16.2	1.98	0.62	34.1
C	96-035	12.2	2.75	0.80	53.3
D	96-043	18.7	2.27	0.48	75.8
E	96-042	13.9	1.82	0.52	93.6
F	96-045	11.1	2.44	0.67	99.4
G	96-050	10.0	2.30	0.44	128.5
H	97-093	2.9	3.20	0.40	170.3
I	96-060	6.1	1.00	0.38	184.5

	HOLE ID	Interval (m)	Cu %	Au g/t	From (m)
1	96-002	2.9	2.46	0.76	39.0
2	96-013	2.0	2.51	0.72	34.4
3	96-014	2.3	1.45	1.42	30.7
4	96-021	6.6	1.77	1.26	71.7
5	96-028	2.8	1.55	1.38	67.2
6	96-034	2.1	1.99	1.35	74.0
7	96-039	4.2	1.87	1.59	93.5
8	96-036	10.3	2.04	1.59	112.0
9	96-043	6.1	1.39	1.34	133.0
10	96-060	3.0	2.29	1.71	233.9
11	97-094	10.3	1.41	1.36	268.4
12	96-068	10.1	2.66	1.44	309.0
13	97-100	15.6	2.08	1.53	391.2

Figure 7-12: Longitudinal section of the East Kona Zone showing significant intersections. View is to northeast; letters A to I reference upper lens intersections, and numbers 1 to 13 reference lower lens drill intersections of massive sulphide, with corresponding analytical results tabulated.

Source: BMC

7.2.2 Drilling Techniques

All drilling at Kona has used diamond core drilling. Details are presented in Appendix B.

The Kona Property has been tested by 126 diamond holes, totalling 23,248.69 m of NQ2, BQTK and AX core diameter all focused on or about the Kona VHMS Deposit.

Holes were oriented in various directions due to physical access restrictions (000°, 072°, 162°-177° and 212°-252°) at various dip angles (-45° to -90°).

The drill core was geologically and geotechnical logged in detail, exceeding industry standards at the time. This included lithology, mineralogy, RQD, recovery and other attributes.

7.2.3 Sampling and Sub-sampling techniques

Drill holes were logged and selected intervals were manually split lengthwise. The sampled diamond drill core was split in half lengthwise using a manual Longyear core splitter. Any whole sections of

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drill core collected for metallurgical studies or exhibition were permanently marked in the respective core boxes.

Split samples comprised half-core in 1 m intervals adjusted firstly to lithologic boundaries, and secondly to mineralogy of massive sulfide mineralisation.

Earlier exploration sampling has been superseded by the extensive drilling which has subsequently taken place, and therefore details of earlier sampling are not discussed.

No non-core holes have been drilled at the deposit.

The samples were manually split, and half-core samples were double bagged and securely stored prior to direct shipping to either Min-En or later Chemex laboratories in Smithers, BC. There the samples were dried, crushed and pulverised, rolled and bagged.

These procedures are considered industry standard techniques and appropriate for the style of mineralisation. This is considered quite adequate to support MRE.

Subsampling techniques and sample preparation are considered adequate to support Mineral Resource estimation.

Details are presented in Appendix B.

7.2.4 Sample Analysis

Core from the 1996-1997 drilling was dispatched to either Min-En or later Chemex laboratories for prep work (dried, crushed, pulverised) in Smithers, BC and analysis in Vancouver, BC. Approximately 10% of samples were sent for check assay at Acme Analytical Laboratories, no field duplicates were collected during 1996–1997 drill campaigns

Assay analysis was carried out on mineralised subsamples, comprising 0.5–2.0 g splits, were analysed for copper, zinc, lead, and silver content using AAS. The gold content of the subsample pulp was determined after aqua regia digestion by fire assay and AAS procedures. An additional 2,262 core samples were analysed by 31 elements by ICP techniques.

In 1996–97 mineralised subsamples, 0.5–2.0 g splits, were analysed for copper, zinc, lead, and silver using AAS. The gold content of the subsample pulp was determined with aqua regia digestion followed by fire assay and an AAS finish.

Samples from the 1997 programme were digested with 50 mL of aqua regia, diluted to 100 mL with water and finished by AAS to provide copper, lead, zinc analyses to 0.01 wt% detection limit and silver to 0.1 ppm detection limit. 10 g of sample digested with aqua regia, MIBK extracted, finished with graphite furnace AAS to provide gold analyses to 1 ppb detection limit.

In 1998 all samples were analysed using a 0.5 g sample digested in 3 mL of equal parts HCl, HNO_3-H_2O Select higher-grade intervals were initial digestion of 1 g and then later 0.25 g of sample with 30 mL of aqua regia, diluted to 100 mL with water and finished by ICP to provide lead, zinc analyses to 0.01 wt% detection limit and silver to 0.01 oz/t detection limit.

Assaying and analyses were only carried out on selected section of drill core.

The analytical techniques are total analysis and considered to be appropriate for the style of mineralisation.

Quality of assay data are considered adequate to support a Mineral Resource estimate.

Details are presented in Appendix B.

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7.2.5 Wireframing

Six grade domains were used to define the mineralisation based on logged massive sulfide and continuous intervals of significant copper, zinc, gold, and silver mineralisation. Strings were generated for the polymetallic (copper-zinc-gold-silver) VHMS mineralisation using visual logging of semi-massive and massive sulfide mineralisation, which correlated closely to a nominal 0.5% Cu cut-off grade.

3D solid wireframes were generated for the mineralised envelopes where six mineralisation wireframes define grade domains. Figure 7-13 shows the Kona Deposit wireframes with interpreted faults.

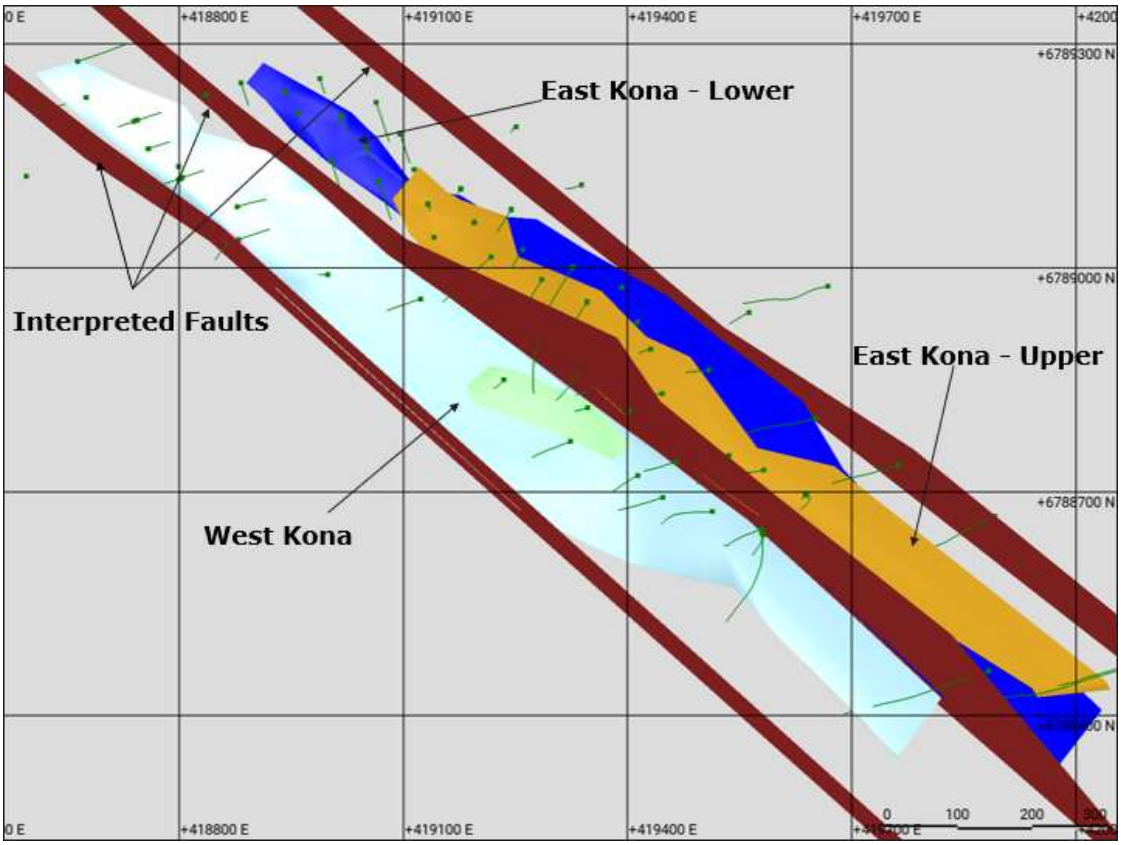


Figure 7-13: Plan view of Kona Mineralisation Wireframes and Interpreted Faults.
Source: BMC

Lithological and structural features were defined from logged and interpreted geology and the following features were created: base of overburden, faults, base of upper sediments, base of mixed volcanic sediments, top of mafic to intermediate volcanics. Wireframes were reviewed in context of the drilling and geological interpretation and ensured all wireframes were "snapped" to drill holes where possible.

A topographic surface was based on aerial photogrammetry with <5 m contour topographic control and this surface correlated well with surveyed drill collars.

A shallow weathering profile is present below the base of overburden, and a base of oxidation was modelled and the MRE was reported excluding the "oxidised" material above the base of oxidation.

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7.2.6 Statistics and Geostatistics

Classical statistical analysis was completed for samples within the mineralised envelope to provide a review of high-grade outliers. Statistical parameters for copper, zinc, gold, and silver for the combined Kona mineralised zones were plotted and reviewed and the modelled histograms and probability plots for the samples contained within mineralised envelopes did not demonstrate obvious mixed populations.

A review of grade outliers was undertaken to ensure that extreme grades are treated appropriately during grade interpolation and although extreme grade outliers within the grade populations of variables are real, they are potentially not representative of the volume they inform during estimation. If these values are not cut, they have the potential to result in significant grade over-estimation on a local basis.

Top cuts were selected following statistical review of the sample population and the strategy applied was based on the skewness of the data, probability plots, and spatial position of extreme grades. Histograms and probability plots were reviewed for copper, zinc, gold, and silver to determine the top cuts and plots were compiled based on the 1 m composites for the individual mineralised zones.

The analysis demonstrated that several elements across the mineralised zones required high-grade cuts to reduce the impact of extreme outliers. The top cuts used are shown in Table 7-13. Values of 999 were applied where top cutting was not required.

Table 7-13: Top cuts used for the Kona mineralised zones.

Object	Cu (%)	Zn (%)	Au (g/t)	Ag (g/t)
1	999	1	1.4	10
2	5	999	3	20
3	7	1.2	999	8
22	999	999	999	999
33	999	999	999	999

Source: 2025 Technical Report

An assessment of spatial anisotropy within the input data was made for each of the main Kona mineralised zones (objects 1, 2 and 3) and experimental semi-variograms were constructed in each of the three principal directions based on the anisotropic directions selected on a per-domain basis.

A semi-variogram model was then fitted to the experimental variogram and the variogram parameters were subsequently used in OK estimation of block grades. Search parameters for domains 22 and 33 – being very small subsidiary domains considered congruous to the larger domains 2 and 3 – had their search parameters copied from their respective larger domains.

Estimation parameters for each variable and each domain (except for domains 22 and 33) were optimised through quantitative KNA and block dimensions of 20 m by 10 m by 5 m (XYZ) were adopted to complete the analysis. A single block was located within the best-informed portion of each of the main domains (1 through 3) and successively optimised for maximum and minimum number of informing samples, search ellipse dimensions and number of discretisation points (used for estimation averaging across the block support). Each of these parameters was selected through the assessment of both kriging efficiency and estimate slope of regression for a range of input values for each parameter.

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7.2.7 Block Modelling

A rotated block model was created to encompass the full extent and orientation of the Kona Deposit using a parent cell size of 20 m(E) by 10 m(N) by 5 m(RL) with standard sub-celling to 5 m(E) by 2.5 m(N) by 1.25 m(RL) to maintain the resolution of the mineralised lenses.

The model cell dimensions were selected to provide sufficient resolution to the block model in the across-strike and down dip directions and a comparison of the wireframe volumes to the block model volume for each of the mineralisation objects showed that the resolution of block model sub-celling was satisfactory for use.

7.2.8 Grade Interpolation and Estimation

The wireframe objects for the six massive sulfide domains were used as hard boundaries in grade interpolation and this process reflects field observations at the mineralisation contacts.

OK was selected for grade interpolation in the mineralised zones and was selected to allow a degree of smoothing within the model based on the measured variability from the variograms. An oriented "ellipsoid" search was used to select data for interpolation and search ellipsoid orientations were based on orientations derived from variogram analysis.

An ellipsoid was produced for each individual element, with bearings varying from 114° to 305°, plunges between 5° and –20°, and dips between 90° and –87° and these orientations honour the orientation of the Kona Deposit.

A two-pass estimation search was used to complete estimation for copper, zinc, gold, and silver within the domain objects based on the variogram ranges. A first pass search radii of 45–132 m, and second pass search radii of 90–264 m along strike were used with the minimum number of samples set to four and maximum samples per hole set to four for both passes.

An average grade was used to inform remaining un-estimated blocks and greater than 75% of the blocks were estimated in the first two passes (45% pass 1, 31% pass 2).

7.2.9 Bulk Density

A large dataset of 3,828 Archimedes "water immersion" bulk density measurements exist for the Kona Deposit and fixed density values based on these data were assigned to the block model for each lithological unit. The bulk density values used for the MRE are summarised in Table 7-14. The massive sulfide density was estimated using ordinary kriging interpolation and resulted in an average bulk density of 3.57 t/m^3 across the deposit.

Table 7-14: Bulk density values applied to Kona MRE

Material type	Bulk density (t/m^3)	Description
Overburden	2.00	Above base of overburden surface and below topographic surface. Assigned directly based on the measured average.
Oxide	2.40	Above base of oxide surface and below overburden surface. Assigned directly based on the measured average.
Mixed volcanic sediments	2.79	Assigned directly to host rock based on the measured average.
Siltstone	2.82	Assigned directly to host rock based on the measured average.
Mafic	2.88	Assigned directly to host rock based on the measured average.

Source: 2025 Technical Report

7.2.10 Mineral Resource Classification

The MRE has been classified as Indicated and Inferred based on the guidelines specified in the JORC Code (2012). The classification level is based upon an assessment of geological understanding of the deposit, geological and grade continuity, drill hole spacing, search and interpolation parameters, and an analysis of the available density information (Figure 7-14).

After considering data quality, data distribution, and the good geological and grade continuity, the following approach was adopted to classify the MRE:

- The Mineral Resource was classified as Indicated where drilling had been completed at pierce points of 35–65 m (or denser), geological and grade continuity was very good and there were two or more holes on individual drill sections.
- The Mineral Resource was classified as Inferred where drilling had been completed on a broader pattern (generally greater than 80 m pierce points) and geological continuity was reasonable. Geological evidence is considered sufficient to imply but not verify geological and grade continuity.

It is the professional opinion of the Competent Person that the Kona Deposit appears to be of sufficient grade, quantity, and continuity to have reasonable prospects for eventual economic extraction as a satellite mining operation to a central processing facility at the ABM Deposit based on preliminary underground optimisation studies (Cube 2025).

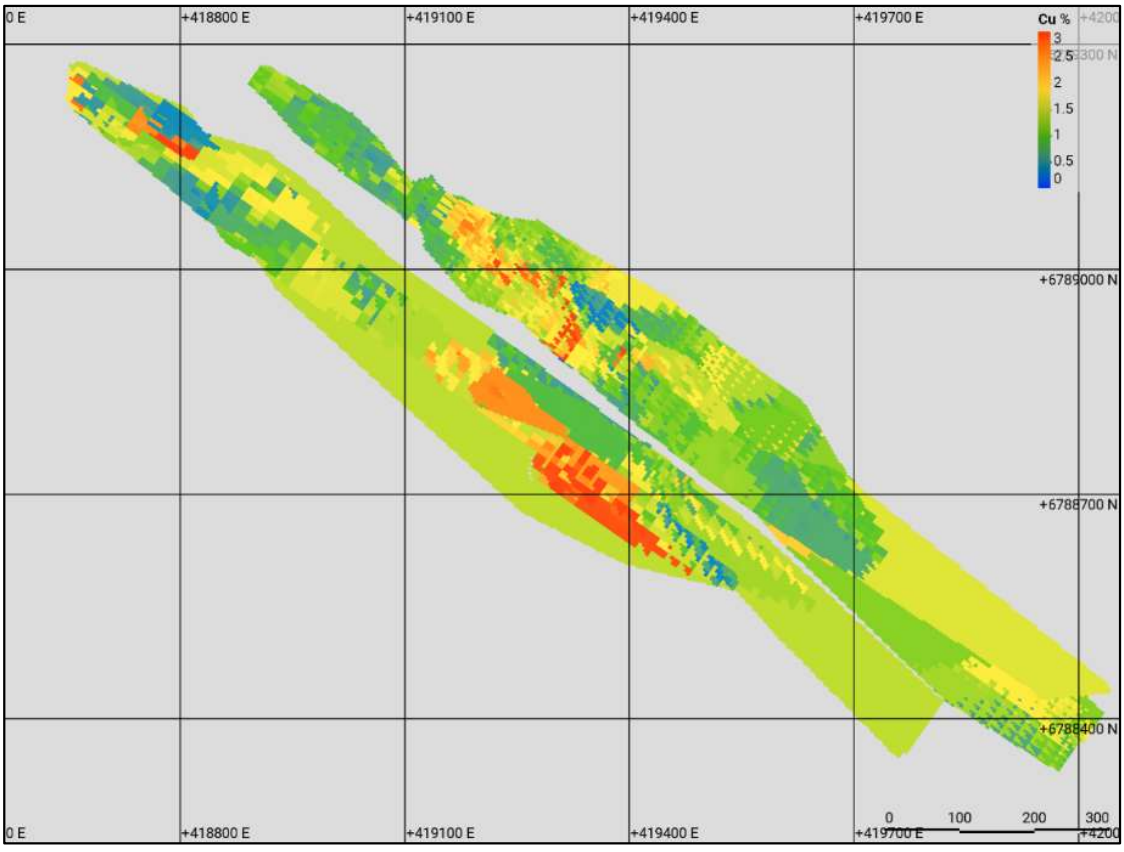


Figure 7-14: Kona block model showing Cu grades (%) (plan view) no cut-off grade applied.
Source: Cube

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7.2.11 NSR Cut-off Grades and RPEEE assessment

Cube Consulting was engaged by BMC to undertake mining optimisations (open pit and underground) for Kona to assess current prospects of eventual economic extraction (Cube 2025).

A gold price of US$3000/oz and a copper price of US$4.50/lb was used along with an exchange rate of 0.75 USD to 1 CAD. Inputs costs were based upon on-site processing and only fresh, unoxidised material being processed.

Together with the revised inputs and pricing, a new Net smelter Return (NSR) formula was derived:

$$NSR\ US\$/t = (68.31*cu_cut) + (60.26*au_cut)$$

The US dollar NSR was converted to Canadian dollars using the exchange rate:

$$NSR\ CAD\$/t = (NSR\ US\$/t)/0.75$$

$$NSR\ CAD\$/t = (91.08*cu_cut) + (80.34*au_cut)$$

Only copper and gold contribute to potential revenue. Silver does not contribute due to uncertainty of eligibility of expected concentrate grades.

Following Whittle optimisation of the Kona block model, it was noted that pit shells were not generated until much higher revenue factors of 1.4 times the base case due to the very high waste to ore stripping ratios. It was concluded that open pit mining was not viable for Kona.

Potential underground mining inventory was assessed across the Kona deposit for fresh, unoxidised material only. Allowing for additional underground mining costs, a NSR cut-off of CAD$113/t was established. Using Deswik™ software stope outlines above this cut-off were produced from the original sub-blocked model.

In addition to cut-off, the following stope outline geometries were used:

- stope outlines of 5 mH by 5mW and averaged 40 m long;
- vertical Walls (85-90°); and
- no further dilution or loss applied.

Results showed significant coverage across the mineralisation and that individual stopes could be combined into larger panels for extraction, supporting RPEEE for an underground only Mineral Resource for Kona. The stope outlines were produced as shown below in Figure 7-15.

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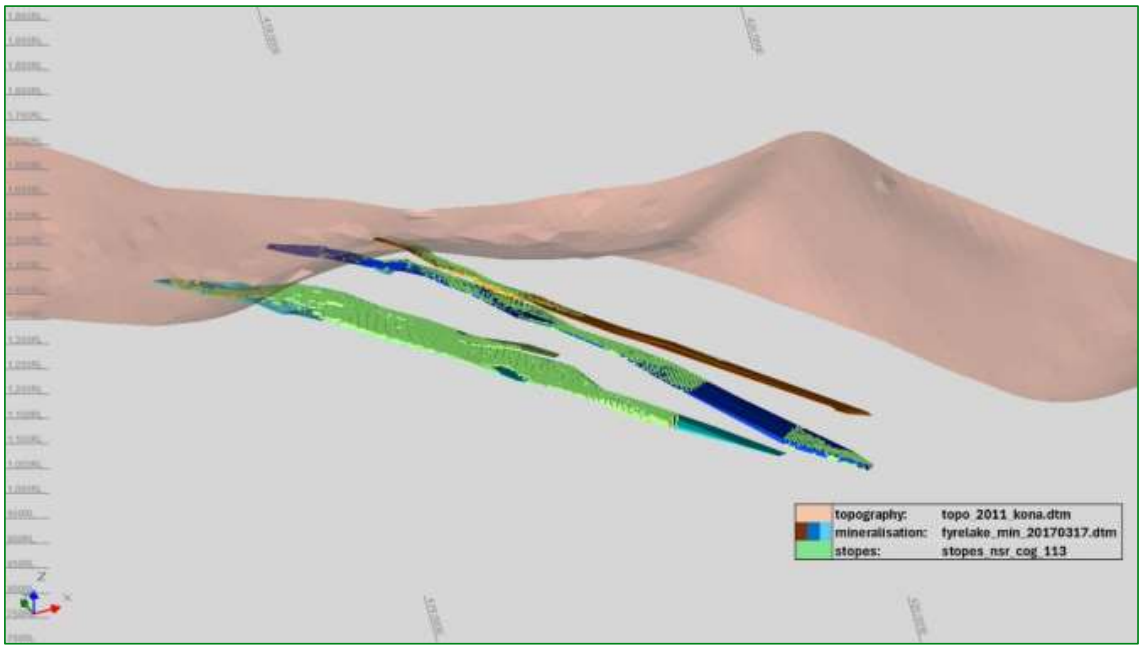


Figure 7-15: Oblique view of the interpreted Kona mineralisation - View Looking NE – Stope Outlines (pale green) over Mineralised Lodes generated for C$113/t cut-off.
Source: Cube

7.2.12 Mining and Metallurgical Methods and Parameters

The ABM Deposit has been the subject of extensive technical studies to a Feasibility Study level. Discussion of Modifying Factors and other material considerations demonstrating a robust basis for the declaration of a Mineral Resource estimate are presented in subsequent sections of this Report.

7.2.13 Mineral Resource Reporting

The estimated Mineral Resources for the Kona Deposit are reported in Table 7-15.

Table 7-15: Kona Deposit MRE

Classification	Tonnes (Mt)	Cu (%)	Au (g/t)	Ag (g/t)	Cu (kt)	Au (koz)	Ag (koz)
Indicated	2.1	1.6	0.8	4	33	53	294
Inferred	6.7	1.7	0.6	4	117	138	762
Total	**8.8**	**1.7**	**0.7**	**4**	**150**	**191**	**1,056**

Notes:

- Source: Cube Consulting
- BMC's interest in the Kona Deposit is 100% through its wholly owned subsidiary, Finlayson Copper Ltd.
- Mineral Resources are reported in accordance with the JORC Code by Aaron Green, Competent Person, FAIG.
- The Effective Date of this MRE is 30th June 2025.
- Numbers have been rounded to reflect the precision of an Indicated and Inferred MRE (noting that MRE are, by nature, approximate, and with a degree of uncertainty).
- The Kona MRE has been reported above an NSR cut-off of C$113/t.
- Silver was concluded not to be economic and thus is not included in the NSR calculation.
- NSR formula: NSR US$/t =((68.31*Cu_cut) + (60.26*Au_cut)).
- An exchange rate of 0.75 CAD:USD.
- Preliminary underground optimisation studies support the reporting of the Mineral Resource above the C$113/t cut-off particularly as a satellite mining operation to a central processing facility at the Kudz Ze Kayah Project.
- The Kona MRE is not included in the feasibility studies completed since 2015.

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7.3 MRE Discussion

7.3.1 ABM Deposit

ERM is of the opinion the drilling, surveying, sampling and analytical methods, and quality assurance processes implemented by BMC during the exploration and resource drilling campaigns are suitable and adequate and reasonable for the style of deposit under consideration in this Report.

In ERM's professional opinion, Ordinary Kriging is an appropriate grade interpolation mechanism for the ABM Deposit given the current level of project development and available data. The KNA undertaken confirmed that reliable block estimates were achieved to enable the resources to be classified as Indicated and Inferred Mineral Resources.

Geological interpretation is considered by ERM to be a risk factor where the revision of mineralisation models, modelling of internal waste domains, modelling of dykes and structural offsets such as faults and shear zones must be completed as new data are obtained and geological understanding improves.

ERM further suggests that infill drilling is required to define the mineralisation and improve the level of confidence in the current Mineral Resource classification.

Based on the results of the 2023 Economic Update captured in the 2025 Technical Report summary of the Feasibility Study work, the ABM Deposit is of sufficient grade, quantity, and continuity to have reasonable prospects for eventual economic extraction.

7.3.2 Kona Deposit

ERM is of the opinion the historical 1996 and 1997 exploration and resource drilling data (validated by BMC), including drill hole spacing, surveying, sampling and analytical methods, and quality assurance processes, was suitable, adequate and reasonable for the style of deposit under consideration in this Report. The Kona Deposit remains open, and infill and extension drilling are required to fully define the mineralisation extents and improve the level of confidence in the current Mineral Resource classification.

ERM further believes that Ordinary Kriging is an appropriate grade interpolation mechanism for the Kona Deposit given the current level of project development and the available data. The KNA undertaken confirmed that reliable block estimates were achieved to enable the resources to be classified as Indicated and Inferred Mineral Resources.

Based on the results of Cube's 2025 RPEEE assessment (which included data from the 2025 Technical Report), the Kona Deposit concluded to be of sufficient grade, quantity, and continuity to have reasonable prospects for eventual economic extraction.

Also, the deposit appears to be of sufficient grade, quantity, and continuity to have reasonable prospects for eventual economic extraction, particularly as a satellite mining operation to a central processing facility at the Kudz Ze Kayah Project, however detailed mining studies are required to validate this opinion.

ERM notes that the NSR defined volumes that define the Mineral Resource estimate were defined solely by copper and gold. The Mineral Resource estimate contains over 1 Moz of silver. It is not clear at this stage whether or not a smelter would recognise the silver in payment for concentrates. But until a Feasibility Study is completed for the Kona Deposit and an offtake contract finalised for the concentrate from Kona, it is ERM's opinion that it is appropriate to include the silver endowment in the Mineral Resource estimate.

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8. HYDROLOGY AND HYDROGEOLOGY

The ABM Mine Project lies in the Geona Creek catchment, central to which is Geona Creek, a north-flowing tributary to Finlayson Creek. Finlayson Creek meets the outflow of Finlayson Lake below the Robert Campbell Highway and flows east to eventually join the Frances River and then the Mackenzie River (Figure 8-1).

The following is a précis of a large body of work that BMC and its consultants have completed over the past decade.

The Geona Creek watershed covers approximately 26 km^2 (Figure 8-1), has a median elevation of 1,479 m ASL and spans from the alpine to forested areas at lower elevations. The Finlayson Creek catchment area is approximately 35 km^2 above the confluence with Geona Creek and expands to 211 km^2 where it flows under the Robert Campbell Highway, shortly before it joins the outflow of Finlayson Lake. The southern watershed divide between Geona Creek and South Creek is located immediately south of the ABM Deposit and is characterised by several small lakes, locally referred to as South Lakes.

Fault Creek is the most significant tributary to Geona Creek in the deposit area, emptying into Geona Creek immediately south of the ABM Deposit. The small Fault Creek catchment area (2 km^2, 1,708 m median elevation ASL), to the west of Geona Creek is steeper, with similar vegetation.

Site discharge is typically characterised by high spring snowmelt-driven flows, lower summer flows sustained by groundwater inflows and periodic rainfall events, followed by large autumn rainfall events. Winter flow is very low due to cold temperatures, freezing conditions and the gradual depletion of groundwater storage. There is typically a distinct flow peak in late May or June and another peak in September and early October and there have been rainfall-induced peaks recorded in mid-summer, particularly in July.

8.1 Water Quality

Creeks that drain the ABM Mine Project are neutral to alkaline (pH 6.4 to 8.7; median 7.7) with hardness increasing from moderately hard (South Creek and Fault Creek) to hard (Geona Creek) in the upper watershed to very hard (Finlayson Creek and East Creek) in the lower watershed.

Water quality is compared against the most recently revised water quality guidelines for protection of aquatic life established by the Canadian Council of Ministers of the Environment, British Columbia Ministry of Environment and Parks, or Environment and Climate Change Canada.

Water quality guideline exceedances are observed regularly for a number of constituents including arsenic, cadmium, copper, fluoride, iron, phosphorus, and zinc, and occasionally for other constituents including aluminium, chromium and cobalt. Most of these exceedances, except selenium, coincide with freshet, when total suspended solid concentrations are highest, and metal(loid)s are largely transported as particulates.

In general, more water quality guideline exceedances are observed for total metal concentrations than their dissolved counterparts, suggesting that a significant portion of the metals were particulate-bound, especially during freshet and/or other periods characterised by elevated total suspended solid levels. The fact that dissolved metal concentrations exhibited much less frequent water quality guideline exceedances is important, since it is the dissolved fraction that is the most bioavailable.

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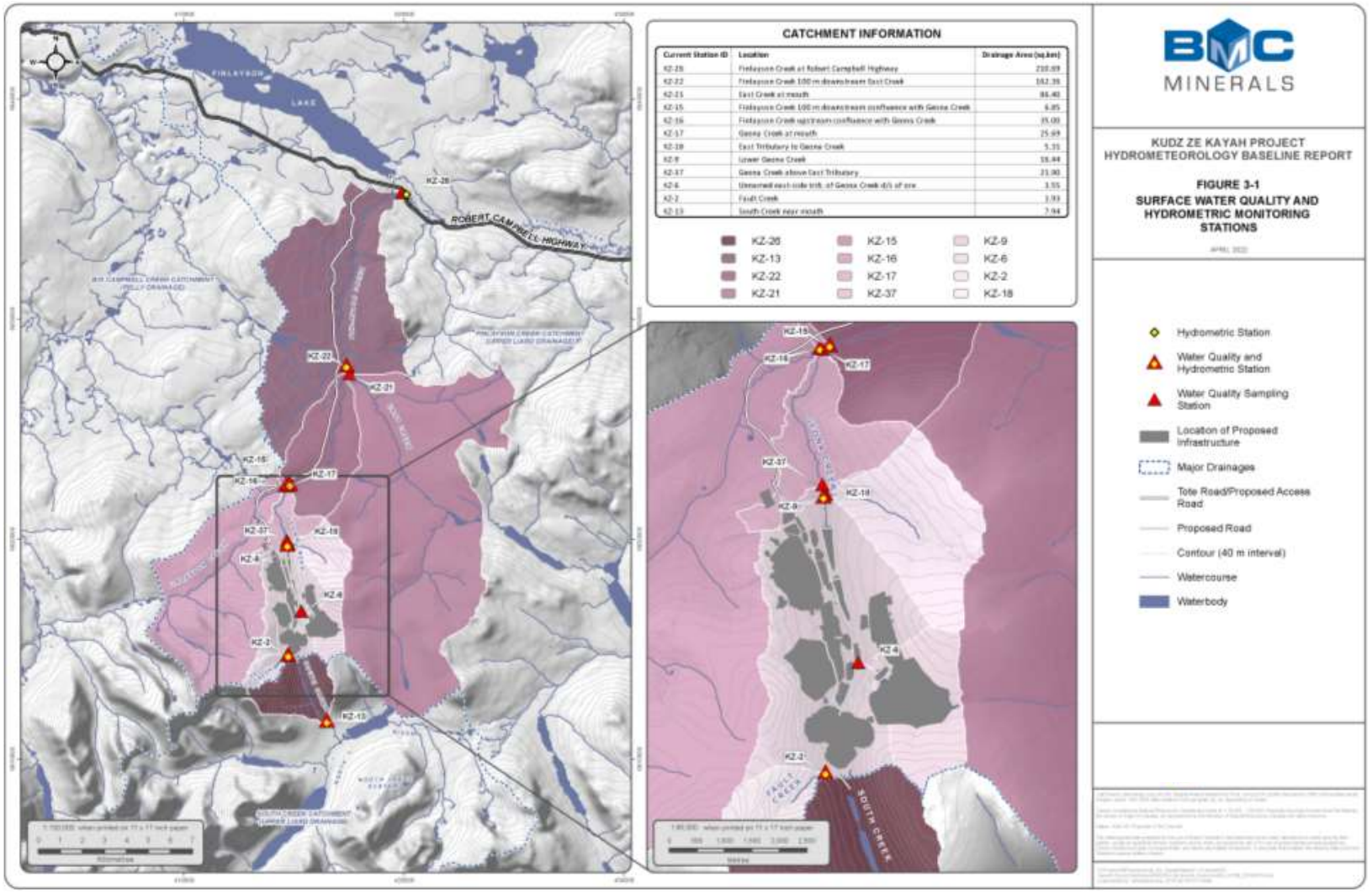


Figure 8-1: Kudz Ze Kayah district catchments and water monitoring locations./Source: BMC

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8.2 Hydrogeology

The principal hydrogeological units are bedrock and overburden where the overburden consists of two subunits comprising fine-grained lower permeability sediments composed of silts and fine sands, and coarse-grained higher permeability sands and gravels.

Bedrock hydraulic conductivity does not appear to exhibit a trend of increasing or decreasing hydraulic conductivity to a depth of approximately 50 m below the bedrock surface. There is generally a decreasing trend in bedrock hydraulic conductivity below this depth, with faults and fracture zones are expected to have higher hydraulic conductivity than the surrounding bedrock.

Groundwater level monitoring was first conducted in 1995 and has been conducted regularly since 2015. Water levels in both bedrock and overburden monitoring wells generally exhibit the following seasonal trends:

- Rising through the summer months (approximately May to August).
- Maximum reached between August and September.
- Falling through the winter months (approximately October to March).
- Minimum reached between April and May.

The seasonal variation in monitoring well levels ranges from 2 m to 8 m in most wells; the maximum observed variation has been 17 m.

Project-wide, the groundwater field pH ranges from acidic to alkaline (5.7 to 10.4, or an average value of 7.4) for both bedrock and overburden monitoring wells.

Groundwater quality results are compared against the *Yukon Contaminated Sites Regulation* or the Federal Interim Groundwater Quality Guidelines, indicating exceedances of arsenic, cadmium, cobalt and zinc.

Sulfate and fluoride concentrations are generally higher in wells screened in bedrock compared to overburden; however, the concentrations of other anions, nutrients, and metals do not show marked differences between overburden and bedrock wells.

Groundwater sampled in the proposed open pit area generally returned higher anion, nutrient, and metal concentrations than groundwater sampled elsewhere on the KZK Property. Groundwater concentrations of cadmium, iron, zinc and other constituents are elevated in the proposed open pit area relative to the rest of the KZK Property, likely due to the subsurface mineralisation present in this area. Additionally, sulfate concentrations are typically more elevated within the proposed pit area and are likely due to the oxidation of the sulfidic minerals in the deposit. The current groundwater monitoring network consists of 43 bedrock and overburden wells strategically installed around the ABM Mine Project area that are monitored quarterly.

Hydrogeological data collected at the KZK Property have been used to develop conceptual and numerical models of groundwater flow at the site. These data include water levels and quality in the monitoring wells, geological information, surface water flows and quality, permafrost distribution and hydraulic conductivity.

The numerical groundwater flow model included both steady-state and transient model simulations. The steady-state model was calibrated to baseline groundwater levels and Geona Creek base flows and was then used as initial conditions for the transient flow model. The transient flow model was calibrated to long-term aquifer tests to determine values for hydraulic conductivity and storage. During calibration, a sensitivity analysis was conducted on the transient flow model to help select parameters that should be adjusted in calibration, and which could be left at values derived from

field observations. The calibrated groundwater flow model was used to simulate the hydrological sequence associated with the 9-year excavation of the ABM open pit and development and operation of the underground mine.

Model simulations were conducted to evaluate pathways for potential contaminant migration and travel time to or from the open pit, the waste storage facilities, and the water management ponds during mine reclamation and closure. Post-mining model simulations assumed the underground workings to be permanently closed and not interacting with the open pit lake.

There is not expected to be significantly increased pressure heads within the sealed underground workings relative to the open pit due to the interconnected nature of the faults traversing the area.

8.2.1 Hydrogeology Conclusions

- The numerical groundwater flow modelling predicts that pre-mining dewatering of overburden at the open pit will require four trenches to be excavated perpendicular to the main trench (Figure 8-2). The initial month of overburden dewatering is predicted to produce flows of around 8,100 m^3/day (94 L/s), decreasing over time to around 2,200 m^3/day (26 L/s).
- Except for areas of faulting or significant fracturing, the open pit bedrock appears to be of sufficiently low permeability to permit water seepage to be managed using face seepage drains and horizontal drains in the pit wall, as necessary. Depending on the nature of the distribution of fracture sets or other prominent fault conduits intersecting the open pit within the bedrock, it was suggested it may be worthwhile to install approximately 15, 100 m deep dewatering wells at 500 m spacing around the perimeter of the excavation, to minimise seepage face flow. More or less wells may be needed depending upon observed conditions during excavation of the pit.
- Fault zones within the underground workings are expected to produce water at variable rates of discharge and require the drilling of horizontal drains to stabilise hydraulic conditions locally. These are predicted by the numerical model to drain an estimated 1,100 m^3/day (13 L/s) from the underground workings. Flow from the faults may be brief as they locally drain or are sustained if they are hydraulically connected to bedrock around an extensive fault-conduit feature.
- Following completion of mining and cessation of mine dewatering, the open pit will begin to refill as a result of direct precipitation, redirected surface water flow from Fault Creek, and groundwater seepage. The open pit is predicted by the numerical model to have filled to half its depth approximately four years after the end of operations and to fill completely to the spill elevation of 1,380 m ASL after approximately 16 years.
- The open pit lake (referred to as ABM lake) will act as a flow-through lake through which streamflow enters and leaves, and with groundwater inflows predicted to be approximately 1,400 m^3/day.
- Particle tracking simulated using the numerical flow model indicates that groundwater originating from the waste storage facilities and ABM lake flows towards Geona Creek. This flow either discharges immediately to Geona Creek or travels through overburden along the valley bottom, eventually discharging to Geona Creek.

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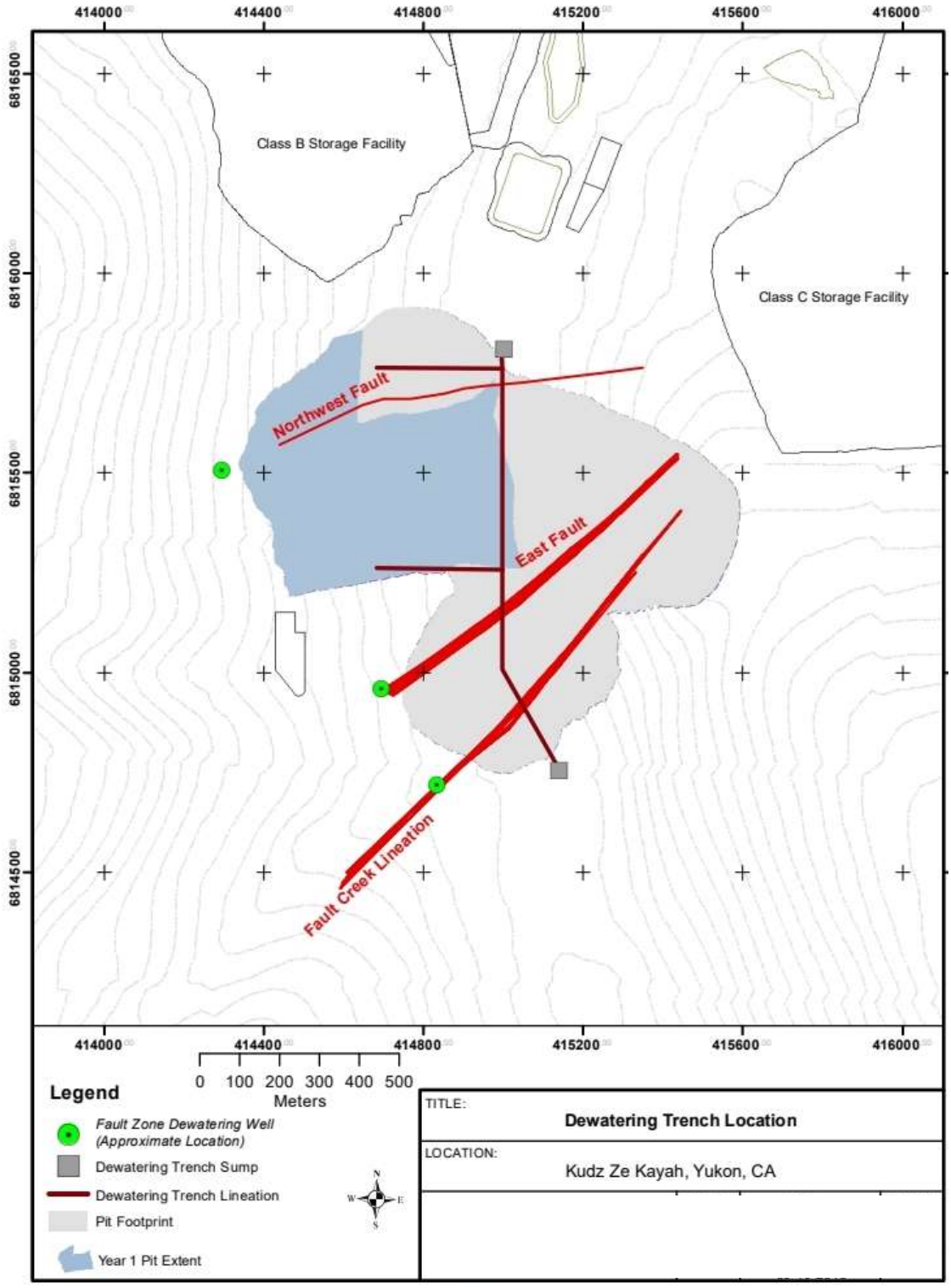


Figure 8-2: Proposed dewatering trench locations
Source: BMC

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8.2.2 Water Quality Modelling

A water quality model has been developed to estimate the water quality in mine discharge and receiving environment waters and to help guide water quality management for the ABM Mine Project. The model incorporates data from the groundwater and surface water quality baseline monitoring, meteorological studies, site water balance data, hydrogeological modelling results, and laboratory and field based geochemical testing of trace element leaching from site material. Water quality modelling was performed on a monthly time step through the construction, operations and closure phases of the project to estimate seasonal variation.

Kinetic testing of waste rock and tailings material for the Project suggested that the time to acid generation is several (Class A) to tens (Class B) of years.

Loading rates were developed for the drainage from each of the storage facilities based on the results of the kinetic tests and the proportions of each domain that comprise each facility.

Multiple sets of source terms were developed to predict neutral and acidic waste rock drainage chemistry throughout the course of the Project. For each these, a Base Case and Upper Case set of source terms were developed:

- Base case source terms used the median of the last 20 weeks of kinetic test loading rates, reflecting steady state conditions in the kinetic tests.
- Upper case source terms used the 75th percentile of the weekly loading rates for each kinetic test, reflecting an increased weathering rate that might be expected from freshly exposed material.

8.2.3 Construction

During the Construction phase of the project, constituents of potential interest concentrations in the Geona and Finlayson Creek receiving environment were estimated to be generally comparable to, or slightly lower than baseline due to the diversion of upstream waters (i.e. Fault Creek) and dilution from discharge of the ABM Open Pit dewatering water for all scenarios.

The Fault Creek diversion results in increased estimated selenium, cadmium and zinc concentrations in South Creek, but do not exceed preliminary water quality objectives.

8.2.4 Operations

During Operations, constituents of potential interest concentrations in discharge from Lower Water Management Pond increase slightly each year, reflecting increases in load contribution from open pit wall runoff as the ABM Mine open pit is excavated.

No water quality parameter concentrations were estimated to exceed their respective preliminary water quality objectives under either the Base Case simulation or the more conservative Upper Case simulation under all precipitation scenarios.

8.2.5 Active and Transition Closure

During the Active and Transition Closure phases, constituents of potential interest concentrations in South Creek were predicted to return to baseline levels as the Fault Creek diversion is removed, allowing South Creek to revert to its pre-Project flow regime.

Elsewhere, constituents of potential interest concentrations in the Geona and Finlayson Creek receiving environments are predicted to increase during Active Closure due to drain-down of the Class A and B Storage Facilities; however, water from the drain-down of these facilities will be treated in the water treatment plant to ensure that water quality objectives are met.

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The Upper Case simulation predicted periodic exceedances of a few constituents of potential interest related to runoff from the Class C Storage Facility, but treating this water in the water treatment plant resolves these exceedances.

During the active and transition to closure phases, the ABM open pit will flood, forming an ABM lake approximately 16 years after the cessation of mine dewatering. During this filling period, *in situ* treatment will be conducted to significantly lower concentrations of antimony, arsenic, cadmium, copper, lead, selenium, uranium, and zinc that are solubilised from the load accumulated on the pit floor and walls.

8.2.6 Post Closure

Outflow from ABM Lake marks the start of the Post Closure phase, resulting in increases in some constituents of potential interest concentrations in Geona Creek. No exceedances of any preliminary water quality objectives were predicted in Geona Creek, Finlayson Creek or South Creek during Post Closure for the Base Case and Upper Case under all precipitation scenarios.

8.3 ERM Opinion

ERM is of the opinion that adequate and reasonable investigative activities and desktop interpretive modelling work has been completed to inform an understanding of the hydrology and hydrogeological framework as it pertains to the proposed operations at the ABM Mine.

While various groundwater flow and water quality models have been employed for evaluation, which are recognised and standard tools in the field, it is important to acknowledge that these models are inherently reliant on the datasets and assumptions that underpin their development.

Ongoing monitoring and the advancement of hydrogeological understanding will be essential throughout the project to both confirm and refine/update the conceptual and numerical models, as well as their associated predictions. This process will necessitate adjustments to mine designs and water management practices as needed.

Regular reviews of data and updates to the models will be important. Ultimately, these efforts will contribute to the updates of the Adaptive Water Management Plan, particularly regarding the proposed management responses and potential mitigation measures that should be implemented as key trigger values are approached.

The primary focus remains on safeguarding the surrounding water environment.

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9. MINING AND ORE RESERVE ESTIMATES

BMC has commissioned and completed a range of technical mining and feasibility studies on a combined open pit and underground mining approach for the ABM Mine Project. Extraction of the ABM Deposit is planned by open pit (89% of ore) and underground (11% of ore) mining methods.

The general arrangement of the mine site is illustrated in Figure 9-1 and shows the location of the processing plant, administration buildings, infrastructure, waste and tailings disposal sites relative to the open pit mining areas.

Four separate phases of open pit mining are proposed for the ABM Zone to manage overall waste stripping requirements, while the adjoining Krakatoa Zone will be mined as a single phase. The underground operations will start in Year 3, extracting the lower Krakatoa Zone. An in-pit portal will be developed once the ABM open pit is deep enough. The underground mining of the Krakatoa Zone beneath the open pit will be predominantly via longhole open stoping with paste fill securing the voids produced. Approximately 14.0 Mt of ore will be mined from the open pit and 1.7 Mt of ore from underground. 138.4 Mt of waste will be mined by open pit mining methods, for an expected average life-of-mine (LOM) strip ratio of 10:1. The initial ABM Zone pit has an expected strip ratio of 6:1, to optimise payback of pre-production capital.

Waste material mined from the open pit and underground would be stored permanently on surface. Wherever possible suitable waste material will be used for the infrastructure construction.

Open pit mining will take approximately nine years, including pre-production mining requirements using an owner operator model.

Mining operations were costed for the 2023 June quarter work adopting an owner-miner strategy for open pit mining costs. BMC prepared this estimate with input and review from an ex-mining contractor peer reviewer. However, the underground mining costs for the 2023 estimate were updated by a mining contractor.

BMC has updated its assessment of the economics of the Kudz Ze Kayah Project (ERM 2025b) and the update has been completed to reflect a June 2023 quarter cost base, commodity price and exchange rate outlook.

A Feasibility Study to assess the economic viability of mining and processing the ABM Deposit has been completed and updated several times. The Feasibility Study-level investigations, with key metrics having been recently reviewed and updated, is summarised in the 2025 Technical Report (ERM 2025b).

ERM notes that whilst the Feasibility Study-level investigations, Mineral Resource Estimate and Ore Reserve Estimate were completed in accordance with Canadian Institute of Mining, Metallurgy and Petroleum Standards (CIM 2014), and reported in accordance with NI 43-101, the Canadian standards are functionally equivalent to Australian JORC Code standards and definitions, and as such are able to be reported in accordance with the JORC Code in this report.

All Ore Reserves are classified as Probable Ore Reserves, since no Measured Mineral Resources were declared for the ABM Deposit.

The Ore Reserve includes external dilution that will be mined in conjunction with the Ore Reserve shapes and delivered to the process plant.

No Inferred Mineral Resources are included in the ORE.

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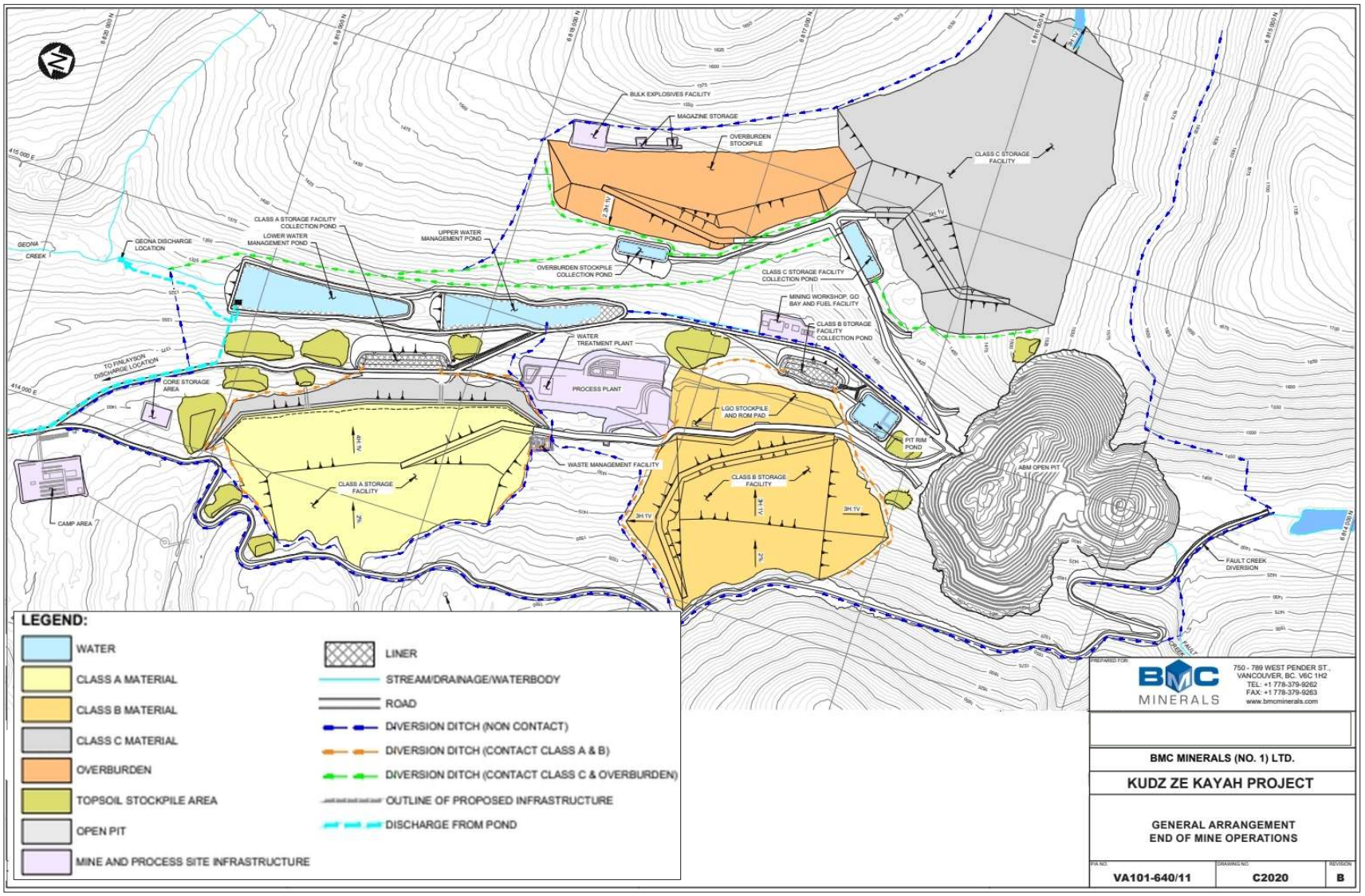


Figure 9-1: General Site layout for the ABM Mine Project (at the end of mining).
Source: BMC

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9.1 Mining Schedule – Life-of-Mine Plan

Open pit mining (from the ABM pit) forms the largest portion of the LOM plan with an estimated production period of nearly nine years mining ore following construction. The total production from the Krakatoa component of the open pit and Krakatoa underground is scheduled to fall within the timeframe of the ABM open pit production.

Considering pre-strip (following construction, Year -1), mining ore, and processing (which continues after mining stops), LOM activity extends over approximately nine years.

The mining schedule is summarised in Table 9-1.

Table 9-1: Kudz Ze Kayah Project – ABM mine schedule

Source	Unit	Total	Year -1	Year 1*	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8
Open pit (ABM and Krakatoa)											
Ore to be mined	Mt	14.0	<0.1	1.8	2.2	1.8	2.1	2.3	1.4	1.5	0.9
Ore grade (Zn)	% Zn	5.9	8.1	6.5	6.3	6.5	5.3	5.6	5.9	5.5	5.4
Ore grade (Cu)	% Cu	0.9	0.4	0.5	0.9	1.1	1.2	1.0	1.0	0.7	0.8
Ore grade (Pb)	% Pb	1.6	2.9	2.0	1.7	1.6	1.3	1.5	1.4	1.6	2.2
Ore grade (Au)	g/t Au	1.3	2.0	1.7	1.5	1.3	1.2	1.2	1.0	1.2	1.6
Ore grade (Ag)	g/t Ag	136	221	165	147	142	121	123	107	126	174
Ore grade (Fe)	% Fe	30	28	29	31	32	32	29	31	29	27
Ore grade (As)	ppm As	2,530	3,094	3,261	3,244	2,534	2,209	2,411	1,572	1,806	3,051
Ore grade (Hg)	ppm Hg	18	16	23	23	21	18	15	9	16	18
Ore grade (Sb)	ppm Sb	464	1,059	712	646	485	376	413	246	307	408
Ore grade (Se)	ppm Se	208	122	160	202	197	187	181	270	273	244
Waste	Mt	138	6	14	30	32	27	10	10	6	3
Strip ratio	t:t	9.9	303.1	7.8	13.7	17.8	12.9	4.4	7.4	4.1	2.9
Underground (Krakatoa only)											
Ore to be mined	Mt	1.7	-	-	-	-	-	0.3	0.6	0.5	0.3
Ore grade (Zn)	% Zn	5.0	-	-	-	-	-	4.9	5.1	5.2	4.6
Ore grade (Cu)	% Cu	0.4	-	-	-	-	-	0.4	0.4	0.5	0.4
Ore grade (Pb)	% Pb	2.3	-	-	-	-	-	2.6	2.5	2.3	1.7
Ore grade (Au)	g/t Au	1.3	-	-	-	-	-	1.3	1.2	1.3	1.2
Ore grade (Ag)	g/t Ag	147	-	-	-	-	-	144	147	154	137
Ore grade (Fe)	% Fe	19	-	-	-	-	-	18	19	19	18
Ore grade (As)	ppm As	2,978	-	-	-	-	-	3,349	3,063	3,064	2,415
Ore grade (Hg)	ppm Hg	15	-	-	-	-	-	11	14	17	14
Ore grade (Sb)	ppm Sb	456	-	-	-	-	-	503	436	478	421
Ore grade (Se)	ppm Se	108	-	-	-	-	-	96	116	110	101
Waste	Mt	0.6	-	-	-	0.0	0.1	0.3	0.2	0.0	0.0
TOTAL											
Ore to be mined	Mt	15.7	0.0	1.8	2.2	1.8	2.1	2.5	2.0	2.0	1.3
Ore grade (Zn)	% Zn	5.8	8.1	6.5	6.3	6.5	5.3	5.5	5.7	5.5	5.2
Ore grade (Cu)	% Cu	0.9	0.4	0.5	0.9	1.1	1.2	0.9	0.8	0.7	0.7
Ore grade (Pb)	% Pb	1.7	2.9	2.0	1.7	1.6	1.3	1.6	1.7	1.7	2.1
Ore grade (Au)	g/t Au	1.3	2.0	1.7	1.5	1.3	1.2	1.2	1.1	1.2	1.5
Ore grade (Ag)	g/t Ag	138	221	165	147	142	121	125	119	133	164
Ore grade (Fe)	% Fe	29	28	29	31	32	32	28	27	26	25
Ore grade (As)	ppm As	2,579	3,094	3,261	3,244	2,534	2,209	2,507	2,015	2,138	2,882
Ore grade (Hg)	ppm Hg	18	16	23	23	21	18	15	11	16	17
Ore grade (Sb)	ppm Sb	463	1,059	712	646	485	376	423	302	352	412
Ore grade (Se)	ppm Se	197	122	160	202	197	187	172	224	230	206
Waste	Mt	139	6	14	30	32	27	10	11	6	3

* Year 1 is post construction

Source: 2025 Technical Report

9.2 Revenue Parameters

The Resource model was populated with an NSR field to represent the revenue received from each unit of metal at the mine gate, hence net of all downstream costs. The NSR (*Free on Board (FOB) Mine Gate and Royalties by unit of metal in ROM Feed*) was calculated on a block-by-block basis for copper, lead, zinc, gold and silver based on the following:

- Metal prices
  - Copper – US$3.80/lb
  - Lead – US$0.95/lb
  - Zinc – US$1.20/lb
  - Gold – US$1,700/oz
  - Silver – US$22.60/oz.
- Diluted block grade for copper, lead, zinc, gold and silver.
- Processing recovery to concentrate of all revenue elements for each of the three concentrate products.
- Grade of any contaminant elements based on concentrates produced from testwork.
- Metallurgical domain (+1340 RL, Met 2-4, Met 5-7, Met 8 and Krakatoa).

The NSR field represents the net revenue to Mine Gate after accounting for the following deductions

- Treatment and refining charges.
- Penalties due to contaminant elements (if present).
- Transport costs
  - Road transport
  - Port charges
  - Shipping
- Royalties
  - Yukon Government
  - First Nations payments

9.3 Open Pit Mining

The open pit mining study for the ABM and Krakatoa Zones consisted of an optimisation, stage sequence selection and mine design where the stages were designed and subsequently scheduled to produce a mining and production schedule that was appropriate for development.

9.3.1 Geotechnical Parameters

A geotechnical structural model was developed using geotechnically logged core, televiewer data and core photos. Geotechnical data informing the project comprised geotechnical logs of geotechnical drill holes (7,378 m), supplemented with exploration drilling logs from core photographs and a structural interpretation of televiewer surveys.

A total of 29 significant geotechnical features were identified and modelled in 3D and these have been classified according to orientation.

A range of analyses were conducted to determine stable open pit slope parameters and included a rock bridge analysis, a structural stability analysis, and limit equilibrium and stress reduction analyses.

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The Mining Rock Mass Model was interrogated in section and in plan to assess the variability of the input parameters and the effect of the overall slope angle for the proposed open pit design. The project area has been subsequently divided into seven domains with specific design parameters for the open pits related to these individual geotechnical domains and features within the open pit designs.

The geotechnical domains and slope sections evaluated using limit equilibrium are Figure 9-2.

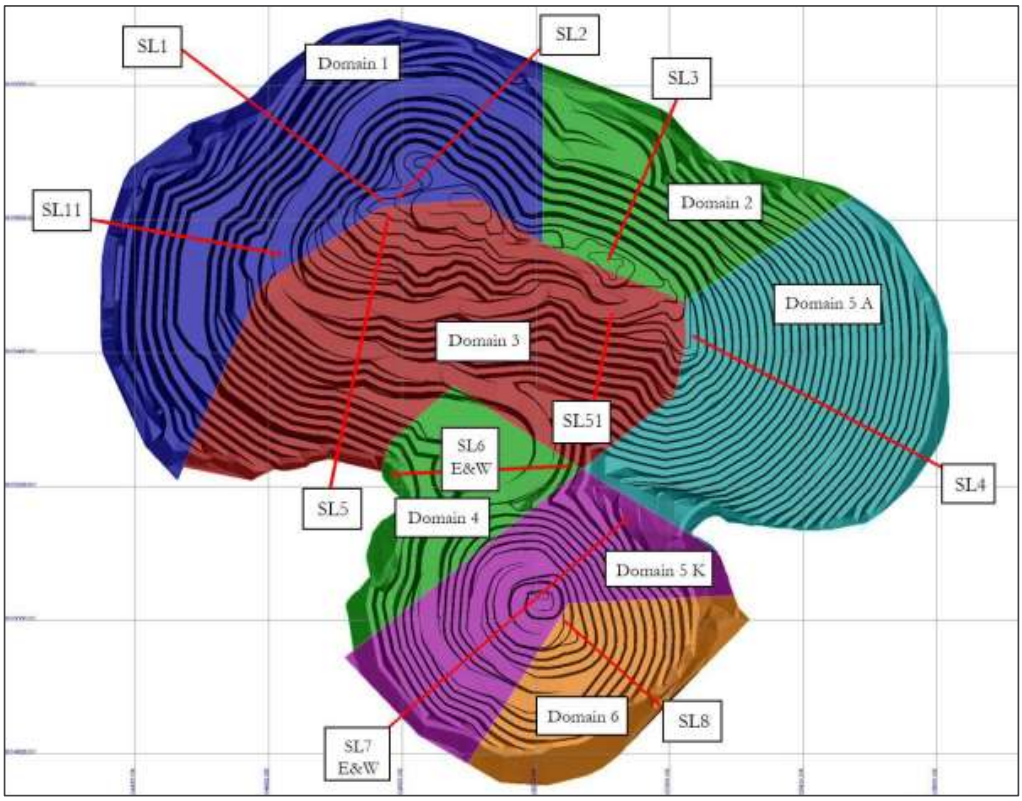


Figure 9-2: Geotechnical slope zones for ABM and Krakatoa pits
Source: BMC

The open pit optimisation evaluated several slope sets with the primary aim of placing the haul roads on the hangingwall or the footwall of the main open pit development. A complete set of slope profiles implemented in the final pit optimisations are shown in Table 9-2.

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Table 9-2: Slope profiles – Final Open Pit Optimisation

Zone code	Profile	North (0°)	East (90°)	South (180°)	West (270°)
1	Domain 1 ABM	44.5	46.7	42.9	42.9
2	Domain 2 East	46.7	38.3	34.0	46.5
3	Domain 3 ABM	44.5	38.3	27.5	42.9
4	Domain 4 K	34.0	43.2	40.7	43.2
5	Domain 5 ABM	39.0	38.3	38.3	47.0
6	Domain 6 K	35.0	34.3	26.3	34.3
7	Default	45.0	45.0	45.0	45.0
8	Krakatoa (D5K)	36.3	36.3	27.6	27.6
9	Overburden	25.0	25.0	25.0	25.0
10	ABM West Fault	46.1	47.0	34.0	34.0
11	Domain 2 West	47.0	38.3	27.5	42.9

Source: BMC

The final pit design was evaluated for overall slope stability using limit equilibrium analyses and the resultant Factors of Safety were equal to or exceed 1.2 and are within accepted guidelines for open pit slope stability.

A slope monitoring programme including tension crack mapping, surveys and groundwater monitoring will be implemented at the commencement of mining to minimise the adverse effects of any instability on slope development.

9.3.2 Whittle™ Optimisation

A Whittle™ optimisation process was undertaken for both the ABM and Krakatoa zones. The resultant selected ABM pit shells, by tonnes of waste and ore, including cash flows (undiscounted and discounted), are shown in Figure 9-3.

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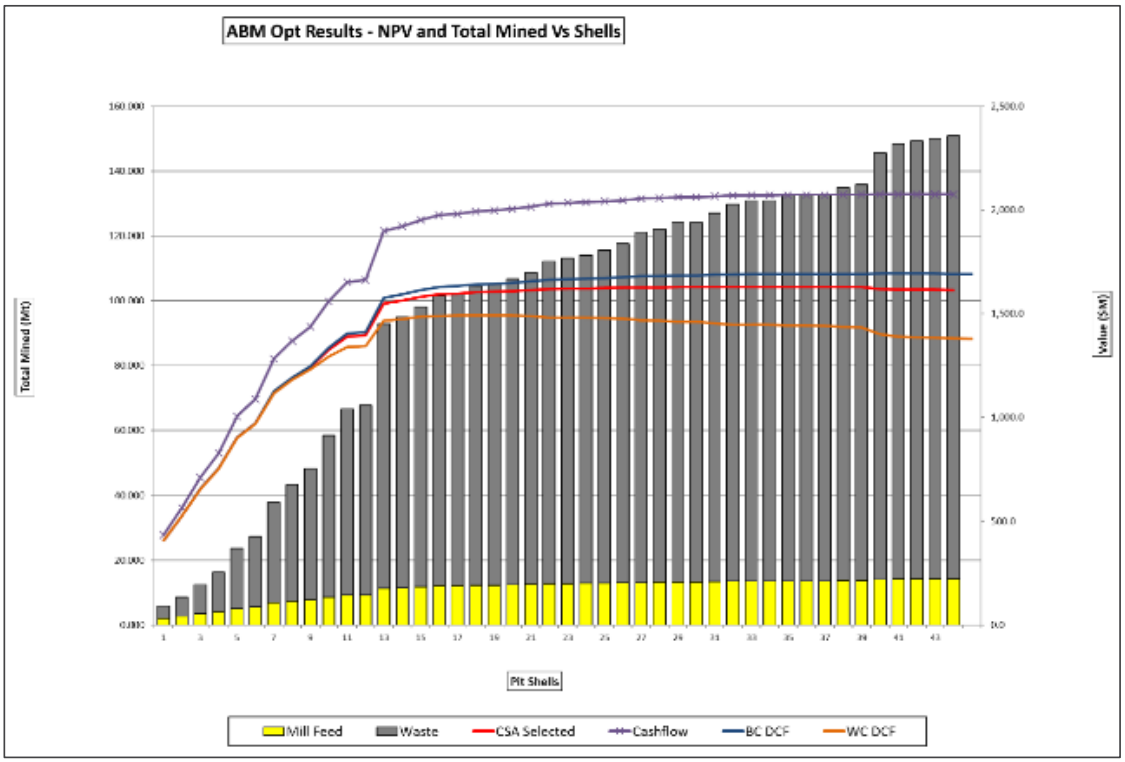


Figure 9-3: ABM optimisation results – NPV and mined material

Pit shell 33 was selected as the final pit shell for the ABM open pit. Pit shells 2, 6 and 12 were selected to guide the design for the interim stages (i.e. pushbacks) of the pit. The key properties of the ABM pit stages (as defined during the Whittle™ optimisation process) for the selected shells, are shown cumulatively in Table 9-3.

Table 9-3: Selected pit shells cumulative properties – ABM pit

Shell no.	Revenue factor	Pit shell depth	Total mined (Mt)	Waste mined (Mt)	Strip ratio	ROM feed (Mt)	Grade Cu%	Grade Pb %	Grade Zn%	Grade Au g/t	Grade Ag g/t	CSA Global NPV (CAD $M)	Opex (C$/t)
2	0.22	245	8.6	5.9	2.2	2.7	0.7	1.9	6.6	1.6	162	526	48.72
6	0.30	290	27.2	21.6	3.9	5.6	0.8	1.8	6.5	1.5	149	972	56.13
12	0.42	325	67.7	58.4	6.3	9.2	1.0	1.7	6.1	1.4	144	1,395	67.31
33	0.84	350	130.8	117.3	8.7	13.5	0.9	1.5	5.9	1.3	130	1,629	78.20

Source: 2025 Technical Report

The Krakatoa pit will be mined as a single stage, as the pit is small and mined near the end of the project life. Pit shell 13 was selected as a candidate for the pit design (Table 9-4). A portion of the waste material in the Krakatoa pit will be mined early to create a lay down and portal staging area for the planned underground operation. The remainder of the pit is planned to be mined toward the end of the project and concurrently with underground mining.

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Table 9-4: Selected pit shell properties – Krakatoa

Shell no.	Revenue factor	Pit shell depth	Total mined (Mt)	Waste mined (Mt)	Strip ratio	ROM feed (Mt)	Grade Cu%	Grade Pb %	Grade Zn%	Grade Au g/t	Grade Ag g/t	CSA Global NPV (C$M)	Opex (C$/t)
13	1.00	300	14.6	14.0	23.5	0.6	0.4	3.1	6.3	1.9	246	94	138.01

Source: 2025 Technical Report

9.3.3 Mine Design

The ABM open pit will be designed with at least three cutbacks of the open pit prior to reaching the final design limits and the Krakatoa open pit will be mined as a single stage given the excavation is small and is mined near the end of the project life.

Waste rock from the Krakatoa open pit will be mined early to create a lay down and portal staging area for the planned underground operation while the remainder of the open pit will be mined towards the end of the project life and in conjunction with the underground mine.

The ABM Zone dips to the northeast and the deposit at surface is constrained by the valley running approximately north to south and mining will involve removal of hills on both sides of the valley.

The main ramp entrance was placed on the north side of the open pit to coincide with the lowest point possible thereby minimising the amount of pioneering road works leading to the processing plant, various stockpiles and other site infrastructure.

The main ramp follows the western side of the open pit as it allows for a shorter ramp accessing the Krakatoa open pit and the underground mine portal area. The open pit slopes are shallower on the footwall side of the deposit and therefore a more economical location for the final open pit ramps, including switchbacks. The eastern side of the valley is predominantly composed of the weaker Wind Lake formation and unsuitable for the locating of a permanent ramp system.

The mineralised zones are crosscut by a complex fault system (Figure 9-4) and this structural complexity has been considered during the design process. Orientations suggest that the more parallel and closer to the fault a wall is, the more significant impact it could have on that section of the open pit wall.

This condition has been identified in relation to the west wall of the open pit where it is affected by the north-northeast faults. Consequently, the impact of the north-northeast fault was reduced by ensuring the open pit wall steps behind the fault when mining gets within 10 m of interpreted position of the fault.

A 40 m-wide geotechnical bench at 1,400 mRL was included in the design to reduce the overall slope angle and an 8 m-wide perimeter bench will be established where the design intersects the base of the overburden. The perimeter bench does not have a fixed elevation; rather, it follows the surface of the transition zone as the bench face angle through the overburden layer is related to its thickness.

The haul road designs are based on a fleet of 140 tonne haul trucks, for which 27 m-wide ramps are designed for a double-lane road, including a safety berm on the pit crest side and a drainage ditch on the pit wall side. Single-lane ramps were designed to be 20 m wide.

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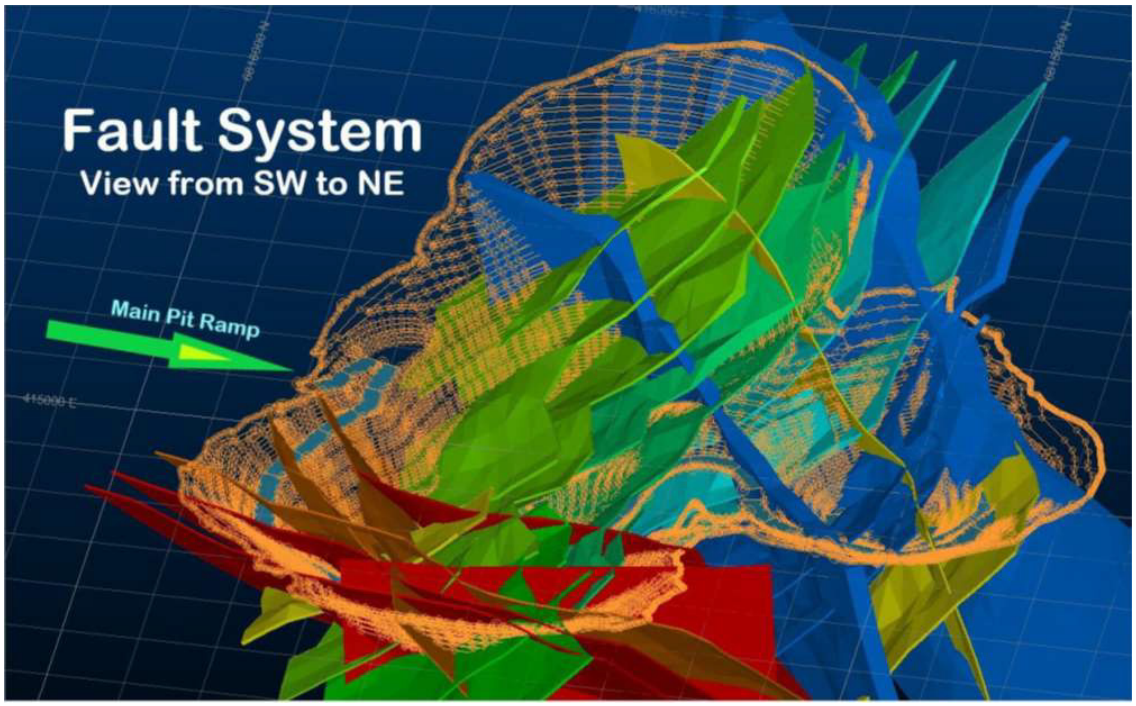


Figure 9-4: Isometric View of the Open Pit Design and Interpreted Faults
Source: BMC

9.3.4 Mining Dilution and Recovery

Mining dilution and mining recovery were estimated by coding mining dilution and ore loss distances into the block model for each area of the deposit using the relationships of the domains surrounding each individual block (Table 9-5). Some blocks are surrounded by either or both hangingwall and footwall waste and many blocks are only in contact with other ore blocks.

Table 9-5: Mining dilution and mining recovery distances as applied within the block model

Deposit area exposed to mining dilution and ore loss	Dilution distance (m)	Ore loss distance (m)
ABM both FW and HW	1.50	0.50
ABM FW or HW	0.75	0.25
ABM internal	0.00	0.00
Krakatoa both FW and HW	2.00	0.80
Krakatoa FW or HW	1.00	0.40
Krakatoa internal	0.00	0.00

Source: BMC

Table 9-6 shows the average mining dilution and recovery for each metallurgical domain.

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Table 9-6: Mining dilution and ore loss estimated by metallurgical domain

Metallurgical domain	Average mining Dilution (%)	Average mining Recovery (%)
+1,340RL (ABM Domain 1)	6.0	97.6
MET2-4 (ABM Domain 2)	2.0	99.1
MET5-7 (ABM Domain 3)	3.9	98.4
MET8 (ABM Domain 4)	9.9	96.6
Krakatoa (Krakatoa Domain 5)	13.1	94.4

Source: BMC

9.3.5 Ore and Waste Differentiation

An NSR approach was used to differentiate between ore and waste during mining. Each block classified as at least Indicated Mineral Resource within the block model had an NSR estimated where the total block revenue for each economic metal after the application of processing recoveries, operating costs incurred after the mine gate, government royalties and First Nations payments.

9.3.6 Open Pit Mine Scheduling

The mining schedule reflects a processing plant production ramp-up of at least eight months to reach the planned annual throughput capacity of 2.0 Mtpa after wet commissioning.

The key constraint on the plant is the mass of zinc fed to the zinc flotation circuit and to account for this, the production schedule limits the maximum run-of-mine throughput capacity to 357 t of contained zinc metal per day.

The mining sequence aims for low strip ratio and high yield early in the schedule for the best economic outcome for the project which is followed by a near steady-state strip ratio that meets the processing schedule.

To that end, ABM pit stages 1A and 1B are prioritised first to meet the construction waste volume requirements followed by the sequential mining of ABM pit stages 2, 3, 4, and Krakatoa to maintain waste stripping and ore access to meet the processing targets.

The mining schedule maintains total material movements that match the nominated mining fleet where each excavator shift added to the mining schedule has the capacity to mine at a rate of 750 kt per month. Total mining movement has been capped at 3 Mt per month based on fleet configuration.

Mining vertical advance rates have been limited to two benches per month and the only time this mining rate occurs is when narrow benches are mined on the upper hill slopes. A maximum of three active mining locations and a maximum of three active mining benches is considered appropriate for the mine design and fleet chosen.

The underground mining portal is available upon the completion of the ABM pit stage 1C and this stage is completed two years after mining commences. The production schedule includes underground ROM ore being produced and fed another three years later until the end of mine life.

Underground ore production has been incorporated with the open pit production where the open pit mining and production schedule was prepared on the basis of reducing the open pit processing throughput by the quantity of monthly underground ore production.

Mining commences with pre-production mining targeting the waste materials required for construction purposes. ABM pit stages 1 and 2 are prioritised for the first 22 months of mining for both pre-production and initial low waste stripping mining to meet the production targets.

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The large jump in total material movement from the higher waste stripping pits, ABM stage 3 and ABM stage 4, are deferred until 14 months after the commencement of ore commissioning of the processing (Figure 9-5).

The total mining rate progressively reduces approximately four and half years after mining commences as less waste movement is required to maintain an adequate feed rate of ore to the processing plant.

9.3.7 Open Pit Equipment

The open pit operations will apply conventional open pit drill and blast mining techniques where the ore and waste will be mined using excavators and off-highway haul trucks. The drill, blast, load and haul operations will be supported by a fleet of ancillary equipment such as dozers, graders, water carts and front-end loaders.

Two sizes of excavator have been selected for the ABM and Krakatoa open pits:

Hitachi EX3600 (or equivalent) – 360 t operating weight

Hitachi EX1900 (or equivalent) – 190 t operating weight.

The smaller 190-tonne excavator is scheduled for production in the early stages of the mine life where a single unit can comfortably handle the first 24 months of the mine life where mining is characterised by the narrow and inclined flanks of the open pits. The 360-tonne excavator will be the primary loading tool for all open pit production.

A 140-t truck has been selected for the mine plan where a maximum of 20 trucks are mobilised to site during the peak material movement period. Trucks have been scheduled on an as-needed basis and where necessary trucks will be mobilised and demobilised as required.

A summary of the equipment requirements for the open pit mine is detailed in Table 9-7. Make and models are provided for reference purposes only.

Table 9-7: Open Pit Equipment List

Equipment class	Make/Model (example only)
Excavator, 360 t Excavator, 190 t	Hitachi EX3600 Hitachi EX1900
Truck, 140 t Truck, 40 t	Komatsu HD1500 Caterpillar 740
Dozer, 70 t Dozer, 50 t Dozer, 25 t	Caterpillar D10 Caterpillar D9 Caterpillar D6
Wheel Dozer	Caterpillar 834
Wheel Loader. 100 t Wheel Loader,30 t	Caterpillar 992 Caterpillar 980
Compactor	Caterpillar CP56
Blast Hole Drill Rig (DHH) Blast Hole Drill Rig (THH)	EpirocDM45 Sandvik DX700
Grader	Caterpillar 16M
Water Cart	Water Cart
Service Truck	Service Truck
IT Loader	IT Loader
Rockbreaker	Rockbreaker
light vehicle	light vehicle

Source: BMC

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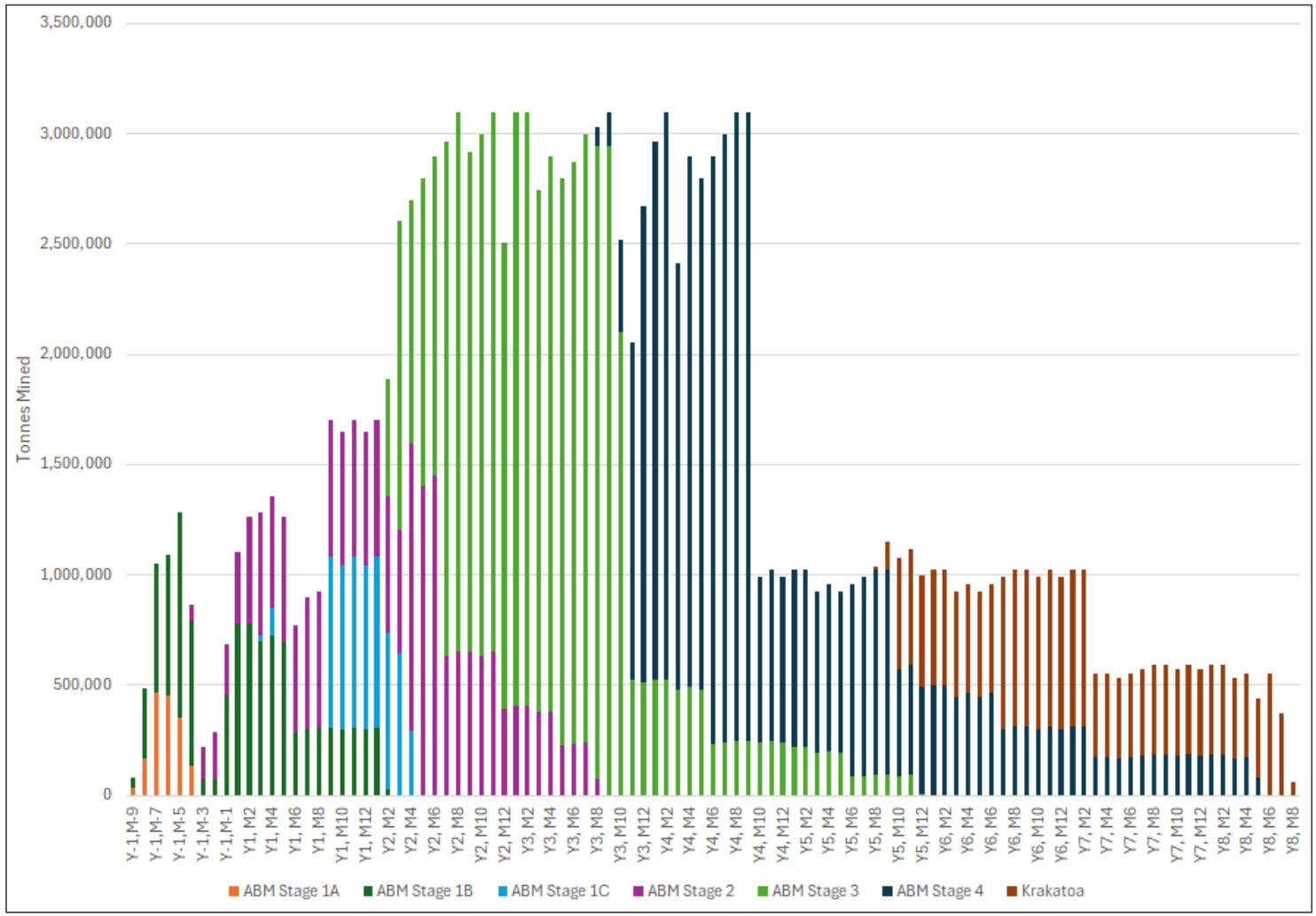


Figure 9-5: Material Movement by Open pit stage
Source: BMC

9.3.8 Open Pit Work Schedule & Personnel

The work schedule assumes continuous operation – a 24 hr per day, seven days per week and 365 days per year.

Operations and maintenance personnel will work two 12-hour shifts per day. All mining personnel will work on a two-week on/one-week off rotation under the open pit schedule.

Personnel numbers range from 110–220 persons and peak during years 3 to 6 of the 10-year schedule.

9.4 Underground Mining

Underground mining has only been considered for the Krakatoa Zone (Figure 9-6) as the vast majority of the ABM Zone is extracted using open pit mining methods. Insufficient mineralisation has been defined below the current ABM open pit design to justify underground mining in this area.

Underhand longhole stoping with cemented paste fill for footwall and hangingwall mining areas has been selected as the primary mining method.

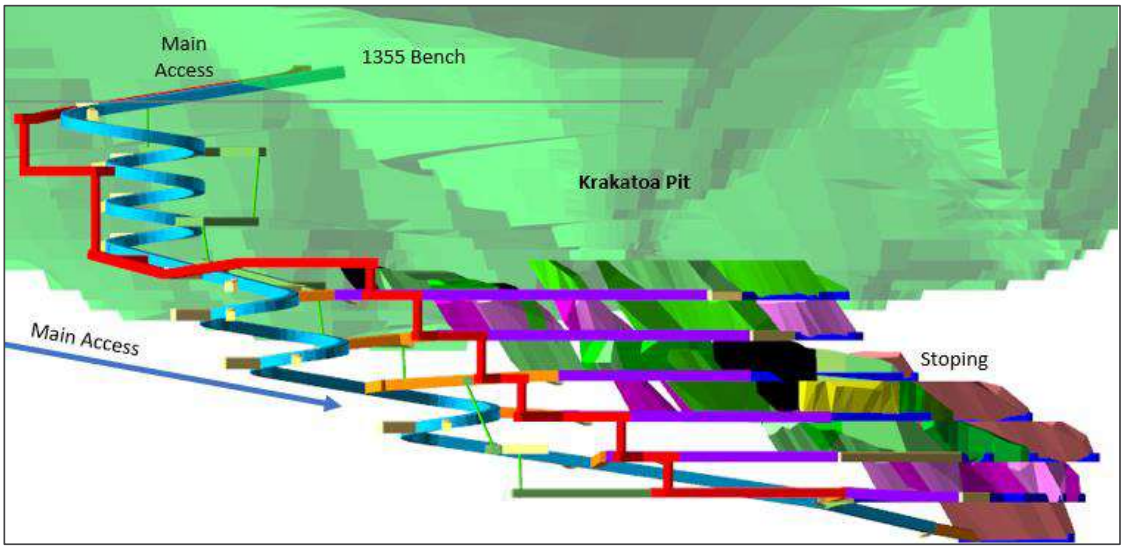


Figure 9-6: Diagrammatic isometric long section of the Krakatoa underground mine, looking west.
Source: BMC

9.4.1 Geotechnical Parameters

The data collected for the Krakatoa underground study was incorporated into the overall Kudz Ze Kayah geotechnical database and Mining Rock Mass Model that covers the ABM and Krakatoa open pits.

Eleven mine-scale geotechnical structural features that impact the planned underground mining zone were identified and the fault structures impacting the underground development and stope designs are of variable thickness and are generally greater than 3 m and up to 30 m in width. All the structures have greater than 300 m strike and dip extents and extend from the base of the overburden through to the proposed underground mining zone.

Rock mass domains were established based on the Norwegian Geotechnical Institute Q-Index and ground condition characteristics and recommended support regimes were determined (Table 9-8). Groundwater inflows may impact the underground mining conditions and so the ground support

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recommendations assume saturated conditions. The planned sequence of mining will see the upper levels of the underground mine extracted and paste-filled, and the open pit mined down towards this paste pillar later in the schedule.

Table 9-8: Support by Rock Mass Domain.

Rock Mass Domain	Q-range	Ground Conditions	Recommended Support Regimes
D1	<0.1	Exceptionally and Extremely Poor	FRS 120 mm with Fibrecrete arches, screen and MD bolts with yielding cable bolts -develop with short rounds and spilling bars
D2	0.1-1	Very Poor	FRS 100 mm with MD bolts and yielding cable bolts – develop with short rounds and spilling rounds
D3	1-4	Poor	FRS 75/50 mm on backs/walls, with grouted DCP bolts
D4	4-10	Fair	Screen and grouted DCP bolts
D5	>10	Good	

Source: BMC

Note: FRS – fibre reinforced shotcrete, DCP – double corrosion protected, MD – mechanical dynamic.

Note that the DCP bolt is not currently available in Canada and the CT-bolt is recommended to be used in its place.

Hydrogeological investigations and groundwater modelling (Section 8.2.1) indicate a discharge rate of 13 L/s from the Creek and East Faults which are interpreted to be bounding structures to the underground mining area.

Combined with groundwater inflows from the general rock mass through the mine workings an overall dewatering requirement of up to 50 L/s in the first few years of the underground mine life is modelled, decreasing to a longer-term average of around 20 L/s.

9.4.2 Mine Access

Access to the underground mine will be via a single ramp with portal at the 1,355 mRL bench from the saddle area within stage 1 of the ABM open pit. Underground trucks will haul ore and waste out of the mine and dump on pads adjacent to the portal, where the open pit load and haul fleet will re-handle the material to the processing plant or waste storage facility.

A second ramp is proposed for ventilation of the underground workings as there is a significant layer of overburden material overlying the competent bedrock for vertical development contend with. This makes raise boring or conventional raising difficult and uneconomic, given the likelihood that shaft sinking would be required through the overburden before commencing any vertical development. The second ramp will also act as the second means of egress from the underground workings if the main ramp becomes unserviceable. The dual ramp configuration is shown in Figure 9-7.

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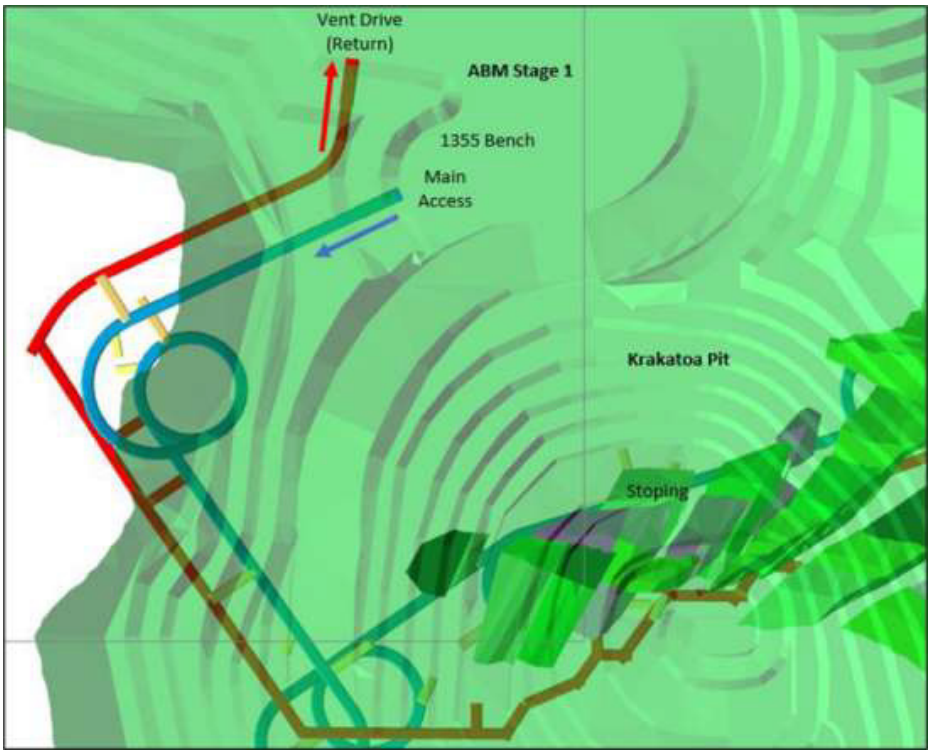


Figure 9-7: Krakatoa – Diagrammatic sketch of main access and ventilation ramp (plan view).
Source: BMC

Development will use standard mechanised underground mining equipment and methods. Utilities including compressed air, water and dewatering pump lines will be installed as headings progress and electrical cables and paste backfill lines will be installed as required. Air and water pipelines will be 4-inch diameter polylines in the decline (Table 9-9).

Table 9-9: Development Profiles

Development type	Profile no.	Width (m)	Height (m)
Ramp	PL01	5.5	5.8
Level Access, Footwall drive	PL02	5.5	5.5
Stockpile	PL03	5.0	6.0
Crosscut, Return Air drives	PI04	5.0	5.0
Ore drives, Escapeway drive	PL05	4.5	4.5
Sump	PL06	5.0	4.5
Infrastructure Development	PL07	8.0	5.0
Initial Ramp (first 20 m from Portal)	PL08	6.1	6.1

Source: BMC

9.4.3 Mine Design and Method

Stopes were manually designed based on orebody thickness and orientation taking cognisance of geotechnical constraints, the proposed stoping method, and the practical limits of the proposed mining fleet. The stopes were reviewed for economic viability by comparing estimated NSR value to

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the estimated cut-off requirements, after applying estimated mining factors for dilution and recovery. Those stopes not meeting economic criteria were removed from the stoping inventory.

The selected mining method for production from Krakatoa is underhand longhole stoping augmented with cemented backfill. A representative mining sequence using this mining method is presented in Figure 9-8 and is specifically a top-down mining sequence for simplicity and earliest ore access.

Level spacing is 20 m with 4.5 m wide by 4.5 m high ore drives. The stoping cycle commences with development of an upper and lower sill drive to the limits of the stoping block. A slot rise is then drilled up to the level above and blasted to create a void space to allow for blasting the rest of the stoping panel. Once the panel is fully excavated, the void will be filled with cemented paste backfill to allow mining the subsequent stopes in the sequence without leaving remnant mineralised support rib pillars.

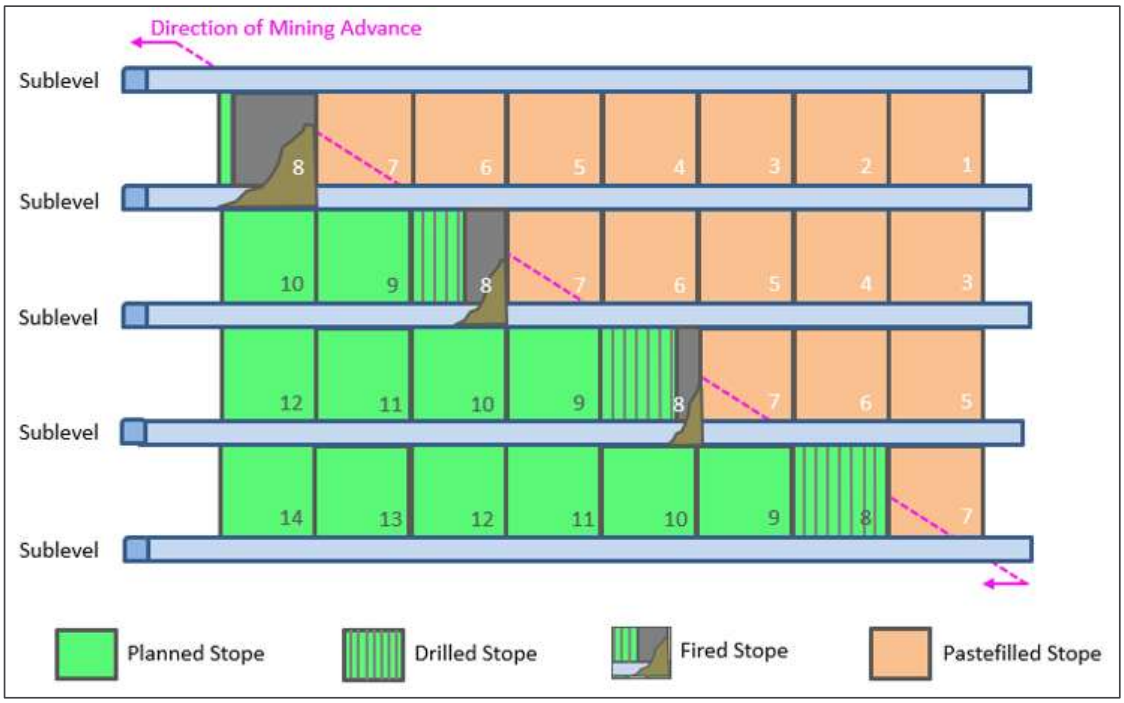


Figure 9-8: Stoping Sequence Schematic.
Source: BMC

9.4.4 Mining Dilution and Recovery

Stoping assumes 90% recovery from each of the stope panels, and any planned dilution is included in stope design shapes. Unplanned dilution (at zero grade) will be variable and depends on the local geotechnical characteristics of the enclosing host rocks. The factors applied for each domain are presented in Table 9-10.

Table 9-10: Stope Dilution

Rock Mass Domain	D1	D2	D3	D4	D5
Dilution	50%	35%	25%	20%	15%
Mining recovery	90%	90%	90%	90%	90%

Source: 2025 Technical Report

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9.4.5 Backfill

Paste backfill will be placed in mined stopes to fill voids and assist with ground control in the stoping block/panel and will be hydraulically placed via a piped network from the paste fill plant.

Analysis of horizontal and vertical exposure while mining under and beside a cemented paste-filled stope was calculated and high strength paste has been allowed for in the cost estimate and will be used for the lower half of all stopes to be undercut by the stope below. For the remainder of the stope, and all other stopes that will not be undercut, regular strength paste is planned with a reduced binder addition rate.

The paste fill plant will be located on surface adjacent to the processing plant and agitator trucks will transport the paste to the portal before dumping into a hopper and piped underground. Paste is then reticulated through the mine to the appropriate locations using the existing mine development.

Permanent paste reticulation has been allowed for in the main ramp, level access and footwall drives, and for all stopes, a temporary high-density polyethylene (HDPE) line is provided for each stope for reticulation through the level from the footwall drive.

Paste fill will be contained within the stope by constructing a bulkhead in the access as close to the stope brow as possible. The curing time after each paste-filled stope is a minimum of 14 days to ensure required paste fill strength of 300 kPa is attained before mining the adjacent stope.

Cemented paste fill requirement within the schedule has been capped at 700 m^3 per day.

9.4.6 Mine Scheduling

The underground mine is scheduled to begin development approximately two years after mining operations commence on site only after the ABM stage 1 open pit has established the portal area on the 1,355 mRL bench. The underground schedule will finish some 60 months later and will produce at a variable annual rate over that time, peaking at 572,000 t of ore in any single year.

Life of mine physical quantities are presented in Table 9-11.

A base case schedule was created linking all development and stoping related tasks in line with the geotechnical recommendations for the mining methods applied. These included:

- All stopes being mined top-down (underhand) and retreating to the access crosscut, and
- Lead/lag between sublevels (vertically) to prevent any safety risks from premature undercutting of the above stope.

The schedule is designed to ensure a smooth ramp-up to production and, where possible, minimise variations in development rates and production to avoid additional project costs due to under-utilisation of equipment.

Development rates are scheduled according to the geotechnical domain of the rock that the development occurs within and considers the ground conditions, development cut length and required ground support.

The principal aim of the mine schedule was to build enough detail into sequencing the mine and applying operational constraints such that the schedule represents what is reasonably achievable.

The tonnes and grade presented are inclusive of mining dilution and recovery (see section 9.4.4).

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Table 9-11: LOM Physicals Summary

Mining summary	Units	LOM
Capital lateral development	m	4,013
Operating lateral development	m	5,823
Total lateral development	m	9,836
Total vertical development	m	2,985
Production drilling 89 mm	m	215,409
Cemented paste fill	m^3	440,143
Development ore tonnes	Mt	0.2
Longhole stope ore tonnes	Mt	1.5
Total ore tonnes	Mt	1.7
Total waste tonnes	Mt	0.6
Total mined tonnes	Mt	2.4
Ore grades		
Zinc	%	5.0
Copper	%	0.4
Lead	%	2.3
Gold	g/t	1.3
Silver	g/t	147

Source: BMC

9.4.7 Mine Services

Infrastructure located at the main ramp portal location will include:

- Mine air heating equipment including the heating unit, mixing box and fuel storage.
- A mine control room fitted with a tag board, Very High Frequency (VHF) radio communications, emergency services room, lighting, primary ventilation monitoring showing primary fan status, and stench gas cylinders and release point in case of emergency evacuation.
- Ore and waste re-handling pads to store ore and waste from underground prior to hauling to the processing plant.
- Designated heavy and light vehicle parking areas.

9.4.8 Ventilation

Primary

Fresh air will be drawn into the mine via the main decline and return to surface by a dedicated rise system. This dedicated return air system comprises inter-linking return air drives and connecting vertical development, returning to surface via a second portal access to the pit (Figure 9-7). Three primary exhaust fans are to be mounted in a bulkhead positioned nominally 20 m inside the return air portal located on the 1,355 mRL bench. The bulkhead will also be fitted with a man door to provide secondary egress.

The primary fans selected are a single-stage 132 kW axial fan and the downwind installation of the bulkhead provides for inspection and maintenance from the open pit entry side.

The Yukon climate requires that the air entering the portals be heated during the coldest part of the year and this will be achieved with a portal fan which heats air using diesel fired burners and then injects the air into the intake airway using an additional fan.

The capacity of the primary ventilation system has been designed to meet the required ventilation standards, based on the operating equipment. A computer simulation analysis of the primary ventilation circuit confirmed that sufficient airflow will be provided by the ventilation network.

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Auxiliary

Axial fans, suspended from the backs, will fulfil secondary ventilation requirements. The fans will be of appropriate size, nominally with motors in multiples of 55 kW, 90 kW or 110 kW. This will provide fans sizes of 55 kW, 90 kW, 110 kW, 180 kW or 220 kW, depending on the ventilation requirement on the level, with sufficient volumes to supply all working headings.

Typically, 1,400 mm ducting will be run off the main decline onto the level and reduce to 1,220 mm ducting leading into the footwall drive, with T-pieces branching into active crosscuts (up to five) which will be approximately 150 m from the footwall drive.

A single access drive from the footwall zone to the hangingwall zone is designed and will require a dedicated duct from the main decline and will have around a 350–400 m maximum length. Even with pressure loss and leakage, the axial fans will be sufficient to push this volume of air to the hangingwall heading on each level.

9.4.9 Dewatering

The underground dewatering system will consist of two pumps located at or near the 1,205 mRL with the helical rotor pumps fed from a settling sump just above them in the decline. These pumps will transfer water directly to a pond outside of the mining area. A single 8-inch dewatering line is planned for the main decline to manage the expected water flow.

Provision will be made for additional travelling pumps that can be used to centralise the water back to the pump station. Given that the water ingress locations are not firmly known and the relatively short mine life, helical rotor pumps will provide a flexible solution to remove water from the mine as they can be easily relocated to the source of the water and connected to the decline pump-line.

Minor sumps around the mine will have submersible pumps, or similar, as needed to meet the water removal requirements. This water will be pumped into the travelling helical rotor pumps then up to the main pump station.

9.4.10 Services

Power

The power station will supply power to the underground mine and power to the underground mine area will be facilitated through the installation of direct buried supply cable, installed on the western side of the valley, adjacent to the open pit.

High voltage (HV) power will be supplied to the underground mine at 13.8 kV, with 90 mm^2 HV cable extending between substations positioned approximately 100 m vertically throughout the mine. Substations will typically be 2 MVA capacity and distribute low voltage power at 1,000 V, generally via 70 mm^2 cable between the substation and distribution boxes positioned near active working areas.

Low voltage power will then be reticulated to working areas via 35 mm^2 cable to starter boxes for electrical equipment (e.g. development jumbos, longhole drills, etc.), pumps and secondary ventilation.

Compressed Air

Compressed air will be required for shotcrete application, refuge chambers, blasthole charging, production drilling and various miscellaneous activities. A compressor will be initially situated outside the main portal to commence underground mining and will be moved down lower into the mine once a suitable location becomes available. The recommended location is the 1,305 mRL return air drive, as fresh air and access to the main decline services is readily available.

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9.4.11 Refuge Chambers and Secondary Egress

Refuge chambers will be installed in various locations to provide safe refuge for mining personnel when/if required. All refuge chambers will be fitted with radio communications, drinking water and breathing air sufficient for a minimum of 36 hours of refuge.

Portable four-person refuge chambers will also be sourced for use in single entry headings where the escape route is obstructed by heavy mobile machinery operating. Twelve-person refuge chambers will be installed in disused main decline stockpile bays, to minimise the distance required to travel in an emergency. Walking distances to the nearest refuge chamber are not expected to be greater than 750 m.

In addition, a dedicated second means of egress (escape route) will be established. This will enable egress from the mine in the case that the main access (the ramp) becomes inaccessible. Escapeways raises are designed between 70° and 80° and are to be excavated using a raise bore. The total length of raise boring is estimated to be 192 m for the mine.

9.4.12 Equipment

Mine equipment types have been determined following a review of the mine design and schedule and discussion with various contractors through an RFQ process. The equipment must perform the following:

- Excavate lateral and decline development in both ore and waste,
- Install all ground support including rock bolting and surface support,
- Maintain the underground road surfaces,
- Drill, charge and muck (including remote mucking) of all stoped ore,
- Haul all muck to designated stockpiles on surface,
- Install all underground services for development and production, and
- Install pipework and manage all activities underground related to paste filling.

A summary of the equipment requirements for the underground mine is detailed in Table 9-12. Make and models are provided for reference purposes only.

Table 9-12: Mining Equipment

Equipment class	Make/Model (example only)
2 boom Jumbo drill	Sandvik DD421
Production drill	Sandvik DL311
LHD (17-t capacity)	Sandvik LH517i
Truck (45-t capacity)	Sandvik TH545i
Charge rig	Normet Charmec 605
Service vehicle	Volvo ITC L90F

Equipment class	Make/Model (example only)
Grader	Cat 12K
Fibrecrete sprayer	Normet Spraymec SF-050
Fibrecrete transmixer	Normet Utimec LF600
Surface agitator truck	Surface agitator truck
Light vehicle	Light vehicle TBC

Source: BMC

9.4.13 Work Schedule & Personnel

The work schedule assumes a 24 hours per day, seven days per week and 365 days per year mining operation. Operations and maintenance personnel will work two 12-hour shifts per day. All mining personnel will work on a 2-week in/2-week out rotation.

Personnel numbers range from 60 to 100 persons and peak during Year 3 and Year 4 of the 6-year underground schedule.

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9.4.14 Ore and Waste Differentiation

A NSR approach was used to differentiate between ore and waste during mining in a similar manner to the open pit operations. The NSR was used to determine whether the mineralised material met the following criteria:

- Incremental cut-off grade (ICOG) – Measured and Indicated Mineral Resource that covers underground ore mining, load and haul, direct processing, and general and administration (G&A) costs (Table 9-13).
- Fully costed cut-off grade (FCCOG) - Measured and Indicated Mineral Resource that covers all operating costs associated with mining including development mining and outstanding costs such as mobilisation and demobilisation, indirect processing, dayworks, and all other costs that have not been capitalised (Table 9-13).

Table 9-13: Cut-off Grade Calculations

Parameter	C$/Total UG Ore tonne
Mining – Long Hole Open Stope with Cemented fill	$50.70
Treatment Direct	$16.03
Treatment Indirect	$5.94
G&A	$10.78
ICOG	**$66.72**
Mobilisation, Demobilisation, Development, Ground Support, Dayworks, BMC, G&A	$100.16
FCCOG	**$172.83**

Source: BMC 2019

NB. Cost estimates are developed to determine cutoff grades for ore / waste, which leads to mine schedule development, which then feeds into financial model and costs are developed from the overall mine schedule, and will be different (although should not be materially so) from the cut-off cost estimates.

The FCCOG was applied to the NSR and used to determine the lateral and depth extents of the mine and includes all site operating costs, and capital costs associated with the underground mining. The ICOG was applied to the NSR and used to identify potentially economic material once development was in place, which covers the costs associated with stoping, load and haul, and direct processing costs.

The original stope shapes were assessed against the NSR values applicable to the project parameters used in the 2023 Feasibility Study Economic Update. All stopes returned an NSR above the ICOG and the average NSR value for all underground ore production is greater than the FCCOG.

9.5 Ore Reserve Estimates

The ORE for the ABM Deposit is reported in accordance with JORC (2012) and detailed in Table 9-14. All reserves are classified as "Probable Ore Reserve", as no Measured Resources have been defined for the project. Inferred Mineral Resources were not considered in this Ore Reserve estimate.

The ORE includes material extracted from open pit and underground and is sourced from Indicated Mineral Resources only where the block value is greater than the NSR cut-off for the relevant mining method.

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Table 9-14: ABM Deposit Ore Reserve Estimate

Mine	Category	Tonnes (Mt)	Cu %	Pb %	Zn %	Au g/t	Ag g/t	AgEq g/t	Cu (kt)	Pb (kt)	Zn (kt)	Au (koz)	Ag (Moz)	AgEq (Moz)
Open Pit	Probable	14.0	0.9	1.6	5.9	1.3	136	604	128	226	828	596	61	272
Underground	Probable	1.7	0.4	2.3	5.0	1.3	147	539	7	40	87	70	8	30
Total	**Probable**	**15.7**	**0.9**	**1.7**	**5.8**	**1.3**	**138**	**597**	**136**	**266**	**915**	**666**	**70**	**302**

Source: 2025 Technical Report

- BMC's interest in the ABM Deposit is 100%.
- The Ore Reserves in this disclosure were estimated in accordance with the JORC Code by Karl van Olden as Competent Person.
- The effective date of this Ore Reserve is 30th October 2023.
- Numbers have been rounded to reflect the precision of the estimates.
- Open pit Ore Reserves are reported within a practical design for an open pit using a NSR cut-off.
- Practical open pit designs were informed by economic mining envelopes determined using Whittle pit optimisation software.
- Overall slope angles for the designed open pit range from 27° to 47°.
- Underground Ore Reserves are based on an underhand longhole stoping with cemented paste fill mining method and reported to a NSR cut-off
- Ore Reserves incorporate estimates of mining dilution and mining recovery.
- Processing recoveries have been calculated for each of the defined metallurgical domains. Average processing recoveries are 73.8% for copper, 73.5% for lead, 85.9% for zinc, 64.9% for gold and 86.0% for silver.
- NSR calculations represent the net revenue to Mine Gate after accounting for concentrate treatment and refining charges, concentrate penalties, concentrate transport costs, government royalties and payments to First Nations.

Metal Equivalents

- Metal equivalent grade is the sum of the value of the grade of each metal, divided by the price of the metal being used for metal equivalent reporting.
- Metal grades used for calculations are the diluted mined reserve grades: Ag 138g/t, Au 1.3g/t, Zn 5.8%, Cu 0.9%, Pb 1.7%.
- Processing recoveries are considered in the assessment of whether a block of mineralisation is economic or not and therefore whether it can be included in the stated Ore Reserve estimate. Processing recoveries have not been specifically applied in the calculation of metal grade equivalents for reserves.
- Long term consensus metal prices have been used for all calculations: Ag US$22.60/oz, Au US$1,700/oz, Zn US$1.20/lb, Cu US$3.80/lb, Pb US$0.95/lb.
- The metal grade equivalent formula (for reserves) is as follows:
- AgEq (g/t) = (Ag grade (g/t) * Ag price (US$/g) + Au grade (g/t) * Au price (US$/g) + Zn grade (%) * Zn price (US$/t) / 100 + Cu grade (%) * Cu price (US$/t) / 100 + Pb grade (%) * Pb price (US$/t) / 100) / Ag price (US$/g)
- In the Company's opinion, all of the elements included in the metal equivalents calculation have a reasonable potential to be recovered and sold, as supported by feasibility metallurgical testwork and executed offtake agreements.
- The basis for the selection of silver is the chosen equivalent metal is based on the net revenue likely to be derived from each metal in the ABM Deposit. Silver is the primary contributor to revenue. Zinc, along with copper and lead are more heavily affected by metal payabilities and also concentrate treatment charges.
- In 2023 terms silver contributed 30.5% of the net revenue from the Ore Reserve estimate, with zinc contributing 30.4%. However, considering the price escalation reflected in current pricing, as at the Report date, silver's contribution to net revenue is now 33.0% and zinc has fallen to 21.2%.

The differentiation between ABM open pit ore and waste was not revisited. The 2019 ore schedule was evaluated against the economic parameters of the 2025 Technical Report with a substantial increase in project economics, demonstrating that the updated commodity prices and exchange rates have offset the increases in project operating costs (*pers. comm.* Karl van Olden (AMC) September 2025).

For the Krakatoa underground mine, the original stope shapes from the 2020 Re-stated Feasibility Study (CSA Global, 2020) were assessed against the NSR values applicable to the project parameters used in the 2025 Technical Report (which included the June 2023 quarter economic inputs). All stopes returned an NSR above the ICOG and the average NSR value for all underground ore production is greater than the FCCOG, demonstrating that the underground mine returns a positive economic outcome.

It is understood that there remains an opportunity to optimise cut-off grade decisions at future stages of the mine planning and into operations. The mining operation should take a view to continually assess and adjust cut-off grades throughout the mine life to optimise the project value across changing project parameters.

The Net Smelter Return (NSR) method was used to determine economic mineralisation for the ABM Deposit (Cube 2024). NSR values have been calculated from long-term consensus metal prices (Table 9-15) using an exchange rate of US$0.77:C$1.00, current at the time of commencement of open pit and underground mine design work.

Table 9-15: June 2023 quarter commodity prices as used in the current (2025) Technical Report

Commodity	Unit	Price assumptions ($US)
Copper	$/lb	$3.80
Lead	$/lb	$0.95
Zinc	$/lb	$1.20
Gold	$/oz	$1,700.00
Silver	$/oz	$22.60

Source: BMC

The Ore Resource estimate includes material extracted from the designed open pit and underground excavations that is sourced from Indicated Mineral Resources only and has a block value greater than the NSR cut-off for the relevant type of mining. All open pit Ore Reserves are reported to a cut-off NSR value of US22.56/t, while underground Reserves are reported to a cut-off NSR value of US$133.00/t (using an exchange rate of C$1.00 = US$0.77).

All tonnes and grades have been adjusted for mining dilution and ore loss, and any dilution has been assigned a zero grade.

The 2019 ore schedule was evaluated against the economic parameters of the June 2023 quarter estimates that resulted is a substantially positive economic result, demonstrating that the updated commodity prices and exchange rates adequately offset the escalation and changes to the project operating costs.

Following the update to the Feasibility Study-level investigations, using the June 2023 quarter cost estimates, the Ore Reserve estimate remains unchanged, with the Ore Reserve estimate reported in accordance with the JORC Code (ERM 2025b).

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9.6 ERM Opinion

ERM notes that whilst the Feasibility Study-level investigations, Mineral Resource Estimate and Mineral Reserve Estimate were completed in accordance with Canadian Institute of Mining, Metallurgy and Petroleum Standards (CIM 2014), and reported in accordance with NI 43-101, the Canadian standards are functionally equivalent to Australian JORC Code standards and definitions, and as such are able to be reported in accordance with the JORC Code in this report.

ERM is of the opinion that there are no fatal flaws in the current mine planning and designs for both the open pit and underground mines. The development approach and transition to underground mining from an open pit development is reasonable and all aspects of the proposed operation have been considered in a sound and logical manner.

An Ore Reserve Estimate (ORE) was prepared for the ABM Deposit following the completion of the original 2019 Feasibility Study. A 2023 Economic Update Review was released in October 2023 using June 2023 quarter cost estimates. The metal prices used in the revised economic modelling were higher than those of the 2020 Re-stated Feasibility Study and used in the 2025 Technical Report.

The ORE was formally reviewed under the revised metal price and exchange rate scenarios and no adjustments to the calculated ORE were considered necessary. The modelling considered all capital, operating, and realisation costs as outlined in the 2025 Technical Report.

The ore schedule initially outlined in the 2019 Feasibility Study was evaluated using the economic parameters from the June 2023 quarter economic parameters and reported in the 2025 Technical Report. This showed a substantial positive economic outcome, demonstrating that the updated commodity prices and exchange rates offset the escalation in and changes to the project operating costs.

Following the 2025 Technical Report, the declared Ore Reserve estimate remains unchanged, with the ORE reported in accordance with the JORC Code.

In ERM's opinion the operating and capital cost estimates informing the Ore Reserve estimate are considered accurate to within the normal limits expected for a Feasibility Study as defined in the JORC Code, and the costs (real terms) remain valid. The inputs and assumptions of the Feasibility Study-level investigations reported in this Report (and the reports informing it) remain applicable and appropriate for the disclosed information.

ERM notes however that considerable effort will be required to source, train and retain the necessary mining skills at the operation against the backdrop of scarcity of skilled and experienced mining employees.

There is an opportunity for BMC to develop a loyal and capable employee base to recognise and maximise opportunities as the ABM Mine Project moves through construction to steady-state mining.

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10. METALLURGY AND PROCESSING

10.1 Testwork

Significant metallurgical testwork has been completed on the ABM Deposit with testing commencing during the 1990s. BMC commenced metallurgical testwork in 2016 with SGS in Burnaby, Canada for the PFS before moving the testwork programme to ALS Metallurgy in Perth, Australia. ALS Metallurgy in Kamloops, Canada have completed confirmatory comminution testwork and the metallurgical testwork for the Feasibility Study continued in 2017 and 2018 with ALS Metallurgy in Adelaide, Australia and supervised by Minnovo in Perth, Australia.

10.2 Orebody Characterisation and Metallurgical Domains

The ABM Deposit comprises the ABM Zone and the adjacent Krakatoa Zone and five metallurgical domains were recognised for the ABM Deposit in diamond core based on texture and mineralogy (Section 6.5).

- MET2-4 – massive sulfide mineralisation with a significant magnetite component.
- MET5-7 – massive sulfide mineralisation lacking significant magnetite component.
- MET8 – vein/stockwork mineralisation with a significant silicate gangue component.
- A fourth metallurgical domain for the ABM Zone (+1,340RL) was defined by spatially controlled mineralogical zonation above 1,340 m RL, with a higher level of copper-bearing sulfosalt mineralisation (primarily tennantite-tetrahedrite).
- The fifth metallurgical domain was recognised for the Krakatoa Zone, which is like the +1,340RL domain but with silver-rich freibergite as the material sulfosalt component in place of tennantite-tetrahedrite.

10.2.1 Sample Preparation and Composites

Ten composite samples were generated for the 2016 PFS testwork and were used for comminution and flotation testing.

- ABM master composites 1 and 2.
- ABM LOM composite.
- ABM domain composites (four samples): +1,340RL, MET2-4, MET5-7, and MET8.
- Krakatoa composites (three samples): In-Pit Main, In-Pit Upper, and -1250RL.

These samples were selected from cores that were drilled in 2015 and 2016 and were large samples, typically from three or four holes and included approximately 10% dilution. Some of these samples were reused for the initial Feasibility Study flowsheet optimisation testwork performed in 2017.

Five samples for each of the five metallurgical domains (also known as the domain variability samples) were generated for the Feasibility Study variability testwork performed in 2017 and 2018:

- Main composites (five samples): Krakatoa, +1,340RL, MET2-4, MET5-7, and MET8.
- Krakatoa variability composites (five samples): Krakatoa-1 through Krakatoa-5.
- ABM variability composites (five samples): +1,340RL-1 through +1,340RL-5.
- ABM variability composites (five samples): MET2-4-1 through MET2-4-5.
- ABM variability composites (five samples): MET5-7-1 through MET5-7-5.
- ABM variability composites (five samples): MET8-1 through MET8-5.

These samples were selected by BMC based after discussion with Minnovo and were primarily intended to assess variability in flotation performance and comminution properties over a range of head grades Table 10-1).

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Table 10-1: Summary of Feasibility Study sample head grades

Domain	Sample	Cu (%)	Pb (%)	Zn (%)	Au (ppm)	Ag (ppm)	As (ppm)	Sb (ppm)	Se (ppm)	Hg (ppm)
+1,340RL	Main Composite	0.50	1.77	5.73	1.68	142	3,360	599	115	32
	Variability minimum grades	0.19	0.87	2.02	0.59	74	2,200	533	65	14
	Variability maximum grades	1.18	2.95	9.30	2.02	248	6,200	1,034	365	58
MET2-4	Main Composite	0.88	1.23	6.30	0.73	84	1,530	271	345	6
	Variability minimum grades	0.63	0.16	2.13	0.36	26	40	4	280	1
	Variability maximum grades	1.43	2.83	10.2	1.18	202	5,000	531	515	10
MET5-7	Main Composite	1.13	1.24	6.25	1.06	118	1,850	247	180	52
	Variability minimum grades	0.26	0.51	2.41	0.43	64	290	29	155	4
	Variability maximum grades	4.35	1.78	12.0	2.25	160	8,400	851	305	205
MET8	Main Composite	1.00	0.88	3.59	0.52	66	880	138	180	13
	Variability minimum grades	0.24	0.40	0.96	0.14	14	680	20	40	2
	Variability maximum grades	2.21	1.14	7.36	1.23	174	3,930	476	400	23
Krakatoa	Main Composite	0.35	2.18	5.04	1.53	184	4,230	497	65	27
	Variability minimum grades	0.15	1.11	3.75	1.29	114	1,400	202	30	7
	Variability maximum grades	0.84	3.63	8.38	2.21	292	8,000	1,038	180	41

Source: 2025 Technical Report

Five waste samples were selected by BMC for comminution testing only.

10.2.2 Comminution

Eleven composites plus the additional five Feasibility Study domain composites were submitted for SMC Testing and a summary of the consolidated statistics for the testwork is shown in Table 10-2.

Table 10-2: SMC testwork summary

	DWI (kWh/m³)	A x b	t_a	SG (t/m³)	SCSE (kWh/t)
Minimum	2.76	68.7	0.42	3.15	5.72
Maximum	6.05	145.3	0.94	4.58	8.15
Average	4.40	94.9	0.62	3.99	6.97
80th percentile	5.43	75.8	0.74	-	7.50
85th percentile	5.63	73.8	0.76	-	7.55

Source: 2025 Technical Report

Notes:

- DWI – Drop Weight Index.
- A x b – Impact breakage parameters.
- T_a – Abrasion breakage parameter.
- SG – Specific gravity.
- SCSE – SAG circuit specific energy.

The extreme values for A x b and Drop Weight Index (DWI) of 68.7 and 6.05 kWh/m^3 were used for design purposes due to the lengthy down-hole intervals of many of the composite samples that were tested.

Six of the eleven PFS composites, five of the Feasibility Study domain composites, and four of the Feasibility Study variability samples were submitted for Bond Work Index testing and the relevant data from Cominco's earlier metallurgical testwork was also considered. A summary of the consolidated statistics for the testwork is shown in Table 10-3.

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Table 10-3: Bond Work Index testwork summary

	BWI at 75 µm (kWh/t)	RWI (kWh/t)	AI (g)
Minimum	7.6	6.1	0.0425
Maximum	14.7	10.7	0.3683
Average	11.8	8.9	0.115
Standard Deviation	1.5	1.7	0.078
80th percentile	12.8	10.3	-
85th percentile	13.3	10.4	-

Notes: BWI – Bond Ball Mill Work Index. RWI – Bond Rod Mill Work Index. AI – Abrasion Index.
Source: 2025 Technical Report

For design purposes, the 85th percentile Bond Rod Mill Work Index (RWI) value was selected for use due to the lengthy down-hole intervals of many of the composite samples tested and potential for reduced variability in these samples, and the limited number of RWI results. The 80th percentile BWI value was used for design purposes due to the greater number of BWI results.

The SMC Test results showed that waste is marginally harder than mineralisation based on BWI values. Typically, plant feed (containing mineralisation and waste dilution) can be expected to require more grinding energy in the ball mill than mineralisation alone.

The testwork results indicated that mineralisation with waste dilution during mining is not expected to cause a material change to grinding energy requirements and the results of the five waste samples submitted for BWI and SMC testing are summarised in Table 10-4.

Table 10-4: Waste samples SMC and BWI testwork summary

	DWI (kWh/m^3)	A x b	t_a	SG (t/m^3)	SCSE (kWh/t)	BWI at 75 µm (kWh/t)
Minimum	3.08	63.4	0.58	2.64	7.19	7.7
Maximum	4.45	85.9	0.84	2.82	8.25	15.1
Average	3.79	73.6	0.69	2.75	7.73	12.8

Source: 2025 Technical Report

10.3 Flotation

Flotation testing in the earlier PFS and Feasibility Study included:

- Batch open circuit and locked cycle tests on the PFS composites.
- Large batch open circuit tests on ABM Master Composite 2 to produce concentrate for settling and filtration tests.
- Large batch open circuit tests on ABM Master Composite 1, +1,340RL composite, and MET5-7 composite to produce additional flotation tailings for filtration tests.
- Batch open circuit and locked cycle tests on the Feasibility Study domain composites.
- Batch open circuit tests on the Feasibility Study variability samples.

The Feasibility Study batch open circuit flowsheet typically included:

- Primary grinding to 80% passing 70 µm.
- Copper pre-float rougher flotation, cleaning of the pre-float rougher concentrate without regrinding, to produce final copper concentrate.

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- Copper rougher flotation, regrinding of rougher concentrate and pre-float cleaner tailings to 80% passing 30 µm, two stages of cleaner flotation.
- Lead rougher flotation, regrinding of rougher concentrate and pre-float cleaner tailings to 80% passing 30 µm, two stages of cleaner flotation.
- Zinc pre-float rougher flotation, cleaning of the pre-float rougher concentrate without regrinding, to produce final zinc concentrate.
- Zinc rougher flotation, regrinding of rougher concentrate and pre-float cleaner tailings to 80% passing 35 µm, two stages of cleaner flotation.

The Feasibility Study variability sample initial batch float tests generally provided results in line with the Feasibility Study main composite results, although some samples showed less than optimal results. Follow-up tests were performed with increased collector addition which, in nearly all cases, resulted in significantly improved results.

One Feasibility Study variability sample (+1,340RL-3) showed limited improvement with increased collector addition. This sample was tested at a finer primary grind of 60 µm and higher collector addition with greatly improved results.

A summary of the optimised Feasibility Study variability sample batch open circuit tests is shown in Table 10-5.

Table 10-5: Summary of variability sample batch open circuit tests

Variability sample	Head grade					Cu concentrate		HPM concentrate		Zn concentrate		Au, Ag recovery to Cu, HPM concentrates	
	Cu %	Pb %	Zn %	Au ppm	Ag ppm	Grade %Cu	Rec. %Cu	Grade %Pb	Rec. %Pb	Grade %Zn	Rec. %Zn	%Au	%Ag
+1,340RL – 1	0.19	0.87	2.02	0.59	74	20.4	77.3	51.6	61.9	49.0	91.6	69.8	83.3
+1,340RL – 2	0.40	1.37	4.22	1.03	150	27.3	62.6	49.6	53.6	51.8	81.4	36.2	69.1
+1,340RL – 3	1.18	1.69	5.98	2.01	126	24.7	69.1	44.8	48.1	46.7	85.8	29.0	60.0
+1,340RL – 4	0.47	1.75	7.03	1.98	208	23.9	71.5	63.3	55.7	51.2	93.3	52.1	76.6
+1,340RL – 5	0.24	2.95	9.30	2.02	248	26.2	60.6	55.4	83.2	52.5	94.3	57.4	83.4
MET2-4 – 1	1.43	0.16	2.13	0.36	26	27.8	93.0	5.6	27.4	29.8	61.9	53.6	74.2
MET2-4 – 2	0.63	0.97	5.22	0.48	60	24.3	46.1	51.0	67.9	49.3	91.0	22.1	38.2
MET2-4 – 3	0.64	1.44	6.11	1.01	98	26.7	56.6	40.8	53.7	42.0	79.6	31.6	49.4
MET2-4 – 4	1.34	0.54	6.85	1.05	88	25.9	73.3	25.8	40.4	46.0	90.8	47.8	41.7
MET2-4 – 5	0.64	2.83	10.2	1.18	202	25.9	65.5	47.0	77.0	53.1	85.3	38.2	73.0
MET5-7 – 1	0.67	0.72	2.41	0.62	64	21.4	63.9	30.5	18.9	47.1	83.1	34.0	38.0
MET5-7 – 2	4.35	0.51	3.31	2.25	142	30.7	96.8	38.0	29.5	51.1	91.2	89.1	87.9
MET5-7 – 3	0.26	1.63	6.76	2.14	160	25.7	40.8	45.2	63.8	50.0	89.0	40.5	63.7
MET5-7 – 4	0.37	1.78	6.47	1.13	142	31.8	64.9	67.6	73.3	58.0	95.2	42.6	83.0
MET5-7 – 5	0.91	0.59	12.0	0.43	104	22.0	79.4	28.6	53.9	52.4	96.2	51.2	62.7
MET8 – 1	0.24	0.40	0.96	0.14	14	27.5	86.9	78.2	46.0	48.3	90.1	35.7	52.4
MET8 – 2	1.23	0.55	2.54	0.36	60	30.2	90.7	60.4	44.6	48.5	93.8	72.8	67.9
MET8 – 3	2.21	1.05	4.50	1.23	174	30.7	78.2	48.4	76.6	57.3	94.0	57.2	80.3
MET8 – 4	0.46	0.97	4.64	0.62	84	26.8	82.8	59.5	80.3	58.3	91.1	71.0	83.7
MET8 – 5	0.36	1.14	7.36	0.74	74	22.5	63.1	67.3	73.8	57.6	95.3	41.9	69.1
Krakatoa – 1	0.84	1.93	3.80	1.98	114	29.1	86.9	65.5	72.1	52.1	92.2	53.9	81.3
Krakatoa – 2	0.19	1.11	3.75	1.95	186	21.1	41.2	29.3	66.6	49.8	88.4	65.0	75.5
Krakatoa – 3	0.15	1.64	4.92	1.29	208	16.9	50.2	36.7	70.7	53.0	86.0	54.9	69.6
Krakatoa – 4	0.25	3.63	5.58	2.21	292	22.2	43.4	55.7	82.3	50.5	84.1	50.3	79.1
Krakatoa – 5	0.32	2.33	8.38	1.77	190	23.5	64.1	55.6	71.4	50.2	86.0	50.3	70.6

Source: 2025 Technical Report

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The Feasibility Study locked cycle tests were satisfactory except for MET5-7 main composite, and this test was repeated at increased collector addition to obtain improved results. A summary of the final locked cycle test results for all Feasibility Study metallurgical domain composites is shown in Table 10-6.

Table 10-6: Locked Cycle Test Results

Domain	Head grade					Cu concentrate		HPM concentrate		Zn concentrate		Au, Ag recovery to Cu, HPM concentrates	
	Cu %	Pb %	Zn %	Au ppm	Ag ppm	Grade %Cu	Rec. %Cu	Grade %Pb	Rec. %Pb	Grade %Zn	Rec. %Zn	%Au	%Ag
+1,340RL	0.50	1.77	5.73	1.68	142	24.5	73.6	53.9	76.8	54.8	83.0	52.0	75.6
MET2-4	0.88	1.23	6.30	0.73	84	24.8	76.2	45.2	66.4	50.9	88.4	52.7	64.3
MET5-7	1.13	1.24	6.25	1.06	118	27.7	85.0	48.0	67.4	53.8	93.4	64.4	79.3
MET8	1.00	0.88	3.59	0.52	66	29.1	85.9	64.6	64.8	55.5	91.5	59.9	74.1
Krakatoa	0.35	2.18	5.05	1.53	184	27.3	58.5	57.9	80.2	53.1	91.0	57.5	73.1

Source: 2025 Technical Report

The optimised variability results that were completed were considered suitable as the basis for predictive recovery and concentrate grade models and the locked cycle test results correlated well with the optimised batch test results.

The differences in performance between the batch and locked cycle results were applied to the predictive models developed using the batch results and are considered to provide a reasonable basis for prediction of plant-scale performance.

10.3.1 Precious Metal Recovery

ABM and Krakatoa mineralisation contains gold and silver that are recovered to the copper, HPM, and zinc concentrates during sequential flotation and are contained in composite particles. Recovery of gold and silver into copper and HPM concentrates is preferable than into zinc concentrate as payability levels are higher.

Bench-scale tests were performed with the aims of:

- Characterising the deportment of gold and silver to the various concentrates.
- Increasing the overall recovery of gold and silver to flotation and/or gravity concentrates, as compared to the typical overall recovery to copper and HPM flotation concentrates.

These focused tests included:

- Amalgamation of milled mineralisation and of lead circuit tailings as a diagnostic assessment of free gold and silver.
- Gravity concentration of mineralisation and lead circuit tailings to minimise gold and silver deportment to the zinc concentrate and final tailings.
- Flotation tests using a gold specific collector in the copper flotation circuit to maximise gold recovery to copper concentrate.

The testwork showed:

- A high proportion of the gold and silver is recovered into the copper and HPM flotation concentrates with average aggregate recoveries of 60.9% for gold and 70.9% for silver.
- A very low proportion of free gold is present in the mineralisation confirmed by a low recovery to gravity concentrate. The average recovery of gold to gravity concentrates for all mineralised samples tested was 9.4% and the addition of gravity concentration to the flowsheet is generally

unlikely to significantly increase the aggregate gold and silver recovery, although opportunities remain to be investigated with the +1,340RL metallurgical domain.

The gold is likely very fine and is distributed mainly in (or associated with) copper, iron, and lead sulfides. The gold essentially exhibits a linear distribution by size fraction.

Using a gold specific collector in the copper circuit increases the proportion of gold and silver recovered to the copper concentrate and reduces the proportion recovered to the HPM concentrate but does not increase the aggregate recovery of gold and silver.

The aggregate recovery of gold and silver to gravity, copper, and HPM flotation concentrates was largely consistent, regardless of the use of gravity concentration or a gold specific collector, with the exception of the +1,340RL metallurgical domain.

10.3.2 Concentrate Dewatering

Dynamic settling and filtration testwork on copper, HPM, and zinc concentrate samples and determination of the transportable moisture limit (TML) was completed during the 2017 PFS.

The concentrate samples achieved very high solids concentration in the underflow, ranging from 75% to 83%, at low flocculant addition rates of 5–10 g/t, and produced overflow with low suspended solids (<100 ppm).

Competent concentrate filter cakes were formed, with low moisture content ranging from 7% to 9%, and with filtration rates ranging from 756 kg/h/m^2 to 1,240 kg/h/ m^2. Concentrate filter cake TML ranged from 8% to 10%.

The bulk tailings sample achieved very high solids concentration in the underflow, ranging from 73% to 75%, at low flocculant addition rates of 5–10 g/t, and produced overflow with low suspended solids (<120 ppm).

The 2017 PFS selected vacuum disc filters for dewatering the tailings and during the 2019 Feasibility Study, the use of vacuum disc filters was identified as a significant project risk, based on the reported inability of vacuum filtration to consistently produce suitable (low moisture) filter cake.

Additional filtration testwork was completed on the Feasibility Study flotation tailings samples from the +1,340RL, MET5-7, and ABM Master Composite 1 samples, including repeat tests on the ABM Master Composite 1 sample at a finer grind. This testing included three vacuum filtration methods and two pressure filtration methods. For the initial Feasibility Study tests, the vacuum filtration methods compared to pressure filtration, showed:

- higher cake moisture,
- inconsistent cake moisture,
- greater filtration rate, and
- inconsistent filtration rate.

During the repeat tests, vacuum filtration showed a higher moisture content and lower filtration rate for the finer sample compared to the initial tests while pressure filtration showed consistent moisture and filtration rates for the finer sample. Based on these results pressure filtration was selected for the Feasibility Study design.

A filter cake moisture less than 14% will be required for reliable operational performance and is achievable with the pressure filters selected for the Feasibility Study based on observations made during the filtration testwork. A filter cake moisture level of 10-11% was achieved by the subsequent testwork.

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10.3.3 Recovery and Grade Models

Mathematical models derived for each metallurgical domain were investigated from open circuit batch tests for:

- Major base metal recoveries to concentrates, as functions of Cu, Pb, and Zn head grades.
- Flotation concentrate grades (Cu, HPM, Zn), as functions of Cu, Pb, and Zn head grades.
- Recoveries of gold and silver to flotation concentrates.
- Recoveries of Pb, Zn, Fe, and S to copper concentrate, as functions of various head grade ratios (e.g. S/Cu).
- Recoveries of Cu, Zn, Fe, and S to HPM concentrate, as functions of various head grade ratios (e.g. S/Pb).
- Recoveries of Cu, Pb, Fe, and S to zinc concentrate, as functions of various head grade ratios (e.g. S/Zn).
- Grades of contaminants (As, Sb, Bi, Cd, Hg, Se) in flotation concentrates, as functions of various head grade ratios (e.g. Sb/Cu).

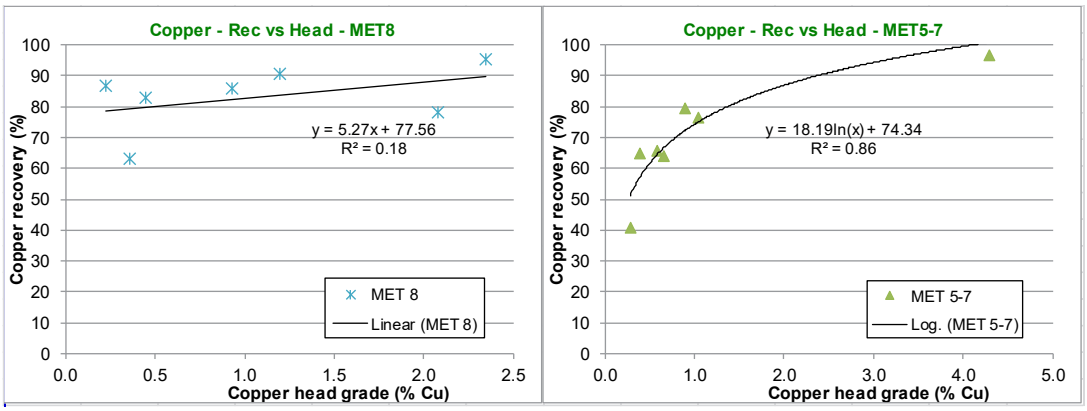
Most of the models showed moderate to strong correlation coefficients (R^2 in the range 0.3 to 0.99) and were adopted for predicting metallurgical performance. Certain datasets did not demonstrate a reliable relationship and in these instances the weighted average has been used. Weighted averages were adopted for:

- +1,340RL copper recovery to copper concentrate.
- Krakatoa zinc recovery to zinc concentrate.
- Gold and silver recovery to all base metal concentrates.
- Arsenic grade in HPM concentrate.

The presence of tennantite-tetrahedrite sulfosalts, which contain varying gold and varying silver up to 30% Ag, is partly responsible for the difficulty in deriving relationships of gold and silver recovery to head grade.

Recovery curves were based on open circuit batch tests for copper into copper concentrate (Figure 10-1), lead into the HPM concentrate (Figure 10-2) and zinc into zinc concentrate (Figure 10-3).

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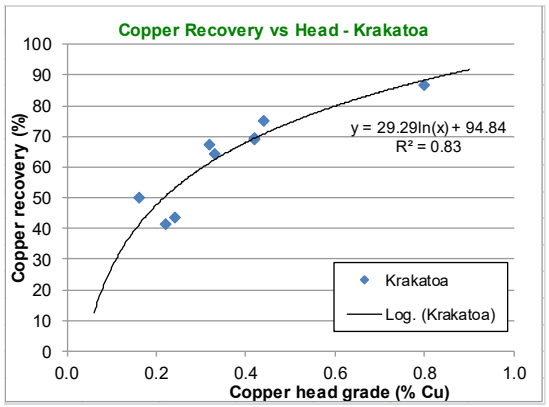


Figure 10-1: Copper head grade vs recovery (source: 2025 Technical Report)

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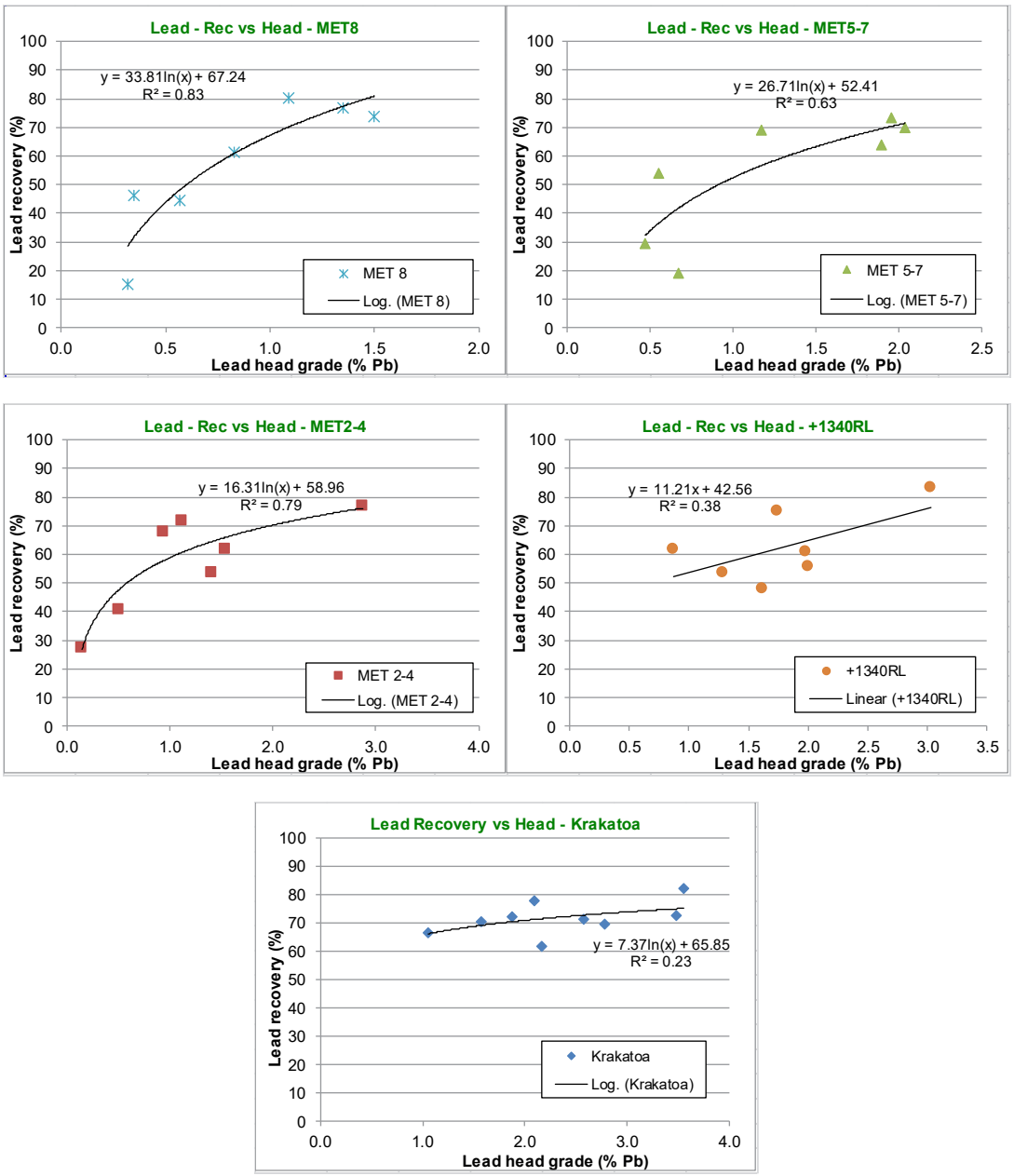


Figure 10-2: Lead head grade vs recovery

source: 2025 Technical Report

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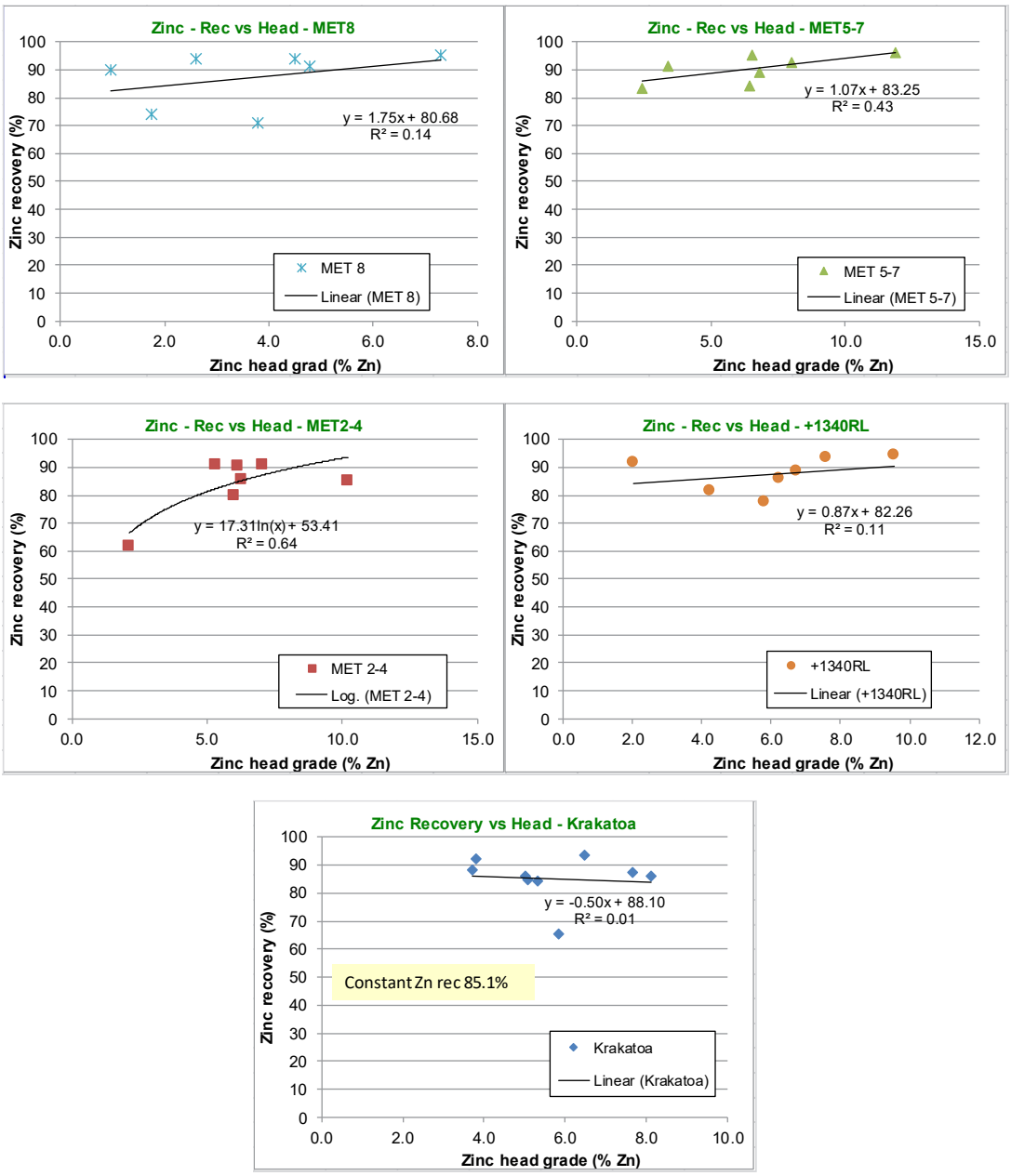


Figure 10-3: Zinc head grade vs recovery
source: 2025 Technical Report

All models were validated by examining the predicted performance for the locked cycle test samples against the actual locked cycle test results, with offsets applied to align batch test predictions to the locked cycle test results. The final recovery models, inclusive of offsets, for base and precious metals are detailed in Table 10-7.

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Table 10-7: Process Recovery Models

Concentrate	Met domain	Base metal recovery	Gold recovery	Silver recovery
Copper Concentrate	+1,340RL	67.5	18.6	33.9
	MET2-4	34.08*ln(Cu head)+79.54	34.2	36.6
	MET5-7	18.19*ln(Cu head)+69.04	27.3	34.2
	MET8	5.27*(Cu head)+82.16	56.0	31.1
	Krakatoa	29.29*ln(Cu head)+85.84	29.8	49.1
HPM Concentrate	+1,340RL	11.21*(Pb head)+56.36	35.5	37.2
	MET2-4	16.31*ln(Pb head)+59.76	20.5	40.6
	MET5-7	26.71*ln(Pb head)+62.41	33.1	42.2
	MET8	33.81*ln(Pb head)+61.44	5.7	25.2
	Krakatoa	7.37*ln(Pb head)+71.45	27.2	36.5
Zinc Concentrate	+1,340RL	0.87*(Zn head)+77.66	6.8	11.0
	MET2-4	17.31*ln(Zn head)+57.01	9.5	17.0
	MET5-7	1.07*(Zn head)+81.35	9.1	11.2
	MET8	1.75*(Zn head)+78.58	9.2	7.7
	Krakatoa	89.2	7.5	9.0

Source: 2025 Technical Report

10.3.4 Processing Schedule

The mineralisation has been scheduled to be processed at a maximum throughput rate of 2.2 Mtpa. When the scheduled zinc grade processed is more than that considered in each of the design cases, process plant throughput has been reduced so that the design case metal content (2.0 Mtpa throughput rate at 6.52% zinc grade, or 357 t of contained zinc per day) is not exceeded.

Copper and lead grades are typically inversely related (high copper with low lead and vice versa). Capacity constraints are associated with copper rather than lead and when high copper grades are scheduled lead grades are typically well below the design capacity indicating surplus capacity in the lead circuit. It is proposed that when periods of high copper grades are planned in the mine schedule some of the lead circuit capacity could be repurposed to provide additional copper circuit capacity.

A commissioning plan for the mineralised production has been prepared for the commissioning and ramp-up of the processing facilities where ore commissioning will commence with mineralised waste to facilitate testing the operational capacity of the grinding and tailings circuits.

Flotation circuits will then be progressively commissioned starting with the copper circuit followed by the lead and then zinc circuits. The progressive increase in throughput rates, processing recoveries and concentrate grades are detailed in Table 10-8.

Table 10-8: Process Plant Commissioning Schedule

Month of Commissioning	Plant feed[1] (%)	Copper concentrate				HPM concentrate				Zinc concentrate			
		Recovery (%)[2]			Concentrate grade (%)[3]	Recovery (%)[2]			Concentrate grade (%)[3]	Recovery (%)[2]			Concentrate grade (%)[3]
		Cu	Au	Ag		Pb	Au	Ag		Zn	Au	Ag	
1	10.7	N/A (Mineralised Waste Only)											
2	36.0	48.9	48.9	48.9	73.7	14.5	14.5	14.5	53.4	0	0	0	0
3	64.2	79.2	79.2	79.2	92.4	48.9	48.9	48.9	80	61.8	61.8	61.8	83.4
4	79.0	91.1	91.1	91.1	99.2	68.0	68.0	68.0	95.7	79.7	79.7	79.7	92.6
5	89.3	97.0	97.0	97.0	100	80.1	80.1	80.1	99.1	88.0	88.0	88.0	95.6
6	92.4	99.7	99.7	99.7	100	88.0	88.0	88.0	99.9	94.9	94.9	94.9	97.7

Month of Commissioning	Plant feed[1] (%)	Copper concentrate				HPM concentrate				Zinc concentrate			
		Recovery (%)[2]			Concentrate grade (%)[3]	Recovery (%)[2]			Concentrate grade (%)[3]	Recovery (%)[2]			Concentrate grade (%)[3]
		Cu	Au	Ag		Pb	Au	Ag		Zn	Au	Ag	
7	95.5	100	100	100	100	95.3	95.3	95.3	100	99.2	99.2	99.2	99.6
8	96.8	100	100	100	100	99.3	99.3	99.3	100	100	100	100	100
9	100	100	100	100	100	100	100	100	100	100	100	100	100
10	100	100	100	100	100	100	100	100	100	100	100	100	100

Source: 2025 Technical Report

Notes:

1. Percent of designed plant throughput.
2. Percent of expected recovery.
3. Percent of expected concentrate grade.

The LOM processing schedule, plant recoveries and proportions of each metallurgical domain are summarised in Table 10-9.

While relationships were developed for predicting concentrate grades for each domain, constant concentrate grades have been applied in the financial model of 25%, 52% and 52% for the copper, HPM and zinc concentrates, respectively. The process plant will be operated to target a steady concentrate grade and the financial model reflects this operating practice.

The predictive recovery models were applied to the LOM processing schedule to predict concentrate qualities for those elements where sufficient data exists (the economic elements and those deleterious elements that will attract penalty costs for marketing). For assessing the marketability of concentrates, two separate concentrate qualities have been defined and are detailed in Section 10.2.1.

In the first 18 months of the project, the +1,340RL metallurgical domain will be the sole source of ore for processing (Type A Concentrate Quality), until the open pit reaches sufficient depth to access other metallurgical domains and enable blending (Type B Concentrate Quality). Estimates of concentrations of the other elements in each concentrate were prepared by reviewing ICP data of the various concentrate products produced from locked cycle laboratory testing.

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Table 10-9: LOM Processing Schedule

Parameter	Units	Total	Yr 1					Yr 2					Yr 3	Yr 4	Yr 5	Yr 6	Yr 7	Yr 8
			Q1	Q2	Q3	Q4	Total	Q1	Q2	Q3	Q4	Total						
Ore processed	Mt	15.7	0.2	0.5	0.5	0.5	1.7	0.5	0.5	0.5	0.5	2.0	1.9	2.2	2.1	2.1	2.2	1.6
Mineralised waste	Mt	0.0	0.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Zinc grade	% Zn	5.8	6.6	6.5	6.6	6.5	6.5	6.2	6.4	6.3	7.1	6.5	6.7	5.2	5.9	5.7	5.3	4.7
Copper grade	% Cu	0.9	0.4	0.5	0.5	0.7	0.5	0.8	0.9	0.7	0.9	0.8	1.0	1.2	1.0	0.8	0.7	0.7
Lead grade	% Pb	1.7	2.1	2.1	2.0	1.9	2.0	1.8	1.8	1.7	1.7	1.7	1.7	1.2	1.7	1.8	1.7	1.8
Gold grade	g/t Au	1.3	1.7	1.7	1.7	1.6	1.7	1.6	1.5	1.5	1.4	1.5	1.4	1.2	1.3	1.1	1.2	1.3
Silver grade	g/t Ag	138	170	169	166	161	166	157	154	145	143	150	147	118	135	121	128	146
Iron grade	% Fe	29	27	28	29	29	29	30	31	30	33	31	32	31	30	27	26	24
Arsenic grade	ppm As	2,579	3,131	3,108	3,330	3,366	3,256	3,143	3,240	3,428	3,187	3,250	2,817	2,126	2,768	2,131	1,992	2,512
Mercury grade	ppm Hg	18	20	21	23	27	23	21	23	25	26	24	23	17	17	11	15	15
Antimony grade	ppm Sb	463	669	620	679	823	706	742	697	662	567	670	537	358	464	327	336	354
Selenium grade	ppm Se	197	142	148	149	176	156	196	200	196	233	205	201	184	185	214	218	204
Zinc concentrate																		
Zinc recovery	%	86	33	73	83	83	75	83	84	83	89	85	89	86	88	89	88	88
Gold recovery	%	8	3	6	7	7	6	7	7	7	9	7	9	9	9	9	9	8
Silver recovery	%	11	4	10	11	11	10	11	11	11	12	11	12	12	12	11	10	9
Copper concentrate																		
Copper recovery	%	74	46	65	68	68	65	68	68	68	72	69	75	81	75	71	70	75
Gold recovery	%	27	13	18	19	19	18	19	19	19	28	21	28	30	30	31	31	33
Silver recovery	%	37	23	33	34	34	32	34	34	34	35	34	35	34	36	40	40	44
HPM concentrate																		
Lead recovery	%	74	29	63	78	78	68	77	76	75	75	76	76	69	75	75	74	75
Gold recovery	%	29	13	28	35	36	31	36	35	36	31	34	30	28	29	27	28	25
Silver recovery	%	38	14	29	37	37	32	37	37	37	42	38	41	40	41	39	38	36
Ore processed by domain																		
+1,340RL domain	%	24	100	100	100	100	100	100	96	100	6	77	11	17	0	0	0	0
MET2-4 domain	%	12	0	0	0	0	0	0	2	0	21	5	24	18	25	13	6	1
MET5-7 domain	%	38	0	0	0	0	0	0	2	0	73	17	62	47	59	41	47	21
MET8 domain	%	10	0	0	0	0	0	0	0	0	0	0	3	17	7	14	16	26
Krakatoa domain	%	15	0	0	0	0	0	0	0	0	0	0	0	0	9	33	31	51

Source: 2025 Technical Report

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10.4 Plant Design

The processing plant and associated facilities have been designed to process mine production at an average rate of 2.0 Mtpa to produce separate copper, HPM and zinc concentrates. The plant will be capable of processing at a higher throughput rate of 270 t/h based on average ore comminution properties and average plant feed grades. The process rate can be varied on the grade of the ore presented to the plant. The process flowsheet (Figure 10-4) consists of following key stages:

- Crushing, stockpiling and grinding of the ROM production.
- Pre-float, rougher and cleaner flotation of copper (including a regrind of copper rougher concentrate).
- Sequential pre-float, rougher and cleaner flotation of lead (including regrind of lead rougher concentrate).
- Sequential pre-float, rougher and cleaner flotation of zinc (including regrind of zinc rougher concentrate).
- Thickening, filtration, and stockpiling on site of copper, HPM, and zinc flotation concentrates. Copper and zinc concentrates will be loaded in bulk onto trucks for transport off site, while HPM concentrate will be loaded into sealable containers before transport by truck off site.
- Dewatering of flotation tailings by thickening and pressure filtration.
- Transportation of filtered flotation tailings to the Class A Waste Storage Facility for disposal.

10.4.1 Process Design Criteria

A process design criteria (PDC) and mass balance detail was developed on the basis of annual ore production. The PDC considered major flows and availability of processes within the facility.

Three cases were considered in the design, based on the grade distribution from the PFS (CSA Global, 2017a) processing schedule and comminution data:

- Design Case: 2.0 Mtpa at 95th percentile of copper and lead grades, 99th percentile of zinc grade (85th percentile considered to provide inadequate design contingency) and 80th to 85th percentile of comminution data, as noted below.
- Average Case: 2.2 Mtpa at average copper, lead and zinc grades and average comminution data.
- Alternate Design Case: Design Case, but with the production of lower-grade concentrates.

A summary of the key process design criteria is given in Table 10-10 showing the performance of the plant for the Design Case and the Average Case, being the two key scenarios. Operating parameters across all three cases were considered in equipment sizing in the flowsheet.

The plant will have a design availability of 93% (after ramp-up) which was considered appropriate for a plant of this type and in this location. To support this, all essential pumps will have operational standby units and there is provision for non-essential pumps to have standbys installed as a risk mitigation if shown to be required. Selection and sizing of the crushing and grinding circuits was based on a conservative assessment of all testwork and historical data available. The comminution parameters used in the Design Case are:

- The 80th percentile value of the available data set of Bond Ball Mill Work indices.
- The 85th percentile value of the available data set of Bond Rod Mill Work indices.
- The maximum A x b value from the SMC Test results.

Ore will be blended from ROM stockpiles with a front-end loader (FEL) to feed the ROM bin.

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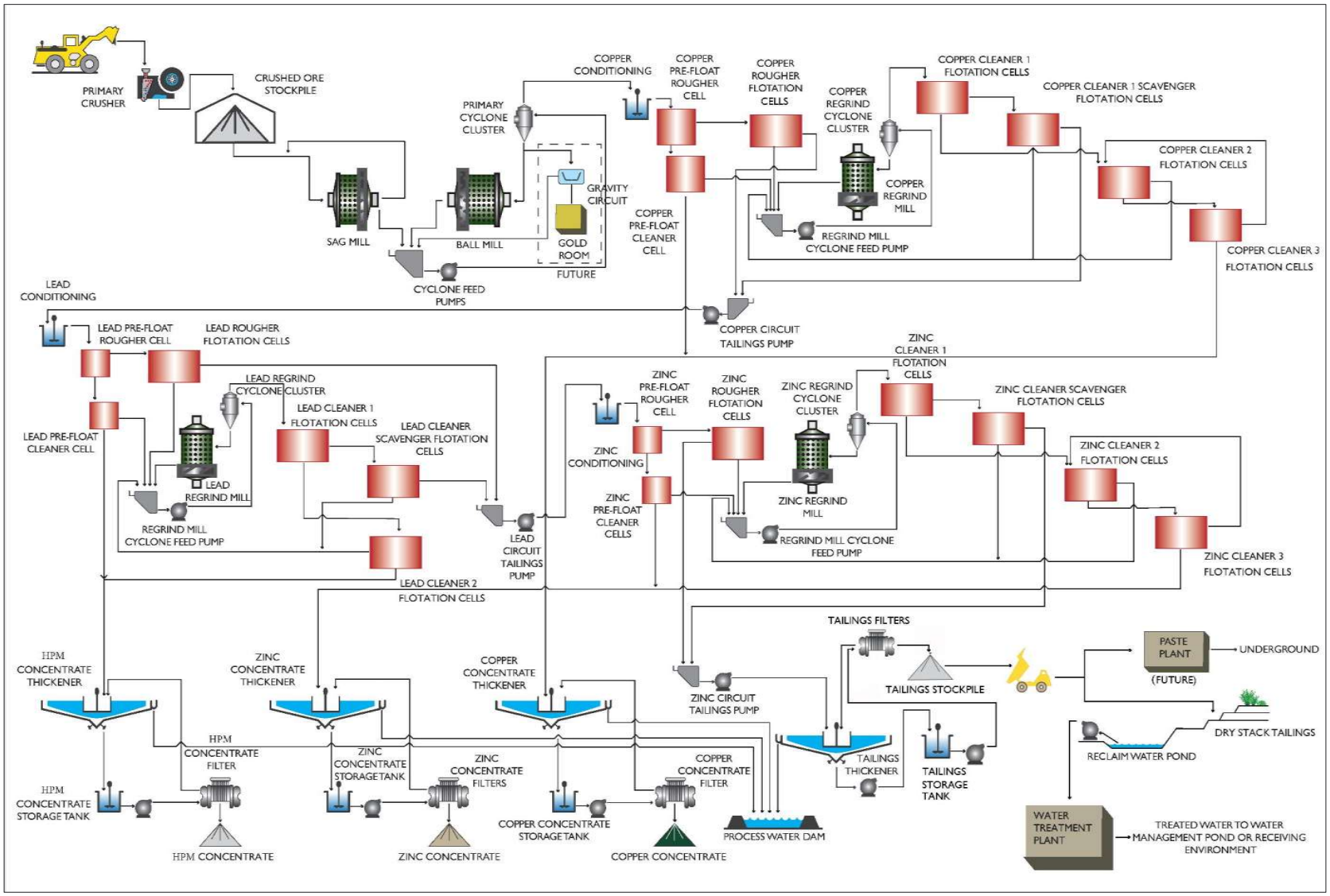


Figure 10-4: Process Flow Diagram
Source: BMC

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Table 10-10: Process Design Criteria

Criteria		Units	Design	Average	Source
Ore throughput		Mtpa	2.0	2.2	BMC
		t/h	245.5	270	Calc.
Plant availability	Design	%	93.0	93.0	BMC, Minnovo
Head grades		% Cu	1.12	0.82	BMC PFS mine schedule
		% Pb	2.33	1.62	BMC PFS mine schedule
		% Zn	6.52	5.52	BMC PFS mine schedule
Concentrate grades	Copper	% Cu	25	24	Testwork
	Lead	% Pb	52	50	Testwork
	Zinc	% Zn	52	50	Testwork
Recovery		% Cu	84	82	Testwork
		% Pb	76	72	Testwork
		% Zn	90	88	Testwork
Physical characteristics	BWI	kWh/t	12.8	11.8	Testwork
	RWI	kWh/t	10.4	8.9	Testwork
	AI	g	-	0.115	Testwork
	Axb	-	68.7	94.9	Testwork
	DWI	kW/m³	6.05	4.40	Testwork
Grind size	P_{80}	µm	70	70	Testwork
Gravity gold recovery			Future	Future	Minnovo
Copper circuit					
Pre-float and rougher lab residence time		minutes	8.5	8.5	Testwork
Pre-float cleaner lab residence time		minutes	1.0	1.0	Testwork
Concentrate regrind size P_{80}		µm	30	30	Testwork
Cleaner 1 lab residence time		minutes	4.5	4.5	Testwork
Cleaner 1 scavenger lab residence time		minutes	3.0	3.0	Assumed
Cleaner 2 lab residence time		minutes	4.0	4.0	Testwork
Cleaner 3 lab residence time		minutes	4.0	4.0	As Cleaner 2
Flotation residence time scale-up factors:					
- Rougher, cleaner 1 scavenger		-	2.5	2.5	Minnovo
- Pre-float cleaner		-	3.0	3.0	Minnovo
- Cleaner 1, cleaner 2, cleaner 3		-	3.0	3.0	BMC
Concentrate thickener solids flux		t/m²/h	0.20	0.20	Minnovo
Concentrate thickener u/f solids concentration		% w/w	65	65	Testwork
Filter type		-	Pressure	Pressure	Typical
Concentrate filter cake moisture – target		% w/w	9.6	9.6	Testwork
Lead circuit					
Pre-float and rougher lab residence time		minutes	7.0	7.0	Testwork
Pre-float cleaner lab residence time		minutes	1.0	1.0	Testwork
Concentrate regrind size P_{80}		µm	30	30	Testwork
Cleaner 1 lab residence time		minutes	7.0	7.0	Testwork
Cleaner 1 scavenger lab residence time		minutes	3.0	3.0	Assumed
Cleaner 2 lab residence time		minutes	4.0	4.0	Testwork
Flotation residence time scale-up factors:					
- Rougher, cleaner 1 scavenger		-	2.5	2.5	Minnovo
- Pre-float cleaner		-	3.0	3.0	Minnovo
- Cleaner 1, Cleaner 2		-	3.0	3.0	BMC
Concentrate thickener solids flux		t/m²/h	0.20	0.20	Minnovo
Concentrate thickener u/f solids concentration		% w/w	65	65	Testwork
Filter type		-	Pressure	Pressure	Typical
Concentrate filter cake moisture – target		% w/w	7.5	7.5	Testwork
Zinc circuit					
Pre-float and rougher lab residence time		minutes	9.0	9.0	Testwork
Pre-float cleaner lab residence time		minutes	2.4	2.4	Testwork
Concentrate regrind size P_{80}		µm	35	35	Testwork
Cleaner 1 lab residence time		minutes	6.0	6.0	Testwork
Cleaner 1 scavenger lab residence time		minutes	3.0	3.0	Assumed
Cleaner 2 lab residence time		minutes	6.0	6.0	Testwork
Cleaner 3 lab residence time		minutes	6.0	6.0	As Cleaner 2
Flotation residence time scale-up factors:					
Rougher, cleaner 1 scavenger		-	2.5	2.5	Minnovo
Pre-float cleaner		-	3.0	3.0	Minnovo

Criteria	Units	Design	Average	Source
Cleaner 1, cleaner 2, cleaner 3	-	3.0	3.0	BMC
Concentrate thickener solids flux	t/m²/h	0.20	0.20	Minnovo
Con thickener u/f solids concentration	% w/w	65	65	Testwork
Filter type	-	Pressure	Pressure	Typical
Concentrate filter cake moisture – target	% w/w	9.5	9.5	Testwork
Concentrate storage				
Copper	tonnes	5,000	5,000	BMC
	-	Containers	Containers	BMC
Zinc	tonnes	10,000	10,000	BMC
Off spec concentrate	tonnes	700 to 1,000	700 to 1,000	BMC
Tailings thickener solids flux	t/m²/h	1.0	1.0	Testwork
Tailings thickener u/f solids concentration	% w/w	60	60	Testwork
Tailings filter type	-	Pressure	Pressure	Testwork
Tailings filter cake moisture – target	% w/w	13	13	Testwork
Paste feed solids type	-	Filter cake	Filter cake	BMC
Paste binder addition (dry solids basis)	%	4.0	4.0	Testwork
Reagent addition:				
Lime	kg/t	1.31	1.31	Testwork review
SMBS	g/t	648	648	Testwork review
Collector A3894	g/t	31	31	Testwork review
Sodium cyanide	g/t	121	121	Testwork review
Zinc sulfate	g/t	374	374	Testwork review
Collector 3418A	g/t	9	9	Testwork review
Copper sulfate	g/t	634	634	Testwork review
Collector A208	g/t	77	77	Testwork review
Frother	g/t	41	41	Testwork review
Flocculant	g/t	20	20	Testwork review

Source: 2025 Technical Report

10.4.2 Process Description

An overview of the processing facilities and general arrangement is shown in Figure 10-5. The facilities comprise the following main areas: crushing; transfer station; coarse ore stockpile; grinding – SAG and Ball mills; flotation; regrind – vertical mills; concentrate thickeners and filters; concentrate storage and loadout; tailings thickening and filtration; reagents – storage, mixing and distribution; general plant services; process building; and assay laboratory.

10.4.3 Equipment Selection

Equipment selection has been in accordance with the following criteria:

- All equipment will be new.
- Proven performance in similar application.
- Ability to operate continuously 24 hours per day.
- Be readily capable of performing the specified duty with minimum maintenance.
- Incorporate the best materials and practices in line with modern engineering concepts to ensure maximum serviceability of the equipment in operation.
- Provide for the replacement of wearing parts with the least possible downtime.
- Provide features which will reduce the cost of maintenance and operation and improve accessibility for maintenance purposes.

Preference has been given to the use of standard proprietary items of equipment and components. The number and sizes used have been kept to a minimum to reduce the size of spares inventories.

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10.4.4 Crushing

A reinforced concrete steel bridge, with a retaining wall, extends from the ROM pad to the ROM bin dump point. This bridge provides access for an appropriately sized FEL. A 900 mm grizzly for scalping oversize material is installed on the ROM Bin which will have 20 minutes retention time (135 t).

ROM ore is withdrawn from the bin by an apron feeder and fed to a vibrating grizzly for removal of fines. The vibrating grizzly will operate ahead of the primary crusher to remove fines from the crusher feed. The Design Case throughput rate for the crusher was estimated to be 446 t/h, operating 13.5 hours per day.

Provision was made for a tramp metal magnet on the Primary Crusher Discharge Conveyor, as well as a metal detector on the Coarse Ore Stockpile Feed Conveyor. Insertable bag type dust collectors are provided to collect and filter out fugitive dust emissions from the materials handling circuit.

Normal crusher feeding practice will entail the crusher operator manning the FEL and loading the ROM bin. Video monitors in the FEL cab will allow the operator to monitor the status of the crusher during loading operations. An emergency stop switch located in the FEL cab will be capable of shutting down all crushing operations remotely from the cab.

10.4.5 Transfer Station

The Transfer Station is a braced steel structure that supports the head end of the Primary Crusher Discharge Conveyor and the tail end of the Coarse Ore Stockpile Feed Conveyor. A pneumatically actuated flop-gate can divert crushed rock into a bunker if required to produce crushed waste rock for road base or blast hole stemming. It can also be used as a short-term stockpile for crushed ore in the event of a downstream stoppage. Tramp metal collected by the Primary Crusher Discharge Conveyor will also be collected in a skip bin at this facility.

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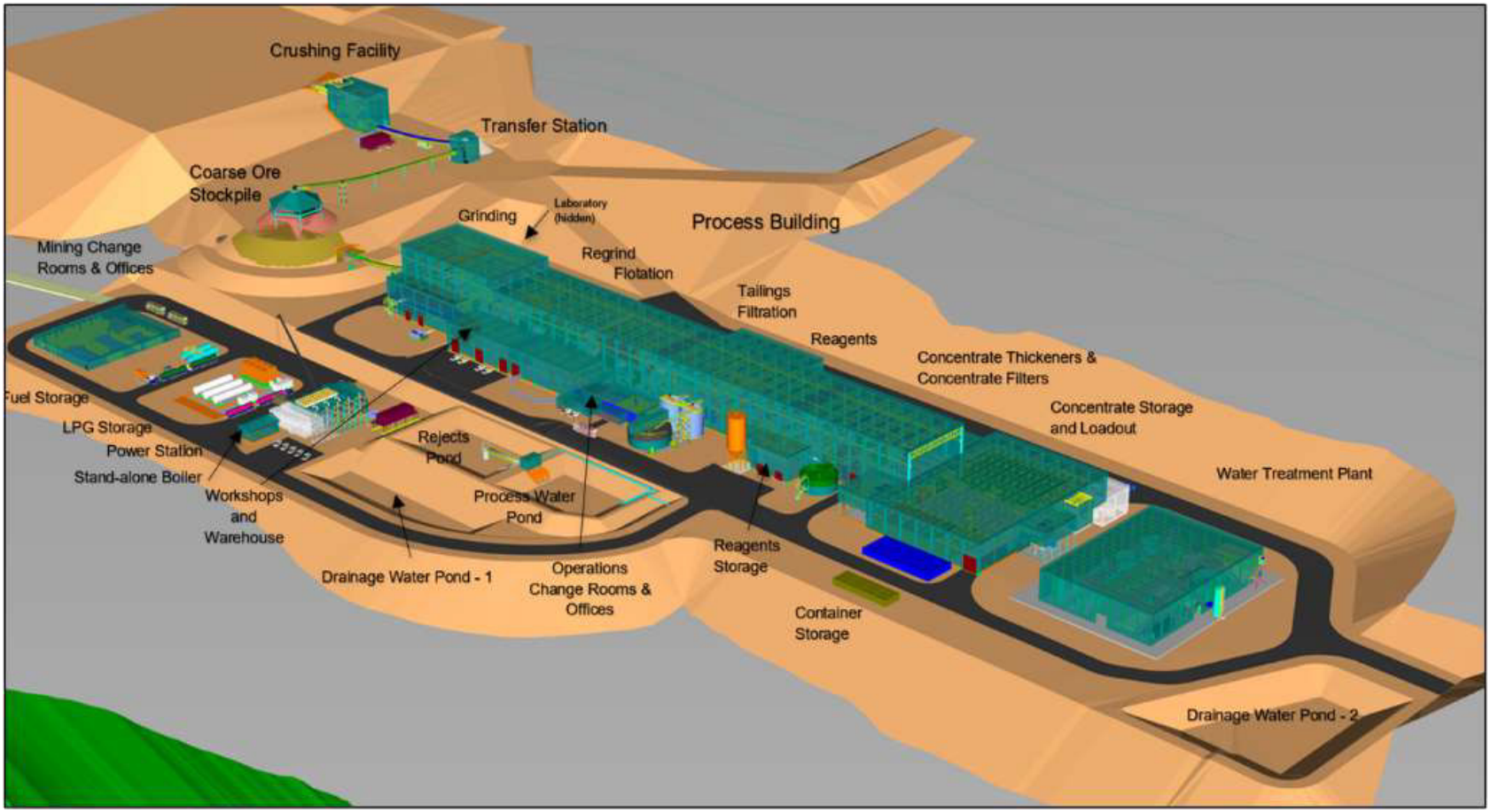


Figure 10-5: Planned Processing Facilities
Source: 2025 Technical Report

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10.4.6 Coarse Ore Stockpile

The Coarse Ore Stockpile facility is of the conventional open stockpile type, receiving crushed ore via the 1,200 mm-wide Coarse Ore Stockpile Feed Conveyor. Ore reclaim is by a passive slot type Reclaim Hopper via two in-line apron type reclaim feeders discharging onto the 1,200 mm-wide SAG Mill Feed Conveyor.

The Coarse Ore Stockpile has a target live capacity of 12-hours of SAG Mill new feed. The total stockpile capacity (including dead capacity) will be approximately two days. A dozer can be used to reclaim the "dead" stockpile material to provide emergency feed to the grinding circuit. Two apron feeders have been selected to reclaim ore from the stockpile, each able to deliver 100% of the design SAG Mill feed rate.

10.4.7 Grinding – SAG and Ball Mills

The SAG Mill and Ball Mill grinding circuit are located at the southern end of the Process Building where the ore is fed from the Coarse Ore Stockpile via the SAG Mill Feed Conveyor. The grinding circuit will comprise an open circuit SAG Mill and a Ball Mill in closed-circuit with cyclones.

The SAG Mill will be a 5.79 m diameter by 5.49 m effective grinding length (EGL), grate discharge, steel-lined mill, driven by a 2.7 MW single pinion drive. The SAG Mill will discharge over a 12 mm aperture trommel screen. Trommel oversize (pebbles and steel scats) will be returned to the SAG Mill Feed Conveyor by three recycle conveyors in series.

The Ball Mill will be a 4.72 m diameter by 7.32 m EGL, overflow discharge, rubber-lined mill driven by a 2.7 MW single pinion drive. The mill will be driven by a fixed speed drive and will operate at nominally 75% of critical speed. The Ball Mill will discharge over a 10 mm aperture trommel screen. The oversize will discharge into a bunker for disposal as waste. The undersize will gravitate into the mill discharge hopper.

The SAG Mill trommel screen undersize will also gravitate to the mill discharge hopper, where the combined mill discharge will be diluted with process water and pumped via duty/standby pumps to a hydrocyclone cluster for classification. The overflow from the cluster will flow by gravity to the flotation feed trash screen, to remove any trash prior to flotation. A portion of the cyclone underflow can be directed to the SAG Mill to facilitate balancing of the grinding in the SAG Mill and Ball Mill as the SAG Mill will generally have spare capacity on most ore types.

A common liner handler will be used to facilitate removal and installation of the SAG Mill and Ball Mill liners during planned mill relines. An overhead gantry crane will be used for recharging grinding media as well as maintenance of the mills and cyclones.

Provision has been made within the Grinding and Classification area to receive a gold recovery facility if required in the future.

10.4.8 Flotation

The flotation circuit is sequential, with copper, lead, and zinc recovered in that order. All flotation cells are mechanically agitated, forced air conventional cells. In addition to the flotation cells noted below, the plant layout has allowed space for additional flotation cells to be installed within the plant footprint should future ore sources warrant this.

Copper

Trash screen underflow slurry is pumped to the first of two 40 m^3 agitated copper conditioning tanks, where flotation reagents are added. Conditioned slurry flows to the first of six 38 m^3 rougher flotation cells in series. The first rougher cell will operate as a pre-float rougher which is then pumped to a

single 8 m³ pre-float cleaner cell and the concentrate pumped to the copper final concentrate hopper. Pre-float cleaner tailings flows to the copper regrind mill. Tails from the pre-float rougher passes to the remaining rougher cells. Concentrate from the rougher cells is pumped to the copper regrind mill.

The regrind mill treats several streams from in the copper circuit: the pre-float tails; rougher concentrate; and cleaner tails. Regrind mill product flows to the cleaner circuit which includes three cleaner stages, with a cleaner-scavenger operating after the first cleaner. The copper first cleaner consists of four 8 m³ cells in series and two 8 m³ copper cleaner-scavenger cells in series. The copper second cleaner consists of four 4.3 m³ cells in series. The copper third cleaner consists of three 4.3 m³ cells in series. The third cleaner concentrate is pumped to the copper final concentrate hopper, where it combines with the copper pre-float cleaner concentrate. Rougher and scavenger tailings flow to the copper flotation tailings hopper feeding the lead circuit.

HPM

Combined copper flotation tailings are pumped to the first of two 40 m³ agitated lead conditioning tanks, where flotation reagents are added. Conditioned slurry flows to the first of five 38 m³ rougher flotation cells in series. The first rougher cell will operate as a pre-float rougher. Pre-float rougher concentrate is pumped to a single 8 m³ pre-float cleaner, where the concentrate flows to the HPM final concentrate hopper. Pre-float cleaner tailings are pumped to the lead rougher concentrate hopper. Rougher concentrate from the other four rougher cells is pumped to the lead regrind mill.

The regrind mill treats several streams from in the HPM circuit: the pre-float tails; rougher concentrate; and cleaner tails. Regrind mill product flows to the lead cleaner circuit, which includes two cleaner stages with a cleaner-scavenger operating after the first cleaner. The lead first cleaner consists of four 16 m³ cells in series and two 16 m³ lead cleaner-scavenger cells in series. The lead second cleaner consists of three 4.3 m³ cells in series. The second cleaner concentrate flows to the HPM final concentrate hopper where it combines with the HPM pre-float cleaner concentrate. Rougher and scavenger tailings flow to the lead flotation tailings hopper feeding the zinc circuit.

Zinc

Combined lead flotation tailings are pumped to the first of two 40 m³ agitated zinc rougher conditioning tanks, where flotation reagents are added. Conditioned slurry flows to the first of six 38 m³ zinc rougher flotation cells in series. The first rougher cell will operate as a pre-float rougher. Pre-float rougher concentrate is pumped to two 16 m³ pre-float cleaners in series, where the concentrate is pumped to the zinc final concentrate hopper.

The regrind mill treats several streams from in the zinc circuit: the pre-float tails; rougher concentrate; and cleaner tails. Regrind mill product flows to the zinc cleaner circuit which includes three cleaner stages, with a cleaner-scavenger operating after the first cleaner. The zinc first cleaner consists of three 38 m³ cells in series and two 38 m³ cleaner-scavenger cells in series. The zinc second cleaner consists of three 16 m³ cells in series. The zinc third cleaner consists of three 16 m³ cells in series. Zinc third cleaner concentrate flows to the zinc final concentrate hopper, where it combines with the zinc pre-float cleaner concentrate. Rougher and scavenger tailings flow to the zinc flotation tailings hopper feeding the tails thickener.

10.4.9 Regrind – Vertical Mills

Regrinding the copper, lead and zinc rougher concentrates to P_{80} of 30 µm, 30 µm and 35 µm respectively has been included based on testwork. A single Metso SMD 355 kW unit was selected for each of the copper, lead, and zinc regrind duties. The plant layout has allowed space for an additional regrind mill should future expansion be required.

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10.4.10 Thickener and Concentrate Filters

High-rate thickeners have been selected for concentrate thickening. The copper concentrate duty requires a 9 m diameter thickener. The same diameter thickener has been selected for the HPM concentrate thickener to allow commonality of spares. The zinc concentrate duty requires a larger thickener of 14 m diameter.

Thickened concentrates will be pumped from the underflow to agitated filter feed tanks. There is one 220 m³ filter feed tank for each of copper and HPM concentrates, and two 300 m³ filter feed tanks for zinc concentrate.

Vertical plate pressure filters have been selected for concentrate filtration, based on the relatively fine concentrate regrind sizes and to consistently achieve concentrate TML's. Filters have been specified with membrane squeeze and air blow capability, to ensure the target moistures are achieved. A common filter size was selected for all three concentrate filtration duties to minimise spares. The zinc duty requires two filters operating in parallel to cater for its higher production rate. The recommended (common size) pressure filter has 85 m² of filtration area.

The concentrate filters will be installed onto an elevated steel platform. Discharge from the filters will be via chute and into the bunkers located within the Concentrate Handling and Loadout section of the Process Building. The filter discharge chutes will be fitted with doors for separation of the heating, ventilation and air conditioning (HVAC) for the main Process Plant building.

10.4.11 Concentrate Storage and Loadout

Filtered concentrate (filter cake) will be discharged into individual reinforced concrete bunkers directly below each filter in the Concentrate Storage and Loadout Shed. The copper and zinc filter cake will be removed by FEL and stacked in reinforced concrete bunkers inside the shed. HPM concentrate will be loaded directly into sealed transportable containers. Concentrate will be dewatered to a nominal 9% moisture content.

The storage capacity of copper and zinc concentrate in the bunkers is 5,000 t and 10,000 t, respectively. There is also provision for storage of off-specification concentrate in a separate bunker of 700 t to 1,000 t capacity (depending on concentrate type). The bottom section of the building walls will be made of reinforced concrete panels and walls against which the bulk concentrate will be retained. The walls have been designed to allow the FEL to reclaim against them and the loads from building columns.

Zinc concentrate will be bulk loaded into trucks and HPM concentrate will be loaded into sealed containers for transport by road to the port of Stewart. The Concentrate Storage and Loadout Shed has been designed to receive a Double-B type truck with bogey for the transport of concentrate to the port. Loading will be by FEL while the truck is on the weighbridge. HPM concentrate will be loaded from the bunker under the HPM filter into empty containers located within a segregated loading facility. The containers will be loaded onto the truck by a container lifter for transport to port. The loading facility will also contain a container washing system. Space is allowed in the layout for a future truck wash facility if operational needs require it.

Provision has been made for transportation of copper concentrate to a potential rail head, for subsequent loading and transportation on the Canadian rail network to domestic customers, if required.

10.4.12 Tailings Thickening and Filtration

A high-rate thickener will be used to thicken the flotation tailings stream prior to pressure filtration. The tailings duty requires a 20 m diameter thickener. The tailings thickener sizing has also considered reclaimed tailings slurry pumped from the reject pond.

Thickener underflow is pumped to two 750 m³ filter feed tanks that will operate in parallel to provide surge volume for the thickened tailings slurry. The tanks have been designed with a total live residence time of eight hours, being four hours per tank. A waste stream from the WTP will also be pumped to the Tailings Filter.

Two vertical plate pressure filters, each having 467 m² filtration area, have been selected to operate in parallel for tailings filtration. Selection of duty-duty filters minimises the impact of the filter downtime on slurry surge requirements, as at least one filter will be operating at any time.

At those times when a single tailings filter is operating and the level of the filter feed tanks is high, excess tailings slurry can be temporarily diverted to the HDPE lined Rejects Pond, which has a 12-hour capacity. This allows the plant to continue operating at normal solids feed rate in the expectation that the second tailings filter will shortly return to service. Tailings slurry reclaimed from the Rejects Pond will be pumped back to the tailings thickener feed box.

The Tailings Filters will be installed onto an elevated steel platform within the Process Building. The platform will be provided with a suspended concrete floor. The bottom section of the building walls will comprise of reinforced concrete panels and walls against which the bulk filtered tailings will be retained. The walls will be designed to allow the FEL to reclaim against them.

The tailings filter area has been designed to receive 50 t articulated dump trucks. One truck can be loaded at any one time. Loading will be by FEL.

10.4.13 Reagents – Storage, Mixing and Distribution

Majority of the reagent storage and mixing facilities are contained within the Process Building, apart from Lime Slaking and Lead Circuit Depressant 1 (sodium cyanide), which will be contained within separate building structures annexed to the Process Building. Sodium cyanide mixing equipment requires an enclosed building and bunding and will be annexed to the Process Building. All reagent mixing and storage tanks located indoors will be provided with a roof and vented either naturally or through forced extraction systems outdoors as nominated.

Reagents will be delivered to site in several forms. Dry bulk deliveries including quicklime and binder for paste backfill (Year 3 onward) will be delivered to site in bulk and transferred to dry storage silos. Bulk bag solid deliveries (750 kg to 1,000 kg) will be in dry solid form in bulk bags. Bulk liquid deliveries will be as 100% strength liquid in 1 m³ intermediate bulk containers, which will be used as storage vessels on site by connecting at least two intermediate bulk containers into a pipe manifold to the dosing pumps. Steel and ceramic grinding media will be delivered to site in 1 tonne bulk bags and stored outside.

Dry bulk delivered reagents will have up to seven days onsite storage. Copper circuit depressant will have up to 14 days storage onsite. All other reagents will have up to 30 days storage onsite. Grinding media storage is unrestricted.

Lime will be mixed using raw water in an automated lime slaking system (Vertimill™). Milk of lime slurry will be dosed to the grinding and flotation circuits from a ring main using actuated on-off valves.

Bag breaking systems will be elevated and installed on steel structures supported by reinforced concrete pedestals. Placement of the reagent package into the bag splitters will be by motorised

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monorail hoist. The reagents will be mixed with raw water and placed in a storage tank, where it will be distributed to the Process Plant. Reagent distribution to the dosing points will be by pressure pipeline except for the pH modifier (lime) which will be by ring main.

10.4.14 General Plant Services

Compressed Air

Plant and instrument air will be provided via two screw type air compressors. The air will pass through a dryer before use. The dried air will be fed to the Plant Air Receiver, from which it will be distributed to smaller air receivers such as those for instrumentation, SAG Mill and Ball Mill.

Five duty blowers and one standby blower will be installed to supply low pressure air to the flotation cells. Two screw type air compressors will produce compressed air that will feed the copper, lead, and zinc filter air receivers. Compressed air will be reticulated from the air receivers to each concentrate filter. A single dedicated screw type air compressor will produce compressed to the tailing filters air receiver.

Process Control

The plant will be appropriately automated to reduce the need for continuous or frequent operator intervention. Moderate levels of process and engineering data collection and equipment monitoring will be provided.

The plant will have a central control room from which the status of major electrical and mechanical equipment can be monitored, and process control loops can be monitored and adjusted. The Plant Control Room will be networked to the programmable logic controllers (PLCs) and operate a Supervisory Control and Data Acquisition (SCADA) system that provides an interface to the PLCs for control and monitoring of the plant. The SCADA system is configured to provide outputs to alarms, control the function of process equipment, and provide logging and trending facilities to assist in analysis of plant operations.

Video monitors and remote controls in the FEL cab will allow the Primary Crusher operator to monitor the status of the crusher during loading operations. A particle size analyser will provide grind size data on the Ball Mill cyclone overflow, and copper, lead and zinc regrind mill cyclone overflow streams.

Flotation feed concentrates and tailings streams as well as copper, lead and zinc regrind cyclone overflow streams are sampled and pumped to the online sample analyser area. Sampling and assay of the selected streams will be continuous by the online sample analyser with data returned to the Control Room. Field instruments provide inputs to a set of PLCs. Process control cubicles are in the motor control centres, and contain the PLC hardware, power supplies, and input/output cards for instrument monitoring and loop control.

10.4.15 Process Building

The main operating area of the Process Building is approximately 340 m long and 33 m wide. The Concentrate Storage and Loadout is approximately 54 m long and 78 m wide. The building will be 28 m at its highest point, above the grinding mills. The pad for the building will be excavated by cut to fill methods with key foundations located in rock.

The Process Building will be a pre-engineered building, fully clad with profiled insulated sheet metal (sandwich panel type) on the roof and all sides. Wall panels will be reverse lined at the concentrate storage area to assist with housekeeping and HPM concentrate clean-up. To eliminate ice, snow shed and icicle formation from the building roofs, a flat roof design will include heated parapets around the perimeter and internal downspouts to avoid freeze up.

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The design isolates the main operating area from potential fugitive dust, and diesel emissions of the concentrate storage and handling operations. Only the main operating area will be provided with HVAC supplied by heat recovery from the power station. For the concentrate storage and handling facility, a dedicated dust collection system will be provided.

A service way, accessible to mobile equipment, is located adjacent to the grinding area for grinding media recharge and maintenance activities. A second service way is located adjacent to the concentrate thickening and filtration equipment.

The main operating area is designed as a portalised structure such that internal columns are eliminated to enable unencumbered Overhead Travelling crane access. A total of four cranes operates within the main operating area of the building including: one 25 t Safe Lifting Limit (SLL) with an auxiliary 2.5 t SLL servicing the horizontal and vertical mills; and three 15 t SLL overhead gantry-type cranes with an auxiliary 1.5 t SLL servicing the flotation area, tailings filters, thickeners and concentrate filters within the low bay of the building. A fifth 10 t SLL overhead gantry crane will service the Concentrate filters, within the concentrate filter facility and its operation will be independent of the other cranes. Motorised hoists have also been provided where access is denied to these cranes due to overhead structures.

A transportable type of Plant Control Room will be installed inside the building, elevated to enable the Operator to view the flotation floor. A lean-to workshop is in the main operating area. Site administration, metallurgical offices and first aid will adjoin the building. Three Electrical Rooms will be located adjacent to the Concentrate building, one at each of the following facilities: Grinding, Flotation and Thickeners.

10.4.16 Assay Lab

A laboratory will be built on site for day-to-day analytical requirements. The laboratory will process around 300 samples per day. A laboratory services provider will be appointed to carry out design, equipping and operation of the laboratory. The laboratory will provide analytical services for the following sampling requirements:

- Open pit grade control sample preparation only (assaying at offsite laboratory).
- Underground grade control.
- Metallurgical investigation work.
- Process plant online sample analyser checks.
- Copper, HPM, and zinc concentrates.
- Waste rock acid generation potential.

Given that open pit grade control samples will be generated on a campaign basis, open pit grade control samples will be conducted at an offsite laboratory. Fire assaying for gold will also be completed at an offsite laboratory, considering that only base metal grades will be used for day-to-day operational control of the plant, and gold assays will only be used for reconciliation purposes. Exploration and environmental analytical testwork will also be conducted at offsite laboratories.

10.4.17 Services

Power

The power consumption required for processing was estimated to be approximately 44 kWh/t and an estimated 692 GWh will be required for the Process Plant over the LOM.

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Water

Average process water demand from the Process Water Dam was estimated to be 757 m³/h (including bleed water to WTP) and the dam will have capacity for two hours (live) residence time. The plant water balance is maintained by returning WTP treated water (68 m^3/h) to the Process Water Dam and through additional raw water input (18 m^3/h) from the Lower Water Management Pond. Make-up water from these two sources was estimated to be approximately 86 m^3/h in total. When the paste plant is in operation an additional 21 m^3/h will be required from the Lower Water Management Pond.

10.4.18 Reagents and Consumables

Projected requirements for reagents and consumables are given in Table 10-11.

Table 10-11: Annual average process plant reagents and consumables

Reagent/Consumable	Units	Consumption rate
Reagents		
Quicklime	t/yr	2,873
SMBS	t/yr	1,426
NaCN	t/yr	266
$ZnSO_4$	t/yr	823
$CuSO_4$	t/yr	1,395
DF469	t/yr	68
3418A	t/yr	20
DF262	t/yr	169
Frother	t/yr	135
Flocculant	t/yr	59
Consumables		
Grinding media steel (total)	t/yr	1,078
Grinding media ceramic	t/yr	80
Liners	t/yr	105
Filter cloths (concentrate)	No./yr	2,048
Filter cloths (tailings)	No./yr	2,880

Source: 2025 Technical Report

10.5 ERM Opinion

ERM believes the metallurgical testwork programme has been completed on appropriate representative samples of the expected polymetallic mineralisation that will be treated at the Kudz Ze Kayah Project, and geometallurgical domaining of the deposit has adequately informed the flowsheet development and design for the intended processing plant.

11. MARKET STUDIES AND OFFTAKE AGREEMENTS

Three separate concentrates will be produced during operations: copper, HPM and zinc, all with varying levels of precious metal credits and deleterious elements.

11.1 Product Quality

Metallurgical testwork completed for the Feasibility Study included production of typical concentrates with subsequent full elemental analysis to assess the quality of each concentrate.

In the first 18 months of the Project, the +1340 RL metallurgical domain will be the sole source of ore for processing (Type A Concentrate Quality), until the open pit reaches sufficient depth to access other metallurgical domains and enable blending (Type B Concentrate Quality). On this basis, two concentrate qualities (Quality A and B) were estimated for each product, for the purpose of assessing marketability, as shown in Table 11-1 and Table 11-2.

Table 11-1 Concentrate qualities – Quality A

Element	Unit	Copper concentrate Quality A		HPM concentrate Quality A		Zinc concentrate Quality A	
		Typical	Range of key elements	Typical	Range of key elements	Typical	Range of key elements
Cu	%	25.0	21.0-26.0	1.1	0.9-1.3	0.5	0.3-0.5
Pb	%	6.2	6.0-7.0	52.0	49.0-52.0	1.5	1.0-2.0
Zn	%	6.0	5.0-9.0	4.5	3.9-5.8	52.0	46.0-52.0
Au	g/t	18	15-24	20	16-21	1.2	1.0-1.3
Ag	g/t	3,500	2,500-4,500	2,100	1,800-2,500	165	150-180
As	ppm	6,000	4,800-6,000	5,650	5,350-6,100	2,450	2,400-2,580
Sb	ppm	16,500	11,500-20,000	8,000	6,700-9,500	500	-
Se	ppm	580	550-620	2,800	2,300-3,500	220	190-250
Hg	ppm	25	18-28	18	15-19	160	140-170
Cd	ppm	500	-	350	-	3,500	3,300-3,800
Fe	%	25	-	13	-	10	9-12
F	ppm	70	-	<20	-	200	100-300
Cl	ppm	<100	-	<100	-	<100	<100
Mo	ppm	90	-	80	-	80	-
Co	ppm	30	-	50	-	<20	-
S	%	33	-	25	-	33	-
SiO_2	%	0.2	-	0.3	-	0.1	-
Sr	ppm	<10	-	<10	-	<10	-
Al	ppm	200	-	200	-	200	-
Ba	ppm	900	-	600	-	550	-
Be	ppm	<5	-	<5	-	<5	-
Bi	ppm	130	-	1,000	-	60	-
Ca	ppm	1,000	-	700	-	1,700	-
Cr	ppm	20	-	30	-	30	-
K	ppm	200	-	<100	-	400	-
Li	ppm	<5	-	<5	-	<5	-
Mg	ppm	700	-	200	-	600	-
Mn	ppm	200	-	100	-	200	-
Na	ppm	80	-	100	-	<50	-
Ni	ppm	200	-	500	-	300	-
P	ppm	<100	-	<100	-	<100	-
Ti	ppm	<100	-	<100	-	<100	-
V	ppm	10	-	<10	-	<10	-
Y	ppm	<100	-	<100	-	<100	-
Si	%	0.72	-	0.12	-	0.05	-
Sn	ppm	<200	-	<100	-	<100	-
Te	ppm	0.4	-	0.4	-	<0.2	-
U	ppm	<2	-	<2	-	<2	-
Zr	ppm	20	-	<20	-	<20	-

Source: 2025 Technical Report

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Table 11-2: Concentrate qualities – Quality B

Element	Unit	Copper concentrate Quality B		HPM concentrate Quality B		Zinc concentrate Quality B	
		Typical	Range of key elements	Typical	Range of key elements	Typical	Range of key elements
Cu	%	25.0	21.0-26.0	1.2	0.8-1.4	0.5	0.3-0.5
Pb	%	3.5	2.0-5.0	52.0	49.0-52.0	1.5	1.0-2.0
Zn	%	3.8	2.0-5.0	3.3	3.1-3.6	52.0	50.0-52.0
Au	g/t	15	9-22	15	10-20	1.2	1.0-1.3
Ag	g/t	2,150	1,000-3,500	2,100	1,800-2,500	150	110-180
As	ppm	3,100	2,200-4,750	8,100	5,700-12,000	1,800	1,250-2,380
Sb	ppm	4,500	1,800-7,500	5,800	4,000-7,500	250	-
Se	ppm	530	400-680	2,950	2,400-3,800	300	220-500
Hg	ppm	12	9-16	15	9-23	150	100-170
Cd	ppm	500	-	250	-	3,500	3,300-3,800
Fe	%	27	-	15	-	9.4	8.5-11.0
F	ppm	70	-	<50	-	200	100-300
Cl	ppm	<100	-	<100	-	<100	<100
Mo	ppm	90	-	120	-	80	-
Co	ppm	30	-	50	-	<20	-
S	%	33	-	27	-	33	-
SiO_2	%	0.2	-	0.3	-	0.1	-
Sr	ppm	<10	-	<10	-	10	-
Al	ppm	200	-	200	-	200	-
Ba	ppm	900	-	700	-	700	-
Be	ppm	<5	-	<5	-	<5	-
Bi	ppm	130	-	1,000	-	90	-
Ca	ppm	1,000	-	700	-	2,400	-
Cr	ppm	20	-	30	-	30	-
K	ppm	200	-	<100	-	400	-
Li	ppm	<5	-	<5	-	<5	-
Mg	ppm	700	-	800	-	1,000	-
Mn	ppm	200	-	100	-	250	-
Na	ppm	80	-	100	-	80	-
Ni	ppm	200	-	500	-	300	-
P	ppm	<100	-	<100	-	<100	-
Ti	ppm	<100	-	<100	-	<100	-
V	ppm	10	-	<10	-	<10	-
Y	ppm	<100	-	<100	-	<100	-
Si	%	0.72	-	0.12	-	0.08	-
Sn	ppm	<200	-	<100	-	<100	-
Te	ppm	0.4	-	0.2	-	<0.2	-
U	ppm	<2	-	<2	-	<2	-
Zr	ppm	20	-	<20	-	<20	-

Source: 2025 Technical Report

Deleterious elements that will attract penalty costs were identified from the concentrate qualities in Table 11-1 and Table 11-2, and predictive algorithms for the recovery to concentrate of these elements have been developed.

11.2 Sales Contracts

The Company has definitive sales contracts (that have been seen by the author) in place to sell:

- around 95% of the ABM Mine Project's zinc concentrate;
- 100% of the copper concentrate; and,
- 100% of the HPM concentrate;

expected to be produced in the first five years of production of operation of the ABM Mine.

All definitive contracts are with reputable international buyers.

BMC has chosen to preserve most concentrate beyond the initial five years for future sales negotiations in line with its strategy to negotiate these concentrates into standard industry-based contracts on a case-by-case basis, with a combination of long-term, medium-term, and spot contracts

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where the Company can its then position as an established producer of products that are well-known and understood by the global concentrate market.

The terms of the definitive contracts are described as market-standard for these types of metal concentrates. The definitive contracts use a pricing structure based on an industry-standard model with concentrate delivered on the basis of CIF FO (cost, insurance, freight, free out).

The concentrate sales prices reference the prevailing LME cash settlement prices for zinc, copper and lead, and the prevailing London Bullion Market Exchange silver and gold spot prices (averaged over applicable quote periods), less specific charges (including treatment charges) and penalties based on the concentrations of certain elements.

ERM notes that pricing and the economic impacts of the contracts are consistent with that used in the 2025 Technical Report.

11.3 Zinc Concentrate Marketing and Concentrate Terms

The zinc concentrate produced will be a mid-grade material with payable silver content. There are some elements that may attract penalties, especially mercury and cadmium. The cadmium level exceeds the current limit for import into China; however, this market could be accessible through blending the product with other concentrates via trading houses. Other potential markets exist in the Asia region such as Korea, Japan and Europe but will be subject to respective concentrate quality criteria.

There are several advantages of this concentrate. With many of the world's smelters integrated with additional processing facilities, the copper and lead content of the zinc concentrate represent value added opportunities. The very low silica content of the concentrate (0.1%) will be very attractive, as many of the world's large zinc mines contain silica levels of 4% and higher, and smelters are struggling with the silica load.

11.4 Copper Concentrate Marketing and Concentrate Terms

The copper concentrate quality for the first 18 months (Quality A concentrate) will be complex, with elevated levels of lead, zinc, antimony and arsenic. The arsenic and lead levels exceed the current Chinese import limit for copper concentrates, but since the silver and gold levels are elevated, this concentrate could possibly be sold directly into China as a precious metals concentrate. Alternatively, it could be blended with product from other producers via a trading house.

The precious metals content of the Quality B concentrate is lower compared to Quality A; however, the arsenic and lead levels are comfortably below the Chinese import limit, although cadmium is still at the limit. With the lower impurities, the Quality B product has more flexibility with respect to smelter destinations. Whilst still incurring penalties for arsenic and antimony, and to a lesser extent zinc and lead, the Quality B concentrate is expected to be directly marketable to mainstream smelters in China, Korea, Japan and Canada. In addition, given the high level of silver in the Quality B concentrate, the copper concentrate could possibly be shipped into China as a silver concentrate, depending on the final grades.

Copper concentrate is currently planned to be transported to the port of Stewart or to the rail head in BC for transport to domestic customers in North America.

11.5 HPM Concentrate Marketing and Concentrate Terms

The HPM concentrate is a mid-grade concentrate with good silver and gold values.

The HPM concentrate contains levels of zinc, copper and antimony, which could potentially be recovered by Chinese lead smelters as economic by-products. The Quality A HPM concentrate is expected to be directly sold into China, whereas the Quality B concentrate will exceed the current arsenic import limit in China of 0.7%. This together with elevated chromium levels means the Quality B concentrate is expected to be sold directly to Western smelters, or to trading houses for blending.

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12. NON-PROCESSING INFRASTRUCTURE AND LOGISTICS

12.1 Travel

Travel through the area is primarily by road along the Robert Campbell Highway (Highway 4), 24 km north of the ABM Deposit, and this is the major transport route between the local centres. Each of the local population centres is also serviced by an airstrip, with Watson Lake being the only sealed runway.

Air travel specifically for the Kudz Ze Kayah Project will be via the Finlayson airstrip, located adjacent to the Robert Campbell Highway, approximately 15 km north of the Tote Road.

12.2 Services

The closest grid power is located at Ross River and given the distance; it was determined to be more viable to generate power on site for the Kudz Ze Kayah Project. Water for the operations will be sourced from groundwater produced from dewatering the mine and surface runoff captured within the footprint of the operation.

12.3 Local Employment

It was identified through consultation with local communities and the Kaska First Nations that unemployment and underemployment within local communities is high. It is proposed to preferentially hire local people for the operation. Scholarship and training programmes are already underway to encourage participation and improve local skills.

The point of hire for most personnel required for the operations will be in Yukon, with transportation to site being a combination of road and/or air transport. Contractors and other third parties may source locally or from further afield as required.

12.4 Tailings and Waste Rock

Sufficient suitable areas are available for the permanent storage of all tailings and waste rock that will be produced during operation. The storage areas are located along the side of the valley above Geona Creek, and the proposed landforms have been determined to be permanently stable.

12.5 Infrastructure Sites

Several locations for the process plant were considered during the PFS, and the final location was decided during the Feasibility Study. The proposed site for the process plant is located on the western side of the valley above Geona Creek, approximately 1.5 km north of the mining operation. There is enough area available to construct all required infrastructure for the plant. However, earthworks will be required to create a level and stable site on which to construct these facilities.

12.6 Project Infrastructure

The general arrangement of the Kudz Ze Kayah Project is shown in Figure 9-1.

The key items of infrastructure include:

- Open pit and underground mines.
- Processing facility, associated ROM, and low-grade stockpile facilities.
- Paste backfill plant.

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- Three waste storage facilities for tailings and waste rock. Waste rock will be placed in different storage facilities based on the assessed potential for generation of acid drainage and metal leaching.
- Overburden and topsoil stockpiles that will be used for site reclamation during operations and eventual closure.
- Water management infrastructure, including a pond for mine dewatering, collection ponds, water management ponds and surface water diversion ditches.
- Camp facilities.
- General mine infrastructure including explosives facilities, workshops, and fuel facilities.

12.7 Tailings and Waste Storage Facilities

Tailings are managed as a waste material and require a geotechnically and geochemically stable storage option that will manage the tailings throughout the mine life and after closure.

Filtered tailings storage was selected as the preferred storage method after consideration of the various tailings storage methodologies, together with potential storage sites. This method requires the tailings to be dewatered to produce a filter cake which is then transported by truck to the Class A Storage Facility where they will be comingled and stored together with Class A waste rock.

The waste storage facilities (WSF) have been designed to cater for the maximum production of each material type from the mining and processing operations.

Waste rock will be classified as either Class A, B or C, based on the acid drainage and metal leaching potential, when placed in a waste storage facility over short-term and long-term periods. The identification of the waste rock "Class" is based on laboratory analysis for sulfur and carbonate content to estimate the acid and neutralisation potential as separate facilities will be constructed to store each Class of waste rock.

12.7.1 Class A

Class A waste rock is defined as potentially acid generating (PAG) and/or metal leaching in the short term (i.e. within the life of the operation). This material will be contained in a storage facility with controlled drainage during operations and will be encapsulated and reclaimed after completion of mining to minimise contact with oxygen and water.

Class A Storage

The Class A Storage Facility will be located on the western hillside of Geona Creek, north of the processing plant (Figure 9-1). It has been designed to manage filtered tailings and waste rock material that is classified as potentially strongly acid generating and/or metal leaching in the short term (i.e. within the life of the operation). During operations, tailings from the process plant and Class A waste rock excavated from the pit will be co-mingled, placed in thin lifts, and compacted.

The footprint of the Class A WSF will be cleared of trees and topsoil stockpiled to expose the relatively thin layer of glacial till overburden and weathered bedrock and constructed.

The design of the facility incorporates basin and cover layers, each comprising a layer of low permeability glacial till material, an 80 mm textured HDPE geomembrane and a final layer of crushed sand and gravel placed above the geomembrane for protection from construction vehicle traffic and to collect and convey seepage within the facility. Seepage will be pumped from the sumps to the Class A collection pond where it will be pumped to the WTP.

The cover layer of the facility will be capped with a layer of a minimum of 3 m of Class C material for frost and erosion protection, and to improve long-term geotechnical stability. Overburden and topsoil

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will be spread above the Class C rock, and the facility will be revegetated to mimic pre-mining conditions on the hillside.

The Class A WSF has been designed with a capacity of approximately 14 Mm^3 and the design considered potential variations in actual volumes that may be encountered during operations, as more accurate methods are developed for the identification and management of the different classes of waste rock.

12.7.2 Class B

Class B waste rock is defined as PAG and/or with metal leaching potential over the longer term (after cessation of mining activities). Storage of this material will require controlled drainage during operations and encapsulation will be required after cessation of mining as part of the reclamation plan.

Class B Storage

The Class B Storage Facility will be located on the western hillside of Geona Creek, north of the open pit and south of the process plant area (Figure 9-1). It is designed to contain waste rock classified as weakly PAG, and the ROM pad and Low-Grade Ore stockpile are incorporated into the design.

The footprint of the Class B WSF will be cleared of trees and topsoil stockpiled, exposing the relatively thin layer of glacial till overburden and weathered bedrock.

Class B material requires encapsulation to limit contact with oxygen and water and the facility is designed with the same composite liner and cover system as the Class A Storage Facility. In addition to the closure layer, the Class B facility will be covered with a 3 m to 8.5 m layer of Class C waste rock for stability, as well as frost and erosion protection. Overburden and topsoil will be spread above the Class C rock, and the facility will be revegetated to mimic pre-mining conditions on the hillside.

The Class B WSF has been designed with a capacity of approximately 21 million m^3 which is more than sufficient for storage of the estimated quantity of Class B waste rock.

12.7.3 Class C

Class C waste rock is defined as material that is non-reactive or potentially acid consuming and will have low metal leaching potential and specific ARD management strategies are not required. This material is suitable for construction purposes around the site as well as capping material required for reclamation during closure.

Class C Storage

The Class C WSF will be located on the eastern hillside of Geona Creek, in a hanging valley northeast of the open pit (Figure 9-1) and specific ARD management strategies are not required.

Prior to operating the facility, the footprint of the Class C Waste Storage Facility will be cleared of trees and topsoil stockpiled, exposing the relatively thin layer of glacial till overburden and weathered bedrock. At the end of operations, the facility will be contoured and revegetated to resemble slopes at a similar elevation.

The Class C WSF has been designed to have a capacity of approximately 44 Mm^3, which is more than sufficient for storage of all Class C waste rock.

12.7.4 Overburden Stockpile

The Overburden Stockpile is designed to temporarily store overburden material comprising glacial till and glaciolacustrine sediments excavated from the open pit area or beneath site infrastructure. It is located along eastern side of Geona Creek, north of the Class C Waste Storage Facility.

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Overburden material will be selectively stored in and sourced from the stockpile and will be used during operations as a construction material as well as during closure for reclamation and select cover material for the other facilities. The stockpile will be completely removed after the end of operations during the closure phase.

Approximately 8.5 Mm^3 of overburden will need to be excavated for construction and operation of the mine and this is expected to satisfy the overall requirement for closure.

12.7.5 Topsoil Stockpile

Topsoil will be removed from the base of the Overburden Stockpile, Class A, B and C WSF and the footprint of the open pit and other surface infrastructure (such as ponds, process plant, admin buildings, power plant, etc) during construction. Topsoil will be used during closure and reclamation to revegetate the Class A, B and C WSF as well as the Overburden Stockpile area itself.

The total estimated volume of topsoil, based on the average thickness, is approximately 1.5 Mm^3 and the stockpile surfaces will be temporarily revegetated during operations to stabilise the slope surfaces and control erosion from runoff.

12.8 Water Storage and Management

12.8.1 Water Management

Water management planning has formed an integral part of the project infrastructure design where the plan involves collecting and managing site runoff from disturbed areas and maximising the recycle of mining and process water. Surplus water will be stored on site with excess water treated (if required) prior to being released to Geona Creek or pumped to Finlayson Creek.

All water in contact with the mine facilities, including the Class A, B and C WSF, overburden stockpile, open pit and the process plant site and other infrastructure will be collected in ponds for sediment control prior to pumping to either the WTP or water management ponds. The water will ultimately be released into Geona Creek or Finlayson Creek when contaminants are within project water quality guidelines.

The WTP will be constructed adjacent to the process plant and is designed to reduce contaminants in the contact water to acceptable levels in accordance with project water quality guidelines.

12.8.2 Erosion and sediment Control

Erosion and sediment control management strategies will include limiting mine site disturbance, establishing diversion and collection ditches to manage surface water runoff, constructing sediment management devices such as collection and diversion ditches (Figure 9-1), sediment traps and sediment ponds, stabilising disturbed land surfaces to minimise erosion, ripping of rehabilitation areas to promote infiltration, establishing temporary vegetative covers, re-establishing vegetation that is similar in structure to natural vegetation where final slopes are created and restricting access to rehabilitated areas.

12.8.3 Overburden Dewatering

Overburden dewatering in the open pit area will occur during the pre-production period to facilitate mining. The overburden dewatering design incorporates a series of trenches and sumps (Figure 8-2) that will be used to collect water for pumping to the staging pond, where sediment will be allowed to settle out prior to water being reused or discharged.

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12.8.4 Creek Diversion

Fault Creek will be diverted south (Figure 9-1) towards the North Lakes during operations to temporarily interrupt flow towards the open pit area. The current design incorporates a lined diversion ditch constructed alongside the access road.

12.8.5 Water Balance Modelling

A water balance model has been developed to simulate the potential effects of climate variability on surface and groundwater flows and assess the effectiveness of the proposed mine water management system.

Forty-six different climate scenarios were simulated, and the results indicated that water may need to be held in the Lower Water Management Pond (LWMP) during years with lower winter flows in the receiving environment to meet water quality guidelines. The results also indicated that water storage in the LWMP during years with higher mine dewatering flows is likely, even when winter flows are relatively high. All iterations predicted that the maximum volume of water held in the LWMP would be less than the design pond volume.

12.8.6 Closure

The closure objective for site water management will be to breach diversions around the mine site and return water courses to their natural directions of flow. The Class A Collection Pond will be pumped to the WTP until such time that water quality is suitable for passive release from the ponds.

12.8.7 Water Treatment

A water treatment plant (WTP) has been designed to meet the objectives relating to the discharge of excess water to the environment and the influent water streams consist of runoff from the Class A WSF, process water from the process plant, ROM pad runoff, process plant site runoff, and water generated from mine dewatering.

Water quality from each of these sources will be monitored to determine if treatment through the WTP is required.

The main contaminants identified from these sources are selenium, aluminium, arsenic, cadmium, copper, zinc and iron. The treatment system is designed to discharge into a staging pond prior to release to the receiving environment.

The proposed treatment system consists of a metals removal circuit and an additional process for selenium removal that involves an ion exchange circuit followed by an electroreduction circuit from which selenium is precipitated as a stable iron oxyhydroxide solid containing selenium for non-hazardous disposal.

In the first five years of the project, metals removal will be conducted by ferric and sulfide precipitation. In Year 6, before the Class A Water might potentially turn acidic, the WTP will be modified to include a high-density sludge (HDS) lime neutralisation system which will treat the Class A Water.

The system is designed to keep the different sources of water segregated across different treatment trains due to variable chemistry. This allows selective treatment to reduce costs and provide for a staged deployment of the treatment system.

12.8.8 By-Products

The by-products of the WTP will be:

- A highly stable cake consisting of iron-selenium precipitates generated in the selenium removal circuit and will be disposed of in the Class A WSF.

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- "Spent" electroreduction cell anodes that have been consumed to a size no longer efficient to use in the electrocell and will be either sold as scrap or disposed of in the Class A WSF.
- Thickened sludge from the metal's removal and HDS clarifiers. These will be pumped to the process plant and disposed of with filtered tailings from the process plant. Thickening within the WTP will be required after closure of the processing plant.

Labour requirements for the operation of the plant will be limited and shared maintenance and supervision from within the main processing plant operations is likely given the proximity and integration within the main control room.

12.9 Services

12.9.1 Power Generation

Several diesel-powered generators will be established during the pre-production period for the camp facilities including camp water and sewage system and the open pit mine activities including pumping, equipment maintenance, wash bay, mine workshop and heavy vehicle fuel facility.

Once operational, power for the mine will be generated at a power station where power will be generated at 13.8 kV by up to five 5.5 MW main generators with a 750-kW diesel generator for powering main generator auxiliaries during black start operation.

The generators will be dual fuel (natural gas and diesel) generators capable of running a range from 100% diesel to 99% natural gas/1% diesel.

The development of the power station will be staged with respect to installation of the main generators as the project scope widens to include underground operations. The camp facilities and systems will remain connected to a standalone local generator.

Remote equipment and systems such as pumps in water collection ponds and storage facilities will not be connected to the main power distribution system and will be powered from individual skid-mounted diesel generators.

12.9.2 Electrical Distribution

Power generators will connect to the 13.8 kV main switchgear assembly incorporated into the power station and will feed the processing plant infrastructure directly without the need for any intermediary transformers.

12.9.3 Fuels

Fuel supply and storage will include liquified natural gas (LNG) for the power station, and diesel fuel for standalone generators, mining equipment and the power station.

12.9.4 LNG Storage

The storage facility will comprise three 100 m^3 LNG tanks and each tank has the capacity to operate the power station for 16 hours at a peak load of 15 MW – two days capacity at peak load. An LNG vaporiser system is used to supply natural gas fuel to the generators at the required pressure and flow rate.

LNG will be sourced from a liquefication facility and transported to site using LNG trailers in a B-train configuration to minimise transportation costs.

12.9.5 Diesel Storage

The main diesel storage facility (four tanks of 100,000 L each) will be located adjacent to the mine workshop and maintenance area and has enough storage capacity for nine days of normal mining operations.

Two 113,500 L diesel fuel tanks will be installed at the power station – approximately three days operation. The tanks will be refilled by delivery tankers, or if needed, from the main diesel storage facility.

12.9.6 Other

It is intended to minimise the use of petrol-powered equipment at the site, but a 30,000 L storage facility is planned for fuelling miscellaneous road vehicles and small engines.

12.9.7 Heating, Ventilation and Air Conditioning

Heat Recovery

It was determined economic to include full heat recovery, including jacket water heat exchangers and exhaust gas heat recovery units in consideration of the long heating season and high fuel costs required to maintain operations. Any waste heat will be used by the heating, ventilation and air conditioning system (HVAC) to heat the processing plant building through a glycol loop.

It has been estimated that 12 MW of heat can be recovered from four fully operating generators, and this is suitable to meet the heating requirements for the building. However, during the first two years of operation, only three generators will be installed and operating with less available heat to transfer to the glycol. To counteract this, heat generation capacity will be supplemented with standalone natural gas fired boilers to the glycol heat distribution system.

12.10 Mining Infrastructure

12.10.1 Workshop Facilities

Mine workshop facilities will be constructed in stages for both the open pit and underground mining operations, approximately 1 km north of the open pit. Both the open pit and underground mine workshops will be a fabric-on-frame type structure anchored to sea containers, which will serve as additional working and storage areas for the workshop facilities.

The mine workshop area will have sufficient space available for site offices and parking for the mobile fleet. A vehicle wash bay will also be constructed adjacent to the mine workshop facilities and will be utilised by both the open pit and underground mining teams.

12.10.2 Explosives

Explosives will not be manufactured on site, and the explosives trucks will be capable of mixing blasting agents in varying ratios to meet the specific requirements of each blast such as the presence of wet holes and the need to vary explosive density.

Explosives will be stored in secure, fenced facilities adjacent to the overburden stockpile. Bulk explosives will be stored within a bulk explosives compound, and an explosive magazine will store all packaged explosive products required for the open pit and underground operations. Detonators are stored in a separate magazine within the facility.

Bulk ammonium nitrate prill and bulk ammonium nitrate emulsion will be transported to site in 25 t bulk transport trailers and 20 t tanker trailers respectively and stored in separate prill and emulsion silos within the bulk explosive compound. The bulk explosive compound will also contain a garage for the explosives loading trucks and a small office for the explosive's contractor. Packaged explosives and detonators will be delivered separately by approved explosives freight trucks.

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12.10.3 Communications

Phone Network

Site communications will be established via microwave link to connect directly into the existing terrestrial network. The nearest existing access point is the McEvoy Tower located approximately 36 km northeast of the Kudz Ze Kayah Project area.

The link from the McEvoy Tower will require one intermediate repeater approximately 3 km from the camp to relay the signal into the mine site and this location also provides two-way coverage along the Access Road as well as into the proposed mine site.

An antenna will be installed on the existing McEvoy Tower connected to a new 20 m tower with 0.6 m parabolic dish installed adjacent to the existing tower and equipment will be housed in a fabricated shelter that is skid-mounted to allow for easy transportation and positioning. An additional shelter has been included to house the diesel-powered direct current (DC) generator, battery bank and associated controls and monitoring if required.

At site, a 10 m tower was installed in 2024. The tower will be supported by a local communications shelter and will support a 0.6 m antenna. Neither of these latter features have yet been installed.

Radio Communications

An eight-channel site radio communication system will consist of base station radios with external antennae for office and other buildings as required, a remote site repeater for road coverage, and a site headend with interconnection to underground leaky feeder radio system (Year 3 onward).

A VHF leaky feeder system will be used in the underground mine to integrate with the surface communications and comprises a head end unit along with line amplifiers, DC power supplies, splitters, and a leaky feeder cable.

12.11 Roads

12.11.1 Access Roads

The Tote Road is approximately 24 km in length and extends from the Robert Campbell Highway, south to the Kudz Ze Kayah Project site (Figure 12-1).

The current Tote Road is not suitable for the vehicle traffic expected during the construction and production phases and an upgrade and realignment of the existing road is proposed to improve road user safety, increase the travel speed, and provide all-season access.

The road upgrade will be carried out in two phases where an initial upgrade completed during the early stages of construction to improve access for heavy construction traffic. This will include reducing existing gradients, improving visibility on bends, constructing pull outs and some culvert replacements, among other works. The balance of the upgrade work will be carried out during the early stages of the processing plant commissioning phase, when traffic movements along the road are expected to be light.

The designed upgrade is for an all-weather, single-lane road with sufficient pullouts to safely support two-way, radio-controlled traffic travelling at a speed limit of 50 km/h. The portion of the existing road between the camp and the open pit will be upgraded to allow larger two-way construction truck traffic.

Wherever possible, conventional cut to fill construction techniques will be implemented to minimise material movements.

The Tote Road crosses ten streams, nine of which are culverts with the tenth being an existing steel portable bridge at Finlayson Creek. All culverts require upgrading, eight of which will require complete replacement. The bridge over Finlayson Creek was upgraded in 2015 and no work is proposed for this crossing.

Access to the site is currently controlled with a gatehouse located on the Tote Road, immediately after turning off the Robert Campbell Highway. This facility will be maintained throughout construction, operations and closure activities.

12.11.2 Site Road Network

Approximately 25 km of roads will be constructed around the site to facilitate pre-production and production activities (Figure 12-2). The portion of the Tote Road that extends south of the camp will be upgraded to allow larger two-way construction vehicle traffic and will serve as access to construct the Tote Road Diversion Channel that initially diverts non-contact water from Geona Valley to begin dewatering in the project area. The upper diversion road will access the Fault Creek Diversion Channel and later it will serve as access to construct the Upper Diversion Channel.

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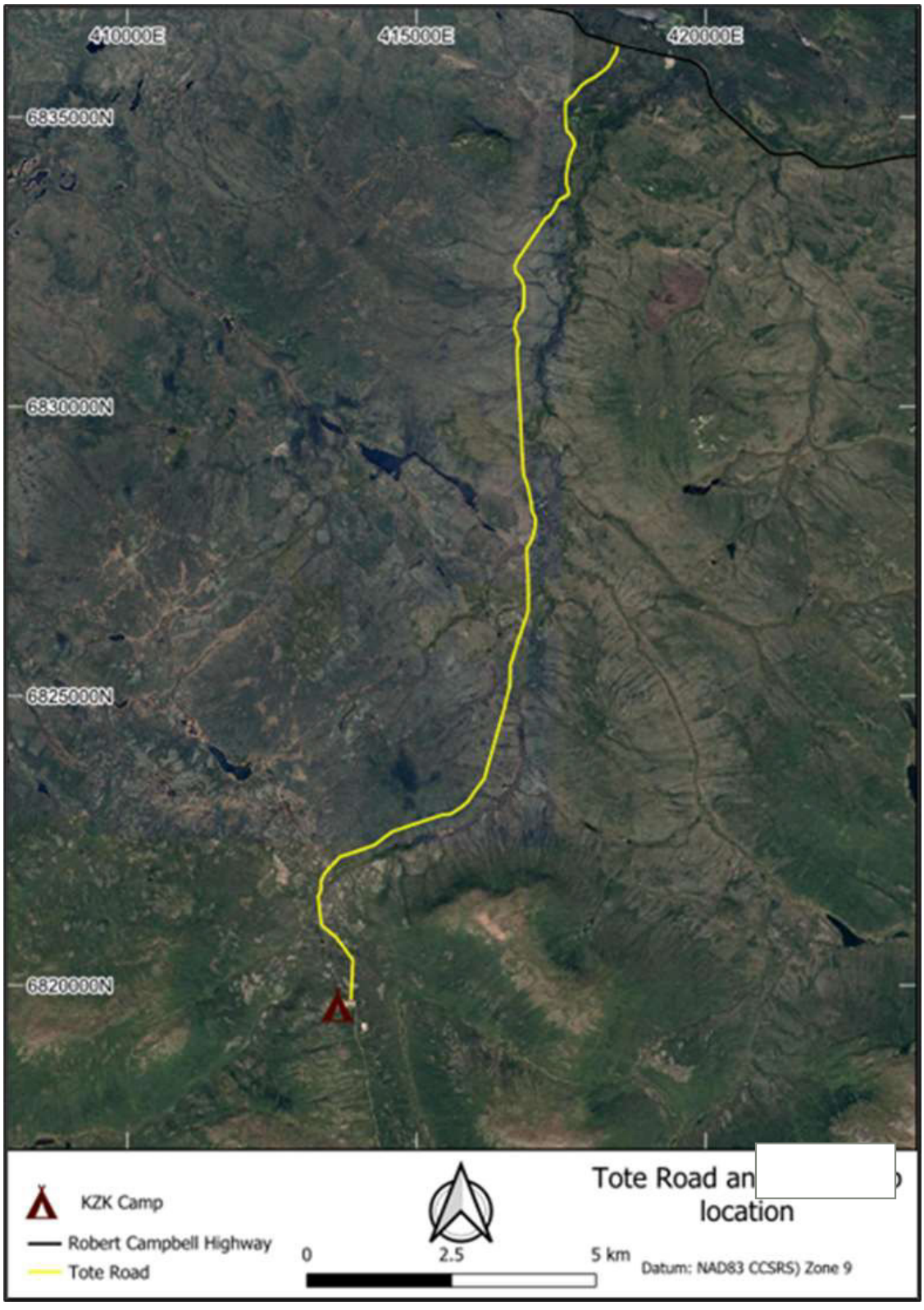


Figure 12-1: Tote Road
Source: BMC

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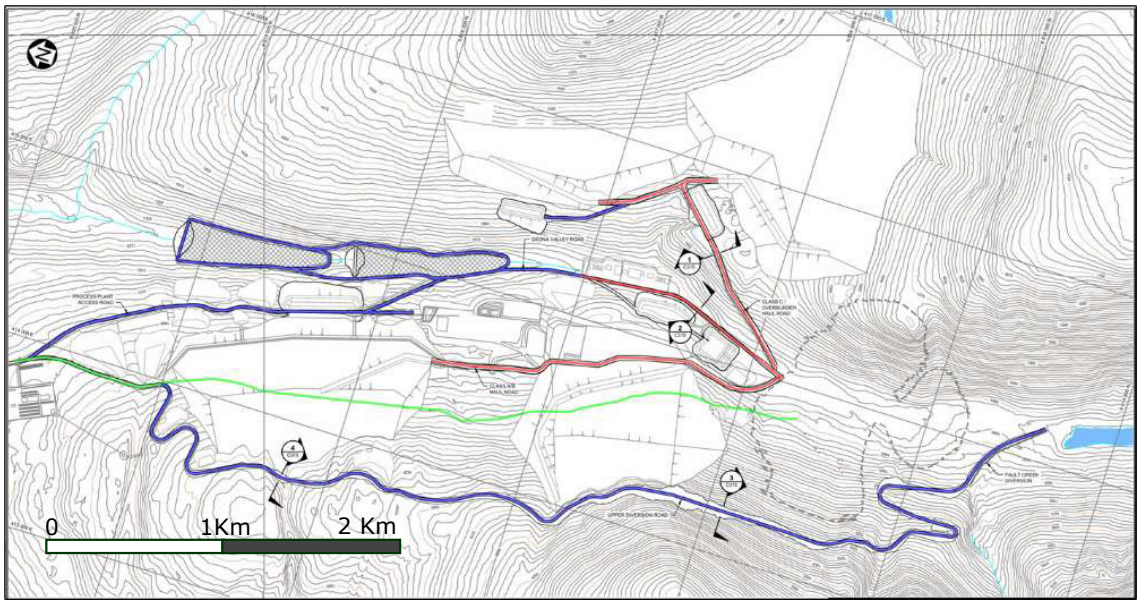


Figure 12-2: Proposed site road network; Green indicates road upgrade, blue indicates new light vehicle road, red indicates mine haul road.

Source: BMC

The Mill Access Road will commence from an intersection adjacent to the camp and extend through to the main process plant pad. This road will carry all heavy construction traffic and later serve as the first stage of the concentrate haul route. The Mill Access Road leads to the Geona Valley Road via a link road.

The Geona Valley Road will be constructed below the processing plant site and traverses the valley floor, providing access to the upper and lower water management ponds, the mine workshops, Class B Collection Pond and Pit Rim Pond. The road terminates at the open pit entrance and will be constructed to mine haul road specifications for use by the open pit and underground mining fleet to access the workshops and fuel storage areas.

Several mine haul roads will be constructed during pre-production activities for the 140 t mine dump trucks to access the main WSF and ROM pad. These roads will also provide access via a ramp from the filter building for tails haulage to the Class A WSF and for the agitator trucks to haul paste backfill to the discharge hopper in the pit during underground mining operations.

12.12 Accommodation

A permanent accommodation camp will be constructed adjacent to the existing exploration camp complete with dormitories, kitchen, mess hall, and recreation facilities for the work force during construction, and this will be partially retained for operations personnel.

Ninety-eight rooms of the permanent camp are installed on site with 60 of these fully integrated into the site services. The remaining rooms will be integrated into the camp services during 2025 and 2026 on an as-needed basis. The camp will ultimately be expanded to 348 dormitory rooms, including temporary double-bunks to cater for the peak construction phase, and that will be expanded to 348 dormitory rooms (including temporary double-bunks) to cater for the peak construction phase.

The camp size has been determined from the resourcing schedules and has been based on a motel system for room allocation, and a heated building is planned with lockers for the storage of personal effects and safety gear between rotations.

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The camp dormitory buildings are supplied as modular units interconnected by enclosed arctic breezeways. Onboard services are supplied with the modules, including lighting, wiring, HVAC, plumbing, and fire detection/suppression. The common modules for kitchen, mess hall, recreation, and laundry are similarly supplied and fit for purpose.

Services for the accommodation complex include local power generation (complete with emergency backup), fuel storage for five days, potable and fire water, and a sewerage treatment plant and disposal field. The camp communications system will be integrated into the nearby site microwave network.

Catering services will be outsourced to a catering contractor and the catering staff will be housed within the accommodation facility on the same basis as the main workforce.

12.13 Airstrip

The Finlayson airstrip is the closest public airstrip to the project and is located approximately 40 km from the site and is currently used for servicing the current exploration and environmental monitoring programmes.

It is a 563 m gravel strip that is capable of being serviced by aircraft of up to a 14-seat capacity and is currently identified as the primary airstrip for all phases of the project. Specific contingency plans are required due to the inherent weather variability that can affect flight conditions in Yukon throughout the year and alternative airstrips at Faro and Watson Lake are essential to flight operation planning.

An average of eight flights per week will be required to service personnel roster requirements during operations and up to 12 flights per week could be required to service construction requirements.

During the construction phase, it may prove more efficient to utilise larger aircraft and fly to either the Faro or Watson Lake airstrips and this option is not expected to materially impact the cost or timing of construction.

12.14 Concentrate Haulage

Zinc and HPM concentrates will be hauled to the Port of Stewart along a 905 km southerly route utilising a combination of gravel and sealed secondary highways and paved primary highways. Provision has been made for transportation of copper concentrate to a potential rail head, for subsequent loading and transportation on the Canadian rail network to domestic customers, if required (Figure 12-3).

Copper Concentrates

The transportation haul will be executed based on a non-restricted operation with up to 100% legal axle loading for most of the year (312 days). A portion of the highway system in Yukon (Highway 4 Robert Campbell) is subject to seasonal payload restrictions of 75% of legal axle loading during the spring break-up period and during this period (approximately 45 days), transportation of concentrate will be executed as a restricted operation.

Seven axle tractor/trailer units will be utilised to haul single sealed containers from the mine site to Watson Lake during Highway 4 restricted operations. There, a 30-t forklift will transfer sealed containers onto the nine axle Super B units for road transport on the road network that is not subject to seasonal payload restrictions.

Copper concentrate may be sold into the North American market. To account for this, provision has been made for transportation of copper concentrate to a potential rail head, for subsequent loading and transportation on the Canadian rail network to domestic customers, if required.

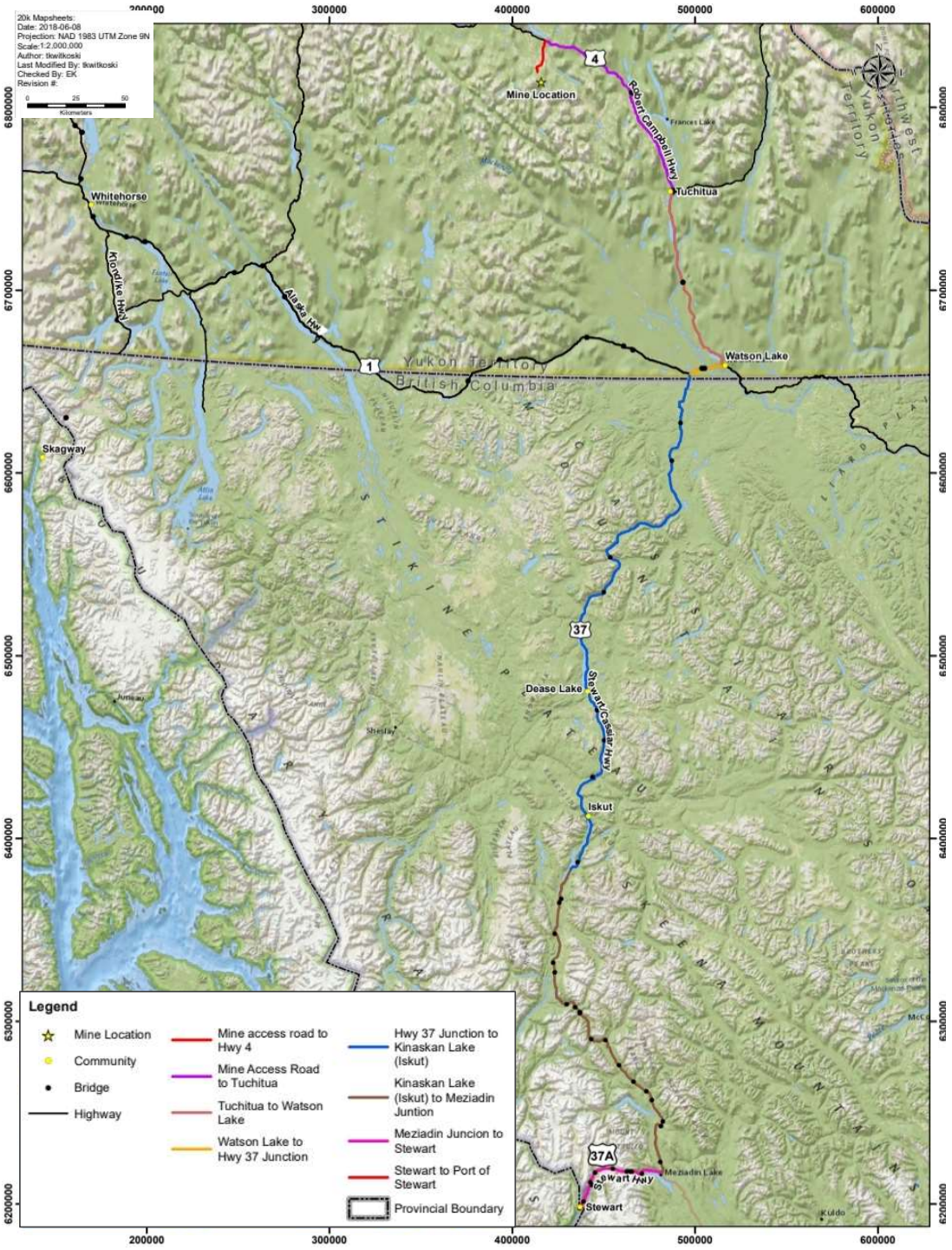


Figure 12-3: Haul route from Site to the port of Stewart.
Source: BMC

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Zinc Concentrates

Non-Restricted operations will transport zinc concentrate in covered bulk boxes and during Restricted operations, zinc concentrate products will be transported with modified containers capable of side dumping.

The product will be stored within a separate covered, open bulk pile, within the concentrate storage facility until it is ready to be loaded onto a ship.

HPM Concentrates

HPM concentrate will be transported and stored in sealed containers at the port. When a ship arrives to transport the HPM concentrate, the containers will be trucked to the berth alongside the ship then emptied directly into the ship's hold.

Containerised storage capacity at Stewart will provide up to 60 days plus an additional 14 surge days of haul production for a total of 9,176 wet tonnes.

12.15 Stewart World Port

The preferred port facility for export of the zinc and HPM concentrates is the SWP at the Port of Stewart on the northwest coast of Canada, at the head of the Portland Waterway about 80 nautical miles from the open sea.

The SWP currently comprises of a concrete deck and steel pile jetty with one berth suitable for Handysize and Handymax class vessels. The berth has also been designed for Panamax vessels, subject to the installation of a mooring buoy.

The SWP includes good access from the project for trucks via existing highways, winter access for shipping, and little competing demand for port access. Issues identified with SWP include the distance to the nearest pilot and tug facilities (115 nautical miles to Prince Rupert), restriction of berthing operations to daylight hours and likely loading delays from a high average rainfall precipitation.

Concentrates from the mine will be stored at a purpose-built storage facility where zinc concentrates will be bulk stored until a ship arrives prior to being conveyor fed to a ship loader for vessel loading. HPM concentrate will be transported from site to SWP via dual carriage sealed purpose-built half height containers that will be stored in an outdoor hardstand area until vessel loading via a container rotating system and the ship's crane.

Zinc concentrate operations are anticipated to be undertaken using a 2,500 t/h ship loader yielding a maximum loading rate of 50,000 t/day. The loading rate for HPM concentrate will be slower and is estimated to be up to 3,700 t/day.

12.16 Rail Head

Copper concentrate may be sold into the North American market and to account for this potential, provision has been made for transportation of copper concentrate to a rail head. Copper concentrates from the mine will be stored in a purpose-built storage facility for bulk storage. Concentrate will subsequently be loaded into covered gondola rail cars by front-end loader (FEL), with locomotives available on a 7-to-14-day basis for transportation of loaded cars.

12.17 Security

Access to site is currently controlled with a gatehouse located on the Tote Road entrance, immediately after turning off the Robert Campbell Highway. All vehicles entering the project area are required to

stop before continuing into the property. This gatehouse will be maintained during construction and operations as an initial security point for access to site.

A second gatehouse will be established on the Access Road prior to arriving at the accommodation facility and will function as the key access to the operating site. A register of all vehicles and personnel visiting the site will be maintained to ensure that accurate data is available in the event of an emergency.

Security fencing and gate access will be constructed around the explosives facilities to limit access to authorised personnel only. The incinerator, landfill facility and all ponds will also be stock fenced to prevent access by wildlife.

12.18 ERM Opinion

ERM is of the opinion that the work completed for the supporting infrastructure required for a remote mine project development has been well considered and appropriately costed.

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13. PROJECT ECONOMICS

Detailed Feasibility-level studies were first completed on the Kudz Ze Kayah Project in 2019 and demonstrated a robust positive financial outcome. An updated economic assessment of the project was completed in November 2020 – and was solely a cost and revenue update to the Project, with engineering designs, and schedules remaining unchanged from that of the 2019 Feasibility Study.

In October 2023, a full economic update was completed to reflect a June 2023 quarter cost base to the past studies. This update of the Project economics was completed as the Project continued to advance through the regulatory phase of the licensing process and the Company commences preparations for financing the project development.

On 3rd April 2025, the Company published its latest NI 43-101 Technical Report on SEDAR with the effective date of 3rd January 2025.

The Ore Reserve estimate (2023) were used as the basis for the project economics reported in the 2025 Technical Report.

Physical aspects of the Project and supporting engineering work remained largely unchanged from that detailed in previous iterations of Feasibility Study work since the designs were to the requisite level of detail and confidence. Changes introduced predominantly resulted from the concentrate offtake agreements that BMC has executed with various offtake customers since 2021.

All capital and operating costs were reviewed and updated by the consultants that contributed to the Feasibility Study-level investigations and the Company reviewed and updated all other cost elements. Updates were achieved through a combination of updated quotations for equipment and consumables, consultant in-house cost databases, and escalation of the previous cost estimate to bring to a June 2023 quarter cost base.

All revenues and costs presented below are in United States dollars (USD, US$) and in real dollar terms unless otherwise noted.

13.1 Feasibility Studies

Feasibility Study-level investigations to assess the economic viability of mining and processing the ABM Deposit have been completed and updated several times by BMC.

Commencing June 2019, the Company presented its first Feasibility Study for the ABM Mine (CSA Global 2019a). This Technical Report disclosed material changes to the Property including the results of recent exploration activities, an updated Ore Reserve estimate for the ABM Deposit, and results of the Kudz Ze Kayah Project Feasibility Study.

In November 2020, the Feasibility Study was updated following a review (CSA Global, 2020) to ensure that all assumptions underpinning the Mineral Resource estimate and Ore Reserve estimate remained current to the technical and economic assumptions (costs and revenue) that formed the basis of the project's viability.

Following the Covid-19 pandemic and after several years of high worldwide inflation, a comprehensive review and update of the Kudz Ze Kayah Project economics was completed in October 2023 (BMC 2023) to reflect a June 2023 quarter cost base as the Kudz Ze Kayah Project continued to advance through the regulatory phase of the licensing process.

Key consultants that contributed to iterations of the Feasibility Study were again re-engaged to review their respective areas of the project and update the delivery timing and costs, including obtaining quotes for supply and delivery of major equipment from third party suppliers.

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While there were increases in both capital and operating costs, the economic outcome forecast by the 2023 review demonstrated that the project remains financially robust. Therefore, the ORE (2019) was unchanged from that of the 2020 NI43-101 Technical Report. Other physical aspects of the Kudz Ze Kayah Project and supporting engineering work remain largely unchanged.

The most recent iteration of the Feasibility Study-level investigations, with key inputs having been reviewed and updated as required, is summarised in a Technical Report completed in accordance with NI 43-101 requirements with an Effective Date of 3rd January 2025 that was lodged on SEDAR on 3rd April 2025 (ERM, 2025b).

Important areas updated in the review included:

- Updated offtake agreements.
- Minor modification to the zinc concentrate thickening circuit has been adopted to allow for the optional flexibility of production of two different qualities of zinc concentrate (pre-float and recleaner concentrates) if the market provides the opportunity and if the Company so desires.
- Provision for delivery of copper concentrate to a potential rail head, for transport to domestic customers if required.
- Corresponding "right sizing" of the size of the bulk concentrate storage shed at SWP to reflect scheduling and shipping expectations through that facility.
- The open pit mining cost "contractor" model was replaced by an "owner operator" model prepared in-house and using manufacturer supplied operating and maintenance costs. The underground mine is assumed to remain under a contract mining model.
- Costs associated with the PMPA,
- Canada's *Greenhouse Gas Pollution Pricing Act* (Canada Carbon Tax),
- Costs associated with the 2022 Decision Document conditions, and
- Updating consensus metal prices and foreign exchange rates.

The 2025 Technical Report demonstrates that the ABM Mine Project is commercially viable given the Base Case economic results.

ERM notes that the Feasibility Study-level investigations, Mineral Resource Estimates and Mineral (Ore) Reserve Estimate in this Technical Report were completed in accordance with (Canadian Institute of Mining, Metallurgy and Petroleum) CIM Definition Standards for Mineral Resources and Mineral Reserves (CIM 2014). These Mineral Resources, Mineral (Ore) Reserves, and mining study definitions are incorporated, by reference, into National Instrument 43-101 – *Standards of Disclosure for Mineral Projects* (NI 43-101). As a CRIRSCO family code, these definitions are equivalent to the JORC Code definitions.

The Mineral Resources and Mineral (Ore) Reserves were generated in conformity with generally accepted CIM "Estimation of Mineral Resource and Mineral Reserves Best Practice Guidelines" (CIM Council, 2003) and CIM "Definition Standards for Mineral Resources and Mineral Reserves" (CIM Council, 2014).

ERM notes that the operating and capital cost estimates reported in the Technical Report are considered accurate to within the normal limits expected for a Feasibility Study as defined in the CIM Standards, and the costs (real terms) remain valid. The inputs and assumptions of the Feasibility Study-level investigations reported in this Report (and the reports informing it) remain applicable and appropriate for the disclosed information.

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13.2 Project Capital Work Packages

An estimated US$492 million will be required in pre-production capital to bring the mine into production, while an additional US$200 million of sustaining capital will be required during operations and closure (Table 13-1).

The capital cost estimate is considered accurate to within the normal limits expected for a feasibility study; and the costs (real terms) remain valid. The inputs and assumptions of the Feasibility Study-level investigations reported in this Report (and the reports informing it) remain applicable and appropriate for the disclosed information.

All costs are in United States dollars unless otherwise noted.

Table 13-1: LOM Capital Cost Summary

Capital Cost Area	Pre-production (US$M)	Sustaining (US$M)	Total (US$M)
Process plant	190	13	202
Open pit mine development and infrastructure	51	5	56
Underground mine	0	72	72
Non-process infrastructure	30	10	40
Waste storage facilities	20	35	55
Water storage and management facilities	17	11	28
Water treatment plant	21	4	25
Port and rail facilities	17	0	17
Other infrastructure	7	5	12
Subtotal Direct Costs	351	155	506
Closure	0	45	45
Total Direct Costs	351	200	552
Owners' costs	18	Included	18
Indirect costs	67		67
Contingency	55		55
Total Capital Cost	**492**	**200**	**692**

Source: 2025 Technical Report

Notes:

- Costs are rounded to nearest $1M. Totals may not sum precisely.
- Costs exclude amounts for equipment assumed leased. Refer to Section 13.3.6 for more information.
- 100% equity financing assumed.
- Excludes project finance interest, offtake agreement financing, reclamation bonding and other financing arrangements and costs, working capital, exchange rate fluctuations and all licence fees.
- Mining of open pit waste is treated as an operating expense, except for pre-production mining activity which is capitalised as a pre-production expense.

13.2.1 Processing Plant

The capital cost estimate for the processing plant (Table 13-2) summarises the new direct capital costs and contingency provisions for the construction of the Process Plant facilities and is based on the supply and installation of new equipment. It was developed by updating estimates for major process equipment and infrastructure costs and delivery times with updated prices for supply and delivery from feasibility study vendors, or from new or alternative vendors. Canadian price indices were used to escalate many direct and indirect estimates such as concrete, steelwork, platework, piping, electrical, steel fabrication, or labour that were not re-validated so as to update them to current for the June 2023 quarter.

Major equipment and infrastructure items were re-validated with updated budget pricing and freight allowances. Updated supply and delivery times were compared to those used in the 2020 Re-stated Feasibility Study and the timing for supply and delivery of concentrate filters and the process plant building resulted in an increase being required in the project construction schedule.

The revised timing was included in a new EPCM schedule with the main alteration including an earlier start to works by two months compared to that planned in the 2020 Re-stated Feasibility Study.

Table 13-2: Process Plant Capital Costs

Description	Pre-production Cost (US$M)	Contingency (%)
Earthworks and drainage	10.9	13.9
Crushing and reclaim	14.4	13.2
Grinding and classification	20.0	12.2
Flotation and regrind	34.5	12.4
Concentrate handling and storage	19.4	13.2
Tailings management	19.8	12.6
Reagents	9.2	13.1
Process plant utilities	18.3	13.9
Plant building	43.0	13.9
Process Plant Direct Costs	**189.5**	**13.1**

Source: 2025 Technical Report

13.2.2 Open Pit Mining

The Company elected to develop an owner operator mining cost estimate for open pit mining for the 2023 Economic Update rather than using the mining contractor approach adopted for the 2020 Re-stated Feasibility Study.

Open pit mine development and infrastructure costs include pre-production mining costs for the establishment of open pit mining operations, production of waste rock for construction of site infrastructure and production of an initial ore stockpile (Table 13-3).

Open pit mine development costs are the capitalised operating costs of the initial mine development and allow for mobilisation, drill, blast, load and haul of waste material either to surface infrastructure sites or designated WSF and stockpiles, as well as production of an initial ore stockpile to commence production.

Table 13-3: Open Pit Mine Development and Infrastructure Costs

Description	Pre-production Cost (US$M)	Contingency (%)
Open pit dewatering	4.7	22.2
Mine infrastructure	6.5	25.0
Open pit mine development	40.1	-
Total Open Pit Mining Capital Costs	**51.3**	**5.2**

Source: 2025 Technical Report

13.2.3 Underground Mining

Underground mine development and associated infrastructure capital costs are considered to be sustaining capital given that they are incurred in the third year after production commences.

Ony a portion of the mine development costs will be capitalised and include the main decline, return air access, escapeway access, footwall access drives, stockpile bays and drainage sumps.

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13.2.4 Non-Process Infrastructure

The estimated non-process infrastructure costs are shown in Table 13-4. Site administration costs include construction and fit out of site office complexes, the laboratory building and equipping the processing plant workshop, warehouse, first aid facilities, the supply and installation of computers, software, site telephone system and survey equipment.

The camp cost includes all costs associated with development of the final camp and is based on an estimate prepared in 2022.

Major capital equipment for power generation and the LNG fuel facility will be financed on an operating lease basis and initial power for commissioning and production provided through a rental diesel powerhouse.

Services and utilities costs cover the buried services required, lighting infrastructure and the site waste management facility.

Table 13-4: Non-Process Infrastructure Capital Costs

Description	Pre-production Cost (US$M)	Contingency (%)
Site administration	7.4	14.6
Camp	8.0	13.9
Process plant roads	1.7	13.9
Power generation and transmission	8.0	13.9
Fuel storage and distribution	0.0	N/A
Communications	0.8	13.9
Services and utilities	2.8	13.9
Miscellaneous	0.9	10.0
Total Non-Process Infrastructure Costs	**29.6**	**13.9**

Source: BMC

Waste Storage Facilities

The estimated costs cover the initial development of all surface waste storage facilities (WSF) and includes construction of the first stage of the facilities and involves preparation of the basins, including lining and drainage where applicable, construction of the Class A buttress, stockpiling of associated topsoil and other spoil, and the engineering work required to prepare detailed designs for construction (Table 13-5).

The construction of the Class C WSF from the 2020 Re-stated Feasibility Study remains deferred until the commencement of operations as all Class C rock generated by pre-production mining activities will be used for the construction of the various surface infrastructure components of the operation.

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Table 13-5: WSF Capital Costs

Description	Pre-production Cost (US$M)	Contingency (%)
Class A waste storage facilities	9.4	20.0
Class B waste storage facilities	9.0	16.5
Class C waste storage facilities	-	-
Overburden stockpile	0.2	20.0
Topsoil stockpile	0.1	30.0
Miscellaneous	0.1	10.0
Subtotal Site Costs	18.9	18.3
Engineering	1.3	10.0
Total Waste Storage Facilities Costs	**20.2**	**17.7**

Source: BMC

Water Storage and Water Management Facilities

The estimated costs cover the development of all surface water storage facilities and allow for earthworks and associated lining of the facilities, as well as installation of the pumps and pipework required to complete and integrated system (Table 13-6).

Water Treatment Plant

An expansion of the water treatment plant to include the high-density lime neutralisation system for Class A WSF water has been included in the sustaining capital costs (Table 13-7).

13.2.5 Concentrate Transport including Port and Rail Facilities

The 2023 cost update has allowed for the additional costs of creating optionality for potential delivery of copper concentrate to a rail head for transport to domestic customers if required.

In conjunction with this, the size of the bulk concentrate storage shed at Stewart World Port has been "right sized" to reflect scheduling and shipping expectations through that facility to a capacity of 17,500 dmt of concentrate. The estimated cost for the port facility is US$10.4 million, with a 10% contingency allowance.

The Company prepared a cost estimate for construction of a rail loadout facility of US$6.3 million.

Table 13-6: Water Storage and Water Management Capital Costs

Description	Pre-production Cost (US$M)	Contingency (%)
Lower water management pond	5.2	23.0
Upper water management pond	-	-
Class A storage facility collection pond	1.9	21.8
Class B storage facility collection pond	0.8	19.6
Class C storage facility collection pond	1.2	25.2
Overburden stockpile collection pond	0.5	21.0
Pit rim pond	1.1	22.5
Collection and diversion ditches	2.1	18.0
Mechanical systems and pipelines	1.4	18.5
Finlayson creek discharge pipeline	-	-
Miscellaneous	1.2	6.8
Subtotal Site Costs	15.4	20.4
Engineering	1.3	10.0
Total Water Storage and Management Facilities	**16.7**	**19.6**

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Description	Pre-production Cost (US$M)	Contingency (%)
Costs		

Source: BMC

Table 13-7: Water Treatment Plant Capital Costs

Description	Pre-production Cost (US$M)	Contingency (%)
Modularisation	5.2	25.0
Metals removal circuit	1.9	25.0
Selenium removal circuit	3.9	25.0
Reagents and utilities	1.7	25.0
Freight	0.5	25.0
Infrastructure	4.9	25.0
Subtotal Direct Costs	18.2	25.0
EPCM	1.3	25.0
Other indirects	1.0	25.0
Commissioning	0.4	25.0
Total WTP Capital Costs	**20.9**	**25.0**

Source: BMC

13.2.6 Other Infrastructure

Costs to construct roads to the Class A, B and C WSF and overburden stockpile are covered under Mine Roads, while all other site roads are covered under Site Roads (Table 13-8).

Table 13-8: Other Infrastructure Capital Costs

Description	Pre-production Cost (US$M)	Contingency (%)
Access road	2.5	10.0
Mine roads	0.4	20.1
Site roads	1.8	20.0
Fish offset measures	1.8	10.0
Total Other Infrastructure Capital Costs	**6.5**	**13.4**

Source: BMC

13.2.7 Owners Costs

Owner's costs include an estimate of spares and inventory costs based on a percentage of direct costs for major and minor capitalised spares and the methodology remains unchanged to that of the 2020 Re-stated Feasibility Study (Table 13-9).

First fills costs were based on 2023 reagent and consumables costs.

Owner's team staffing for construction has been included but management, mining and geology staff for the commencement of pre-production mining activity has been included separately in open pit mining costs for capitalisation purposes. Processing plant operators will be employed two months prior to commissioning for training and plant familiarisation.

The number of personnel in the owner's team has been increased from that detailed in the 2020 Re-stated Feasibility Study and the key changes involve an increase in environmental staff, increases in

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gatehouse security, and an increased establishment for site nurse and OHE & ES officers to improve site coverage under a changed roster arrangement.

Labour costs for the 2023 Economic Update have been benchmarked to current labour costs at comparable northern mining operations.

Table 13-9: Owner's Costs

Description	Pre-production Cost (US$M)	Contingency (%)
Spares and inventory	8.6	13.8
Owner's team	5.8	13.9
Training of process operators	0.7	13.9
Environmental monitoring	2.8	10.0
Total Owner's Costs	**17.8**	**13.2**

Source: BMC

13.2.8 Indirect Costs

Lead times for certain major equipment items have increased from that of the 2020 Re-stated Feasibility Study. The revised equipment lead times, together with the float in the 2020 Re-stated Feasibility Study project construction schedule were reviewed to assess the impact on the required commencement of engineering activities to allow equipment to be ordered, manufactured and delivered to site within the scheduled time frames.

As mentioned earlier, the updated schedule requires engineering works to commence two months earlier than estimated in the 2020 Re-stated Feasibility Study. This has resulted in the timing of the first five months of costs being brought forward to match the changes in activity (Table 13-10).

Table 13-10: Indirect Costs

Description	Pre-production Cost (US$M)	Contingency (%)
EPCM	31.8	2.4
Temporary facilities / site establishment	23.8	13.9
Temporary services and support	1.4	7.4
Construction camp and catering services	6.0	13.9
Winter construction costs	3.3	13.9
Commissioning	1.0	9.2
Total Indirect Costs	**67.3**	**8.2**

Source: BMC

13.2.9 Contingency

Contingency was determined for each major sub-package of work and has considered the quality or source of the underlying quantity and cost data to calculate an estimated cost to cover the uncertainty and variability associated with the estimate (Table 13-11).

The overall contingency provision for the pre-production capital is 12.5%. The underground mine comprises part of the sustaining capital cost and is inherent in the sustaining capital costs and is not reported separately.

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Table 13-11: Pre-production Capital Contingency Provision

Description	Pre-production Contingency Provision (US$M)	Contingency (%)
Open pit mine	2.7	5.2
Process plant	24.8	13.1
Non-process infrastructure	4.1	13.9
Waste storage facilities	3.6	17.7
Water management facilities	3.3	19.6
Water treatment plant	5.2	25.0
Port and rail facilities	2.3	13.8
Other infrastructure	0.9	13.4
Owner's costs	2.4	13.2
Indirect costs	5.6	8.2
Total Contingency	**54.8**	**12.5**

Source: BMC

13.2.10 Working Capital

Working capital is based on 60 days accounts receivable plus inventory minus 30 days accounts payable and accounts receivable is based on 10% of two months of MAMA (month after month of arrival). Both these assumptions are consistent with that of the 2020 Re-stated Feasibility Study.

13.2.11 Sustaining Capital

Contingency has been included in sustaining capital cost estimates and is not reported separately (Table 13-12).

Replacement of mobile equipment at the end of serviceable life is included in sustaining capital cost estimates.

Table 13-12: Sustaining Capital Costs (US$M)

Cost Area	Total	Y1	Y2	Y3	Y4	Y5	Y6	Y7	Y8
Waste storage facilities	34.8	15.0	-	11.0	-	4.7	-	4.1	-
Surface water management	10.9	8.9	-	1.0	-	0.4	-	0.4	-
Pit dewatering infrastructure	4.0	2.7	1.2	-	-	-	-	-	-
Site roads	3.8	0.1	-	3.8	-	-	-	-	-
ROM surface preparation	1.5	0.8	0.8	-	-	-	-	-	-
Vehicle replacement	0.9	-	-	-	0.6	0.3	-	-	-
Subtotal; open pit	55.9	27.4	2.0	15.8	0.7	5.4	0.1	4.6	-
Mining capital development	69.1	-	-	11.4	29.4	22.2	6.1	-	-
Paste fill plant	9.5	-	-	-	5.2	4.3	-	-	-
Mine infrastructure	3.0	-	-	0.7	0.5	1.5	0.2	-	0.2
Power generation and transmission	8.8	-	0.3	8.5	-	-	-	-	-
Subtotal; underground	90.5	-	0.3	20.7	35.1	28.0	6.3	-	0.2
Mobile equipment replacement	3.1	-	-	-	-	3.0	0.1	-	-
WTP HDS circuit	3.7	-	-	-	-	3.7	-	-	-
Subtotal; processing	6.8	-	-	-	-	6.7	0.1	-	-
Mobile equipment replacement	1.3	-	-	-	0.4	0.7	0.2	-	-

Cost Area	Total	Y1	Y2	Y3	Y4	Y5	Y6	Y7	Y8
Miscellaneous	0.3	0.3	-	-	-	-	-	-	-
Subtotal; Administration	1.6	0.3	-	-	0.4	0.7	0.2	-	-
Total, Sustaining Capital Costs	**154.9**	**27.7**	**2.3**	**36.5**	**36.1**	**40.8**	**6.6**	**4.6**	**0.2**

Source: BMC

13.2.12 Closure

Approach

Costs incurred beyond the last period of the economic model (≈10 years) were discounted at a rate of 7% per annum to a net present cost at the end of the financial modelling given the duration of the passive closure phase. This is consistent with the approach taken for the 2020 Re-stated Feasibility Study.

Regulatory Reviews

The closure cost estimate used for the 2020 Re-stated Feasibility Study was updated in 2022 during preparation of the Reclamation and Closure Plan that was submitted to Yukon Government Department of Energy, Mines and Resources as part of the Kudz Ze Kayah Project Quartz Mining Licence application (BMC, 2024).

That submission includes adjustments to costs that arose from the Yukon Water Board's adequacy review of the Reclamation and Closure Plan (included in the Kudz Ze Kayah Project's Type A Water Licence application), and the Company included an escalation of 3.5% to bring to a June 2023 quarter cost basis.

Water Treatment

Active treatment costs were included for the Active and Transition Closure phases and include both the operational treatment costs and a sustaining capital replacement cost. Passive treatment is included in the form of a capital cost for the construction of the Constructed Wetlands Treatment System (CWTS) and maintenance of the CWTS into Post closure.

25 Years of Closure

The annual costs for closure care, maintenance, and monitoring costs were estimated, and applied for 25 years of closure. In addition, the instrumentation, vegetation maintenance, erosion maintenance, and transportation costs were included for completeness.

Bonds

Bonding costs are considered a corporate cost rather than a project cost and are not included in the capital cost estimate in Table 13-1.

However, for the purposes of assessing financial provisions for bonding based on Yukon Government guidelines, interim care, maintenance and monitoring costs have been included to consider the scenario of temporary mine closure. The cost has been estimated inclusive of indirect and contingency cost provisions.

Indirect and Contingency Costs

It has been assumed that the open pit mining fleet, processing plant and other non-process infrastructure will be salvaged and sold, with an estimate of salvage value (US$55 million) being realised during the first year of closure.

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Table 13-13: Closure Costs

Description	Closure Cost (US$M)
Closure Implementation	
G&A, Closure planning	1.7
Open pit	1.2
Waste rock and tailings storage facilities	18.2
Surface facilities	2.9
Water and solutions management	2.1
Other	1.1
Indirects	5.4
Subtotal Closure Implementation	32.7
Post closure costs (undiscounted)	8.0
Contingency	6.1
Total Closure Costs (undiscounted)	46.8
Total Closure Costs (final years discounted)	**45.4**

Source: BMC

13.3 Operating Costs

All operating costs prepared for the 2020 Re-stated Feasibility Study have been reviewed and updated and the new estimate is considered accurate to within the normal limits expected for a feasibility study. The estimated operating costs over the life of the Kudz Ze Kayah Project are expected to be approximately US$2,679 million (Table 13-14).

Over the LOM, unit operating costs are expected to average US$170/t of ore processed, with operating costs ranging between approximately US$144/t and US$195/t.

Table 13-14: LOM Annual Operating Cost Summary (US$M)

Cost	Total	Y1	Y2	Y3	Y4	Y5	Y6	Y7	Y8	Y9	Y10
Open Pit Mining	528	59	112	108	100	48	43	35	23	0	0
Underground Mining	157	0	0	0	0	35	52	42	28	0	0
Processing	318	29	41	39	45	42	43	43	35	0	0
Water Treatment	20	2	2	2	2	2	3	3	3	0	0
Administration	175	31	22	22	21	21	20	20	19	-1	0
Road Transport	305	30	42	43	41	43	41	39	27	0	0
Sea/ Rail Transport	176	15	24	25	26	25	23	22	16	0	0
Sea/ Rail Loading	44	4	6	6	6	6	6	6	4	0	0
Equipment Leases	72	3	9	9	13	13	12	10	4	0	0
First Nations	37	4	4	4	4	4	4	4	4	4	3
Royalties	218	0	29	28	28	27	27	24	37	18	0
TC/RC and Penalties	516	49	74	73	65	74	68	68	46	0	0
PMPA	112	12	17	15	14	17	14	13	10	0	0
Total	**2,679**	**239**	**380**	**375**	**363**	**355**	**356**	**329**	**255**	**21**	**3**

Notes: Total costs include $0.4 million of lease payments and $2.4 million payments to First Nations during the preproduction phase.
Source: BMC

The operating cost estimate is considered accurate to within the normal limits expected for a Feasibility Study; and the costs (real terms) from the June 2023 quarter as reported in the 2025 Technical Report remain valid. The inputs and assumptions of the Feasibility Study-level investigations reported in this Report (and the reports informing it) remain applicable and appropriate for the disclosed information.

All costs are in United States dollars unless otherwise noted.

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Table 13-15: LOM Unit Operating Costs (US$/t ore processed)

Cost	LOM	Y1	Y2	Y3	Y4	Y5	Y6	Y7	Y8
Open Pit Mining	33.60	35.80	55.43	56.44	45.26	22.91	20.62	15.98	14.91
Underground Mining	10.00	0.00	0.00	0.00	0.00	16.86	24.88	19.03	18.11
Processing	20.21	17.57	20.27	20.50	20.28	20.23	20.64	19.80	22.45
Water Treatment	1.27	0.96	1.08	1.17	0.99	1.05	1.52	1.46	2.07
Administration	11.13	18.67	10.69	11.34	9.63	9.93	9.78	9.18	11.98
Road Transport	19.43	18.38	20.64	22.64	18.48	20.43	19.39	17.84	17.30
Sea/ Rail Transport	11.19	9.01	11.83	13.10	11.94	11.96	10.94	10.16	10.02
Sea/ Rail Loading	2.83	2.53	3.12	3.25	2.58	3.01	2.84	2.67	2.56
Equipment Leases	4.58	1.90	4.29	4.70	5.79	6.01	5.66	4.45	2.52
First Nations	2.38	2.15	1.78	1.87	1.63	1.72	1.71	1.63	2.30
Royalties	13.83	0.00	14.25	14.37	12.58	12.82	12.99	10.90	23.92
TC/RC and Penalties	32.83	29.73	36.70	37.83	29.45	35.47	32.41	30.79	29.68
PMPA	7.13	7.37	8.44	8.03	6.54	8.02	6.49	5.95	6.24
Total	**170.41**	**144.07**	**188.51**	**195.24**	**165.15**	**170.42**	**169.87**	**149.85**	**164.07**

Source: BMC

13.3.1 Open Pit Mining

The 2020 Re-stated Feasibility Study was based on open pit mining contractor budget quotations and for the 2023 Economic Update the open pit mining operating cost estimate was prepared based on adopting an owner operator mining fleet strategy. Using this model provides a benefit in that equipment capital and operating costs and productivity assumptions are fully transparent and can be audited and benchmarked across industry standards with the secondary benefit of forming a baseline for comparison of mining costs in the future.

No changes have been made to the physical mine schedule prepared for the 2019 Feasibility Study or ORE upon which that schedule is based.

Table 13-16: Open Pit Mining Operating Cost Summary

Description	LOM Cost (US$M)	LOM Unit Cost (US$/t mined)
Mobilisation	0.0	0.00
Demobilisation	7.0	0.05
Site preparation	2.1	0.01
Drilling	30.6	0.20
Ore and waste load and haul	204.5	1.34
Rehandle underground material and transport	5.4	0.04
Tailings rehandle and management	17.9	0.12
Crushed material	1.9	0.01
Daywork	0.0	0.00
Subtotal mining costs	269.3	1.77
Explosives contractor costs	58.7	0.39
BMC labour	155.6	1.02
Plant and equipment	2.5	0.02
Materials and services	74.8	0.49
Contractors and consultants	3.3	0.02
Total Open Pit Mining Costs	564.2	3.70
Capitalised preproduction mining cost adjustment	(35.9)	(0.24)
Open Pit Mining Operating Costs	**528.3**	**3.47**

Source: BMC

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13.3.2 Underground Mining

The 2019 Feasibility Study sourced budget quotations for underground mining from several underground mining contractors and the contractor selected for this work was also used to update the 2020 Re-stated Feasibility Study cost estimate (Table 13-17).

That same contractor provided an updated cost estimate for the 2023 Economic Update, which adopted a fixed and variable pricing structure that was not used in the 2020 Re-stated Feasibility Study estimate.

Due to the change in the contract structure from a "unit rate" basis to "fixed and variable", individual cost areas are often not directly comparable.

In addition, the 2023 cost estimate assumed that a two weeks on, two weeks off roster would be required to secure the workforce for the Kudz Ze Kayah Project rather than a two week on, one week off roster used for the 2020 Re-stated Feasibility Study estimate.

Table 13-17: Underground Mining Operating Cost Summary

	LOM Cost (US$M)	LOM Unit Cost (US$/t ore mined)
Mobilisation	2.9	1.69
Demobilisation	0.9	0.53
Development cost to drill, blast and excavate	27.0	15.59
Ground support	20.4	11.82
Production drilling and blasting	9.0	5.23
Production mucking	6.8	3.91
Paste fill activities	2.1	1.24
Other construction activities	6.2	3.61
Load and Haul	5.1	2.94
Daywork	3.5	2.01
Fixed equipment costs	21.7	12.55
Fixed labour costs	70.4	40.73
Total Mining Contractor Costs	176.1	101.86
BMC labour costs	7.5	4.32
Plant and equipment costs	1.9	1.08
Material and services costs	38.3	22.16
Contractors and consultants' costs	2.5	1.47
Total underground mining costs	226.3	130.88
Capitalised mine development cost adjustment	(69.1)	(39.99)
Underground Mining Operating Costs	**157.2**	**90.89**

Source: BMC

13.3.3 Processing

Processing operating costs were re-estimated and include all site operating costs associated with processing ore to produce copper, high precious metal (HPM) and zinc concentrates, and filtered tailings (Table 13-18). Reagent consumption rates are the same as that used in the 2020 Re-stated Feasibility Study and although an opportunity exists to utilise new and more efficient or effective reagent treatment regimens as they are developed, this has not been considered in the 2025 Technical Report update.

Table 13-18: Processing Operating Cost Summary

Description	LOM Cost (US$M)	LOM Unit Cost (US$/t processed)
Labour	69.0	4.39
Power	80.4	5.12
Maintenance materials	34.2	2.17
Reagents and consumables	123.4	7.85
Miscellaneous	10.8	0.69
Total ore processing costs	**317.8**	**20.21**

Source: BMC

13.3.4 Water Treatment

Water treatment costs were re-estimated by the consultant responsible for this infrastructure and are presented in Table 13-19.

Table 13-19: Water Treatment Plant Operating Cost Summary

Circuit	Description	LOM Cost (US$M)	LOM Unit Cost (US$/t processed)
Metals removal	Reagents	4.6	0.29
	Maintenance	0.9	0.06
	Power	1.1	0.07
	Other	0.1	0.01
Subtotal Metals Removal		6.7	0.43
Selenium removal	Reagents	8.5	0.54
	Maintenance	2.7	0.17
	Power	2.0	0.13
Subtotal Selenium Removal		13.2	0.84
Total Water Treatment Costs		**20.0**	**1.27**

Source: BMC

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13.3.5 General and Administration

G&A costs (Table 13-20) incurred due to open pit mining activity during the pre-production period have been capitalised and included as open pit mine development costs.

Table 13-20: G&A Operating Cost Summary

Description	LOM Cost (US$M)	LOM Unit Cost (US$/t processed)
Labour	30.4	1.93
Vehicles	0.9	0.05
Power generation rental	8.5	0.54
Power and heating	30.5	1.94
Administration	11.1	0.70
Health and safety	0.7	0.05
Transportation	18.6	1.18
Human resources / Public relations	1.4	0.09
Environment	12.6	0.80
Site services	22.1	1.40
Accommodation	31.2	1.98
Offsite concentrate marketing	11.5	0.73
Total	179.3	11.40
Capitalised preproduction costs	(4.2)	(0.27)
Administration Operating Costs	175.1	11.13

Source: BMC

Labour costs were benchmarked to comparable northern mining operations.

Insufficient heat will be recovered from the power station during the winter months to fully heat the processing facility when only three generators are installed in the permanent power station. Therefore, gas fired boilers will be used to supplement heat production during these periods (November to March).

Offsite concentrate marketing has a provision of US$5/dmt of concentrate sold (to cover marketing of concentrates and logistics planning for transportation to final customers).

13.3.6 Equipment Leases

Certain capital equipment assets for the establishment of the operation are planned to be provided under an operating lease arrangement (Table 13-21). These assets include the power generation plant and associated LNG fuel storage equipment, heavy mobile equipment for the processing facility and light vehicles for processing and administration departments to commence operations. Capital costs for all equipment are based on June 2023 quarter pricing. Leasing interest rates were assumed to be between 8% and 10.45% based on indicative market terms, applied to the declining principal on a monthly basis.

Lease payments of US$72 million related to equipment used during the pre-production phase are summarised in Table 13-21. This includes US$58 million of acquired asset value, of which $40 million relates to pre-production capital expenditure. At the conclusion of the leasing period, ownership of the assets will be transferred to BMC for a nominal payment of $1. Replacement equipment required beyond this period are included in sustaining capital.

Table 13-21: Equipment Lease Cost Summary

Operating Lease	Lease term	(US$M)
Power generation, initial construction	72 months	35.7

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LNG fuel storage	72 months	9.4
Power generation, expansion	60 months	21.4
988 front end loader (1)	60 months	1.6
980 front end loader (1)	60 months	0.7
Emergency response, ambulance (2)	72 months	0.3
Backhoe (1)	60 months	0.1
Electric pick and carry crane (1)	72 months	0.1
Rough terrain crane (2)	72 months	0.6
Elevated work platform (3)	60 months	0.1
Skid steer loader (1)	60 months	0.0
Reach stacker forklift (1)	60 months	0.3
Standard forklift (2)	60 months	0.1
Maintenance truck (2)	60 months	0.3
Bus (3)	72 months	0.2
Light vehicle (19)	48 months	1.2
Total Operating Lease Costs		**72.1**

Source: BMC

Leasing costs for open pit mining equipment have not been included in Table 13-21 and are instead captured in the open pit mining costs.

During the pre-production phase, BMC expects to acquire US$48 million of mining equipment through leasing.

The total value of equipment acquired during the pre-production phase anticipated to be financed through leasing is US$88 million and not included in the pre-production capital total of US$492 million.

13.3.7 Power Generation and Fuel

LNG and diesel fuel costs vary each year in accordance with commodity price forecasts and the higher costs for Year 1 in Table 13-22 are due to the rental diesel power plant and the use of diesel instead of LNG as a fuel source for much of the year.

Table 13-22: Average Annual Power Generation Unit Costs

Year	Unit Power Cost (US$/kWh)
1	0.166
2	0.123
3	0.124
4	0.126
5	0.127
6	0.127
7	0.127
8	0.129
LOM average	**0.130**

Source: 2025 Technical Report

13.3.8 Concentrate Road Transport

Table 13-23Provision has been made for transportation of bulk copper concentrate to a potential rail head, for subsequent loading and transportation on the Canadian rail network to domestic customers,

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if required. Bulk zinc concentrates and containerised HPM concentrate will be transported to Stewart World Port for subsequent loading and transportation on ships to end destinations.

Table 13-23: Road Transport Costs

Description	LOM Cost (US$M)	LOM Unit Cost (US$/wmt)
Copper concentrate to a rail head	45.4	102.96
HPM concentrate to SWP	57.6	139.04
Zinc concentrate to SWP	202.5	121.59
Road Transport Total	305.5	

Source: 2025 Technical Report

13.3.9 Rail Freight and Port/Sea Operations

Budget port operational costs were sourced from SWP for the handling of all concentrate products. Estimates are inclusive of all storage, loading, wharfage and terminal fees. An internal cost estimate was developed for rail head operations in 2022 and an escalation factor of 3.5% was applied to this estimate for use in the 2023 update (Table 13-24).

Table 13-24: Port/Railhead Operating Costs

Description	LOM Cost (US$M)	LOM Unit Cost (US$/wmt)
Copper concentrate at a rail head	6.1	13.86
HPM concentrate at SWP	9.4	22.72
Zinc concentrate at SWP	28.9	17.37
Total Port / Rail Head Operations	**44.5**	

Source: 2025 Technical Report

Sea freight costs are based on the long-term cost basis and adjustments have been made to costs for each offtake agreement to take into consideration the destination of concentrate products as defined in each agreement (Table 13-25).

Table 13-25: Sea/Rail Freight Operating Costs

Description	LOM Cost (US$M)	LOM Unit Cost (US$/wmt)
Copper concentrate from a rail head	53.1	120.55
HPM concentrate from SWP	19.2	46.35
Zinc concentrate from SWP	80.7	48.45
Subtotal	153.0	
Insurance and referee charges	22.9	
Total Sea / Rail Freight Costs	**176.0**	

Source: 2025 Technical Report

13.3.10 Concentrate Treatment and Refining Charges

Concentrate treatment and refining charges are based on the various offtake agreements that have been executed by BMC, and they have not been reproduced here due to the confidential nature of each agreement.

13.3.11 First Nations

The 2025 Technical Report allows for a total of C$48.5 million (US$37.3 million) in payments to Kaska, under the SEPA comprising C$1 million paid upon signing of an updated SEPA, C$1 million payment during construction and annual payments of C$4.650 million over a 10-year period,

commencing with the start of operations and continuing into the active closure phase (C$46.5 million total).

13.3.12 Royalties

Royalties payable under the Quartz Mining Act to the Yukon government are estimated to be US$217.5 million.

13.3.13 Precious Metals Purchase Agreement

In December 2021, BMC entered into a streaming agreement over a portion of the gold and silver produced by the KZK Property (the PMPA). The PMPA is now held by now held by Wheaton Precious Metals Corp (Wheaton). The proportion of gold and silver covered by the PMPA varies over the life of the Kudz Ze Kayah Project.

The cash cost of the PMPA over the life of the Kudz Ze Kayah Project is estimated to be US$112.1 million.

13.3.14 Greenhouse Gas Emissions

The ABM Mine will incur costs for greenhouse gas emissions as established under the Government of Canada's *Greenhouse Gas Pollution Pricing Act* (refer to section 13.4.3 for a discussion of the legislation).

Project costs arising from greenhouse gas emissions are detailed in Table 13-26.

Table 13-26: Greenhouse Gas Emission Costs

	Unit	Total	Y1	Y2	Y3	Y4	Y5	Y6	Y7	Y8	Y9
Base metals contained in concentrates											
Zinc	tonne	786,202	80,858	110,851	114,020	97,435	109,038	106,600	102,582	64,818	-
Copper	tonne	100,230	5,637	11,675	15,094	22,312	14,868	11,261	10,859	8,524	-
Lead	tonne	195,360	22,425	26,826	24,879	18,810	26,547	27,665	26,833	21,376	-
Total	tonne	1,081,792	108,920	149,351	153,993	138,557	150,453	145,525	140,275	94,719	-
Greenhouse gas emissions											
GHG produced	t CO_2-e	701,920	57,701	103,622	106,323	110,424	87,938	90,848	84,115	60,950	-
GHG permitted	t CO_2-e	695,592	70,036	96,033	99,017	89,092	96,741	93,573	90,197	60,904	-
Excess / (Surplus)	t CO_2-e	6,328	(12,334)	7,589	7,305	21,332	(8,804)	(2,724)	(6,082)	46	-
Cost / (Credit)	US$M	2.1	-	-	1.0	1.5	1.9	(1.4)	(0.1)	(1.1)	0.2

Source: 2025 Technical Report

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13.4 Base Case Economic Analysis

The following discussion is extracted from the project Feasibility Study investigations as summarised in the 2025 Technical Report (ERM 2025b).

13.4.1 Metal Prices and Exchange Rates

Consensus metal prices and exchange rates used in the economic analysis are presented in Table 13-27, and are used for the Base Case economic scenario.

Table 13-27: Consensus Metal Prices and Exchange Rate

Parameter	Unit	2023	2024	2025	2026	2027 / Long Term
Zinc	US$/lb Zn	$1.21	$1.21	$1.23	$1.24	$1.20
Silver	US$/oz Ag	$23.6	$23.8	$23.6	$23.4	$22.6
Copper	US$/lb Cu	$3.90	$3.91	$4.13	$4.27	$3.80
Gold	US$/oz Au	$1,922	$1,915	$1,853	$1,808	$1,700
Lead	US$/lb Pb	$0.95	$0.94	$0.93	$0.94	$0.95
Exchange Rate	USD:CAD	1.342	1.327	1.320	1.315	1.297

Source: 2025 Technical Report

13.4.2 Production Metrics

LOM concentrate and metal production is shown in Table 13-28 and Table 13-29, respectively.

Table 13-28: LOM Concentrate Production

Concentrate	Unit	Total	Y1	Y2	Y3	Y4	Y5	Y6	Y7	Y8
Zinc	dmt	1,515,582	159,150	213,174	219,269	187,374	209,689	204,999	197,274	124,651
Copper	dmt	401,161	22,791	46,698	60,375	89,249	59,470	45,043	43,437	34,098
HPM	dmt	376,988	44,419	51,588	47,844	36,173	51,051	53,202	51,602	41,107
Total	**dmt**	**2,293,730**	**226,361**	**311,461**	**327,488**	**312,797**	**320,211**	**303,244**	**292,313**	**199,856**

Source: 2025 Technical Report

Table 13-29: LOM Metal-in-Concentrate Produced

Metal in Concentrate	Unit	Total	Y1	Y2	Y3	Y4	Y5	Y6	Y7	Y8
Zinc in Zn Con	Mlb	1,733	178	244	251	215	240	235	226	143
Gold in Zn Con	oz	54,257	5,419	7,073	7,616	7,566	7,935	6,173	7,042	5,432
Silver in Zn Con	koz	7,674	869	1,101	1,122	994	1,094	871	939	684
Copper in Cu Con	Mlb	221	12	26	33	49	33	25	24	19
Gold in Cu Con	oz	181,891	15,766	20,074	24,201	25,676	26,139	22,570	25,448	22,016
Silver in Cu Con	koz	25,592	2,851	3,315	3,141	2,871	3,252	3,263	3,652	3,247
Lead in HPM Con	Mlb	431	49	59	55	41	59	61	59	47
Gold in HPM Con	oz	195,769	27,242	33,443	25,630	24,234	25,389	19,709	23,034	17,088
Silver in HPM con	koz	26,542	2,830	3,717	3,718	3,318	3,694	3,132	3,480	2,654
Total Gold in Con	koz	432	48	61	57	57	59	48	56	45
Total Silver in Con	Moz	60	7	8	8	7	8	7	8	7

Source: 2025 Technical Report

Annual metal production in concentrate during 'steady state' production (i.e. excluding the first year of production when commissioning and ramp-up are in progress and the last year of production as the project winds down) is detailed in Table 13-30.

Table 13-30: Annual Metal Production in Concentrate During Steady State Operations

	Copper		Zinc		Lead		Gold	Silver
	'000 t	M lb	'000 t	M lb	'000 t	M lb	'000 oz	M oz
Year 1 production	5.6	12	80.9	178	22.4	49	48.4	6.6
Steady state average per annum[1]	14.3	32	106.8	235	25.3	56	56.5	7.8
LOM production	100.2	221	786.2	1,733	195.4	431	431.9	59.8

Note: Excludes Year 1 and final year of production.

Metal production equivalents

To assist in comprehension of the significance of the concentrate production from the ABM Mine project, the Company considers that expressing the total concentrates production in terms of a single metal equivalent may be of assistance.

In the Company's opinion, all of the elements included in the metal equivalents calculation have a reasonable potential to be recovered and sold, as supported by Feasibility Study-level metallurgical testwork and executed offtake agreements informing payability and processing charges.

The basis for the selection of silver is the chosen equivalent metal is based on the net revenue likely to be derived from each metal in the ABM Deposit. Silver is the primary contributor to revenue. Zinc, along with copper and lead are more heavily affected by metal payabilities and also concentrate treatment charges.

In 2023 terms, silver contributed 30.5% of the net revenue from the Ore Reserve estimate, with zinc contributing 30.4%. However, considering the price escalation reflected in current pricing, as at the Report date, silver's contribution to net revenue is now 33.0% and zinc has fallen to 21.2%.

Table 13-31 presents the life of mine concentrate production in terms of the silver equivalents.

Table 13-31: LOM Silver equivalent metal production

Ag Eq Production by Metal	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Total
Ag (Moz)	6.6	8.1	8.0	7.2	8.0	7.3	8.1	6.6	59.8
AgEq From Au (Moz)	3.6	4.6	4.3	4.3	4.5	3.6	4.2	3.4	32.5
AgEq From Zn (Moz)	9.5	13.0	13.3	11.4	12.8	12.5	12.0	7.6	92.0
AgEq From Cu (Moz)	2.1	4.3	5.6	8.3	5.5	4.2	4.0	3.2	37.2
AgEq From Pb (Moz)	2.1	2.5	2.3	1.7	2.5	2.6	2.5	2.0	18.1
Total AgEq (Moz)	**23.8**	**32.5**	**33.5**	**32.9**	**33.2**	**30.1**	**30.8**	**22.7**	**239.6**

Source: BMC

Metal production equivalent is the sum of the value of the metal recovered into concentrate, divided by the price of the metal being used for metal equivalent reporting.

As the calculation is for metal production equivalents, the Company has used the forecast recovered mass of metal in concentrates in calculations.

Processing recoveries have inherently been incorporated in the calculation as it is based on metal recovered into concentrate at the processing plant. Average life of mine processing recoveries that have been incorporated into the metal production in concentrates are detailed in Table 13-32.

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Table 13-32: ABM Mine average LOM processing recoveries

Concentrate	Copper	Lead	Zinc	Gold	Silver
Copper	73.8%	-	-	27.3%	36.8%
HPM	-	73.5%	-	29.4%	38.2%
Zinc	-	-	85.9%	8.1%	11.0%
Total	73.8%	73.5%	85.9%	64.8%	86.0%

Source: BMC

Long term consensus metal prices have been used for all calculations: Ag US$22.60/oz, Au US$1,700/oz, Zn US$1.20/lb, Cu US$3.80/lb, Pb US$0.95/lb.

The metal grade equivalent formula (for physical production and costs) is as follows:

*AgEq (oz) = (Sum of Ag recovered to Cu, HPM and Zn concentrates (oz Ag) * Ag price (US$/oz) + Sum of Au recovered to Cu, HPM and Zn concentrates (oz Au) * Au price (US$/oz) + Zn recovered to Zn concentrate (t Zn) * Zn price (US$/t) + Cu recovered to Cu concentrate (t Cu) * Cu price (US$/t) + Pb recovered to HPM concentrate (t Pb) * Pb price (US$/t)) / Ag price (US$/oz)*

In the Company's opinion, all of the elements included in the metal equivalents calculation have a reasonable potential to be recovered and sold, as supported by feasibility metallurgical testwork and executed offtake agreements.

13.4.3 Taxation Review

The analysis summarises the Canadian corporate income tax, the Yukon Royalty levied under the Quartz Mining Act and associated regulations, and the Canadian carbon tax as levied under the Greenhouse Gas Pollution Pricing Act and its associated regulations.

The analysis pertains only to taxation of the Company and does not address tax considerations that may be applicable to shareholders.

Mining Taxes, Duties or Royalties

Mining producers are required to pay a levy to the Crown (i.e. the Government) as the holder of the mineral rights on the extraction of minerals. In Canada, the majority of the mineral rights are owned by the Crown on behalf of the people of Canada. The mining royalty is deductible in determining taxable income.

Yukon Mining Royalties

Yukon mining royalties under the Quartz Mining Act are payable to the Yukon Government annually. The Quartz Mining Act royalty is a net profits royalty, based on annual mineral production and sales after deduction of eligible expenses and allowances. Deductible, eligible expenses include:

- on-site production costs, including related exploration and development costs;
- off-site costs for preparing and transporting mineral concentrates;
- reclamation costs;
- development allowance (amortising eligible pre-production exploration and development costs to bring the ABM Mine into production);
- depreciation allowance (depreciation of original capital costs of eligible assets on 15% per annum straight line basis until costs are fully deducted); and
- community and economic development allowance (qualifying expenditures in community and economic developments are pooled and deducted at the lesser of the remaining undeducted balance, 15% of the amounts claimed in the year as deductions, development allowance and depreciation allowance, or 20% of the value of output of a mine after other deductions in the year).

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The deductions for eligible expenses of on-site production costs, off-site costs and reclamation costs can only be claimed in the year incurred and there is no carry forward mechanism.

The allowances for development, depreciation and community and economic development are not discretionary deductions and the eligible allowance deductions for a year must be claimed in that year.

The Quartz Mining regulations specifically prohibit the deduction of, amongst others, the following:

- financing costs;
- royalties;
- hedging losses;
- costs for an off-site office; and
- the cost of goods and services not directly related to the ABM Mine.

The royalty is applied in accordance with Table 13-33. The royalty is applied on an incremental cumulative basis until the ABM Mine's calculated net profit is accounted for.

Table 13-33: Quartz Mining Act royalty rates

Value of Output lower band (C$)	Value of Output upper band (C$)	Royalty Rate applicable to band
$0	$10,000	0%
$10,000	$1,000,000	3%
$1,000,000	$5,000,000	5%
$5,000,000	$10,000,000	6%
$10,000,000	$15,000,000	7%
$15,000,000	$20,000,000	8%
$20,000,000	$25,000,000	9%
$25,000,000	$30,000,000	10%
$30,000,000	$35,000,000	11%
	$35,000,000 and above	12%

Source: Quartz Mining Act, SY 2003, c. 14; amended by SY 2008, c.19; SY 2013, c.18; SY 2016, c.5; SY 2016, c.12; SY 2023, c.7

Taxation

Fiscal Regime

The fiscal regime that applies to the mining industry in Canada consists of a combination of income taxation at the federal level, and income taxation and mining taxes, duties or royalties at the provincial and territorial level:

1) Income tax rate:
   a) Federal corporate tax is 15% (after abatements and reductions described below).
   b) Yukon corporate tax is 12%.
2) Investment incentives:
   a) Research and development tax credits.
   b) Clean economy investment tax credits

Corporate Tax

For Canadian income tax purposes, a corporation's worldwide taxable income is computed in accordance with common principles of business (or accounting) practice, modified by certain statutory provisions in the *Income Tax Act* (the "Canadian Tax Act"). In general, no special tax regime applies to mining enterprises.

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Depreciation, depletion or amortisation recorded for financial statement purposes is not deductible; rather, tax deductible capital cost allowances and deductions as specified in the Canadian Tax Act are allowed. The annual tax deductions could vary from 6% to 100% of the capital expenditures depending upon the nature of a capital expenditure.

Mining corporations are taxed at the same rate as other corporations. Corporations are taxed by the Federal Government and by one or more provinces or territories. The basic rate of federal corporate tax is 38%, but it is further reduced to 28% by an abatement of 10% on a corporation's taxable income earned in a province or territory. Further to this, a general tax reduction of 13% is available on qualifying income, bringing the federal income tax rate to 15%. The Yukon tax rate is added to the federal tax.

No tax consolidation, group relief or profit transfer system applies in Canada. Each corporation computes and pays tax on a separate legal-entity basis. Business losses or non-capital losses may be carried back three years and forward 20 years.

Effective for taxation years beginning 1 October 2023, new earnings stripping rules are in place that will, in general, limit the amount of net interest and financing expenses that a corporation may deduct in computing taxable income to no more than a fixed ratio of tax EBITDA. The new earnings-stripping rule will have a fixed ratio of 30% for taxation years beginning on or after 1 January 2024. In addition, a "group ratio" will allow a taxpayer to deduct interest and financing expenses in excess of the fixed ratio where the taxpayer is able to demonstrate that the ratio of net third-party interest and financing expenses to book EBITDA of its consolidated group supports a higher deduction limit. The amount of any interest and financing expenses that is denied under the new earnings stripping rule will generally be able to be carried forward indefinitely.

Gains resulting from a disposal of a capital property are subject to income tax. Capital gains or losses are determined by deducting the adjusted cost base of an asset from proceeds of disposition (net of outlays incurred in connection with the disposition). For corporate taxpayers, one half of the capital gain (taxable capital gain) is taxed at normal income tax rates.

Capital losses are exclusively deductible against capital gains and not against other taxable income. However, non-capital losses are deductible against taxable capital gains, which are included in taxable income. Capital losses can be carried back three years and carried forward indefinitely for use in future years, provided an acquisition of control has not occurred. Mining rights and mineral resource properties are not capital properties for purposes of the Canadian Tax Act.

Canada Carbon Tax

The Government of Canada has enacted the *Greenhouse Gas Pollution Pricing Act* as a means to monitor and encourage the progressive reduction in greenhouse gas emissions in Canada. The Kudz Ze Kayah Project will fall within the Output Based Pricing System for large emitters estimated through the *Output-Based Pricing System Regulations*, established under the Act.

The Regulations establish metrics for the calculation of gas emissions from the combustion of various carbon-based fuels for both stationary engines (power generation equipment) and site transportation equipment (mobile mining equipment), which are then converted to a carbon dioxide equivalent (CO_2-e) and compared to permitted emission levels established by the Regulations. Base metal mines producing concentrates have an allowable emission level of 0.643 t of CO_2-e per tonne of base metal contained in concentrate.

If the quantity of emissions exceeds that of the allowable yearly emission levels, operators must pay for the excess pollution at the legislated cost of pollution or alternatively purchase credits in the open market to offset the excess emissions. In years where the quantity of emissions is less than that of

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the allowable emissions levels, companies may sell their surplus emissions on the open market. New producers are exempt from emissions costs for the first two years of operations (Table 13-26).

For each year of operation, if the quantity of emissions exceeds that of the allowable emission levels, emitters must pay for the excess emissions at the legislated cost of the emissions or alternatively purchase credits in the open market to offset the excess emissions. In years where the quantity of emissions is less than that of the allowable emissions levels, companies may sell their surplus emissions on the open market. New producers are exempt from emissions costs for the first two years of operations.

The cost of carbon emissions set by the Government of Canada is shown in Table 13-34.

Table 13-34: Canada Carbon Pollution Price Schedule

Year	Cost C$/t CO_2-e
2025	$95
2026	$110
2027	$125
2028	$140
2029	$155
2030 onwards	$170

Tax Deductions

BMC Minerals Ltd who owns the Kudz Ze Kayah Project has accumulated tax deductions of US$168.9 million through project acquisition and evaluation, which have been included in determining the tax payable by the Kudz Ze Kayah Project (Table 13-35).

Table 13-35: Tax Deduction Summary (as of June 2025)

Category	Value (US$M)
Canadian Exploration Expense (CEE)	34.4
Canadian Development Expense (CDE)	6.5
Non-Capital Losses Carried Forward (NCL)	128.0
Total Tax Deductions	**168.9**

Source: BMC

13.4.4 Unit Costs

Annual C1 and AISC unit costs are shown in Table 13-36 and as over 75% of the net revenue for the project is generated from zinc, copper, and silver in concentrate, the C1 costs and AISC have been prepared for all three metals for comparative purposes. All other metals are considered to be by-product credits in calculations.

Table 13-36: Annual C1 and All-In-Sustaining Unit Costs ($US)

Cost	Unit	LOM	Y1	Y2	Y3	Y4	Y5	Y6	Y7	Y8
Zinc C1 Unit Cost	US$/lb Zn	-0.44	-0.29	-0.35	-0.30	-0.63	-0.55	-0.18	-0.50	-0.90
Silver C1 Unit Cost	US$/oz Ag	-23.77	-17.28	-22.69	-25.57	-30.47	-26.92	-22.88	-23.14	-20.04
Copper C1 Unit Cost	US$/lb Cu	-7.52	-14.68	-9.38	-6.28	-2.95	-7.75	-7.88	-10.44	-9.87
Zinc AISC Unit Cost	US$/lb Zn	-0.12	-0.01	-0.12	0.07	-0.18	-0.14	0.05	-0.28	-0.51
Silver AISC Unit Cost	US$/oz Ag	-14.77	-9.73	-16.09	-13.62	-17.44	-15.21	-15.21	-17.36	-12.17
Copper AISC Unit Cost	US$/lb Cu	-5.32	-11.18	-7.45	-3.78	-1.29	-5.02	-5.91	-8.64	-7.34

Source: 2025 Technical Report. Note: each metal unit costs includes credits from the other metals

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13.4.5 Cashflow

The annual LOM cashflows for the Base Case are shown in Figure 13-1.

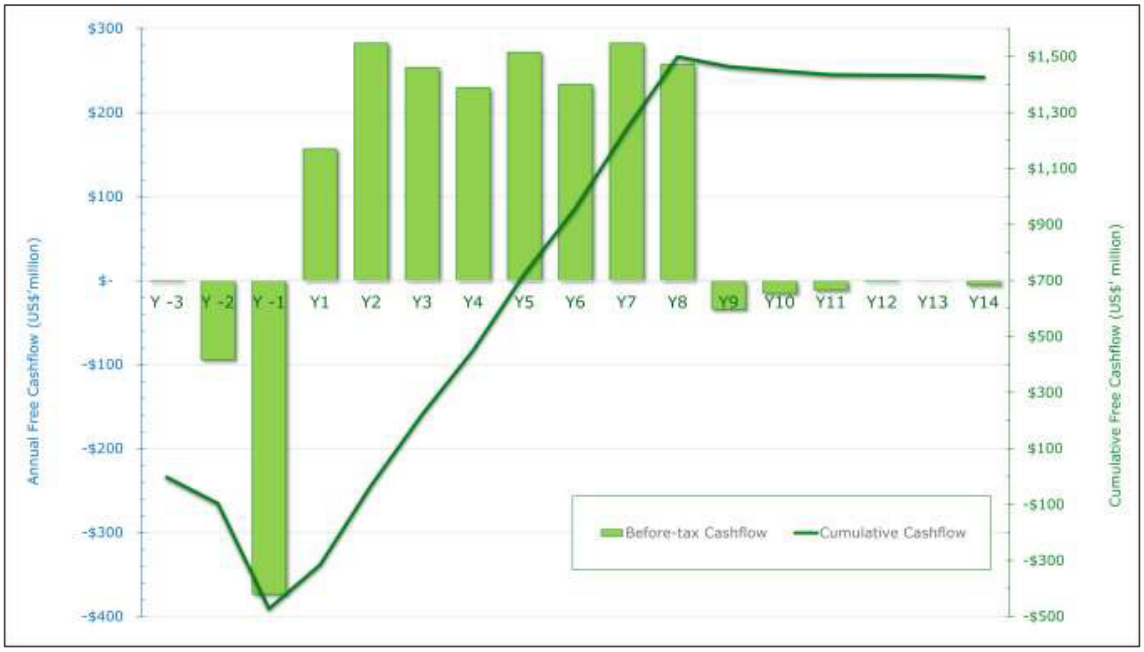


Figure 13-1: Base Cash Project Before-tax Cashflow (US$M)
Source: BMC

13.4.6 Sensitivities

Several additional scenarios were modelled by the Company as variations from the Base Case where an Upside and Downside Case considered flexing of key revenue and cost inputs.

The Project is most sensitive to changes in exchange rate, followed by discount rate, OpEx, metals prices and grades and then CapEx. The sensitivity of changes in key variables on the before-tax net present value (NPV) has been determined through a simple factoring of each element. The relative sensitivity of the before-tax NPV, for the most sensitive variables, is shown below Figure 13-2.

Most variables were assessed on a standard ±10% proportional change while the remaining variables are percentage driven (e.g. metal recovery) and were assessed based on flexing the variable by ±2 units to better represent the expected variability range.

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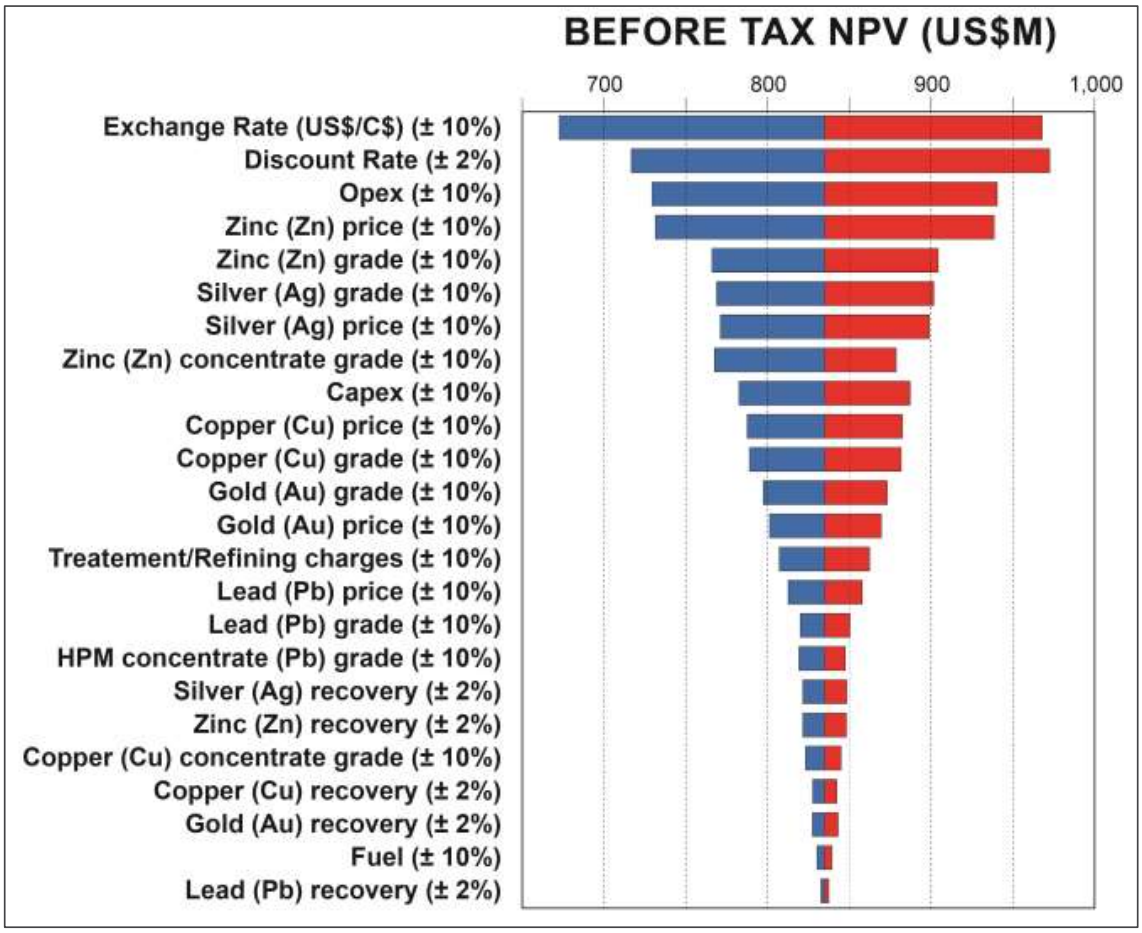


Figure 13-2: Tornado Analysis – before-tax NPV sensitivity results
Source: BMC

13.4.7 Project Financial Metrics

The project financial metrics are presented below in Table 13-37 in United States dollars on a before-tax basis.

Table 13-37: Base Case Economic Results

Parameter	USD
Before-tax cashflow	$1,426 million
Before-tax NPV_7	$835 million
Before-tax IRR	42.1%
Payback period	2.2 years
EBITDA (LOM)	$2,090 million
EBITDA ("steady-state" average per year)	$288 million

Note: steady state excludes Year 1 and final year of production.
Source: from 2025 Technical Report (using June 2023 costs)

All metrics were derived using a 7% discount rate.

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13.5 ERM Opinion

The Company concluded that the 2025 Technical Report has demonstrated that the Kudz Ze Kayah Project maintains strong economic fundamentals.

ERM commends BMC on the work completed for the 2025 Technical Report and its supporting documentation and the level of detail that has been covered (and considered) in the revised cost estimation and revenue analysis for the near-term development of the Kudz Ze Kayah Project.

In ERM's professional opinion, the economic analysis presents a robust 9-year production profile with some optionality to modify operations as opportunities are identified.

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14. PROJECT EXECUTION PLAN

A project execution plan was developed for the ABM Mine Project and describes the strategy for constructing and commissioning of the Kudz Ze Kayah Project to bring it into the operational phase where marketable concentrates can be produced and sold.

14.1 Health, Safety and Environment

BMC has developed an Occupational Health and Safety Management System that forms the base for the implementation phase and transition into operations on a "zero-harm" basis. The engineering, procurement, construction and management (EPCM) consultant and engineering, procurement and construction (EPC) contractors will establish specific health, safety and environment management plans to deliver the scope of work in a manner that aligns with BMC policies and procedures and complies with regulatory requirements.

The Company currently operates in accordance with a site-specific exploration environmental engagement plan (EMP), which includes all relevant environmental conditions that are stipulated in the various existing permits and licences.

14.2 Community Engagement

Although the ABM Mine Project site is considered a remote location, there are several First Nations and other local communities within the region. The Company is committed to supporting these communities through providing employment opportunities during the various phases of the project development and operation.

The Company will engage with community leaders on a regular basis during the implementation phase to assess the potential for members of the First Nations communities to participate in the project.

In addition, it will be a commercial condition of all outsourced construction work that contractors actively seek to engage appropriately skilled First Nations labour where possible. This condition will also apply to all phases of the ABM Mine Project.

Cultural awareness programmes will be implemented at all phases of the ABM Mine Project to broaden the understanding and commitment of the Company, consultants/contractors alike.

14.3 Execution Strategy

The overarching strategy for managing the execution of the Kudz Ze Kayah Project development revolves around clearly defined roles and accountabilities as well as the best use of human resources based on experience and qualifications without the obstruction of corporate barriers.

The execution strategy will use an EPCM contracting approach with many functions shared between the Company and EPCM consultant. BMC propose to operate a four-tier management structure during project implementation as illustrated in Figure 14-1.

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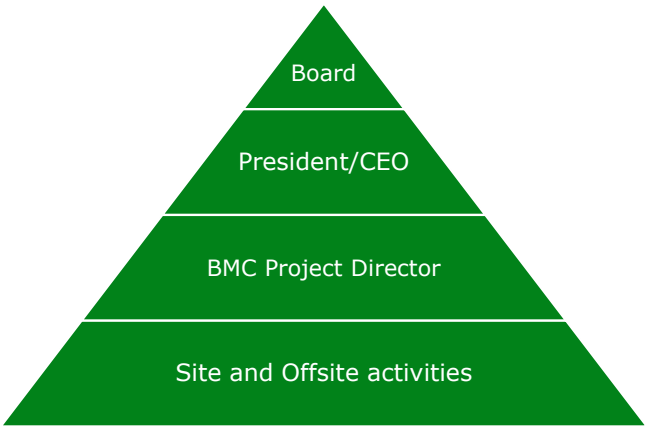


Figure 14-1: Management Structure for Project implementation

Source: BMC

The BMC Project Director will oversee, monitor, and manage the ABM Mine Project from a strategic executive level. This role is critical to the coordination of activities and interoperability of the various departments, both on and off site.

The Project Delivery Team (PDT) will be responsible for the day-to-day management of activities during the execution phase and would operate as an integrated project group, with roles assigned based on competence, qualification and experience, regardless of their organisation. The PDT will be primarily BMC personnel augmented by an EPCM consultant and inclusion may extend to other businesses depending on the talent pool available at the time.

14.4 Plans, Schedules and Project Controls

A detailed Construction Management Plan is developed during the initial stages of Project Execution and is overseen and signed off by the Project Director.

A Project Control Estimate is set up following authority to proceed and includes the original budget, keeps track of the current project budget, current forecast, commitments, and expenditures. Budget and forecast costs are entered into an overarching cost system by the project controls team, from estimates and deviations, in accordance with the PDT procedure.

The initial project master schedule (PMS) is planned to be developed to Level 3 during detailed engineering phase over the course of several workshops. At the conclusion of the workshops, the Project Director would review the PMS and approve for implementation.

A baseline is set following approval to create a project baseline schedule from which the progress of all activities would be monitored and managed. A Level 3 schedule was prepared for the Feasibility Study-level investigations, with key milestones including:

- Decision Document Issued
- Quartz Mining Licence Issued
- EPCM Contract Awarded
- Engineering Start
- Geotechnical Interpretation Report
- Camp Complete
- Commencement of Process Plant earthworks
- Engineering Complete

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- Process Plant Earthworks Completion
- Site Access for EPCM
- Type A Water Licence Issued
- Commence Concrete
- Commence Open Pit Pre-production Works
- Process Plant Building Complete
- Water Treatment Plant Complete
- Power Plant Commissioned
- Construction Complete (Commence Ore Commissioning)
- Port Facilities Complete
- Operations Handover

In April 2025, the Yukon government wrote to BMC advising that they were satisfied that the ABM Mine Project was economically feasible, and that they were consulting with Kaska on the matter. BMC has been advised that consultation between the Yukon, Canadian and Kaska governments is ongoing.

Once the current government to government consultation is completed BMC will receive a new Decision Document.

BMC has submitted applications to the Yukon Water Board for a Water Licence under the Waters Act (Yukon), an application for a Quartz Mining Licence under the Quartz Mining Act (Yukon) and applications for other authorisations required to develop and operate the proposed ABM Mine.

These applications have been reviewed by the Yukon government but are currently on hold until a new Decision Document is issued.

The detailed engineering phase of the ABM Mine Project will begin with updating and finalising of the PDC ready for use by other disciplines. The EPCM Project Manager would approve all designs (after sign-off by the Project Engineers and/or Area Managers) before presenting to the Project Director, who would have the ultimate responsibility for the designs and implementation.

The assigned Project Engineers will be responsible to ensure all presented design documentation, whether it be drawing or otherwise, be amended shortly after construction has been completed to reflect the "as-built" conditions on site.

14.5 Procurement and Contracts

The strategy for implementation of the processing plant and associated facility construction is driven by the opportunity to outsource the work to a suitably experienced contractor where the risk can be better managed and mitigated. The concept of using a consolidated management team is considered the most appropriate method of undertaking a major design and construct project of this nature. The PDT would include the services of an EPCM contractor who is responsible for outsourcing and managing specific packages of work relating to the processing plant, in line with implementation objectives.

The remaining works such as bulk earthworks for plant site, water storage infrastructure, WSF and all road works will be outsourced but managed by BMC personnel within the PDT. Underground mining is also planned to be outsourced to experienced contractors but overseen and technically supported by experienced BMC personnel.

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14.6 Engineering, Procurement and Construction

Construction work will be outsourced in the form of individual work packages where much of the work will be carried out by EPC contractors who will be utilised to complete works associated with mechanical installations, structural and platework steel installation and erection, electrical and instrumentation installation, and piping installations.

Specialist subcontractors will be used to complete bulk earthworks and concrete batching and placement. Table 14-1 lists the major work packages proposed for the ABM Mine implementation.

Table 14-1: Major work packages for Project implementation

Scope	Type of contract	Stakeholder	Managed by
Tote Road Upgrade	Schedule of Rates	Earthworks Contractor 1	BMC
Site Earthworks: Camp, Site Roads, Plant Site, WSF, Water Management Structures, Borrow Pit	Schedule of Rates	Earthworks Contractor 2	BMC
Concrete Supply	Schedule of Rates	Specialist Contractor	EPCM contractor
Camp	Lump Sum	EPC Contractor No. 1	BMC
Non-processing Infrastructure inclusive of Process Plant Pre-Engineered Building, Administration Office, Plant Control Room, Plant Maintenance Workshop, Plant Warehousing Facilities, HVAC Systems, Assay Laboratory, Gatehouse, and Mine Dry Change Room	Lump Sum	EPC Contractor No. 2	EPCM contractor
Water Treatment Plant	Lump Sum	EPC Contractor No. 3	BMC
Bulk Diesel Fuel Storage and light vehicle Fuel Storage and Dispensation System	Lump Sum	EPC Contractor No. 4	EPCM contractor
LNG Storage Facility	Lump Sum	EPC Contractor No. 5	EPCM contractor
Power Station	Lump Sum	EPC Contractor No. 6	EPCM contractor
Site wide power distribution	Lump Sum	EPC Contractor No. 7	EPCM contractor
Major Equipment (e.g. SAG, and Ball Mills, Concentrate, and Tailings Filters, Thickeners, etc.)	Lump Sum	Supplier Type 1	EPCM contractor
Site Communications	Lump Sum	Supplier Type 2	BMC
Port Facilities	Lump Sum	EPC Contractor No. 8	BMC
Mining Services	Schedule of Rates	Mining Contractor	BMC
Explosive Supply	Fixed and Variable	Explosive Services Contractor	BMC
Concentrate Transport Services	Schedule of Rates	Transport Contractor	BMC
BMC Mobile Equipment	Lump Sump	Equipment Vendor	BMC

Source: BMC, 2025 Technical Report

14.7 Mine Development

The ABM open pit requires limited pre-strip given the proximity of the mineralisation to surface and does not need to be developed until nine months prior to the ore commissioning of the processing plant.

The open pit will initially provide borrow material for the construction of the waste and water storage facilities. A stockpile of ore must also be mined for commissioning and further areas developed to ensure continuous feed for the process plant once the operations begin to ramp-up to steady-state production levels.

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14.8 Port Facilities

Construction will ideally be carried out under a separate EPCM arrangement given the remote location of the port. A small onsite team will be based on site at the SWP facility to oversee the construction of the concentrate storage shed, as well as the interfacing of the conveyor system required for ship loading.

14.9 Production Ramp-up

The commencement of ore processing follows no-load wet commissioning and is considered the start of the operational phase of the Kudz Ze Kayah Project.

Provision was made for a production ramp-up in the Feasibility Study.

The process plant is planned to reach "nameplate" throughput capacity within nine months of commissioning, target recoveries within six to nine months of commissioning depending on the flotation circuit, and target concentrate grades within four to seven months of commissioning depending on concentrate products.

In ERM's opinion this ramp up schedule is realistic and is based on the work of experienced processing engineers.

14.10 Mine Closure

14.10.1 Reclamation and Closure Plan

The Reclamation and Closure Plan (RCP) addresses the long-term physical and chemical stability of the site, including decommissioning of the mill and other facilities, reclamation of WSF and surface disturbances, and treatment of mining impacted waters. Additionally, a programme for site management and monitoring will be implemented, both during implementation of the closure activities, and after decommissioning and reclamation measures are completed.

Three distinct closure phases, or "periods" have been identified for reclamation and closure at the end of the operational mining period (year 10): Active Closure Period (years 11 to 13), Transition Closure Period (years 14 to 26), and the Post Closure Period (years 27 to 36).

The bulk of reclamation activities, such as demolition of facilities and placement of covers, will be conducted in the Active Closure Period. Covers for the Class A and B storage facilities will be monitored for effectiveness and compliance with design criteria. The Class A and Class B WSF collection ponds will be pumped to the WTP throughout the Active Closure Period and into the Transition Closure Period, until the waste rock covers have been established and meet design criteria. The Class A and B waste storage facility collection ponds will then be passively released to the Constructed Wetland Treatment Systems if the water quality meets closure criteria. Then the WTP will be stood down unless needed to treat water for the remainder of the Transition Closure Period.

The Transition Closure Period will include the construction and commissioning of the Constructed Wetland Treatment Systems. Monitoring and site care and maintenance will continue through the remainder of the Transition Closure Period. *In situ* treatment of water in the ABM open pit will also continue through the remainder of the Transition Closure Period.

The Post Closure Period will commence when the ABM lake water spills into Geona Creek. This period will include monitoring and site care and maintenance. One to two years will be required for the passive water treatment systems to achieve performance expectations with the new water contribution from the ABM Lake. At this point, the WTP and remaining infrastructure will be demobilised/decommissioned, and site water management will be passive.

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The RCP also contains a cost estimate for implementation of the proposed closure measures as well as the long-term monitoring and maintenance of the site and is the basis for establishing the Reclamation and Closure Liability that will be required on the project.

Closure Objectives

The overall goal of the RCP is to ensure facilities are designed for closure conditions, to ensure physical and chemical stability when decommissioned with no active operation and minimum maintenance. This is achieved with clearly defined closure objectives and measures for each facility and component of the project as described below and summarised in Table 14-2.

Table 14-2: Reclamation and closure objectives

Area	Reclamation and closure objectives
Physical stability	All Mine-related structures and facilities are physically stable and performing in accordance with design. All Mine-related structures, facilities and processes can withstand severe climatic and seismic events.
Chemical stability	Release of constituents of potential interests from mine related waste materials occurs at rates that do not cause unacceptable exposure in the receiving environment.
Health and safety	Reclamation eliminates or minimises existing hazards to the health and safety of the public, workers and area wildlife by achieving conditions similar to local area features. Reclamation and closure implementation avoids or minimises adverse health and safety effects on the public, workers and wildlife.
Ecological conditions and sustainability	Reclamation and closure activities protect the aquatic, terrestrial and atmospheric environments from Mine-related degradation and restore environments that have been degraded by Mine-related activities. The Mine site supports a self-sustaining biological community that achieves land use objectives.
Land use	Lands affected by Mine-related activities (e.g., building sites, chemical and fuel storage sites, roads, sediment ponds, tailings storage facilities, and waste rock storage areas) are restored to conditions that enable and optimise productive long-term use of land by wildlife and Traditional Use by Kaska (focused primarily on hunting). Conditions are typical of surrounding areas or provide for other land uses that meet community needs, interests, and expectations through discussions and involvement from Kaska representatives from RRDC and LFN.
Aesthetics	Restoration outcomes are visually acceptable.
Socio-economic expectations	Reclamation and closure implementation avoids or minimises adverse socio-economic effects on local and Yukon communities, while maximising socio-economic benefits and meeting community and regulatory expectations.
Long-term certainty	Minimise the need for long-term operations, maintenance and monitoring after reclamation activities are complete.
Financial considerations	Minimise outstanding liability and risks after reclamation activities are complete.

Source: 2025 Technical Report

Buildings and Infrastructure

At the end of mine life, all buildings, offices etc. and associated infrastructure will be removed or demolished to return land to original wildlife land use with no active operation or maintenance. Demolition debris will be buried in approved onsite landfill areas or transported off site for disposal as required.

Remaining chemicals, reagents, and hydrocarbons will be removed from site.

The mill and ore pad areas will be excavated, where required, to remove contamination and placed in the Class A storage facility. Excavated areas will be backfilled with material from the overburden stockpile and the mill and pad areas will then be rehabilitated.

Non-essential roads will be rehabilitated. Key or essential roads will be identified to develop a weed control plan.

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Water Management Structures

Water retention and sediment control structures, and appurtenances will be decommissioned or upgraded to ensure that drainage, at and adjacent to the site, is stable in the long term. Additionally, flows will be conveyed throughout the mine footprint, and off site in a controlled, stable fashion under a reasonable range of anticipated conditions by maintaining suitable gradients to permit flow and reduce infiltration and erosion.

Facilities will be designed to minimise contact of surface flow with mine influenced soil, with modifications to flow patterns at site to achieve enhanced stability or accommodate water quality objectives. Temporary (operational) structures, including stream crossings, and diversions, such as the Fault Creek diversion, will be removed and flow paths redirected to their original alignment.

Open Pit Mine

Upon closure, the open pit will be allowed to flood as dewatering will cease, and Fault Creek will be redirected to the open pit. To minimise contaminant loading from the pit, the closure measures will include batch treatment of the pit lake by adding lime and carbon, with a contingency of wetland treatment within Geona Creek.

An engineered spillway will be constructed to control outflow from the pit lake. The safety of people and terrestrial animals in the pit area will be accomplished with catch berms around the highwall, at a setback from the crest.

Slopes and benches will be stabilised with a high factor of safety, minimising erosion and the suspension of sediments. The pit haul road will be left open for walking to allow access into the pit but blocked to vehicles.

14.10.2 Waste Storage Facilities (WSF)

During operations, waste rock will be stored in three WSF.

1) Class A WSF will contain tailings co-deposited with strongly PAG waste rock.
2) Class B WSF will contain weakly PAG waste rock.
3) Class C WSF will contain potentially acid consuming waste rock.

The Class A WSF will be constructed with an overall slope of 4H:1V to ensure long-term stability. This facility will be reclaimed with a 0.5 m layer of protective material underlaying an HDPE geomembrane. Above the liner will be a 0.5 m layer of compacted low permeability natural till cover to assist in encapsulation and preventing water infiltration and ingress of oxygen. It will be capped with a layer of a minimum of 3m of Class C material for frost protection as well as 0.15 m of topsoil for revegetation.

The Class B WSF will be constructed similarly to the Class A WSF and will be reclaimed with the same cover structure as for the Class A WSF.

The Class C WSF will be reclaimed with a minimum 30 cm layer of compacted overburden. All three facilities will be revegetated to reduce erosion and to return the area to the current wildlife habitat. The quick establishment of vegetation may require a preliminary revegetation prescription for stabilisation, with slower growing native community establishment to follow.

14.10.3 Overburden Stockpile

The overburden stockpile will provide foundation material for the Class A and Class B facilities and for construction of the water management and seepage collection ponds over the mine life. Upon closure, all remaining overburden materials will be used for WSF covers. The overburden stockpile

area will be re-contoured to stable slopes, and the area will be covered with a layer of topsoil and reseeded.

Monitoring of closure components will continue during the Active, Transition and Post Closure phases until such a time that closure objectives have been met.

14.11 ERM Opinion

ERM supports the high-level approach that has been included in the above representation of the Project Execution planning for the project and determination of the risks and risk management options. Key senior appointments will be crucial to the success of the project development and to subsequently operate the mining and processing operations throughout the LOM.

ERM also highlights the global paucity of a skilled and transient mining workforce across all disciplines and professions. While initially seen as a potential problem, there is considerable scope to develop a stable local workforce to construct and operate the project and build upon the past ten years of relationship development with local and other Canadian businesses.

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15. ENVIRONMENT, COMMUNITY AND SOCIAL RESPONSIBILITY

15.1 Environment

With acquisition of the Kudz Ze Kayah Project in 2015, the Company initiated a full suite of environmental baseline studies, to support the environmental assessment of the Kudz Ze Kayah Project as part of the YESAB review process, and a range of these studies are ongoing. This is in addition to baseline environmental studies commenced in the 1990s, some of which were ongoing until after acquisition of the project by BMC.

The environmental baseline studies undertaken to assess and evaluate various aspects of the project environment include meteorology, surface water, groundwater, wildlife, aquatic ecosystems, terrains and soils, vegetation, invasive species, air quality, acid rock drainage and metal leaching potential, and heritage resources. The products of these studies were submitted to YESAB for assessment, and they are publicly available online (https://yesabregistry.ca/). Additional environmental study material submitted to the Yukon Water Board as part of the licensing process is also publicly available online through the Waterline portal (https://www.yukonwaterboard.ca/).

Environmental studies and monitoring will be required throughout the life of the proposed mining, including post closure. The Company is committed to undertaking all requisite environmental monitoring and mitigation measures that are expected to arise from the environmental assessment and licensing processes in Yukon.

The Company currently operates in accordance with a site-specific Exploration EMP, which includes all relevant environmental conditions that are stipulated in the various existing permits and licences (i.e. Type B Water Licence, Class 3 Mining Land Use Authorisation, Tote Road Lease). When permits are amended or renewed, they are assessed and any additional or modified conditions are added to the EMP, along with operating strategies to meet required permit conditions as a minimum standard.

The relevant Acts and Regulations that pertain to the Company's current exploration activities include: the *Yukon Environmental and Socio-economic Assessment Act* for the assessment of proposed exploration activities, the territorial *Quartz Mining Act* for Exploration Land Use Permits, the *Territorial Lands (Yukon) Act* for the Tote Road Licence, and the *Waters Act* for the Type B Water Licence. A range of other minor permits are also held, including a Waste Management Permit, a Storage Tank System Permit, a Sewage Disposal System Permit, a Special Waste Permit and a Building Permit.

Recent developments are summarised in section 3.6.3.

15.2 Community Engagement

BMC's employees include local community members, and current community issues are routinely raised and discussed at internal management meetings.

In addition to meetings with First Nation Elders, Chiefs and councils, key community engagement with local First Nations communities, general stakeholders and interested parties occurs through open houses, public meetings, and individual meetings, held in the local Yukon towns of Ross River, Faro, Whitehorse, and Watson Lake.

The Company publicly discloses company notices, documents, and reports regarding the Kudz Ze Kayah Project on the System for Electronic Document Analysis and Retrieval (SEDAR+) online filing system (developed for the regulatory authorities (Canadian Securities Administrators)) for public access and transparency).

Local BMC offices have been established in Whitehorse, Ross River, and Watson Lake, providing an accessible company presence to community members. This provides the opportunity to have face to face conversations with BMC personnel, many of which are First Nation and locals within the community.

BMC hosts, participates in, supports and sponsors assorted local community events, including family BBQ's, festive celebratory luncheons, career and industry presentations, and trade shows.

ABM Mine Project site tours have been undertaken, providing opportunities for interested parties to gain firsthand knowledge and insight of the project area.

15.3 First Nations

The Company has a goal of creating a positive long-term legacy for those communities, within whose traditional territory it operates. To this end, BMC has been involved in a range of projects dedicated to increasing long-term capacity building in Kaska First Nations (Kaska) communities, including:

- The Kaska-BMC Scholarship Programme: BMC, in partnership with RRDC and Yukon University, has thus far provided scholarship funding to 191 secondary and tertiary students from Kaska communities in Yukon to a value of more than C$326,000.
- The Company has also supported vocational training opportunities, including the Yukon College Housing Maintenance Programme and Faro Housing Maintenance Programme.
- BMC has employed several tertiary graduates who participated in the BMC graduate training programme.
- The Mentor and Job Ready Programme was established in 2016 after discussion with RRDC Chief & Council and it is run by Kaska elders with funding and support from BMC. The programme is aimed at providing both opportunities and assistance for Kaska to obtain and maintain employment at the Kudz Ze Kayah site.
- In 2017, BMC and RRDC agreed on a Traditional Knowledge Protocol which describes how traditional knowledge is to be shared with and used by the Company.
- BMC and RRDC, on behalf of the Kaska Nation, are party to a SEPA, in accordance with which BMC has been operating since 2015. In 2019, BMC and RRDC on behalf of Kaska Nations signed a non-binding letter of intent to modernise the SEPA.
- BMC provided funding to RRDC through a services agreement with Dena Cho Environmental, a consultancy business owned by RRDC, for the purpose of evaluating the ABM Mine Project proposal. BMC has implemented a significant number of positive changes to the ABM Mine Project proposal as part of this process, including construction of a purpose-built industrial water treatment plant prior to the mine opening, elimination of wet tailings storage, and changes to specific management plans.
- Similarly, and in collaboration with LFN and Yukon government, BMC also provided capacity funding to LFN to assist in engagement with BMC throughout the various mine assessment phases through the Capacity Funding Agreement for Kaska-Centric Independent Peer Review of the ABM Mine Project proposal.

BMC has processes and procedures that aim to increase local business participation and prosperity, these include supplier and service provider contracts, request for proposal criteria, and procurement guidelines, some which are requirements under the existing SEPA. Subsequently, contractors are required (to the extent that they are able on a competitive, reliable, and practicable basis) to use reasonable efforts in the performance of their obligations under the Company's standard service agreement to engage available labour, professional service consultants, manufacturers, suppliers,

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and subcontractors from within the Yukon, and give the opportunity to tender or quote for services, work, materials, plant equipment and supplies locally.

BMC has an agreed Traditional Knowledge Protocol, signed with RRDC in 2017, that sets out a process for RRDC to provide BMC with Mitigation Measures informed by Traditional Knowledge and RRDC's recommendations such that BMC can avoid, mitigate, manage, or otherwise address potential effects of the ABM Mine Project on Kaska Title and Rights, Ecological Sites, Cultural Sites, values and features to RRDC within the Ross River Area.

15.4 ERM Opinion

ERM believes that all appropriate baseline investigations and monitoring programmes have been completed and the mitigation measures considered are appropriate for this type of project development. There can be no doubt the delays in financing and project commencement have benefited the environmental planning and design activities and also provided time for the Company to build additional and wider-reaching relationships in the immediate area and country.

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16. EXPLORATION

16.1 Historical Exploration

16.1.1 KZK Property Surface Exploration

The exploration at the Kudz Ze Kayah Project is summarised in various previous reports, for example ERM (2025), from which this précis is derived.

Pre-BMC

Cominco conducted a regional geochemical survey in 1977 across the Finlayson Lake area; however, the survey was wide spaced and did not reveal evidence of any VHMS deposits.

Cominco's interest in the area was reignited in 1992 when soil and silt geochemical sample results from a reconnaissance programme confirmed and expanded upon anomalous silt sample data released in the Geological Survey of Canada's regional geochemistry silt survey for NTS map sheet 105G, Open File 1648 (Hornebrooke and Friske, 1988).

In 1993, a follow-up programme within the anomalous drainage resulted in the location of a well mineralised, layered massive sulfide cobble. At the same time potential host rocks for the mineralised float were recognised. A reconnaissance transient electromagnetic (EM) geophysical survey was immediately implemented over the projected trace of the prospective units where they disappear beneath quaternary cover in the valley floor. This survey identified an EM feature representing a possible source for the mineralised float. Further magnetic, horizontal loop electromagnetic (HLEM), soil surveys and staking were completed later that fall and successfully defined a drill target.

The target was drilled in April 1994 with the first hole intersecting 22.5 m of massive sulfides in two zones. Three additional holes were drilled in April; each intersecting mineralisation over significant widths. The weighted average grade of sulfides in the discovery hole was 0.5% Cu, 2.8% Pb, 10.0% Zn, 278 g/t Ag and 2.9 g/t Au over 22.5 m. By the end of 1994, 52 drillholes totalling 8,485 m were completed along with ground and airborne geophysical surveys, detailed mapping in the vicinity of the deposit, regional and detailed exploration geochemistry, and baseline environmental sampling. In 1995, an additional 133 drillholes totalling 16,178 m were completed at the ABM deposit and on regional targets. Additional exploration soil sampling, minor geological mapping and ground geophysical surveys were completed. Geotechnical investigations, detailed engineering/mine planning, bulk metallurgical sampling, environmental monitoring and archaeological studies were well underway or completed, as well as the construction of a 24 km 'tote' road from the Robert Campbell Highway. An initial mining study was completed in July 1995.

Although majority of the work by Cominco post-dating discovery of the ABM deposit was focused on mining studies and support for permitting, additional exploration work was being undertaken to identify additional resources nearby.

From the period 1994 to 1999, Cominco completed 286.0 line km of TEM, 53.7 line km of HLEM, 35.8 line km of gravity and 45.1 line km of ground magnetic surveys in addition to the collection of 2,856 soil samples and property wide mapping at 1:20,000 scale (Cominco also completed 12,362 line km of DIGHEM airborne surveys covering the KZK Property as well as a large part of the Finlayson District outside of the property boundaries.

At the end of 1997, a total of 168 exploration drillholes and 15 metallurgical holes had been completed in the immediate ABM deposit area and another 20 drillholes were completed elsewhere on the KZK Property. This drilling campaign resulted in the identification of Fuego within a kilometre of the ABM deposit. The discovery hole (K97-181) that was drilled by Cominco targeted a HLEM/magnetic feature

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and intersected a 6.4 m thick interval of 5.15% Cu, 1.02% Pb, 5.59% Zn, 140.5 g/t Ag and 2.4 g/t Au from 12.9 m depth. A step out hole intersected a 2.1 m thick interval of 3.4% Cu, 0.9% Pb, 11.5% Zn, 99 g/t Ag, 0.7 g/t Au from 6.1 m depth, however further follow-up drilling with two 50 m step-outs along strike and a single step-out 200 m down dip did not intersect additional massive sulfide.

Cominco's 1998 exploration programme resulted in the delineation of an additional occurrence of mineralisation; GP4F, located approximately 5 km to the southeast of the ABM deposit. The prospect was first drilled in 1995 by Cominco (DDH K95-167) to follow up a HLEM/magnetic geophysical anomaly; however, the hole was completed without intersecting significant mineralisation (approximately 15–20 m above the GP4F mineralised horizon). Nine diamond holes were drilled in the 1998 programme, and all intersected the GP4F mineralised horizon.

In March 2000, Cominco announced an agreement in principle to sell the Kudz Ze Kayah and Pelly Properties to Expatriate Resources Ltd (Expatriate). This agreement resulted in Expatriate controlling most of the favourable stratigraphy in the Finlayson Lake District. Expatriate amalgamated the ABM and the neighbouring 60% owned Wolverine deposits into the "Finlayson Project". A Feasibility Study was completed by Hatch Pty Ltd. Additional drilling was completed by Expatriate on the Wolverine deposit and ground geophysical surveys (TEM, magnetics) were completed in the area south of the ABM deposit, extending their survey south of the Fuego target but no significant results were encountered.

In September 2001, Expatriate allowed the option with Teck Cominco (formed from the merger of Teck Resources and Cominco) for the KZK Project to lapse.

BMC acquired the KZK Project from Teck on 24 January 2015.

Post BMC acquisition

Following project acquisition and prior to the beginning of the 2015 field season, BMC undertook extensive data validation, particularly focused on the previously defined ABM and GP4F deposits.

Throughout 2015 and 2016, majority of the work at the KZK Property was focused on future development of the ABM Deposit but did include modest exploration programmes near the ABM Deposit with the aim to add resources to the mine plan. Elsewhere on the property, exploration built on the work completed previously by Cominco by expanding the property-wide data for developing targets. Emphasis toward developing property-wide targets has increased from 2017 onwards.

To date, two targets that incorporate modelled plates from a VTEM™ survey have been drill tested. These include the Kuril target located approximately 300 m south of and in the footwall to the ABM Zone and the Rhyolite Peak target located 1,000 m west-southwest of ABM. Two modelled VTEM™ plates are located in the Kuril target area; however, only one has been tested.

Hole K15-327 returned intercepts of:

- 2.65 m of 0.6% Cu, 1.5% Pb, 3.3% Zn and 30 g/t Ag starting at 65.3 m downhole and
- 1.1 m of 0.6% Cu, 0.2% Pb, 5.5% Zn and 30 g/t Ag starting at 83.0 m downhole.
- A second hole, hole K15-328 returned
- 0.8 m of 0.15% Cu, 0.06% Pb, 2.6% Zn and 8 g/t Ag starting at 84.7 m downhole.

In the Rhyolite Peak target area, a single hole K16-415, tested a shallow, moderately north dipping VTEM™ modelled plate and returned 0.52 m of 0.8% Cu, 0.3% Pb, 9.0% Zn and 26 g/t Ag starting at 46.5 m depth.

Numerous other significant intercepts of VHMS mineralisation have been recorded in diamond drilling on the KZK Property and these are detailed in Appendix D and discussed in Section 9.1.

16.1.2 KZK Property Geophysics

VHMS mineral deposits are well suited to geophysical exploration techniques, being dense, often magnetically distinct, within chargeable haloes and are electrically conductive and responsive to EM methods. Consequently, substantial geophysical work has been completed at the Kudz Ze Kayah Project (see Figure 16-1).

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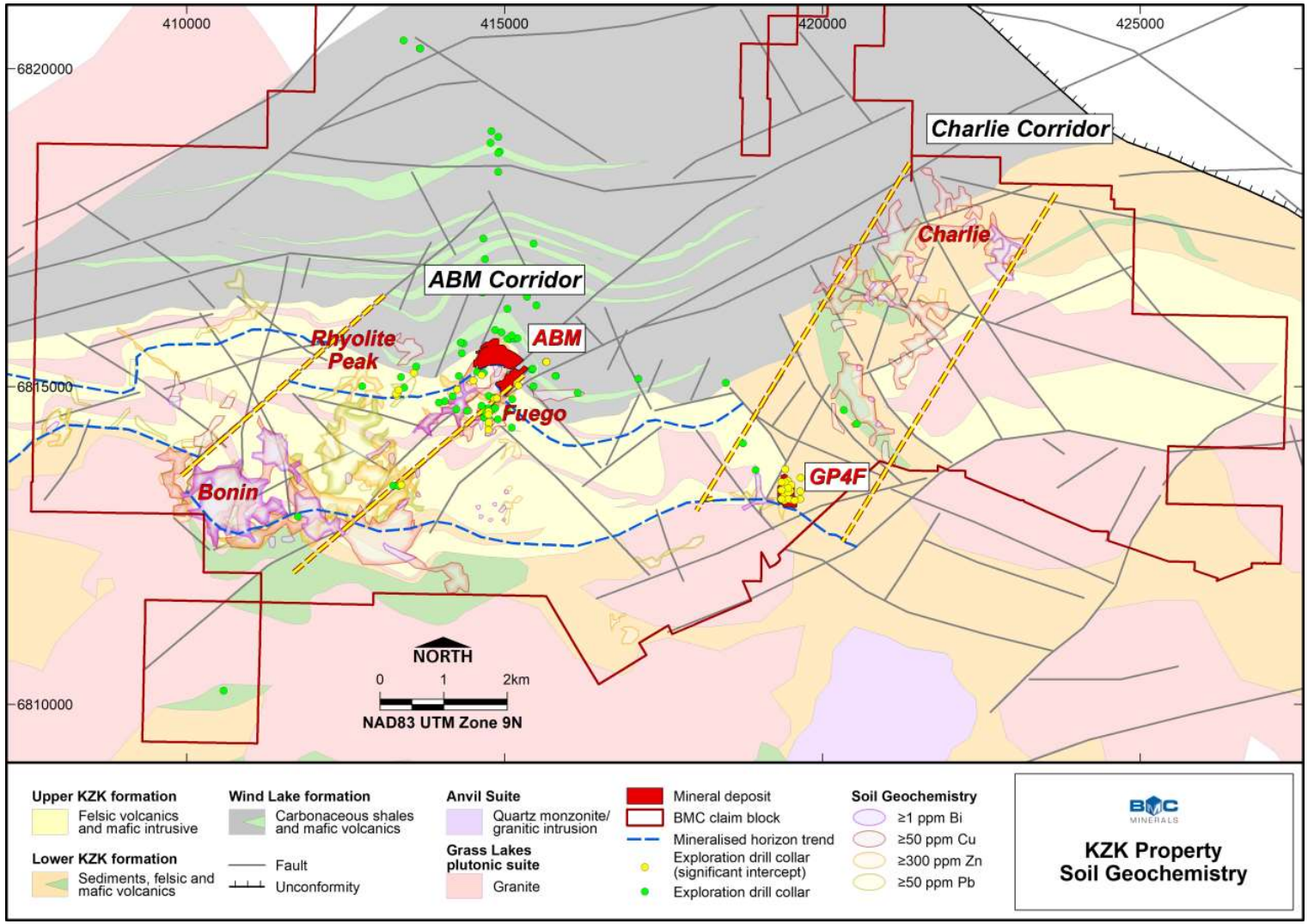


Figure 16-1: Kudz Ze Kayah Property – simplified geology highlighting prospectivity and exploration targets, with soil geochemistry and exploration drill collars shown.
Source: BMC

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VTEM™ Helicopter EM

In 2015, BMC contracted Geotech to fly a 267 line km VTEM™ (Versatile Time-Domain Electromagnetic) survey over the Kudz Ze Kayah formation on the KZK Property (Figure 16-2). The survey lines were flown at an azimuth of 015° with a traverse line spacing of 150 m and tie lines were flown perpendicular to the traverse lines at a spacing of 1,500 m. Subsequent modelling of the 2015 VTEM™ data developed 24 plates of varying size and orientation. Anomalous EM responses were returned coincident with the ABM Deposit and massive sulfide at Fuego to the south of ABM, however the other modelled plates are not necessarily the result of mineralisation and hence follow-up drilling is required to test the targets.

In 2016, BMC expanded the VTEM™ coverage by 902 line km to cover the entire KZK Property using the same survey parameters and procedures used in the 2015 survey (Figure 16-2). Results from the expanded survey indicate broad formational responses, especially for the Wind Lake formation and structurally influenced magnetic lows. Subsequent modelling of the 2016 VTEM™ data resulted in a further 45 plates for follow up and integration into property-wide target ranking, which is ongoing.

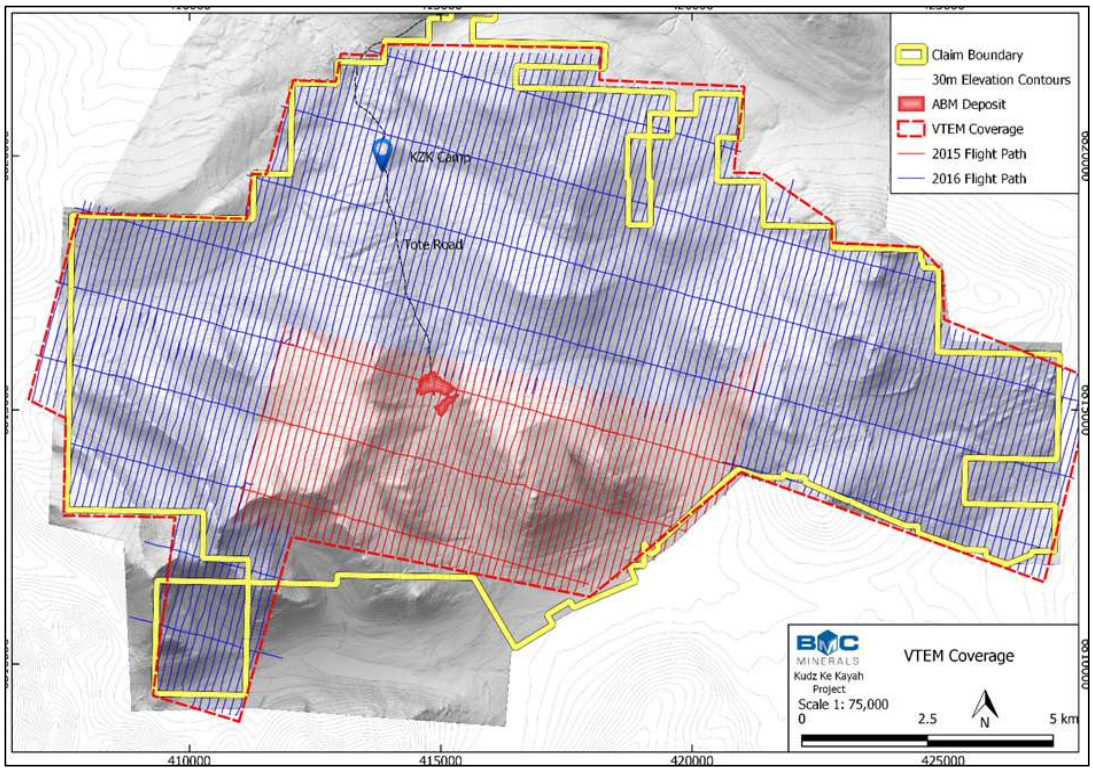


Figure 16-2: VTEM™ coverage
Source: BMC

Ground Electromagnetic

Several fixed loop transient electromagnetic (FLTEM) surveys were conducted through the project area during the 2017 and 2018 field seasons (Figure 16-3). The purpose of these surveys was to target potential mineralisation associated with defined geochemical anomalies throughout the project area, as well as stratigraphically down dip from the ABM Deposit. Transmitter loops were planned to keep potential survey locations inside the loop and positioned to have good coupling with expected

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conductor geometry. All loops were modified on the ground to account for topography, potential avalanches and other obstacles.

The 2017 survey, comprised two loops which covered an area of approximately 6 km^2. A total of 32.9 line-km and 376 stations were surveyed in a north-south line orientation at 200 m line spacing and 50–100 m station spacing.

The following year, Aurora Geoscience out of Whitehorse, YT, Canada was contracted to complete another large survey which consisted of four large loops which covered approximately 25.4 km^2 at various locations through the KZK Property. A total of 40 lines with 1,451 stations were surveyed over a two-phase programme spanning late spring and early summer 2018 (Table 16-1).

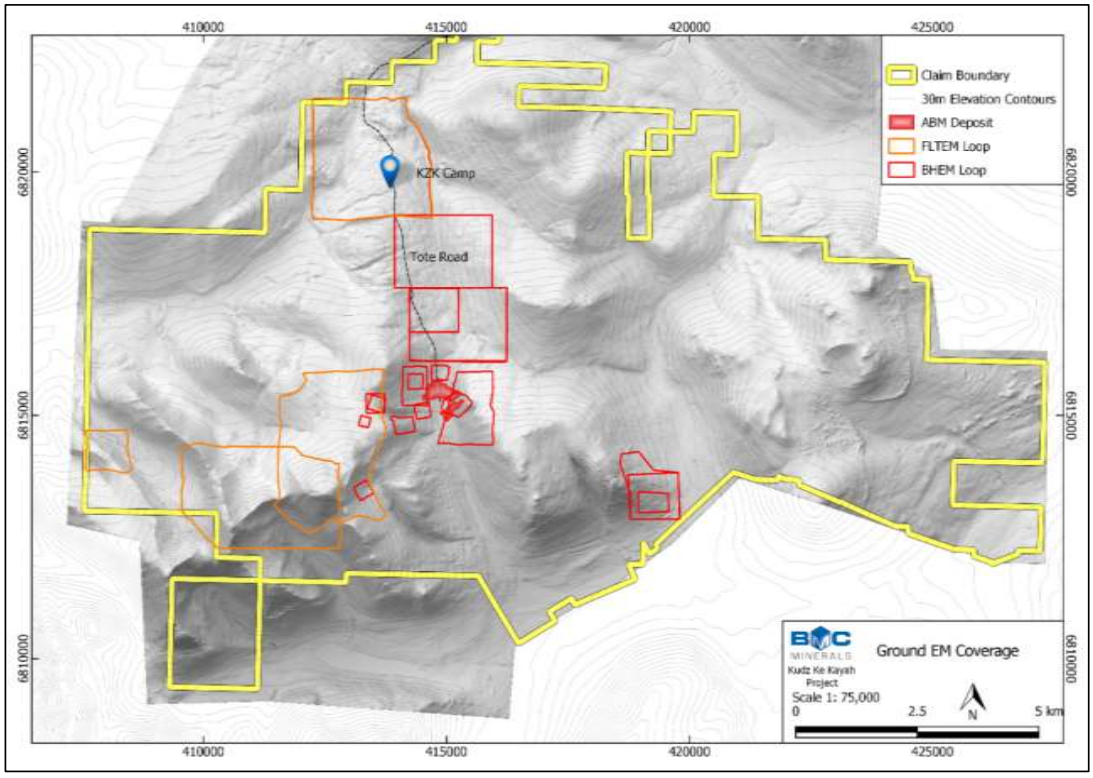


Figure 16-3: FLTEM and DHEM coverage
Source: BMC

Table 16-1: FLTEM surveys completed by BMC since 2015

Year	No. of loops	Survey coverage (km^2)	Lines – stations	Survey company
2017	2	6 km^2	10 – 376	Discovery Geoscience International
2018	4	25.4km^2	40 – 1,451	Aurora Geoscience
Total	6	31.4	50 – 1,827	

Ground Gravity

BMC completed a ground gravity survey in 2015 collecting 1,734 readings over a 6 km by 2 km area extending from the ABM Deposit to the southeast along a portion of the same prospective stratigraphy that was the focus of the VTEM™ survey. Gravity readings were collected every 50 m along lines spaced 200–300 m apart and trending at an azimuth of 015°. No significant targets derived from the gravity data were deemed worthy of immediate follow up.

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Induced Polarisation and Resistivity

An Induced Polarisation (IP) and Resistivity Survey was completed during the 2023 field season (Figure 16-4) with the aim of delineating copper-gold rich mineralisation proximal to the proposed ABM Mine.

The IP and Resistivity surveys have returned numerous elevated chargeability and conductivity responses that are interpreted to reflect potential zones of copper-rich sulfide mineralisation within the stratigraphic footwall to the ABM Deposit.

After reviewing the results alongside existing geological, geochemical, and geophysical datasets, a series of multi-component drill targets have been outlined adjacent to the ABM Deposit that are ready for testing with diamond drilling. Additional data processing will be required to fine tune the final drill programme design.

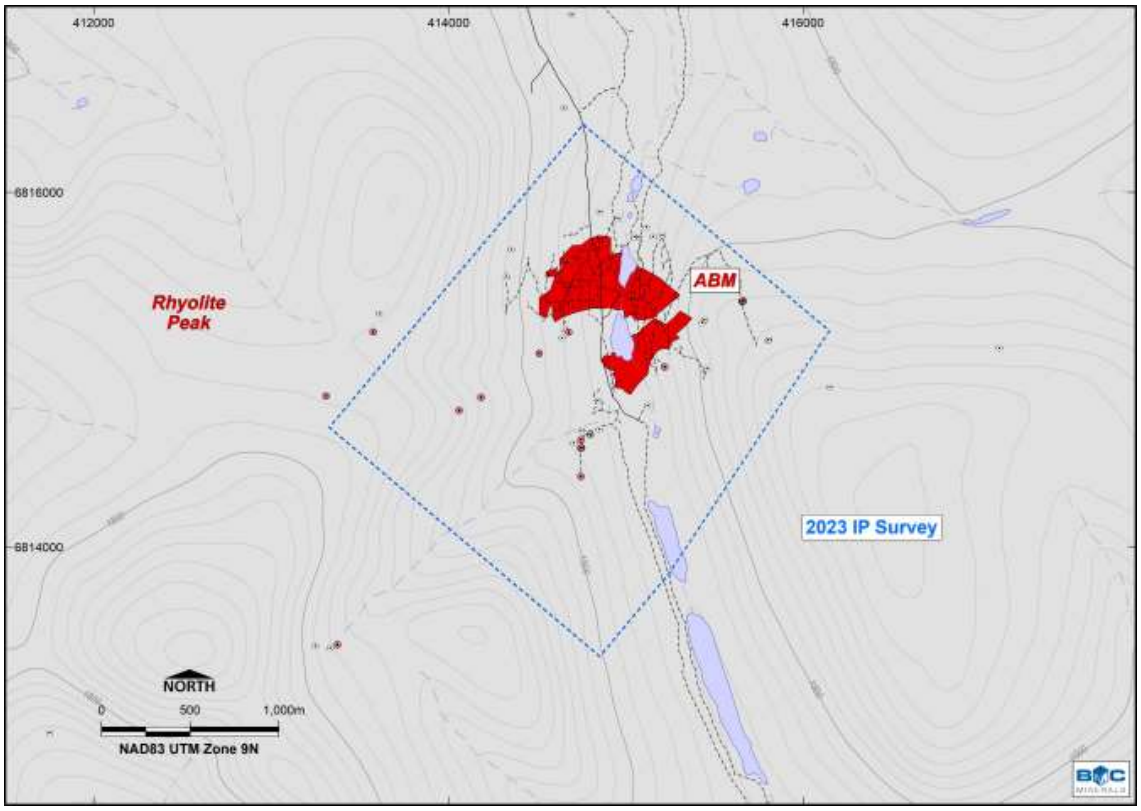


Figure 16-4: IP survey location
Source: BMC

Drill Hole Electromagnetic

Ongoing drill hole electromagnetic (DHEM) surveys have also been an integral aspect of BMC's exploration methodology throughout the KZK Property. Aurora Geoscience and Discovery Geoscience International conducted several surveys since 2015 for a total of 14,874 m of drilling in 33 holes over 17 loops (Table 16-2, Figure 16-3).

DHEM surveys used an EMIT SMART Fluxgate sensor coupled with an EMIT SMARTem24 Receiver unit and involved measurements of the X, Y, and Z components of the secondary EM field (B-field) with a base frequency of 5 Hz similar to the surface FLTEM surveys. The DHEM measurements were captured using an EMIT DigiAtlantis borehole probe which measured all three components of the primary EM

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(B) field; A (axial downhole), U (orthogonal to A and parallel to the azimuth of the drillhole), and V (orthogonal to A and U). The probe was lowered through the hole using a either a winch frame and borehole cable reel or by the wireline on the drill rig. Measurements were made at 20 m intervals throughout the hole with additional infill readings made at 5 m and 10 m increments at the operator's discretion.

Table 16-2: DHEM surveys done by BMC since 2015

Year	No. of loops	No. of holes	Metres surveyed	Survey company
2015	4	8	2,575.5	Aurora Geoscience
2016	4	11	6,790.5	Aurora Geoscience
2017	2	3	2,200	Discovery Geoscience International
2018	7	11	3,308	Aurora Geoscience
2024	3	32	9164.5	Dias Geophysical
Total	20	65	24,038.5	

Source: BMC

Seismic

One two-dimensional (2D) high-resolution seismic reflection survey line was completed on the KZK Property in 2017 by HiSeis Pty Ltd out of Perth, Western Australia. The primary objective was to image the massive sulfides as well as the regional structural architecture. The survey line stretched for approximately 10,510 m, dissecting the KZK Property in a north-south orientation. Survey configuration consisted of a 5 m receiver and 10 m source spacing produced by one 50,000 lb IVI HEMI-50 Vibroseis truck. A total of 1,051 unique source points were recorded along the line with final data referenced in NAD83 Z9 UTMs coordinates. The 2D line was processed using a conventional processing flow adapted to the appropriate site parameters, survey objectives and geology known to exist through the KZK Property. After trialling a variety of migration algorithms, the final product was a pre-stacked time migration. This product provided the most information and correctly positioned data in space and time. Depth conversion was guided by the velocity models used in seismic data processing. The downhole seismic and rock property measurements were valuable for use in checking the depth conversion due to the reflectivity present. Caution was used to ensure no artificial structure was introduced by variations within the velocity model.

The result of the survey was positive and appeared to image both the massive sulfide mineralisation at the ABM Deposit as well as multiple geologic structures in the area.

2025 FLTEM

A fixed-loop electromagnetic (FLTEM) SQUID survey was carried out at BMC Minerals' Kudz Ze Kayah base metal project, targeting areas near the ABM base metal deposit (Figure 16-5). Conducted by Dias Geophysical in 2025, the survey covered 482 stations collecting 22.3 line-kilometres of FLTEM data across three fixed loops at the Rhyolite Peak, ABM West, and Fuego prospects.

The survey aimed to detect and map bedrock conductors associated with base metal massive sulfide mineralisation.

The FLTEM survey identified four significant anomalies. Two which, ABMW- 1 and RP-1, were identified as possibly due to sulfide accumulations. ABMW-1, located near the western edge of the known ABM deposit, was modelled as two shallow to moderately deep (40–70 m) conductors with high conductivity (1650–2250 S), steeply dipping SE-SSE, likely linked to massive sulfide mineralisation. RP-1 is a poorly define, unmodelled response, suggestive of a flat-lying conductor. The other strong responses are some of which are potentially attributable to casing in historical drill holes or system noise.

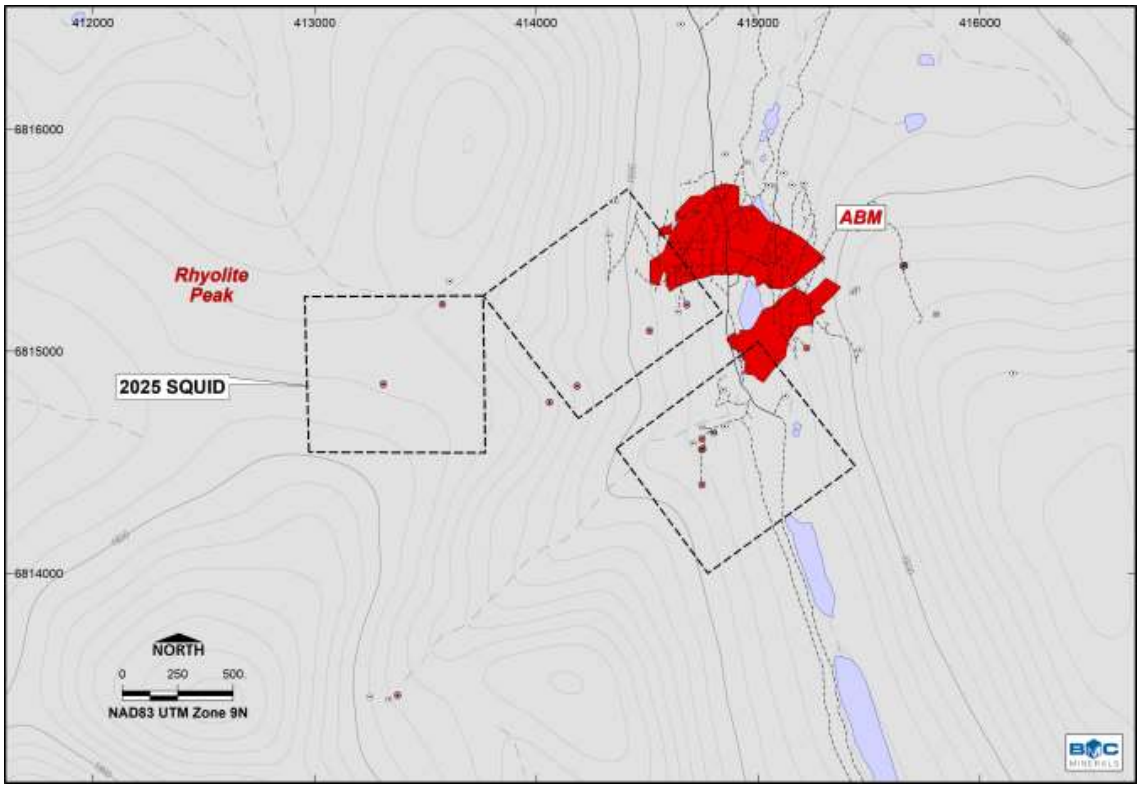


Figure 16-5: Location of 2025 SQUID survey
Source: BMC

Table 16-3 summarises the significant anomalies identified in the FLTEM survey.

Table 16-3: Significant FLTEM anomaly summary

Anomaly ID	Prospect	Priority	Modelled	Comments	Possible Source
RP-1	Rhyolite Peak	Moderate	No	Poorly defined late time FLTEM response in Z and X components.	Flat lying bedrock conductor.
ABMW-1	ABM West	High	Yes	Partially defined early to late-time FLTEM response at the northeastern margin of the ABM West survey.	Massive Sulfide
FU-1	Fuego	Moderate	yes	Narrow, early to late-time FLTEM response	Drill hole casing?.
FU-2	Fuego	Low	No	Early to late-time peak in X and Y component FLTEM response.	Drill hole casing?.
FU-3	Fuego	Low	No	Late-time peak in the Z-component FLTEM response	EM system noise.

Source: BMC

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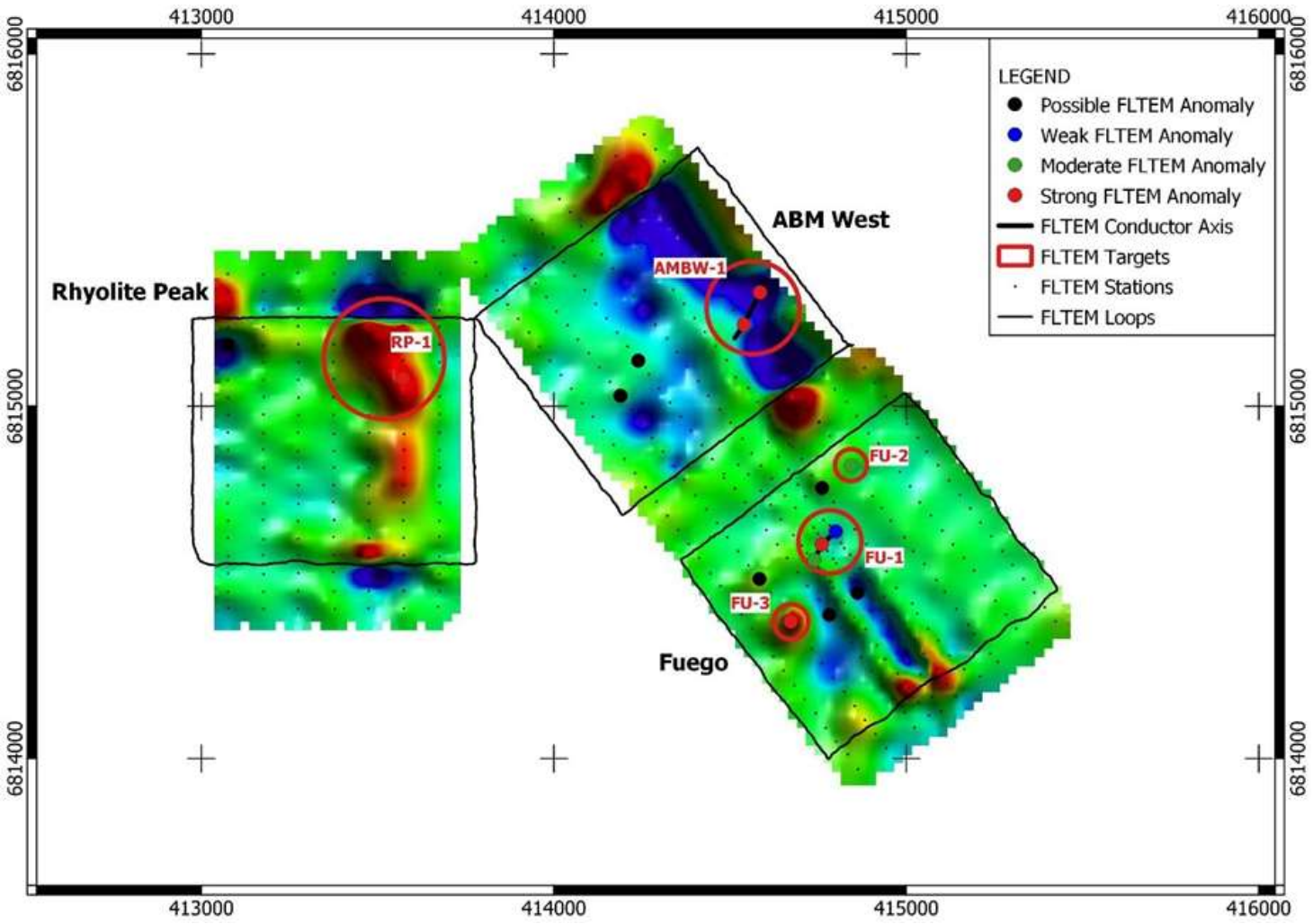


Figure 16-6: FLTEM anomaly locations on a channel 30 Z component image. Source: BMC

16.1.3 Soil Geochemistry

A total of 6,289 B-horizon soils samples have been collected throughout the KZK Property by the BMC since 2017. The soil grid covers approximately 62.45 km with sample spacing at 100 m by 100 m for most of the grid. The spacing was reduced to 50 m by 50 m within infill regions where anomalism was identified either from historical surveys or in camp analyses using a portable XRF handheld analyser. The soil grid covered the prospective stratigraphy of the Kudz Ze Kayah formation within the southern half of the KZK Property (Figure 16-7).

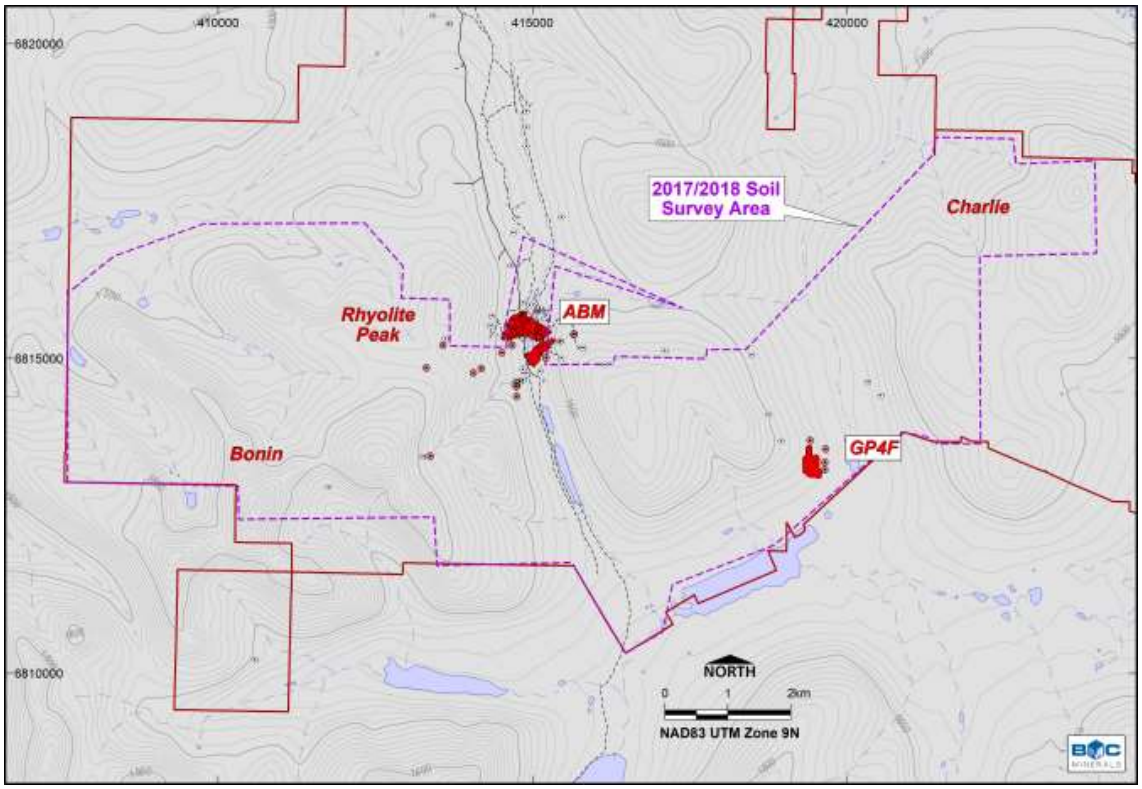


Figure 16-7: Location of soil sampling at the KZK Property.
Source: BMC

Review of the soil analysis data, in conjunction with geological and geophysical datasets, indicates that that there are several elemental associations (Figure 16-8) and the lower thresholds for what is considered anomalous are: Bi – 1 ppm, Cu – 50 ppm, Pb – 50 ppm, Zn – 300 ppm, As – 25 ppm, Sb - 0.8 ppm, and Ag - 0.6 ppm (Figure 16-1).

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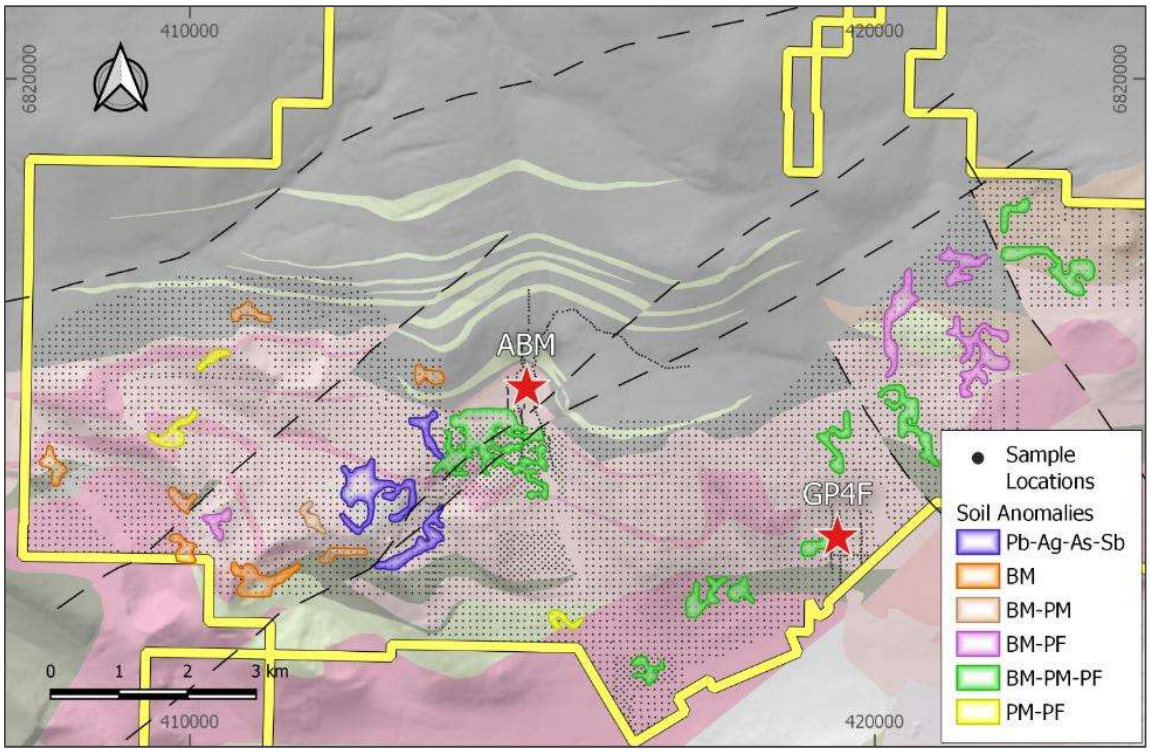


Figure 16-8: Soil geochemistry samples from the Kudz Ze Kayah Property and discrete multi-point anomalies
Soil anomalies are divided into several associations: Base metal (BM: Cu, Pb and Zn), precious metals (PM; Au and Ag), and pathfinder elements (PF; As, Bi, Sb, Sn, Tl and W).

16.1.4 KZK Property Drilling

Drilling has been undertaken on two prospects on the KZK Property – the ABM Deposit and GP4F deposit. A Mineral Resource has been reported for the ABM Deposit. An Exploration Target has been qualified for the GP4F deposit.

Historical (pre-2015)

The ABM Deposit and GP4F deposit have been sampled using diamond drilling only. Drilling prior to 2015 was completed by Cominco and subsequently by BMC. Core drilling completed by Cominco in 1994 and 1995 predominantly targeted the ABM Deposit was carried out by DJ Drilling of Surrey, British Columbia. In 1994, helicopter movable Boyles 25A and Longyear LF70 rigs were used, whilst in 1995 two Longyear 38 drill rigs were operating. Drilling in 1997 and 1998 appears to have also been conducted by DJ Drilling, although details of the drill rigs have not yet been located. The majority of drilling conducted in 1998 was targeted at GP4F. Historical diamond drilling by Cominco is NQ size core, generally sampled at 1.5 m lengths across all drilling programmes.

BMC (2015 Onwards)

Since acquisition, BMC has completed a total of 372 core holes for 65,527 m of drilling, of which 79 drill holes for 22,767 m were for the purpose of exploration. The 2015 exploration programme undertaken by BMC at the ABM Deposit was an outstanding success, highlighted by the discovery of the Krakatoa VHMS Zone in the fault offset block southeast of the ABM Zone. This discovery, coupled with additional mineralisation identified in extension drilling at the ABM Zone and confirmation of historical results, resulted in a significant (47%) increase in reported tonnage for the deposit.

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Additional drilling during the 2016 field season, particularly at the Krakatoa Zone, resulted in an improved understanding of the controls on mineralisation despite the slight reduction in reported tonnage. The increased drilling information and improved confidence allowed 18.3 Mt or 96% of the ABM Zone Mineral Resource to be classified in the Indicated category.

The 2015 and 2016 exploration programmes undertaken by BMC at the GP4F deposit were successful in expanding the known mineralised horizon and resulted in an improved understanding of the controls on mineralisation.

The 2018 drilling programme was aimed at testing a small number of prospects defined by geophysical and geochemical anomalism in prospective host rocks. This was followed up in 2024 with a more intensive drilling programme. Both programmes were successful, returning multiple high grade polymetallic sulphide intersections, the details of which are discussed in the following sections of this report.

16.2 Exploration Potential

Since 2015, the Company has compiled both company and publicly available data both within the properties owned by BMC and in the surrounding region within which the Project is located. Aside from the work completed to define the Mineral Resource estimates and Feasibility Studies, BMC has, since January 2015, also undertaken field programmes aimed at generating and testing prospective targets that may lead to the extension of or discovery of additional VHMS deposits.

The Kudz Ze Kayah Project contains economically significant polymetallic VHMS deposits, with additional prospects / deposits located in the surrounding district. ERM considers the Kudz Ze Kayah Project holds considerable potential for the discovery of further VHMS deposits and extensions to known mineralisation.

To quantify the potential, BMC has completed considerable surface exploration (comprising core drilling, mapping, soil and rock chip sampling, aeromagnetics, airborne EM, and petrology), supported by historical drilling to estimate Exploration Targets for the GP4F, Kona, Wolf and Jackman Prospects, as shown below (detail of the Explorations Targets are provided in the following sections).

Table 16-4: GP4F Prospect Exploration Target

Tonnes Lower Mt	Tonnes Higher Mt	Cu Lower %	Cu Higher %	Pb Lower %	Pb Higher %	Zn Lower %	Zn Higher %	Au Lower g/t	Au Higher g/t	Ag Lower g/t	Ag Higher g/t
1.7	2.6	0.18	0.24	2.3	3.1	4.8	6.4	1.3	1.7	66	88

Source: CSA Global

Table 16-5: Kona Deposit Exploration Target

Tonnes Lower Mt	Tonnes Higher Mt	Cu Lower %	Cu Higher %	Au Lower g/t	Au Higher g/t	Ag Lower g/t	Ag Higher g/t
3.0	5.0	1.5	1.8	0.5	0.8	3	5

Source: BMC

Table 16-6: Wolf Deposit Exploration Target

Tonnes Lower Mt	Tonnes Higher Mt	Zn Lower %	Zn Higher %	Pb Lower g/t	Pb Higher g/t	Ag Lower g/t	Ag Higher g/t
2.7	3.3	4.4	5.4	1.3	1.5	38	46

Source: BMC

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Table 16-7: Jackman Prospect Exploration Target

Tonnes Lower Mt	Tonnes Higher Mt	Zn Lower %	Zn Higher %	Cu Lower %	Cu Higher %	Pb Lower g/t	Pb Higher g/t	Au Higher g/t	Au Lower g/t	Ag Lower g/t	Ag Higher g/t
2.5	5.0	10.0	12.0	1.0	1.2	1.3	1.6	1.4	1.7	240	360

Source: BMC

***Note**: The potential quantity and grade of the Exploration Targets is conceptual in nature. There has been insufficient exploration to estimate a Mineral Resource, and it is uncertain if future exploration will result in an estimation of a Mineral Resource.*

16.2.1 Exploration targeting – KZK Property

The KZK Property has received the bulk of BMC's exploration and development expenditure to date, and this focus is likely to continue with the proposed construction of a mineral processing facility at ABM combined with the excellent prospectivity of the geology.

Two distinct mineralisation horizons (or mineralisation event timelines) have been interpreted as trending along strike east to west from both the ABM and GP4F prospects (Figure 16-1). These are favoured positions for potential discovery of additional stratiform polymetallic massive sulfide lenses analogous to the ABM Deposit, such as identified in drilling at the Rhyolite Peak mineralisation located approximately 1,100 m along strike to the west of the ABM Deposit.

In addition to this, two corridors of particular interest have been identified that transect the local stratigraphy, termed here the "ABM Corridor" and the "Charlie Corridor" (Figure 16-1), within which the ABM Deposit and GP4F Prospect respectively are also located.

The ABM Corridor (Figure 16-10) covers a trend ≈5 km long and ≈2 km wide that cuts across the stratigraphy of the Kudz Ze Kayah formation and extends south, where it is truncated by a thick post-mineralisation intrusion of the Grass Lakes Plutonic Suite at the southern edge of the KZK Property.

Mineralisation identified at both the Fuego and Kuril Prospects appears to parallel the trend of the ABM Corridor, indicating a probable syngenetic structural control on mineralisation.

The ABM Corridor is interpreted to be a synvolcanic graben and, although many currently defined targets within the KZK Property are located within the graben, the ABM Mineralised Horizon (Figure 16-1) still represents a potential target trend for ABM age mineralisation along strike. This is also the case for the projected GP4F Mineralised Horizon (Figure 16-1). However, with the revised bedrock interpretation, the prospective strike may now be restricted to areas west of GP4F.

A degree of topographic relief can almost certainly be attributed to the ancient seafloor at a pre- to syn-mineralisation timing relative to emplacement of the ABM Deposit. Seafloor topography may be affected by varying degrees of synvolcanic faulting, graben formation and the development of volcanic edifices. In this context, simply projecting the ABM mineralised position in a linear fashion to the southwest along the graben may not provide a true reflection of the actual location of the mineralised horizon (or timeline).

A mineralising hydrothermal system within a local topographic low, such as a graben or caldera, may have periods where seafloor emplacement of lithic material is relatively low, and a hydrothermal system can develop a sulfide deposit. This may be in turn be interspersed with periods where emplacement of lithic material is high due to volcanism, the collapse of graben or caldera walls, and/or gravitational emplacement of lithic material derived from more distal sources. This material may dilute or bury the hydrothermal system to the extent that a sulfide deposit cannot develop.

Modern seafloor sulfide mineralisation along the Kermadec Arc is typically associated with calderas developed as a component of submarine volcanoes that display significant relief relative to the seafloor (Figure 16-9). The main caldera developed at the Brothers volcano, for example, is ≈3 km in diameter and is the locus for a modern hydrothermal system emplacing polymetallic sulfide mineralisation. Periodic input of lithological material can be seen to be part of caldera development at the Brothers volcano and episodic volcanism has been described in relation to felsic volcanic host units of the ABM Deposit and how mineralisation was emplaced during periods of relative volcanic quiescence.

If a hydrothermal system endures over an extended period, then a series of stacked sulfide lenses may develop within a large topographic low such as a graben. In this context, the ≈1.4 km by ≈1.4 km coincident Pb-As-Hg-Sb-Ag-Mo response (Target Area B Table 16-8, Figure 16-10) may reflect a low temperature component of the hydrothermal system located lateral to adjacent high-temperature mineralisation as inferred from the copper-bismuth in soil response to the south, or alternatively it may reflect a low temperature halo above of a buried ore deposit that is potentially part of a stacked sulfide lens system.

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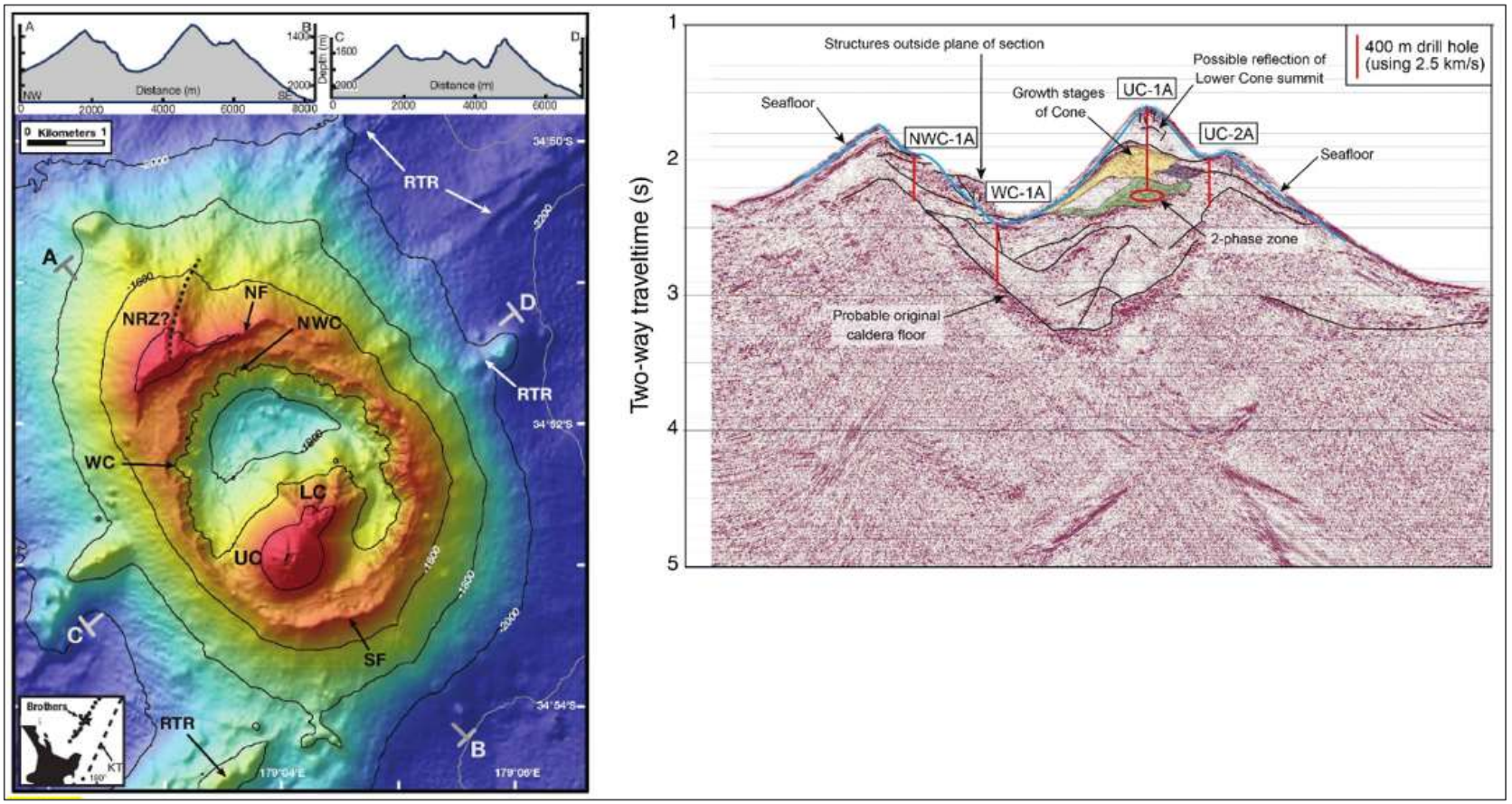


Figure 16-9: Brothers volcano bathymetry (left); Brothers Volcano seismic profile showing progressive caldera development (right)
Source: de Ronde et al., 2019[15].

[15] Noting that these authors have not consented to the use of their technical report in this Report, but it is included as per ASIC RG55 and Instrument 2016/72.

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Table 16-8: Exploration Prospects and target areas of interest – ABM Corridor

Target Areas/ Prospects	Description
Target Area A	In the context of Cu-Bi in soil responses proximal to the ABM Deposit and their relationship to Cu-rich mineralisation returned in drilling, other areas of coincident Cu-Bi in soil are also considered to be of significant interest. A ≈1.4 km by 1.2 km Bi in soil response is located at the southern end of ABM Corridor, west of the UTEM™ survey coverage, within a ≈5 km long Cu in soil response that broadly parallels the east-west trending local stratigraphy. In the context that this target area may reflect the intersection of the northeast trending graben with a large-scale east-west trending synvolcanic structure, now occupied by a Grass Lakes Plutonic Suite intrusion, this area could have been the locus for large-scale hydrothermal fluid conduit. The elevated Bi in soil response in this area corresponds spatially to a change in stratigraphy where the lower Kudz Ze Kayah formation appears to be largely absent at this location (or hydrothermally altered and therefore misidentified), and bedrock magnetic trends in the same area are disrupted in comparison to a more consistent east-west strike trend east of the graben. A scout hole, targeting an area of hydrothermally altered bedrock and anomalous rock chips at the edge of a coincident Pb-Zn-As-Sb-Hg-Cu-Mo in soil response, ≈200 m west of a ≈800 m long northeast trending line of moderate to strong UTEM™ responses returned – 12.6 m at 2.0% Zn, 0.8% Pb, 24 g/t Ag from 20.3 m. This lies along the projected Fuego mineralised trend.
Target Area B	An ≈1.4 km by 1.4 km coincident Pb-As-Hg-Sb-Ag-Mo in soil response, centred ≈2.5 km southwest of the ABM Deposit that has its southern margin coincident with a topographic high that slopes to the north. The element suite in this area is similar to the response in soil in target area E, where in scout drilling encountered massive sulfide at a shallow depth. The anomalous response in soil, which appears somewhat circular in shape, overlies a circular pattern in the aeromagnetic data that is ≈1.2 km in diameter. Although highly speculative, a potential interpretation for the magnetic pattern is that it could reflect the presence of a caldera.
Target Areas C & D	These target areas comprise anomalous multi-element responses in soil of modest scale that warrant further investigation. However, without additional targeting vectors they are currently considered to be of lower priority. Both target areas lie outside the UTEM™ survey coverage. The soil response in area D (the Jefferson Prospect) is coincident with a highly conductive VTEM™ response ≈500 m by 65 m in extent, striking to the northeast broadly parallel to stratigraphy and dipping to the northwest.
Target Area E	The target corresponds to the Rhyolite Peak Prospect (Figure 16-10). Scout holes drilled in 2016 and 2018 intersected base metal-rich massive sulfide at Rhyolite Peak, including K18-484, targeted at a weak single point VTEM™ response and drilled adjacent to a ≈300 m by 200 m coincident Pb-As-Hg-Sb-Ag in soil response. This hole and others completed in 2024 have identified a shallow dipping zone of high-grade massive sulfide mineralisation (refer to results in Appendix E). A 2025 SQUID EM survey returned an anomalous EM response ≈200 m to the east of known mineralisation (Figure 16-10) and To the immediate north, K16-415 intersected massive sulfide just below the base of the Wind Lake formation and returned – 0.5 m at 9.0% Zn, 0.8% Cu, 126 g/t Ag, from 46.5.5 m
Target Area F & G	The 2023 IP and Resistivity survey covered the "Feeder Zone" Prospect abutting the southern edge of the ABM Deposit. An ≈1.2 km long northeast trending Cu-Bi in soil response projects directly into high-temperature Cu-rich zones identified the western end of the ABM Deposit. This corresponds to the Kuril Prospect, where base metal sulfides have been returned in diamond drilling. A 2025 SQUID EM survey also identified an untested EM response beneath the western end of the ABM deposit and located along the Kuril trend. The response is modelled as a steeply east-southeast dipping conductor in an area currently untested by drilling. A second northeast trending Cu-Bi in soil response, located proximal to the Fault Creek fault, is associated with multiple base metal sulfide drill intercepts at the Fuego Prospect, interpreted to comprise mineralisation emplaced within a syn-mineralisation fault.
Target Area H	The ABM Corridor is interpreted to reflect a synvolcanic graben within which the host rocks and the ABM mineralisation were emplaced. There is sufficient evidence to indicate that the graben and related mineralisation extend beneath the Wind Lake formation to the north and northeast of the ABM Deposit. The ABM "Feeder Zone" trend, recognised at surface by a Cu-Bi in soil response, aligns with zones of maximum ore thickness, and with high-temperature indicators within and adjacent to the massive sulfide including elevated Cu:Pb ratio in ore, magnetite-pyrrhotite-rich ore zones and increased chlorite-pyrrhotite-chalcopyrite content in the footwall to the ore. The Feeder Zone trend, especially at the western margin of the ABM Deposit, is likely to extend down plunge from ABM where there exists potential for additional massive sulfide lenses not impacted by weathering or erosion. The Krakatoa Zone has not been closed off down dip by drilling. The deepest massive sulphide intercept at Krakatoa, encountered in K16-369, returning 7.9 m (5.0 m true width) @ 1.5% Cu, 0.5% Pb, 12.2% Zn, 102g/t Ag, 0.8g/t Au, and it is located approximately 68 m directly down-dip from K16-363 which returned 20.8m (14.3 m true width) @ 0.3% Cu, 3.7% Pb, 8.6% Zn, 218g/t Ag, 2.0g/t Au. There is no drilling down-dip of this particular massive sulfide trend. A review of drill holes adjacent to ABM has also resulted in the identification of sulfide mineralisation in drill hole K16-368 which encountered intervals of disseminated and semi-massive sulfide mineralisation returning

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Target Areas/ Prospects	Description
	4.7 m at 1.0% Cu, 2.5% Pb, 6.2% Zn, 87 g/t Ag, 0.9 g/t Au from 100.7 m. This hole is located to the east of Krakatoa and, importantly, to the east of the East fault as mapped in drilling. This may indicate the potential for additional mineralisation to the east of Krakatoa that has not yet been tested. It is currently described as a component of the Fuego Prospect. A coincident magnetic high and down-hole EM conductor has been modelled ≈230 m to the northwest of the ABM Deposit. The moderate off-hole conductor is adjacent to K18-482, which drilled strong sericite alteration and minor sphalerite stringer mineralisation at about the same stratigraphic position as the ABM Deposit.
Target Area I	Centred ≈2.5 km west of the ABM Deposit, immediately east of the westernmost bounding fault of the interpreted graben, is a ≈1 km by ≈1 km UTEM™ response located at the western extent of the UTEM™ survey area. A similar response was identified in the 2025 SQUID EM survey. The UTEM™ response has been described as a "laterally extensive conductive sheet" with modelling indicating a vertical depth range of ≈400 m to > 800 metres. and a dip of ≈45 degrees to the east. The westernmost extent of UTEM™ response is unknown as the survey coverage did not extend further west. The VTEM™ survey data does not show any conductive response where the UTEM™ conductor would project up-dip to the west of the graben. The UTEM™ response was originally dismissed as not being a VHMS-type response. Based on the stratigraphy as it is currently understood, there are no obvious units within the Kudz Ze Kayah formation that display a conductive EM response (in DIGHEM, VTEM™ or UTEM™), other than occurrences of sulfide mineralisation. It is possible that this position reflects elements of the lower Kudz Ze Kayah formation at depth. As the modelled response lies within the interpreted graben further investigation of this feature is recommended.

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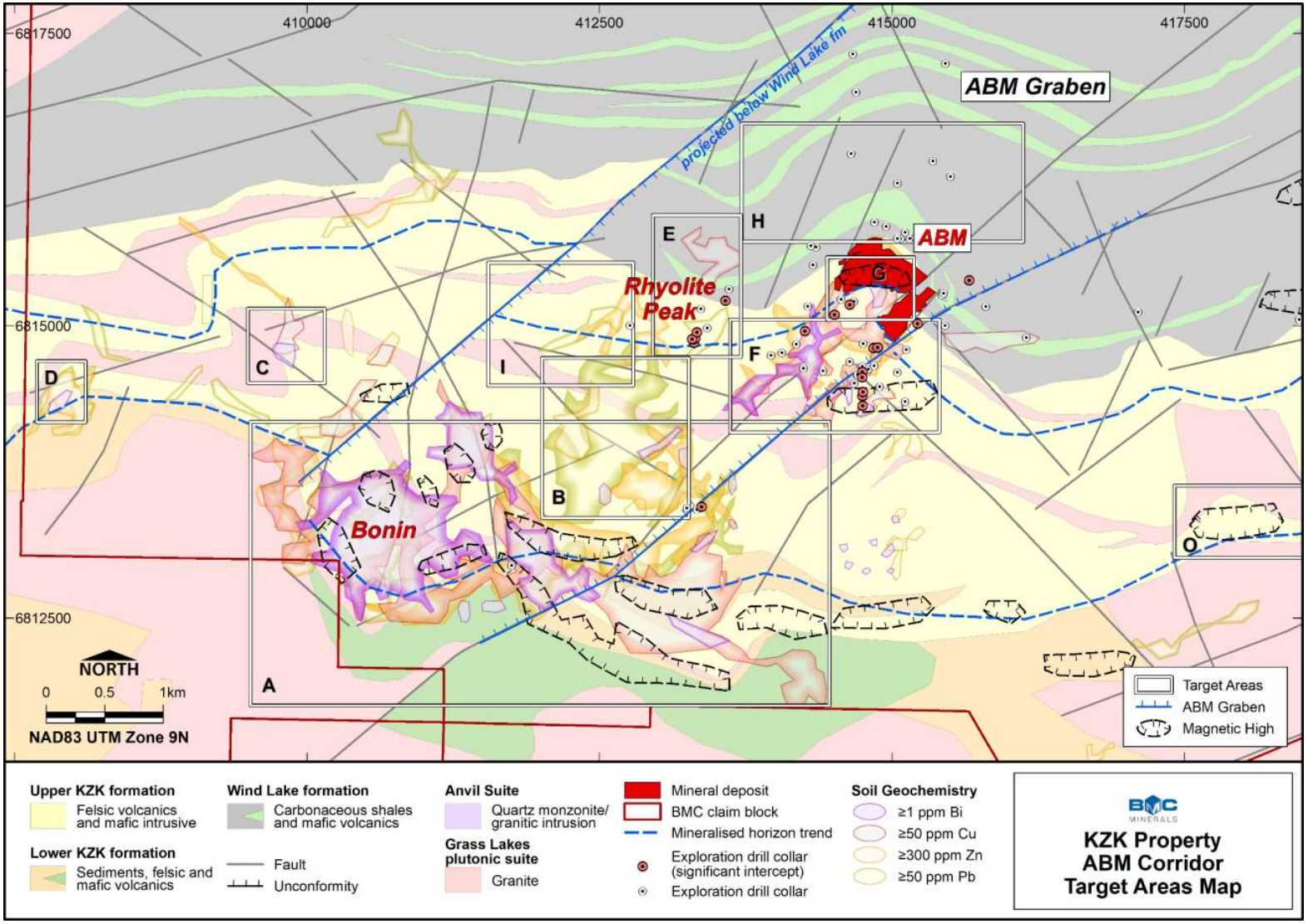


Figure 16-10: ABM Corridor and target areas (A to I)/ Source: BMC

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The Fuego Prospect is located immediately south and east of the ABM Deposit (Figure 16-10) and comprises a >1,000 m long corridor defined by anomalous surface geochemistry, a series of anomalous EM responses and several high-grade massive sulfide intercepts in diamond drilling. The Fuego trend is coincident with the Fault Creek Fault and mineralisation is interpreted to have been emplaced within a syngenetic fault corridor that transgressed the stratigraphy, acting as a hydrothermal fluid conduit, prior to later being disrupted by reactivation of the Fault Creek fault during Cretaceous and Palaeogene deformation events.

High-grade copper and zinc mineralisation occurs as stringer and massive sulfide in drilling at several locations along the Fuego trend (Figure 16-10). The true width and orientation of the mineralisation has not yet been resolved and previous drill coverage along the Fuego trend is wide spaced and, in many cases, not drilled at an orientation that would have effectively tested the mineralised corridor.

Significant drill intercepts along the Fuego trend (Figure 16-11) include:

- K97-181: 6.4 m at 5.2% Cu, 1.0% Pb, 5.6% Zn, 141 g/t Ag, 2.4 g/t Au from 12.9 m.
- K97-183: 2.1 m at 3.4% Cu, 0.9% Pb, 11.5% Zn, 99 g/t Ag, 0.7 g/t Au from 6.1 m.
- K16-368: 4.7 m at 1.0% Cu, 2.5% Pb, 6.2% Zn, 87 g/t Ag, 0.9 g/t Au from 100.7 m.
- K24-527: 16.0 m at 3.5% Cu, 0.5% Pb, 3.2% Zn, 88 g/t Ag, 0.8 g/t Au from 37.5 m.
- K24-551: 3.9 m at 3.5% Cu, 0.1% Pb, 0.3% Zn, 74 g/t Ag, 0.8 g/t Au from 33.7 m, and 2.6 m at 0.3% Cu, 1.8g/t Pb, 6.4% Zn, 63g/t Ag, 0.3 g/t Au from 108.6 m.
- K24-555: 3.8 m at 0.3% Cu, 3.9% Pb, 6.4% Zn, 168 g/t Ag, 0.6 g/t Au from 61.2 m, and 2.4 m at 0.4% Cu, 0.8g/t Pb, 9.9% Zn, 67g/t Ag, 0.1 g/t Au from 80.6 m.
- K24-556: 2.3 m at 0.2% Cu, 1.4% Pb, 8.2% Zn, 125 g/t Ag, 1.8 g/t Au from 26.8 m.

Approximately 1,700 m to the southwest of drill hole K97-183 and along the Fuego trend, drill hole K18-480 intersected an interval comprising bands of semi-massive sphalerite within carbonaceous sediments that returned 12.6 m at 0.1% Cu, 0.8% Pb, 2.0% Zn, 24 g/t Ag from 33.0 m. The hole then intersected 180 m of strong sericite-pyrite alteration.

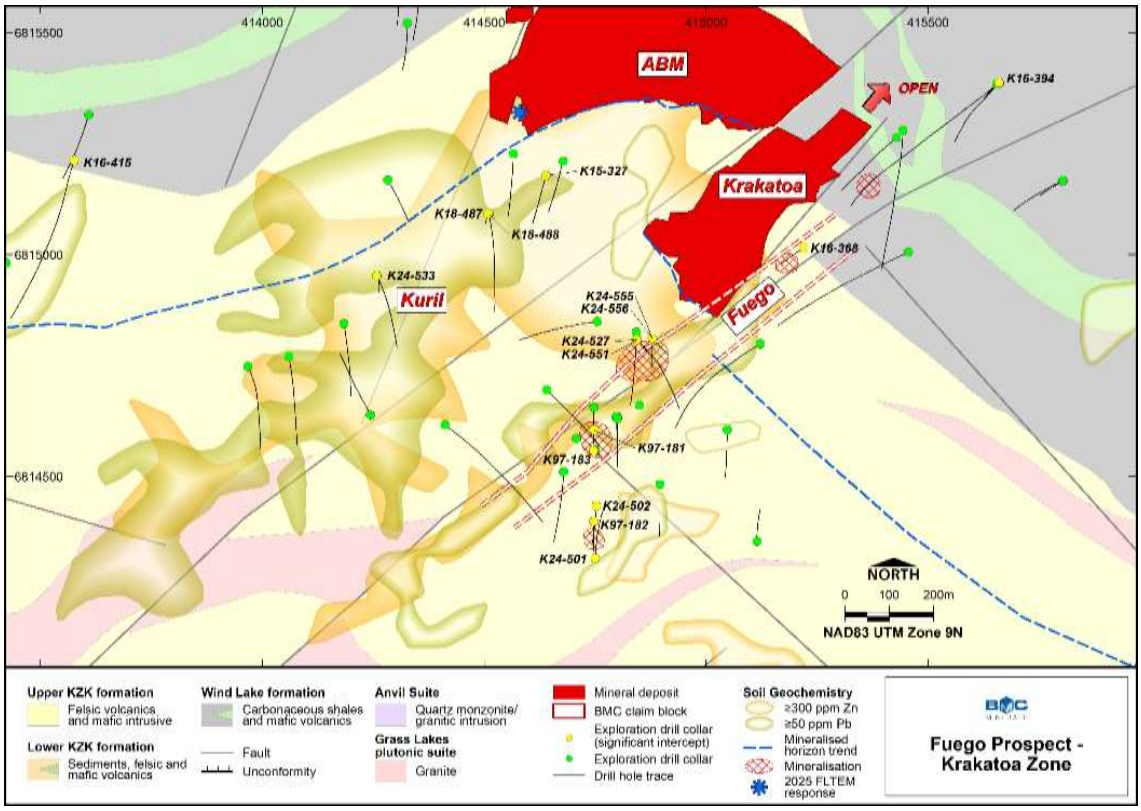


Figure 16-11: Map of the Fuego and Kuril prospects and exploration drillholes with material intercepts.
Source: BMC

The Rhyolite Peak Prospect is located ≈1,100 m west of the ABM Deposit. It comprises a shallow north dipping zone of high-grade mineralisation interpreted to be lying along strike of, and on the same mineralised horizon as, the ABM Deposit (Figure 16-12). The massive sulfide mineralisation is approximately 2.4 m to 4.5 m in true thickness, dips shallowly to the north, and currently remains open both along strike and down dip.

2018 drilling targeted coincident surface geochemical and EM anomalism along the projected position of the ABM Deposit. Drilling has returned several high-grade intercepts, including:

- K18-484: 3.8 m at 0.4% Cu, 1.3% Pb, 5.1% Zn, 128 g/t Ag and 0.8 g/t Au from 7.5 m;
- K24-544: 4.5 m at 0.3% Cu, 2.5% Pb, 8.7% Zn, 291g/t Ag, 1.7g/t Au from 20.1 m;
- K24-545: 2.4 m at 0.5% Cu, 2.4% Pb, 6.7% Zn, 595g/t Ag, 3.2g/t Au from 18.3 m;
- K24-547: 3.7 m at 0.3% Cu, 2.3% Pb, 6.1% Zn, 226g/t Ag, 1.1g/t Au from 43.4 m.

A SQUID FLTEM survey completed in 2025 identified an anomalous EM response located approximately 200 m east of the mineralised drill intercepts at Rhyolite Peak (Figure 16-6). The response is modelled as a flat-lying bedrock conductor in an area currently untested by drilling.

Immediately to the north the Rhyolite Peak Prospect (Figure 16-12), another narrow zone of massive sulfide mineralisation was encountered in drilling a short distance below the stratigraphic contact between the Kudz Ze Kayah formation and the overlying Wind Lake formation. This is a higher position in the stratigraphy than the Rhyolite Peak mineralisation. This drill intercept returned:

- K16-415: 0.5 m at 0.8% Cu, 0.3% Pb, 9.0% Zn and 26 g/t Ag from 46.5 m.

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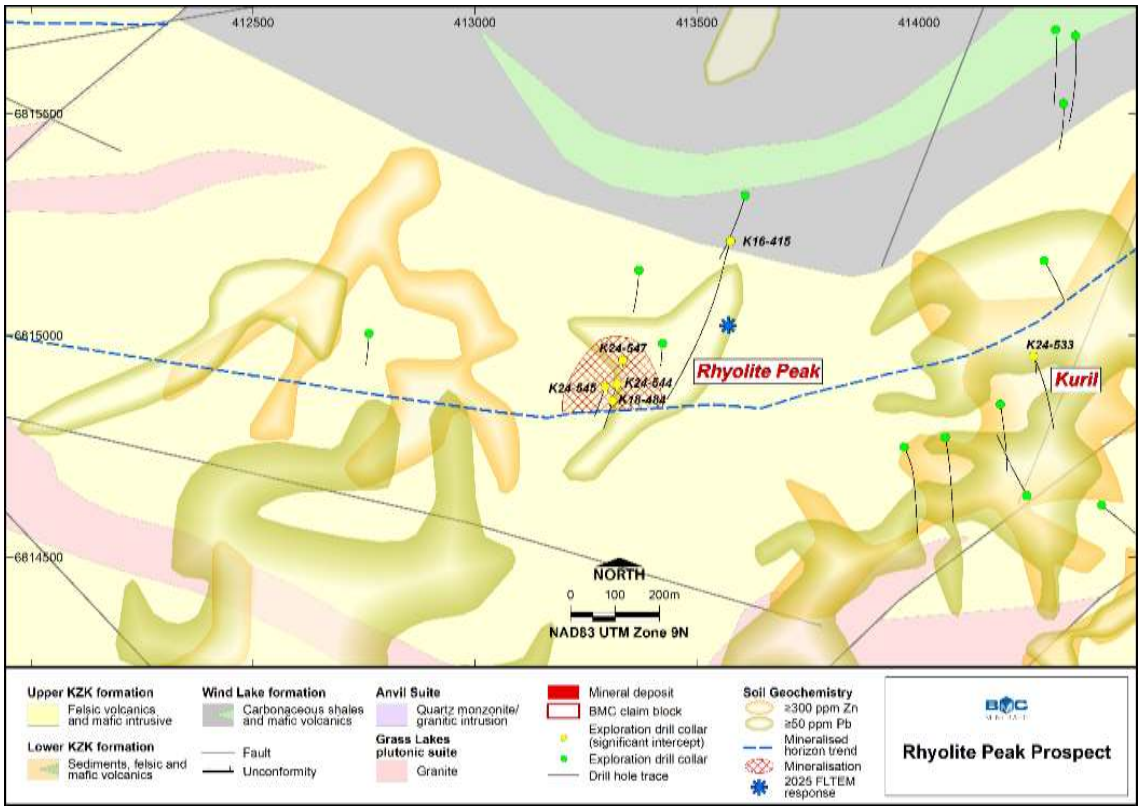


Figure 16-12: Map of the Rhyolite Peak Prospect and exploration drillholes with material intercepts.
Source: BMC

The "Charlie Corridor" comprises a ≈5 km by 2 km area of geochemical anomalism in soil that commences near the GP4F Prospect and extends through to the Charlie Prospect (Figure 16-15), and for the most part overlies bedrock now interpreted to comprise units of the lower Kudz Ze Kayah formation.

GP4F and R15 (NB. not owned by BMC) both appear to be hosted within the upper levels of the lower Kudz Ze Kayah formation close to where it transitions into the predominantly felsic package of the upper Kudz Ze Kayah formation that is host to the ABM Deposit.

The degree of metamorphism at GP4F is higher than at ABM, most likely due to the proximity of the intrusive to the south of GP4F. If VHMS mineralisation is present in the Charlie area, it remains to be seen whether it is related to either the GP4F or the ABM mineralising event.

An Exploration Target has been estimated and reported for the GP4F Prospect in accordance with the JORC Code 2012 (Table 16-9).

The potential quantity and grade of the Exploration Target is conceptual in nature, there has been insufficient exploration to estimate a Mineral Resource, and it is uncertain if further exploration will result in the estimation of a Mineral Resource.

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Table 16-9: GP4F Prospect Exploration Target

Tonnes Lower Mt	Tonnes Higher Mt	Cu Lower %	Cu Higher %	Pb Lower %	Pb Higher %	Zn Lower %	Zn Higher %	Au Lower g/t	Au Higher g/t	Ag Lower g/t	Ag Higher g/t
1.7	2.6	0.18	0.24	2.3	3.1	4.8	6.4	1.3	1.7	66	88

Source: CSA Global

The basis CSA Global used for the estimation of the size and range of the GP4F Exploration Target was like the approach employed to develop the estimate for the ABM Deposit, involving data assessment and validation, statistical analysis, domaining using wireframes, geostatistical analysis, block modelling, grade interpolation using ordinary kriging, density assignment, validation, and reporting (CSA Global, 2015a; CSA Global, 2019a). The Exploration Target is based on actual Exploration Results, and the JORC Table 1 disclosure is as detailed in Appendix B.

Mineralisation at GP4F comprises thin lenses of massive and semi-massive sulfide hosted within a much larger, tabular body of disseminated mineralisation and alteration referred to as the "GP4F Zone". The GP4F Zone is typically 5–10 m thick and is best-developed in a "central area" (the area of most drilling) that measures greater than 500 m in a north-south direction and 300 m from east to west.

The same mineralised zone appears to be weakly defined within a drill hole 400 m to the west of the central area.

A second mineralised zone recognised during 2015, the "Lower Zone", occurs structurally below the GP4F Zone. The alteration and mineralisation are texturally and mineralogically like the ABM Deposit.

A representative cross-section for the GP4F mineralisation is shown in Figure 16-13.

A coincident Zn-Pb in soil geochemical response extends along strike west of the up-dip projection of GP4F mineralisation (Figure 16-14) and a coincident magnetic and EM response extends along strike to the southeast of GP4F

BMC proposes the following actions to further the exploration and evaluation of the GP4F Prospect:

- Additional infill and extension drilling to identify whether the material classified as an Exploration Target can be extended and defined as a Mineral Resource, noting it is uncertain if further exploration will result in the estimation of a Mineral Resource.
- Assessment of existing geophysical data and implementation of ground EM surveys and IP surveys.
- Diamond drill testing of known multi-component anomalies, with DHEM surveying implemented as an aide in detecting "near-miss" off-hole conductive zones.
- Detailed structural and geochemical analysis to understand the timing of mineralisation, stratigraphy, and geological controls. Improved understanding of the deposit controls will additionally aid in more regional exploration efforts across the Kudz Ze Kayah Project.
- Detailed metallurgical testwork using core samples from infill drilling.

BMC proposes to undertake these activities over the next 2–3 years.

The larger exploration prospectivity of the Charlie Corridor is highlighted in Table 16-10 and Figure 16-15.

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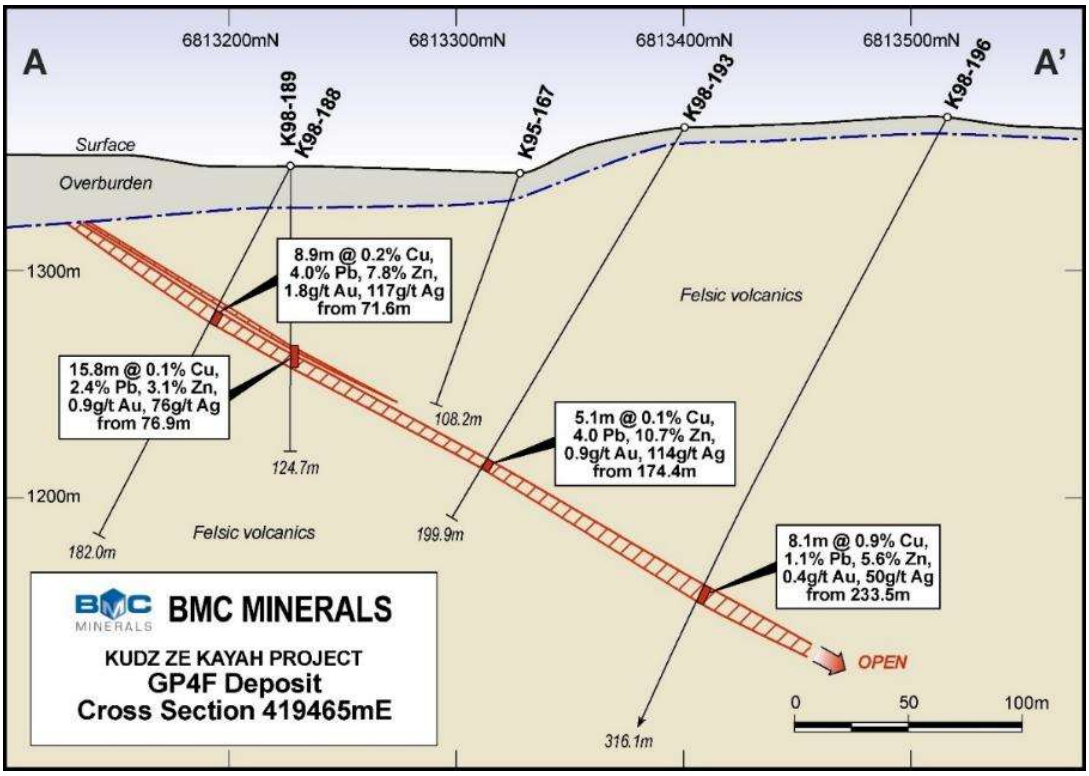


Figure 16-13: Schematic cross-section looking west through the GP4F Zone (419,465 mE) (source: BMC)

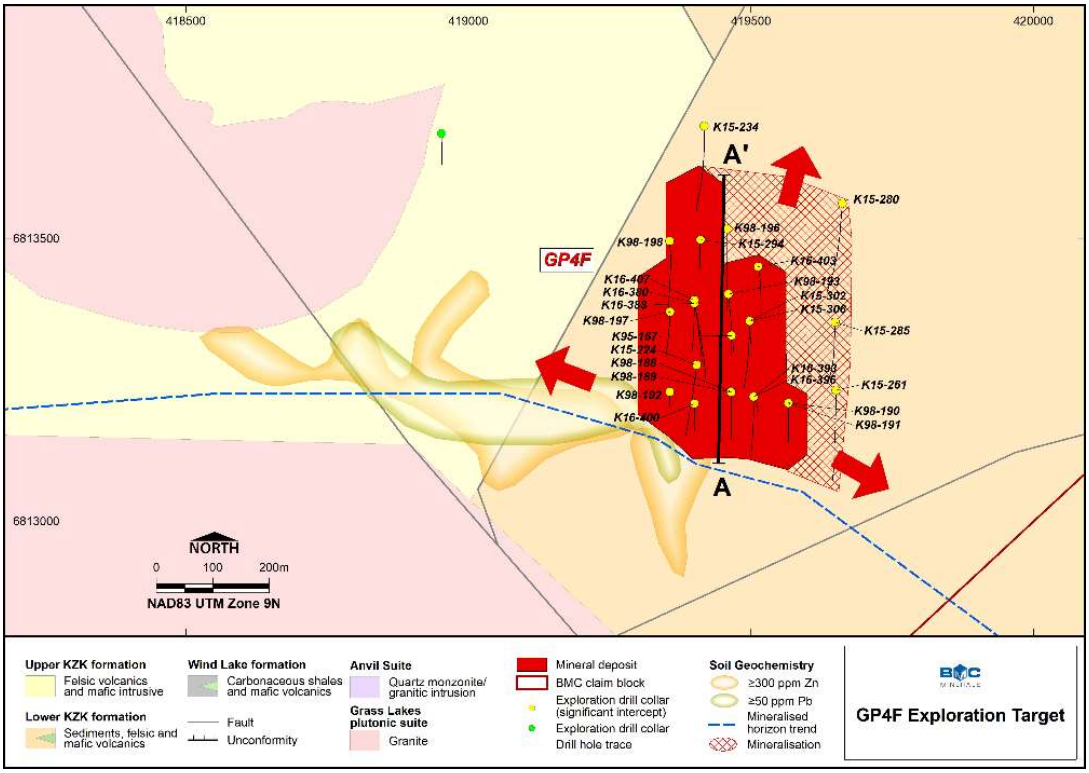


Figure 16-14: Map of the GP4F Prospect and exploration drillholes with material intercepts (source: BMC) (see Appendix E for results).

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Table 16-10: Exploration Prospects and Target Areas of Interest – Charlie Corridor

Target Areas/ Prospects	Description
Target Area J	A ≈2.3 km long coincident Cu-Bi-Pb-As-Sb-Ag-Zn-Mo response in soil is present, trending northwest towards a ≈1.5 km long magnetic response trending to the northeast beneath carbonaceous shales of the Wind Lake formation. The source of the magnetic response has not been identified. It may be a mafic unit but, as it is located proximal to the margin of where the ABM graben could be projected to trend, it cannot be ruled out as possibly being related to magnetite-pyrrhotite mineralisation as seen in the ABM Deposit. In this context, the somewhat linear Bi-Cu response in soil may reflect a potential feeder zone. However, remobilisation of metals during events that created the unconformity to the east and/or during the Cretaceous deformation and intrusion event cannot be ruled out. This target area lies outside the UTEM™ survey coverage. A brief review of compiled historical soil geochemical data has identified a zone of anomalism geochemistry immediately northeast of the Charlie Prospect outside the KZK Property. A Cu (≥50 ppm) in soil response extends over and of ≈2.5 km by 3.0 km, within which are several zones of anomalous Zn (≥300 ppm), Ag (≥0.6 ppm) and Sb (≥50 ppm). This response is directly along the interpreted trend of the Fault Creek fault, and therefore possibly the projected position of the ABM graben. It also straddles carbonaceous shale of the Wind Lake formation and the unconformity at the base of the Wolverine Formation, at a point where the Little Jimmy Formation appears to thin out. In this context, physical or chemical reworking of metals at or near surface is not out of the question. The upside of this may be that erosion of the Wind Lake formation in this area has left the underlying Kudz Ze Kayah formation close to surface.
Target Area K	A ≈2.0 km long coincident Cu-Bi-As-Hg-Sb-Ag-Zn-Mo response in soil is present, trending northwest along the eastern margin of a mafic unit trending in the same direction. A series of northwest trending faults are apparent in the aeromagnetics and, if the mafic unit is an intrusive, then it may be that there was a syngenetic fault present which may have provided a fluid conduit during the GP4F mineralising event.
Target Areas L	A ≈1.3 km long northeast trending copper in soil response with minor coincident Mo and Sb responses. This trend appears to align with a northeast trending fault mapped in the aeromagnetics and it is coincident with the interpreted boundary between the lower and upper Kudz Ze Kayah formation. It should be noted that this boundary is poorly defined east of GP4F due to a lack of outcrop. The eastern end of the Cu in soil response intersects the northwest trending multi-element response outlined in target area N.
Target Area M	This area is centred on the GP4F Prospect which is located beneath ≈30 m of transported overburden which has probably contributed to a subdued soil geochemistry response. The R15 and GP4F Prospects are most likely component parts of a larger deposit. The GP4F-R15 trend may transgress the local stratigraphy, with R15 mainly hosted within fine-grained sediments and GP4F mainly within overlying felsic volcanics. The GP4F-R15 trend is offset by a series of small-scale northeast trending faults with an apparent dextral movement (overhead view). Both the GP4F and R15 Prospects have strong UTEM™, and magnetic responses associated with their up-dip margins. The two deposits are ≈600 m apart and there is an untested coincident UTEM™, and magnetic response located between the two deposits. The R15 Prospect remains open in all directions, and the down dip projection of the Ra5 Deposit trends into the KZK Property. The GP4F Prospect has not been fully closed off by drilling. A coincident Bi-Pb-Zn in soils response extends ≈800 m to the west of the GP4F Prospect, aligned with the overall GP4F-R15 strike trend. This has not been drill tested yet. The GP4F Prospect comprises small lenses of massive sulfide within a halo of disseminated and vein/band-style mineralisation. If this latter style of mineralisation is present west of GP4F, this may explain a lack of UTEM™ response.
Target Area N	A ≈1.8 km long coincident Bi-Cu-Mo-Zn in soil response and an adjacent ≈1.1 km long coincident Cu-Bi-Zn-Mo in soils response, both of which trending to the northwest over a bedrock comprising lower Kudz Ze Kayah formation and mapped as massive basalt and mafic volcaniclastics. The westernmost anomalous geochemical trend in is coincident with a northwest trending fault mapped in the aeromagnetics. Two ≈500 m long magnetic highs are coincident with the northern end of the anomalous soil responses. The magnetic responses may be related to the mafic units but, as this cannot be confirmed in outcrop and the projected ABM graben may lie ≈500 m to the north, there is a possibility that they may be related to magnetite-pyrrhotite mineralisation as seen in the ABM Deposit.
Target Area O	This target is centred on a ≈800 m long magnetic high west of GP4F. The magnetic response may not be related to mineralisation, but it does lie directly along the GP4F-R15 trend. The target lacks a soil geochemical response, but as it straddles a watercourse in the middle of a valley it may just be that the soils profile there is not amenable to providing a suitable response related to any underlying mineralisation.

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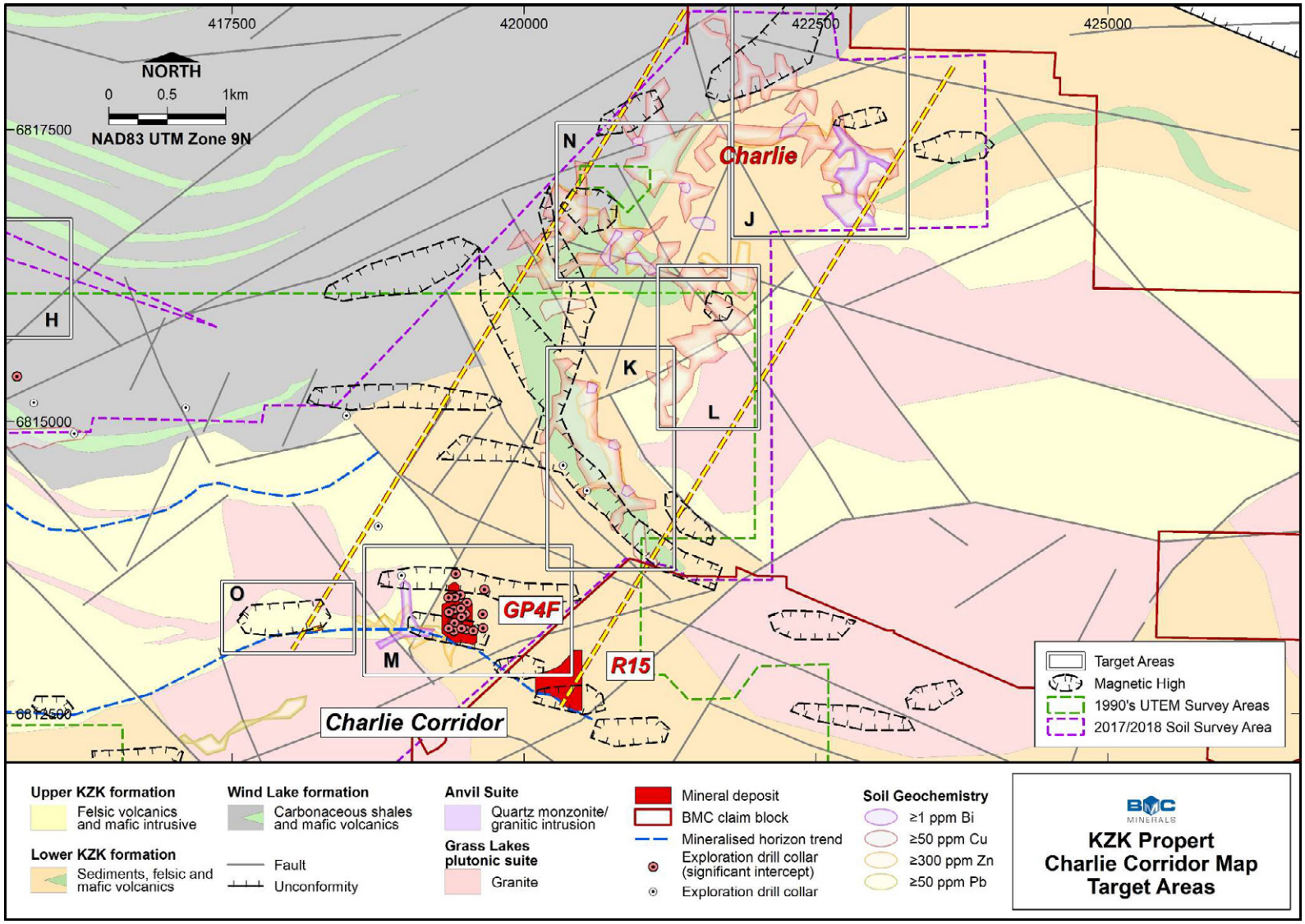


Figure 16-15: Charlie Corridor and target areas (J to O)/ Source: BMC

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16.2.2 Exploration targeting – Kona Property

An Exploration Target has also been reported at Kona (Table 16-11), largely supported by the results of past diamond drilling and highlights the immediate exploration potential adjacent to the Kona Mineral Resource (BMC, 2025b).

The basis used for the estimation of the size and range of the Exploration Target was like the approach employed to develop the Mineral Resource estimate for the Kona Deposit and was undertaken as an adjunct to that assignment. It involved data assessment and validation, statistical analysis, domaining using wireframes, geostatistical analysis, block modelling, grade interpolation using ordinary kriging, density assignment, validation, and reporting. The target is based on exploration data, and the JORC Code Table 1 disclosure is as detailed in Appendix B.

Table 16-11: Kona Exploration Target

Tonnes Lower Mt	Tonnes Higher Mt	Cu Lower %	Cu Higher %	Au Lower g/t	Au Higher g/t	Ag Lower g/t	Ag Higher g/t
3.0	5.0	1.5	1.8	0.5	0.8	3	5

Source: BMC

It is important to note that this Exploration Target statement contains quantity and grade estimations that are conceptual in nature. To date there has been insufficient exploration to estimate a Mineral Resource, and it is uncertain if further exploration will result in the estimation of a Mineral Resource.

In addition to this, drilling has not yet closed off the down plunge extent of mineralisation beyond the Kona Exploration Target area.

BMC proposes the following actions to further the exploration and evaluation of the Kona Deposit:

- Additional resource definition drilling (infill and extension) to identify whether it is possible to upgrade the resource classification (and to identify whether the material classified as an Exploration Target can be extended and defined as a Mineral Resource, noting it is uncertain if further exploration will result in the estimation of a Mineral Resource) and seek to extend the known deposit area, which presently remains open down plunge.
- Additional resource definition drilling into high-grade zones to provide increased confidence in the continuity of mineralisation and grade.
- Assessment of existing geophysical data and drill testing of known anomalies, particularly the Northwest Extension and Western targets, to determine if they represent faulted offset blocks to the known Kona mineralisation.
- Structural and geochemical analysis to understand the timing of mineralisation, stratigraphy, and geological controls.
- Metallurgical testwork using core samples from infill drilling.
- Ground geophysics, mapping and geochemistry to aid in reinterpretation of data and help define drill targets at targets outside Kona

BMC proposes to undertake these activities over the next 2-3 years.

BMC has developed a range of exploration targets within the Kona Property that are at stages ranging from drill ready to conceptual. These are based on BMC's analysis and interpretation of both historical and recent exploration data.

Geochemical and geophysical anomalies indicate that the mineralised horizons comprising the Kona Deposit may continue for at least 600 m, on a trend of 130°, to the Outfitter's Creek drainage. These same anomalies also suggest that there may be similar volcanogenic massive sulfide mineralisation

northeast and southwest of the known mineralisation hosted by fault displaced stratigraphy paralleling the Kona Deposit trend.

BMC geologists believe, and ERM concurs with this interpretation, that available evidence supports sub-seafloor mineralisation controlled by syn- to post-syngenetic faulting; that the linear nature of mineralised lenses suggests strong basement structural control on hydrothermal fluid flow and mineralisation; that mapping and drilling have not yet effectively tested for feeder zone mineralisation; and that Kona mineralisation is characterised by coincident linear EM and magnetic signatures with anomalous copper-gold in rock chip and float. BMC has identified several other targets with signatures which match these key criteria, and which have not been drill tested. Reinterpretation of VTEM™ geophysical surveys have identified three >2,000 m-long trends in anomalous VTEM™ responses, including in association with the known mineralisation to which the other two may be compared, which are illustrated in Figure 16-16.

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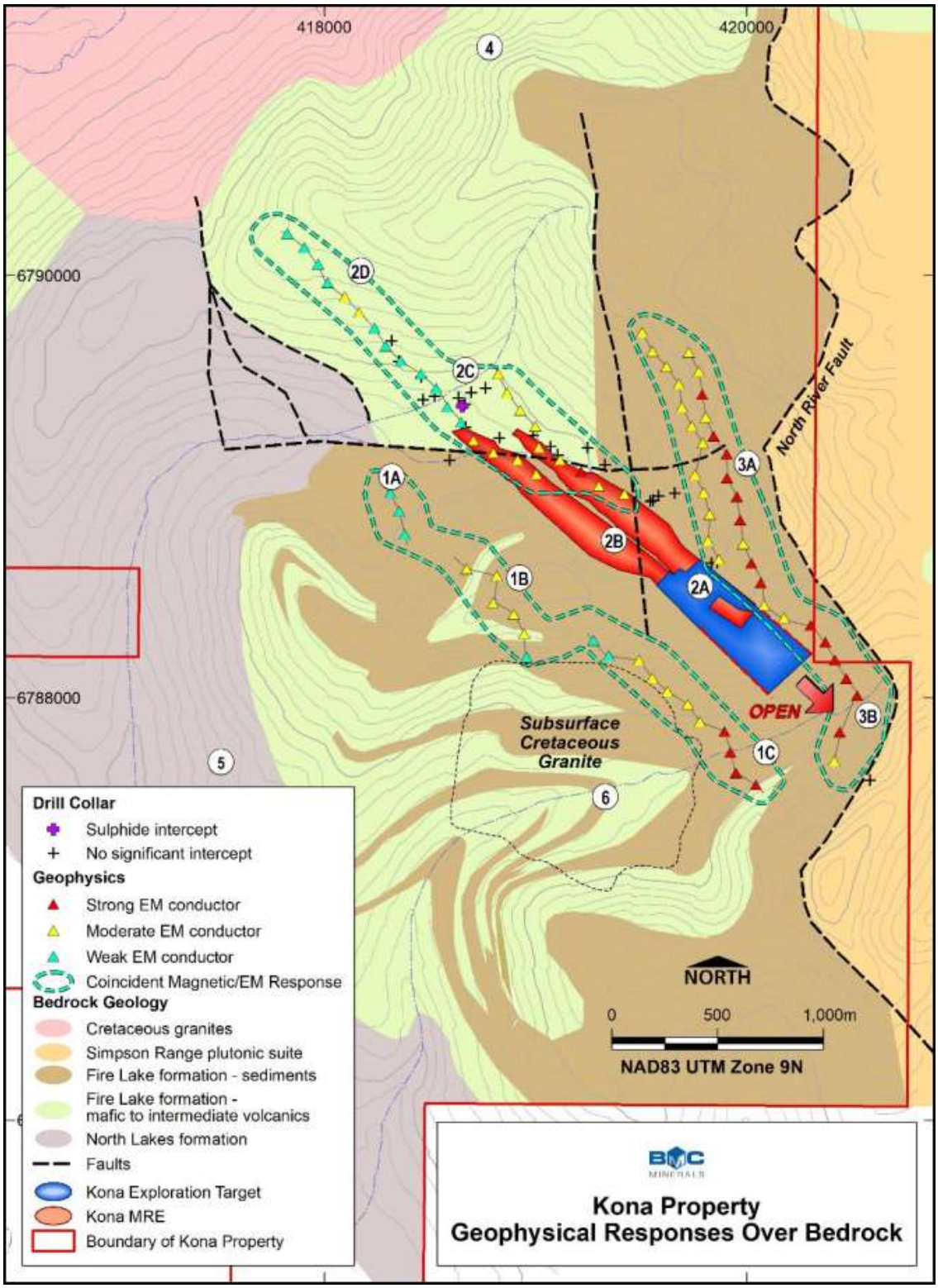


Figure 16-16: Exploration targets of the Kona Property; (Interpreted bedrock geology with mineralisation outline and conductive electromagnetic response trends from VTEM™ both projected to surface)
Source: BMC

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The VTEM™ data, together with BMC's compilation of existing mapping, drilling, and geochemical data, has enabled several high-priority targets to be defined. These are summarised in Table 16-12 and will form the basis of an exploration programme including ground geophysical surveys and significant metres of diamond drilling to test these targets.

Table 16-12: Target area features (refer Figure 16-7) – Kona Property

Target	Description
1	A) Magnetic signature with coincidental weak VTEM™ responses in the same orientation and plunge as the Kona Deposit. Historical rock chip of mineralised float returned values of 3.1% to 3.7% Cu. BMC field inspection noted multiple strongly mineralised magnetite, sulfide and pyrite boulders in the area. B) Anomalous VTEM™ response trend with coincident magnetic high; anomalous Cu-Au in float and rock chip. Possibly same host stratigraphy as Kona, with iron formation present. C) Anomalous VTEM™ response trend close to interpreted subsurface (Cretaceous) granite intrusion; iron formation present.
2	A) Kona Exploration Target as defined in this report and potential further down plunge extension to Kona Deposit. B) Potential for additional "stacked" sulfide lenses within in upper part of mafic unit. C) Same unit hosting Kona mineralisation associated anomalous Cu-Au geochemistry in soils and sulfide intercept in drilling. D) Same unit hosting Kona mineralisation associated with two anomalous VTEM™ responses and anomalous Cu-Au in soils, float and rock chips.
3	A) Two strong and extensive VTEM™ responses trending north-northwest with coincident magnetic highs. B) Sulfide boulders in creeks associated with magnetic highs, anomalous EM responses and Cu anomalism in soils and rock chips.
4	Mineralised horizon close to deep intrusion; highly anomalous geochemical responses in three talus (float) rock samples associated with anomalous VTEM™ responses and magnetic highs.
5	Broad anomalous VTEM™ response.
6	Historical (1997) HLEM response with a weak coincidental magnetic high. Anomalous response in 2015 VTEM™ highlights the same area.

Source: BMC

16.2.3 Exploration targeting – Pelly Property

BMC has developed several prospective exploration targets on the Pelly Property that warrant further work based on integrated interpretation of the historical and recent exploration data with the genetic models for VHMS mineralisation. The locations of these targets are shown in Figure 16-17.

An Exploration Target at the Jackman Prospect (BMC, 2023) has been estimated and reported in accordance with the JORC Code (Table 16-13). It is in large part supported by the results of past diamond drilling which supports the immediate exploration potential adjacent to the Wolverine Deposit.

The basis used for the estimation of the size and range of the Jackman Exploration Target was similar to the approach employed to develop the Exploration Target for the Kona Deposit. It involved primary data assessment and validation, and an assessment of the historical statistical analysis, geological wireframing, geostatistical analysis, block modelling, grade interpolation using OK, density assignment, validation, and reporting available in the public domain. The target is based on exploration data.

The Exploration Target has been reported in accordance with the JORC Code 2012. However, the potential quantity and grade of the Exploration Target is conceptual in nature, there has been insufficient exploration to estimate a Mineral Resource, and it is uncertain if further exploration will result in the estimation of a Mineral Resource.

The Jackman Prospect Exploration Target (No.1, Figure 15-11) represents the down plunge projection of semi-massive and massive sulfide mineralisation from the Wolverine Mine, located on mineral claims held by Yukon Zinc, into adjacent mineral claims held by the Company. Existing drilling has

demonstrated that the massive sulfide mineralisation continues into BMC's Pelly Property as it dips away to the northeast and that the mineralisation is not closed off by drilling over 800 m of strike extent. Two mineralised trends are identified by their thickness, footwall stockwork and copper data: Lynx Zone (northerly) and Wolverine Zone (northeasterly). The geological control on the two plunging shoots of mineralisation is interpreted to be underlying syngenetic faults acting as hydrothermal fluid conduits.

Table 16-13: Jackman Exploration Target

Tonnes Lower Mt	Tonnes Higher Mt	Zn Lower %	Zn Higher %	Cu Lower %	Cu Higher %	Pb Lower g/t	Pb Higher g/t	Au Higher g/t	Au Lower g/t	Ag Lower g/t	Ag Higher g/t
2.5	5.0	10.0	12.0	1.0	1.2	1.3	1.6	1.4	1.7	240	360

Source: BMC

The Exploration Target has been reported in accordance with the JORC Code 2012. However, the potential quantity and grade of the Exploration Target is conceptual in nature, there has been insufficient exploration to estimate a Mineral Resource, and it is uncertain if further exploration will result in the estimation of a Mineral Resource.

Diamond drilling in 2000 included mineralised intercepts within the Pelly claims which demonstrate that the Lynx lens extends at least 200 m down-dip from the mineral claim boundary.

- Drill hole WW00-001 intersected 8.15 m (7.6 m estimated true width) at 13.6% Zn, 1.2% Pb, 0.7% Cu, 155 g/t Ag, 0.6 g/t Au;
- WW00-003 intersected 5.17 m at 4.9% Zn, 0.8% Pb, 0.8% Cu, 160 g/t Ag, 0.6 g/t Au (including 2.5 m at 8.4% Zn, 1.3% Pb, 1.6% Cu, 293 g/t Ag, 1.2 g/t Au).
- Drill hole WW00-002 intersected weak sulfide mineralisation a further 300 m down dip from WW00-001.
- Hole WV96-35, collared outside of BMC mineral tenure, intersected 4.2 m at 15.6% Zn, 0.8% Cu, 3.9% Pb, 2.0 g/t Au and 558 g/t Ag, approximately 20 m inside what is now BMC's Pelly Property, demonstrating that the Wolverine Zone has not been closed off by drilling.

The Fisher Prospect hosts a series of target areas (2A to2 E in Figure 16-17) occurring in the same stratigraphic position as the Wolverine Deposit, with the hangingwall fragmental rhyolite breccia unit and carbonate-rich exhalite mapped immediately to the west within a felsic volcaniclastic package. Geophysical surveys have defined several targets. There is a 2 km corridor along the Wolverine horizon interface with a thick felsic volcanic package representing a felsic pile interpreted as being associated with a caldera fill system and large felsic volcanic centre. A high prospectivity is based on strong base metal soil anomalies with several rock chip samples; base metal sulfide in outcrop with a ≈10 m by 15 m exposure of discontinuous mineralisation identified near a felsic contact; a historical drill hole (WV95-06) that intersected 2.4 m at 2.8% Zn, 1.4% Pb, 0.12% Cu and 66 g/t Ag in sulfides below iron exhalative units; and a number of significant anomalous EM responses that are present.

The Ursa Prospect (3 in Figure 16-17) is located at the northwestern end of the Pelly Property where geological mapping by BMC has confirmed the continuation of the Wolverine Lake group volcanic stratigraphy. In particular, the hangingwall package, which hosts the Wolverine Deposit and the Fisher Zone, was found to extend throughout this northwestern area. A small soil geochemistry anomaly (silver-barium-lead) occurs coincident with mapped carbonate alteration.

The Sable Prospect (6 in Figure 16-17), located southeast directly along strike from the Wolverine Deposit, is premised on potential strike and down-dip extensions to a mineralised drill intercept encountered on adjacent mineral tenure not held by BMC. The 2001 drilling undertaken by Expatriate

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returned a 0.6 m massive sulfide in the same stratigraphic position as the Wolverine Deposit, grading 13.3% Zn, 0.8% Pb, 0.8% Cu, 416g/t Ag and 1.9g/t Au.

Located northwest of the mine and in the same stratigraphic position as the Wolverine Deposit, the Leo prospect (5 in Figure 16-17) comprises a discrete, strong, early- to late-time, double peaked VTEM™ anomaly extending across three survey lines. Geophysical modelling suggests the presence of two extensive, moderately conductive plates with a shallow dip towards the southwest. This is associated with anomalous base metal results in surface geochemical samples. There is only limited drilling to the northwest along strike from Wolverine and the alteration system has not been closed off, with potential for further massive sulfide lenses to be present in this direction.

The Jackman Prospect Exploration Target (Figure 16-18 and Figure 16-19) is at a depth that will require diamond drilling in conjunction with down-hole electromagnetic surveys on each drill hole. An initial programme of eight to ten drill holes for a total of 10,000 metres of drilling will be required to test the Jackman Exploration Target, with additional drilling to be undertaken if suitable results are returned in the first phase.

BMC have several promising exploration prospects within the Kudz Ze Kayah Project, and an Exploration Land Use Permit will be required prior to commencement on the Pelly Property. BMC proposes to undertake these activities over the next 2–3 years.

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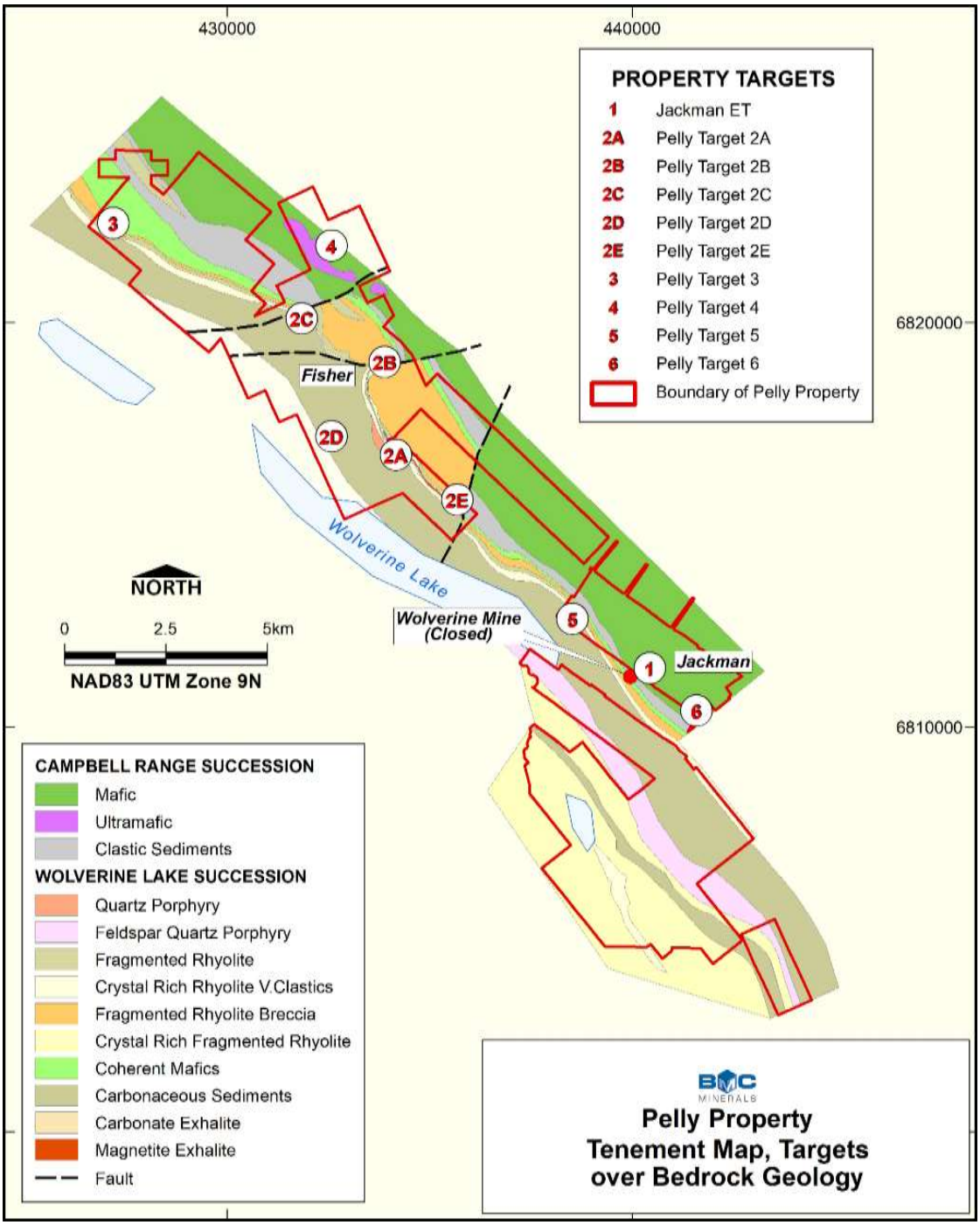


Figure 16-17: Location of prospective targets on the Pelly Property.
Source: BMC

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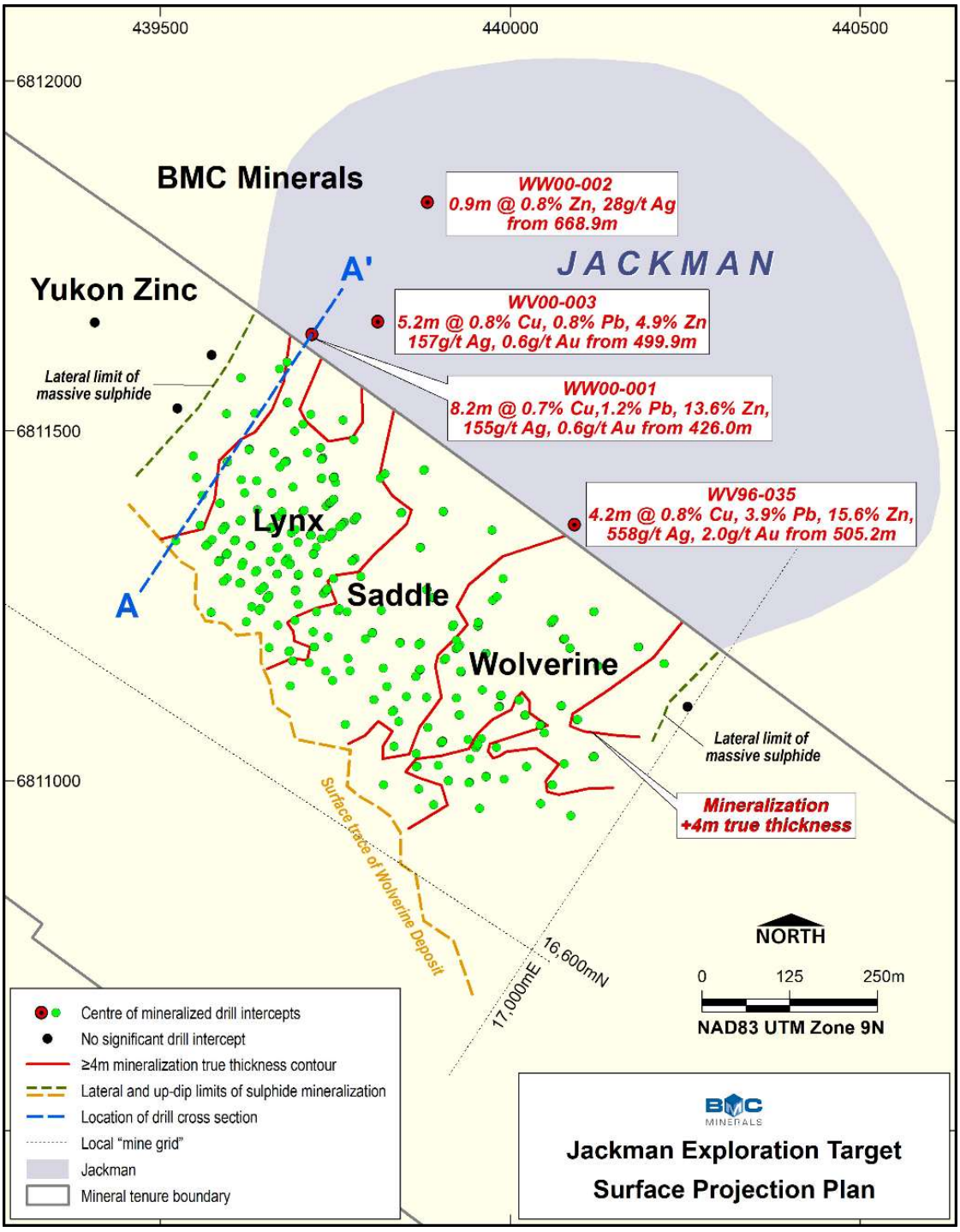


Figure 16-18: Plan view of the Jackman exploration target.
Source: BMC

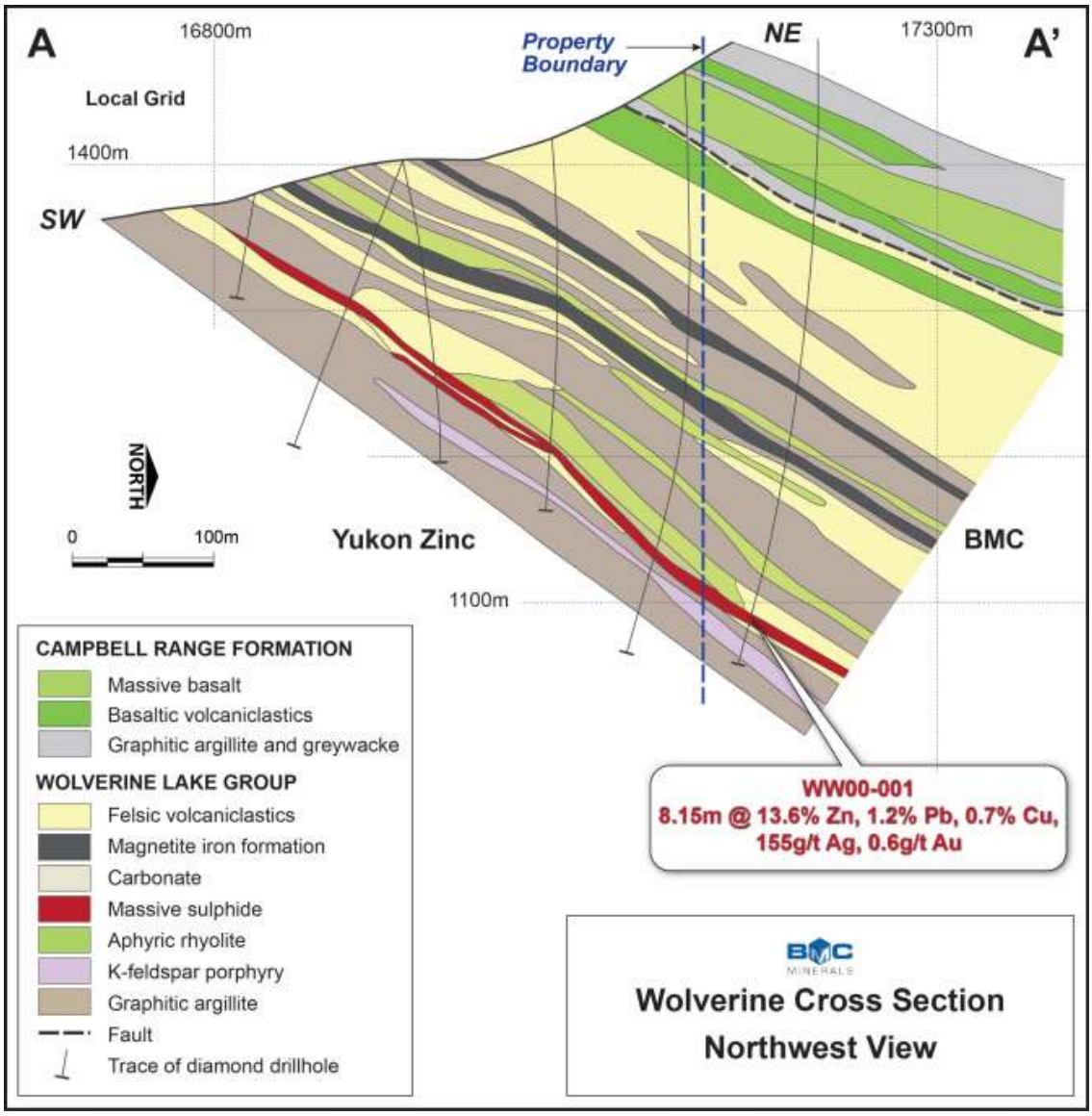


Figure 16-19: Cross Section A-A' through the Wolverine Deposit and the Jackman exploration target
Source: BMC

16.2.4 Exploration targeting – Wolf Property

The Wolf Property covers several VHMS occurrences, the two most significant being the Wolf Deposit and East Slope Zone Prospect, summarised below from (Gibson et al., 1998) and (Gibson and Holbek, 1999).

The Wolf Deposit is hosted within altered lapilli and ash tuffs, pyritic ash tuff and mudstone (Unit 3d), along the structurally highest of the mineralised horizons (Figure 16-21). It has a tabular form that dips 45° to the south, shows continuity for 600 m along strike and 500 m down dip, and ranges from 2 m to 25 m in width (Figure 16-20). The bulk of the mineralisation is hosted within a high-grade "keel" that has a strike length of 125 m, down dip extent of 400 m and average thickness of 12 m (Gibson et al., 1998) (Figure 16-22). The deposit remains open to expansion along strike to the east

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and down dip, but the Vermilion thrust is interpreted to have terminated the mineralised horizon towards the northwest.

Understanding of the East Slope Prospect is limited because only been tested by six holes drilled by Atna. The prospect comprises an ≈80 m thick sequence of disseminated lead-zinc mineralisation hosting five narrow massive sulfide horizons, the fourth lowest having the highest grade over the greatest thickness. The last hole of the 1998 programme, WF98-45, intersected 4.6 m true width of massive to semi-massive, mostly bedded, sulfide, siliceous exhalite and mineralised lapilli tuff grading 5.7% Zn, 2.1% Pb and 42.6 g/t Ag at a stratigraphic level interpreted to be ≈70 m below the Wolf Deposit upper horizon.

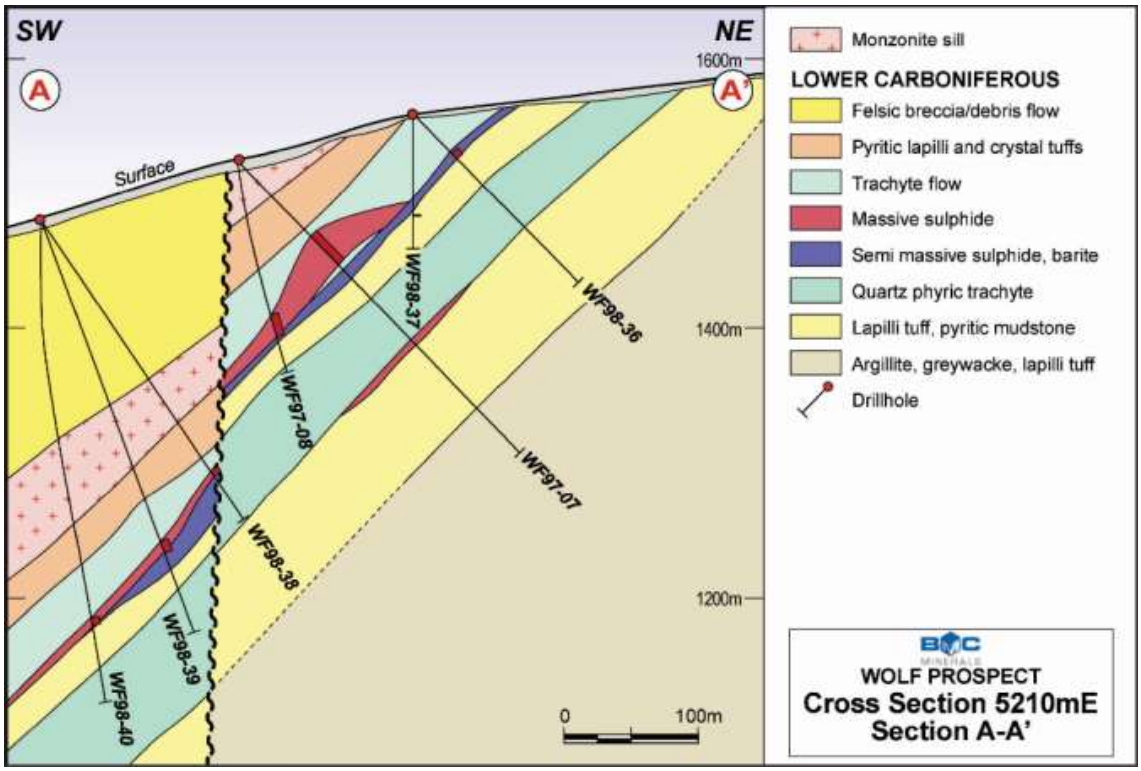


Figure 16-20: Cross-section A-A' (refer Figure 16-21) through the Wolf Deposit.
Source: BMC

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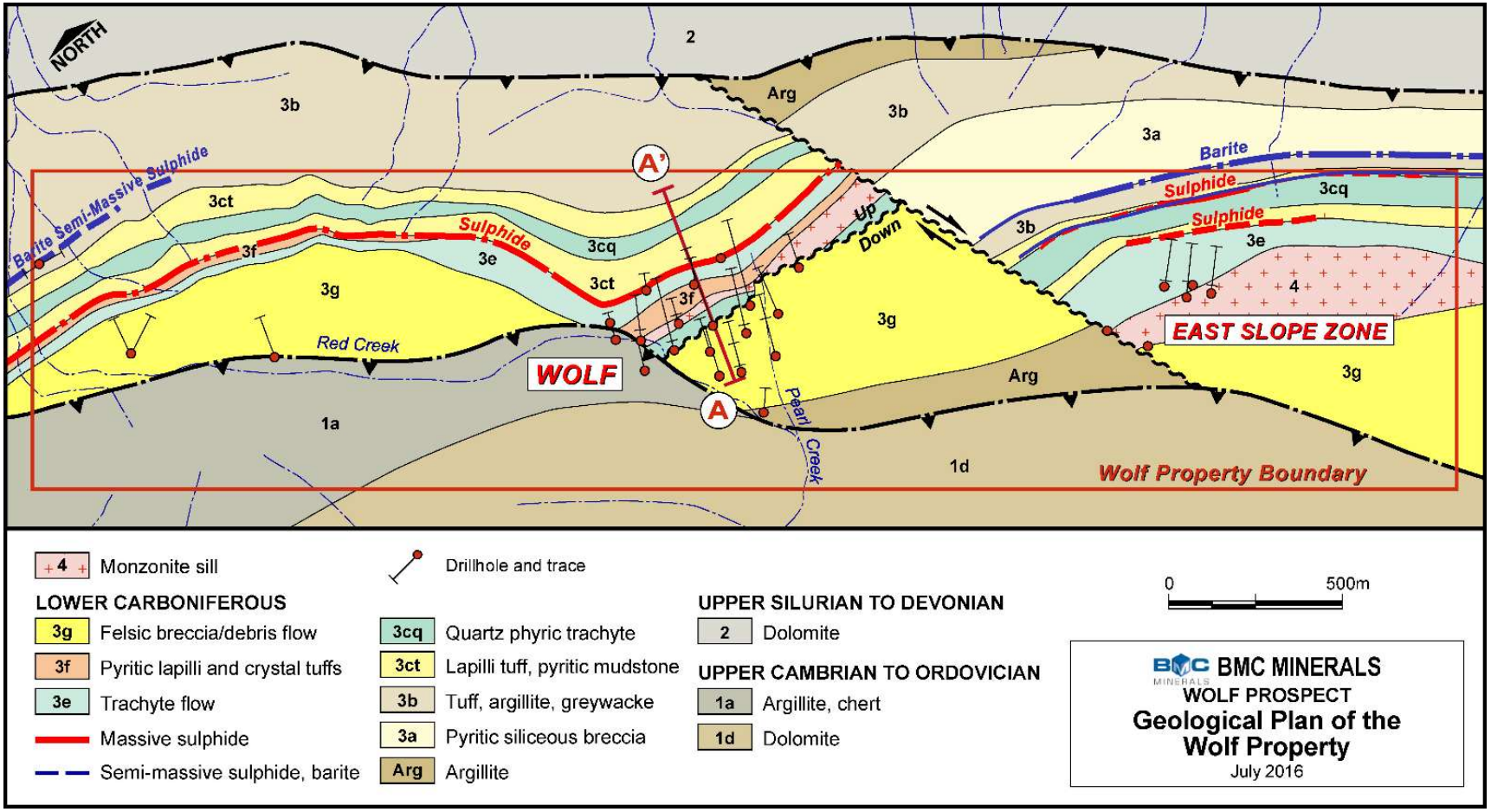


Figure 16-21: Geological plan of the Wolf Property.
Source: BMC

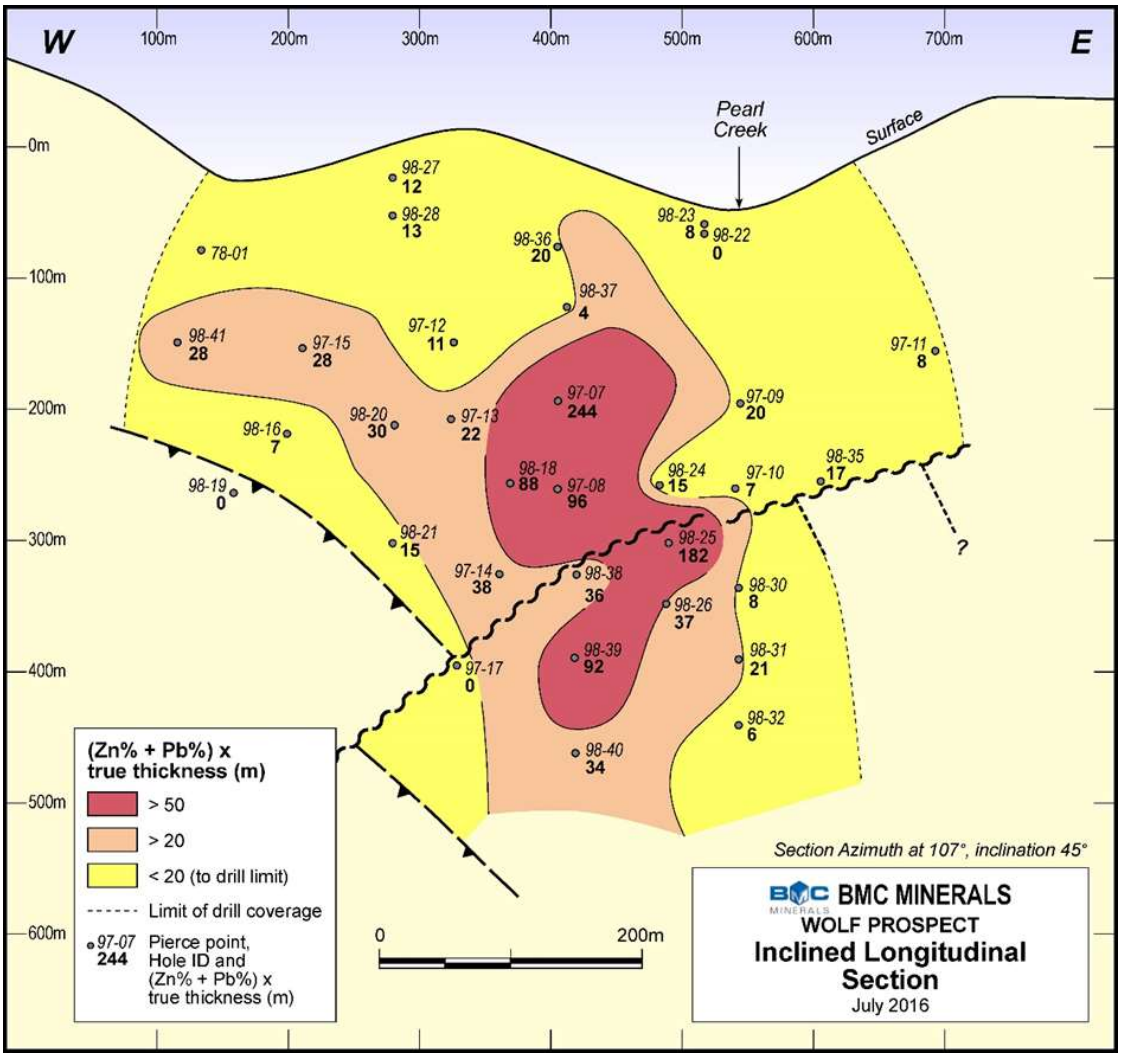


Figure 16-22: Inclined longitudinal section showing drill pierce points and high-grade "keel" to the Wolf Deposit
Source: BMC

An Exploration Target has been estimated for the Wolf Deposit based on 48 diamond drill holes (10,402.3 m) and a total of 28 assayed drill holes that intersected the interpreted mineralisation zones with holes spaced ≈60 m apart on sections spaced ≈60 m to ≈80 m apart (CSA Global 2017e). The Wolf Deposit is "open" in several directions (along strike to the east and down dip) and may be substantially larger than that defined by current drilling (Table 16-14).

The basis used for the estimation of the size and range of the Exploration Target was like the approach employed to develop the Mineral Resource estimate for the Kona Deposit and was undertaken as an adjunct to that assignment. It involved data assessment and validation, statistical analysis, domaining using wireframes, geostatistical analysis, block modelling, grade interpolation using OK, density assignment, validation, and reporting. The target is based on exploration data, and the JORC Table 1 disclosure is as detailed in Appendix C.

The Exploration Target has been reported in accordance with the JORC Code 2012. However, the potential quantity and grade of the Exploration Target is conceptual in nature, there has been

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insufficient exploration to estimate a Mineral Resource, and it is uncertain if further exploration will result in the estimation of a Mineral Resource.

Table 16-14: Wolf Exploration Target

Tonnes Lower Mt	Tonnes Higher Mt	Zn Lower %	Zn Higher %	Pb Lower g/t	Pb Higher g/t	Ag Lower g/t	Ag Higher g/t
2.7	3.3	4.4	5.4	1.3	1.5	38	46

Source: CSA Global

The Wolf Property is in a region known to contain significant VHMS deposits. The Kudz Ze Kayah Project comprises several base metal targets/prospects from near grassroots geochemical anomalies, conceptual geological and geophysical targets to drill ready targets (e.g. East Slope Zone, Wolf Extensions). Good potential exists on the Kudz Ze Kayah Project to identify new mineralised zones.

BMC proposes the following actions to further the exploration and evaluation of the Wolf Deposit:

- Additional diamond drilling of the extension target zones is the highest priority as increasing the size of the deposit is vital to developing the project and to define Mineral Resources.
- Detailed structural and geochemical analysis is undertaken to understand the timing of mineralisation, stratigraphy, and geological controls. Improved understanding of the deposit controls will aid in more regional exploration efforts across the tenement package.
- Further validation of the database is planned, including incorporation of the historical geological logging.
- More detailed bulk density testwork across the mineralised zones and host lithologies is planned.
- Preliminary metallurgical testwork is planned as part of future drilling of the Wolf Deposit.

BMC proposes to undertake these activities over the next 2–3 years.

16.3 Exploration Conclusions

The Kudz Ze Kayah Project contains economically significant polymetallic VHMS deposits, with additional deposits known in the surrounding district. ERM considers that the Kudz Ze Kayah Project holds good potential for the discovery of further VHMS deposits and extensions to known mineralisation.

Numerous targets have been identified that are worthy of drill testing. Geochemical and geophysical anomalies have been identified across the project tenements which are worthy of further exploration work to define drilling targets.

The Kudz Ze Kayah Project comprises a wide range of base metal targets for exploration from near grassroots geochemical anomalies, conceptual geological and geophysical targets to drill ready targets (Fuego, Wolverine extensions, Kona stacked lens, Krakatoa extensions) and advanced stage deposits consisting of Ore Reserves (ABM), Mineral Resources (Kona) and formally defined JORC Code Exploration Targets (GP4F, Wolf and Kona).

In addition to this, large sections of ground within the Kudz Ze Kayah Project remain under-explored. BMC's flagship ABM Deposit remains open beyond the existing Ore Reserves and additional drilling is required to fully define the extents of the mineralisation.

The ABM Deposit belongs to a subset of VHMS systems that can be very large and contain numerous lenses and separate bodies of mineralisation as demonstrated in Figure 16-23.

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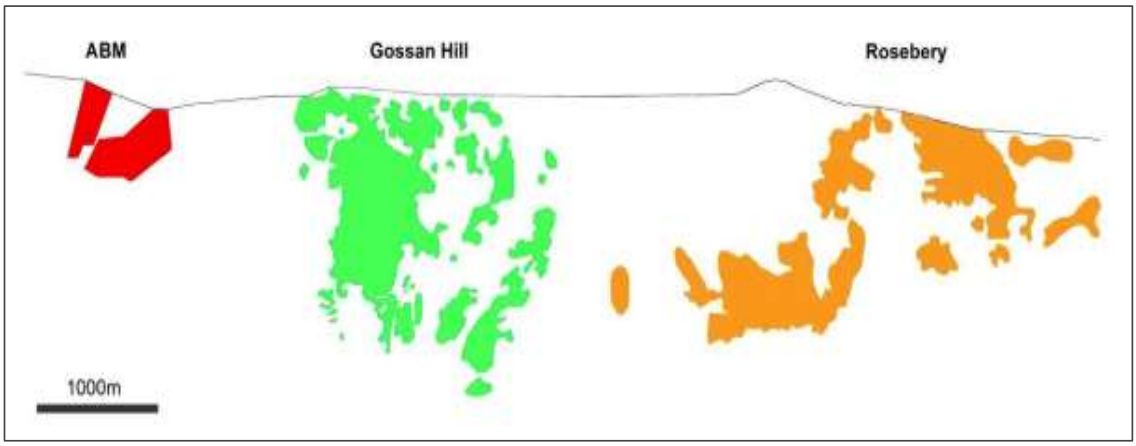


Figure 16-23: Schematic long section projections of the ABM Deposit outline in comparison to schematic projections of the multi-lens Gossan Hill and Rosebery VHMS deposit outlines projected to a common vertical plane and scale. Note ABM Deposit is shallowly dipping and has only been drilled to around 200 m vertical depth so far.
Source: BMC and company annual reports[16]

In ERM's professional opinion there remains good potential to discover material extensions and additions to the ABM Deposit, of which the Krakatoa Zone is an example.

[16] Gossan Hill: 29 Metals 2024 Annual Report – Page 62; Rosebery: MMG - Report of Exploration Results from Las Bambas and Rosebery, 2023 – page 14

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17. STRATEGY AND USE OF FUNDS

The Company provided ERM with a copy of their exploration strategy, proposed work programmes and planned expenditure for the Kudz Ze Kayah Project for an initial two-year period following listing on the ASX.

BMC's overall strategy, as presented elsewhere in the prospectus, is to grow shareholder value and provide benefits to local communities over the long-term, from profitable mining operations in stable areas. The main project is the Kudz Ze Kayah Project that includes the proposed ABM Mine. Based on company documents reviewed by ERM, the Company intends to devote a substantial portion of the funds raised from the initial public offering towards works to support a final investment decision for the ABM Mine and on exploration.

In the two-year period after the company is listed on the ASX, the Company plans activities aiming to discover and define additional Mineral Resources and Ore Reserves that can be treated at the ABM Mine. Exploration will focus on increasing Mineral Resources and Ore Reserves at the Kudz Ze Kayah Property. BMC has identified a pipeline of targets for exploration ranging from early-stage exploration targets through to advanced prospects. By prioritising exploration near the proposed ABM Mine, the Company hopes to extend the potential mine life beyond what is currently outlined in its studies. In the medium term, the Company plans to add mineral assets in the Finlayson District around the Kudz Ze Kayah Project by acquiring or partnering on promising mineral properties.

Project advancement will include continuing to obtain all required permits and licences, and on starting front end engineering design (FEED studies) for the ABM Mine and its infrastructure.

Based on the Company's past exploration success and on the outcomes of the advanced technical studies (at a Feasibility Study level of confidence) completed at the Kudz Ze Kayah Project, the Company has developed an 18–24 month work programme comprising:

- Exploration and evaluation activities aiming to expand and improve the Kudz Ze Kayah Project's resource base.
- Permitting and approvals.
- Feasibility Study optimisation and engineering.
- Detailed Engineering.
- Continuation of community engagement and environmental works.

The use of funds for the project is summarised in Table 17-1.

Table 17-1: BMC's 24-month Proposed Use of Funds

Indicative Allocation of Funds	US$ million	% of use of funds
Exploration and Evaluation	24.6	36
Permitting	7.5	11
Feasibility Optimisation and engineering	4.3	6
Detailed engineering	11.9	17
Community	3.0	4
Camp costs	1.5	2
Corporate and administration	7.7	11
Working Capital	4.5	6
Estimated Costs of the Offer	4.9	7
Total Indicative Allocation of Funds	69.9	100

Source: BMC; Rounded to nearest 10k. Totals may not sum correctly due to rounding.

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17.1 Exploration and Evaluation

The Company plans to undertake systematic exploration and evaluation of the Company's Kudz Ze Kayah Project. Proposed exploration expenditure is aimed at increasing the resource base for the Project, with a particular focus on the KZK Property, and extending the anticipated life of the ABM Mine Project. A detailed breakdown of the proposed expenditure is presented in Table 17-2.

Core Drilling – Exploration: Staged programme of diamond drilling and downhole EM aimed at testing a series of mineralised exploration prospects within the KZK Property and advancing them through to a resource drill out suitable for estimation of a Mineral Resource and potential addition to the Mine Plan. This includes the Rhyolite Peak, Fuego, GP4F and Krakatoa prospects. The programme is expected to comprise 38,000 to 45,000m of core drilling.

Core Drilling – Metallurgical: Diamond drilling programme aimed at collecting mineralised rock for initial metallurgical testwork (Fuego, Rhyolite Peak, GP4F, etc.).

Surface Geochemical Sampling: Soil and rock chip sampling to extend surface geochemical coverage across areas considered prospective for base metal mineralisation.

Regional – Ground Geophysics and Drilling: Ground based EM surveys aimed at refining drill targets in prospective areas (Kona, Jackman, Fisher) and following up with core drilling to test anomalous responses.

Regional - Airborne Geophysical Surveys: Airborne magnetic and EM surveys aimed at extending and refining existing coverage in prospective areas.

Equipment: Purchase of field equipment required to support the proposed field programme.

Table 17-2: Exploration and Evaluation Use of Funds

Indicative Allocation of Funds	US$M
KZK Property	
Diamond Drilling - Exploration	17.14
Diamond Drilling - Metallurgical	0.85
Surface Geochemical Sampling	1.10
Regional	
Geophysics – Ground EM	1.13
Diamond Drilling - Exploration	2.30
Airborne Geophysical Surveys	1.14
Equipment	0.68
Other	0.26
TOTAL	**24.60**

Source: BMC; Rounded to 10k. Totals may not sum correctly due to rounding.

17.2 Permitting and Approvals

Provision for obtaining all material permits and licences required to carry out exploration and resource growth activities at the Kudz Ze Kayah Project, and for the future construction and operation of the proposed ABM Mine Project.

17.3 Feasibility Optimisation and Engineering

An allocation of funds has been provided for de-risking the Project through optimisation of current feasibility level engineering studies to continue to advance mining, processing and infrastructure components of the project.

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17.4 Detailed Engineering

Engineering studies aimed at advancing the Project. Includes studies to support permitting applications and final costing estimates prior to the grant of major permits and a final investment decision.

Mining: Detailed engineering with majority of costs to advance engineering design of the waste rock and tailings storage facilities that will be required for licensing.

Processing: Initial metallurgical testwork on exploration prospects proposed to be drilled (Fuego, Rhyolite Peak, GP4F, etc.).

Transport and Logistics Studies: Advancement and refinement of existing concentrate transport and logistics studies.

Site Infrastructure: Design and engineering studies related to site water management, the water treatment plant, and the fish offset pond.

Front-End Engineering and Design (FEED): Studies aimed at establishing technical specifications, cost estimates, project schedules, risk assessments, and necessary tender documentation prior to construction.

Table 17-3: Detailed Engineering use of funds

Indicative Allocation of Funds	US$M
Mining	1.60
Processing	0.30
Transport & Logistics	1.10
Site Infrastructure	4.70
Front-End Engineering and Design	4.10
TOTAL	**11.90**

Source: BMC; Rounded to 100k. Totals may not sum correctly due to rounding.

17.5 Community

Expenditure for the Company's ongoing engagement and consultation with all stakeholders.

17.6 ERM Opinion

The mineral properties held by the Company are considered to be advanced exploration and pre-development that are intrinsically speculative in nature. ERM considers, however, that the identification and acquisition of the Kudz Ze Kayah Project has been based on sound technical merit, and the work completed by the Company thus far has been to a high technical standard.

The properties of the Kudz Ze Kayah Project are considered to be sufficiently prospective, subject to varying degrees of exploration risk, to warrant further exploration and assessment of their economic potential, consistent with the proposed programmes.

ERM concludes that the Company's portfolio of projects offers prospects for additional discoveries in an environment that has been relatively under explored using modern methods. The exploration activities will also provide insights that may enable further discoveries.

Significant hiatuses in the exploration and mineral development history of the region suggests that application of modern geophysical and geochemical methods, coupled with a relatively well understood mineral system may see new discoveries being made.

The presence of existing and historical mines in the region support the proposed VHMS mineral system model currently underpinning BMC's approach.

The proposed budgets are considered consistent with the exploration potential of the Company's projects and considered adequate to cover the costs of the proposed programmes. Given the nature and risks inherent in undertaking exploration activities, the detail of the programmes is likely to evolve in accordance with results and changing priorities.

The Company has prepared staged exploration, development and production programmes and budgets, specific to the potential of the project, and which are consistent with the budget allocations. ERM considers that the relevant areas have sufficient technical merit to justify the proposed programmes and associated expenditure satisfying the requirements of ASX listing Rules 1.3.3(a).

Based on the work completed by ERM, the Company's commitments to exploration and production activities satisfy the requirements of ASX listing Rules 1.3.2(b) and 1.3.3(b).

ERM also understands that the Company has sufficient working capital to carry out its stated objectives, satisfying the requirements of ASX listing Rules 1.3.3(a).

ERM has reviewed the proposed work programmes as well as the sums assigned to those planned activities.

Based on its review, ERM is of the opinion that the programmes are reasonable for the purpose of advancing exploration and informing a final investment decision by the Company for the ABM Mine proceeding.

The capital designated by the Company for the exploration and technical development of the Kudz Ze Kayah Project are expected to adequately support the intended activities throughout the 18-to-24-month timeframe.

The proposed exploration budget also exceeds the anticipated minimum statutory annual expenditure commitments on the various project tenements.

ERM notes that the use of funds summarised above is indicative only. Actual use of funds will be subject to modification on an ongoing basis depending on the outcomes of exploration activities and progress on planned work, subject to site conditions and any task-specific issues.

Market conditions, weather, technical issues and/or any number of other factors may result in actual expenditure levels differing materially from the estimates above.

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18. RISK DISCUSSION

Investing in exploration and mining development projects carries innate risks. The anticipated future activities of the Company may be influenced by various risks and factors that could affect its performance. While certain risks can be addressed through effective safeguards and controls there are others that remain beyond the reach of the board and management and may not be mitigated.

The risks outlined in this section are not comprehensive and should be considered alongside other information in the Prospectus.

18.1 Tenure

The Company has registered its Mineral Claims with the relevant mining authorities and has submitted all necessary information. However, this does not guarantee future ownership. Some of the Company's properties are recorded Mineral Claims, but not all have been surveyed, which means their exact boundaries and locations may be unclear and could be disputed. Additionally, the Company's properties might be affected by earlier unregistered agreements or future land claims, which could impact its ownership.

The Company's activities rely on keeping its Mineral Claims, which it currently holds or may acquire in the future. To maintain these claims, the Company must meet annual spending requirements set by the Quartz Mining Act in Yukon.

The Kudz Ze Kayah Project is within an area wherein staking and recording of new or additional Mineral Claims is temporarily prohibited due to a moratorium imposed by the Yukon Government in order to consider the implications of Ross River Dena Council v. Government of Yukon (the "2012 Ross River Dena Council case").

18.2 Exploration and appraisal

Exploration is an inherently high-risk undertaking and there can be no guarantee of success in the Company's exploration project areas. Exploration projects involve many risks and are frequently unsuccessful.

The Mineral Resource and Ore Reserve estimates for the proposed ABM Mine, and the Mineral Resource estimate for the Kona Deposit, are assessments of the likely quantities of metals at these deposits. The estimates are based on current geological theory and the best evidence available to the Competent Persons at the time of the work. It is the nature of all scientific conclusions that they are founded on an assessment of probabilities and, however high these probabilities might be, they make no claim for absolute certainty.

Accordingly, such Mineral Resource estimates may require revision as more drilling information becomes available, as actual production experience is gained or as the Company's mining methods are changed.

The actual quality and characteristics of mineral deposits cannot be known until mining takes place and will almost always differ from the assumptions used to develop resources.

Ore Reserves are valued based on future costs and future prices and, consequently, the actual reserves and resources may differ from those estimated if commodity prices and costs change.

18.3 Metallurgy and Concentrate quality

The effectiveness of metallurgical test work results and conclusions in influencing process design, recoveries, and throughput relies on the precision of the test work and the assumption that the

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sample tests accurately represent the entire mineral deposit. There are risks that the test work may be inaccurate or that the sample tests are not representative of the mineral deposit as a whole, leading to adverse outcomes.

The transition from laboratory and other test results to a commercial scale carries inherent risks, as does the subsequent design, construction, and operation of any processing facility.

There is also the risk that the commissioning of the processing plant does not proceed according to plan or that the metallurgical performance of the ore creates unintended or unexpected complications in the processing of the ore which leads to concentrate product that is out of specifications for the offtake agreements.

Given the polymetallic nature of mineralisation contained within the ABM Mineral Resource that is to be exploited at the proposed ABM Mine Project and the need to process the mined ore into multiple mineral concentrates for sale, there is a risk of an inability to produce mineral concentrates within target specification ranges.

Management of the product quality and resultant risk mitigation is addressed in the Company's Feasibility Study-level investigations through a number of measures including but not limited to:

- identification of geological and metallurgical classifications for different ore zones;
- scheduling of mining to ensure that sufficient stocks of each metallurgical and geological domain are available for appropriate blending;
- maintenance of run of mine stockpiles and stockpile blending mechanisms;
- appropriate sampling, metallurgical test work, interpretation and process design conducted;
- appropriate design of the concentrator and the use of metallurgical controls in the operation of the concentrator that provide the desired outcomes;
- concentrate stockpile blending on site;
- concentrate stockpile blending off site; and
- appropriate sales and marketing strategies in order to maximise revenue while minimising risks.

18.4 Feasibility studies

Feasibility studies, including the Feasibility Study-level investigations summarised in the 2025 Technical Report and this Report, are used to determine the potential economic viability of a mineral deposit.

Such studies, by their nature, make numerous assumptions, including assumptions about capital and operating costs and future commodity prices. These assumptions are made at the time the study is completed based on information then available. Actual costs and revenues are impacted by various factors such as global economic factors and other factors outside the control of the Company and therefore may vary significantly and adversely from the estimates used in such studies.

Constructing a new mine involves significant capital investment and long timelines, making it vulnerable to various cost escalation risks. Rising costs for materials, labour and equipment due to geopolitical factors, general inflation and/or sector-specific demand are a material risk for pre-development projects.

Accordingly, the economic viability of the proposed ABM Mine, or the proportion of mineral deposits that the Company will be able to economically extract (if any), may differ materially from previous estimates provided by the Company.

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18.5 Mining risks

Every mineral deposit is unique. The nature and quality of the deposit, as well as its behaviour during mining and processing can never be wholly predicted. Operational risks include geotechnical risks, such as risks of rock falls and collapse within the mine (such as pit walls, ramps and underground features), that mineralisation is not intercepted (spatially) as expected from the Ore Reserve model, slope angles are not optimal (leading, for example, to increased costs), that faulting may cause ore loss and/or dilution and that ore tonnes are lower than modelled.

18.6 Construction and Commissioning

Construction and commissioning of a new mine are complex stages with distinct risks that can lead to cost overruns, delays, or operational inefficiencies.

During construction delays may be caused by delays in site preparation and civil works due to unexpected ground conditions, weather delays, or remote area logistics challenges with transporting materials, equipment, and personnel. Issues with the workforce and contractors, for example difficulty in sourcing skilled labour in a timely fashion, performance issues such as poor productivity, safety incidents, disputes or industrial can delay or halt progress. Procurement and supply chain delays can be caused by delays in delivery of long lead time critical equipment (e.g., crushers, mills, electrical gear), as well as customs and other import delays. Management issues may also arise with the project management and execution leading to schedule drift where poor planning or coordination can lead to cascading delays. Interface risks can result from misalignment between civil, mechanical, electrical, and process contractors.

The commissioning phase of a project faces risks from issues such as systems integration/installation faults that are only recognised during commissioning, or control system failures, with automation and instrumentation not functioning as intended. Operational Readiness may suffer from insufficient training, with operators not be fully prepared to run the plant safely and efficiently; there may be incomplete procedures, with preliminary or absent detailed commissioning plans and SOPs causing confusion and errors. Lastly, there are risks that the project as built fails to meet the design criteria (throughput, recovery, or energy efficiency), or there may be equipment failures – early breakdowns due to manufacturing defects or improper installation.

18.7 Closure

Closure is inextricably part of mining operations. Closure obligations will include requirements to control dispersion of potentially deleterious effluents and to reasonably re-establish pre-disturbance land forms and vegetation. Permits for some of the Company's activities are currently under application and final permits may contain unanticipated reclamation obligations.

18.8 Permits and approvals

The Company holds certain permits and licences to conduct exploration activities at the Kudz Ze Kayah Project and other permits are under application.

Over time existing permits will need to be extended or replaced and additional exploration activities outside the current operating areas will require additional permits.

The Company has not yet been granted mining permits or various other approvals needed to conduct mining operations at the proposed ABM Mine.

The granting and maintaining of permits and licences, and obtaining renewals, depends on the Company being successful in obtaining the required statutory approvals for its proposed activities.

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There is also no certainty that the permits and licences it holds will be renewed as and when required. There is no assurance that such renewals will be given as a matter of course and there is no assurance that new conditions will not be imposed in connection therewith.

18.8.1 Decision Document

The Company is waiting for a new Decision Document for the ABM Mine Project after government consultation with the local Indigenous group, the Kaska First Nation. This document will decide if the mine can move to the final phase of permitting and what conditions will apply. The Company had a previous Decision Document, but it was set aside after procedural issues.

Delays in getting the Decision Document will slow down the Company's efforts to develop the ABM Mine, as other government approvals needed for the mine's development depend on it. The outcome of the new Decision Document is also uncertain; it could approve, reject, or change the recommendations made by the YESAB regarding the mine. Furthermore, it may include conditions that could negatively affect the mine's profitability and economic viability.

18.9 Environment

The Company’s operations are subject to environmental regulation in the jurisdictions in which it operates.

These regulations mandate, among other things, the maintenance of air and water quality standards and land reclamation. They also set out limitations on the generation, management, transportation, storage and disposal of solid and hazardous waste.

Environmental legislation is evolving in a manner which will likely, in the future, require stricter standards and enforcement, increased fines and penalties for non-compliance, more stringent environmental assessments of proposed projects and a heightened degree of responsibility for companies and their officers, directors and employees.

There is no assurance that future changes in environmental regulation, if any, will not adversely affect the Company’s operations.

The Company’s activities are expected to have an impact on the environment. It is the Company’s intention to conduct its activities to an appropriate standard of environmental obligation, including in compliance in all material respects with relevant environmental laws which will mitigate the impact of its activity on the environment.

Nevertheless, there are certain risks inherent in the Company’s activities which could subject the Company to extensive liability.

The concentration process to produce metal concentrates are expected to produce tailings. Tailings are stored in engineered facilities which are designed, constructed, operated and closed in conformance with local requirements and appropriate practices.

Hazards such as equipment failure or failure of tailings storage facilities may result in environmental pollution and consequent liability.

The water collection, treatment and disposal operations at the Company’s projects are subject to strict regulation and involve management of environmental risks.

While the Company will construct and operate the water storage and management systems to all applicable standards and appropriate controls, if collection or management systems fail, overflow or do not operate properly, untreated water or other contaminants could spill onto nearby properties or

into nearby streams and rivers, causing damage to persons or property, injury to aquatic life and economic damages.

The cost and complexity in complying with the applicable environmental laws and regulations may affect the viability of potential developments of the Company's projects, and consequently the value of those projects, and the value of the Company's assets.

18.10 First Nations

First Nation rights and title are still being discussed, claimed, and litigated in Canada, including Yukon. This involves relationships between First Nation governments and federal, provincial, and territorial governments. Future claims could lead to delays, interruptions, or extra costs for the Project. These risks may have increased after the Supreme Court of Canada's decision on June 26, 2014, in the case of Tsilhqot'in Nation v. British Columbia. Governments must consult with Indigenous peoples and sometimes accommodate their interests when granting mineral rights or changing project approvals. This could impact the Company's ability to grow, transfer current operations, or start new projects.

In Yukon, 11 out of 14 First Nations have made land claim agreements under the Yukon Umbrella Final Agreement. The Kaska First Nations have not made such an agreement and claim their traditional rights and ownership of their land. The Kudz Ze Kayah Project is located in Kaska traditional territory. The Company has a Socio-Economic Participation Agreement with the Ross River Dena Council, dated April 1, 2004, and transferred to the Company on January 14, 2015. This agreement allows for cooperation in exploration and development activities. However, the Kaska Nations may still make additional claims against the Company in the future.

Staking and recording Mineral Claims in much of the Watson Lake District and part of the Mayo Mining District is currently not allowed because of a moratorium imposed by the Yukon Government. The Kudz Ze Kayah Project is in this area, but the Company's current mineral claims are not affected. The moratorium gives the Yukon Government time to follow a court ruling from 2012, which states that they must consult with the First Nation before recording any Mineral Claims in their traditional lands. The same rights were also given to the Kaska Dena Council and Liard First Nation through an agreement with the Yukon Government. The Yukon Government has been trying to find a way to include consultations while still allowing free entry for Mineral Claims, but negotiations have not been successful so far, partly because of overlapping land claims by the First Nations.

The Company's advancement from exploration to development and mining relies on maintaining strong relationships with First Nations in its Mineral Claims areas. Future negotiations with Kaska governments and other stakeholders are uncertain. Disputes with First Nations may negatively impact operations and delay exploration or development of Mineral Claims.

18.11 Land access and cultural heritage and archaeological risk

The Company needs access to land to carry out exploration and development work. This access can be influenced by who owns the land, local land use plans, and land claims, which may require compensation agreements with landowners or residents. Nearby communities can impact the Company's work by limiting access for equipment, supplies, and staff, or by raising legal issues. The Company's operations may be adversely affected or delayed in the event of a dispute with a landowner or if there is any other difficulty obtaining land access.

The Company's project areas may contain sites of cultural or archaeological significance, which would need to be avoided when carrying out field programs and project development.

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18.12 Climate change and Carbon Taxes

The Company's activities and operations must comply with laws and regulations, including any amendments, pertaining to climate change mitigation, specific taxes or penalties for carbon emissions, and environmental damage. Additionally, other potential constraints on the mining industry could negatively affect the Company.

Although the Company's financial models include consideration of Canadian carbon tax initiatives, the government policy settings may change over time and there can be no guarantee that the Company will not be impacted by these matters.

Climate change can lead to unexpected physical or environmental risks for the Company. This includes more severe weather, more extreme weather events, and long-term changes in climate. Also, climate change may cause shortages of essential goods needed for the Company's operations, which could affect its ability to produce goods.

18.13 Commodity prices

The value of the Company's assets may be affected by fluctuations in commodity prices and exchange rates, such as the USD denominated copper, zinc, lead, gold and silver prices.

Commodity prices fluctuate and are affected by numerous factors beyond the control of the Company.

Future production from the Company's mineral properties will be dependent upon the copper, zinc, lead, gold and silver prices being sufficient to make these properties economic.

These factors include producer hedging and de-hedging activities, expectations of inflation, expectations of economic activity, investment demand, the exchange rate of the United States dollar to other major currencies, interest rates, global and regional demand, political and economic conditions, production costs, speculative positions taken by investors or traders and changes in supply, including worldwide production levels, global economic trends, confidence and conditions, domestic and international fiscal, monetary and regulatory policy settings, weather patterns and other macro-economic factors. The aggregate effect of these factors is impossible to predict with accuracy.

18.14 Risk Management

A Risk Assessment Workshop was conducted during the 2019 Feasibility Study and a risk register developed to identify the following risks and mitigation measures:

- Five high-level risks.
- 42 medium-level risks.
- 115 low-level risks.

Most risks identified could be mitigated to manageable levels.

ERM notes that an updated risk assessment has not yet been completed. It would be normal practice to revisit the risk assessment as part of ongoing work towards FID, and in ERM's opinion the identified risks from the 2019 work remain a valid and appropriate capture of the project risks.

Of the five remaining high risks, realising full value of the concentrates was the predominant theme of the remaining elevated risks. These risks included:

- Variability in concentrate sea freight costs.
- Variability in treatment charges for concentrates.
- Increasing environmental restrictions on deleterious elements restricting product markets.

- Ability to produce concentrates within target specifications.

Sea freight risks were accounted for through inclusion of the recent market prices in the Feasibility Study financial model. These rates appeared to be near the top of the current cost cycle.

Of the three concentrates produced, zinc concentrates have the highest risk regarding treatment charges due to the volume of zinc concentrate produced and higher treatment charges for zinc concentrates, compared to both copper and HPM concentrates. Uncertainty regarding zinc treatment charges is addressed to some extent through provisions in the Feasibility Study financial model by using the current Agreement's general terms and conditions.

While the expected concentrate qualities are considered complex, assessments have concluded that they can be produced to the target specification, and the Company has mitigated this risk during the project development phase by securing sales agreements ahead of production.

Product quality risks are addressed to an initial extent in the Feasibility Study through testwork, analysis and design initiatives conducted to date. Ongoing management would of course be required during the implementation and operation phases using typical techniques applied to the mining and processing functions.

The fifth remaining high risk was in relation to the Upper and LWMP embankments and reflects the importance of these structures to the operation. It should be noted that these structures are not considered to be an elevated risk. Rather, the rating reflects the conservatism and limitations of the assessment criteria, as far as the "Likelihood" was considered to be at the low end of the "rare" classification (significantly less than 10% chance of occurring threshold for a "rare" classification) and no more appropriate criteria was available to apply.

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19. CONCLUSIONS

The Kudz Ze Kayah Project contains economically significant polymetallic VHMS deposits, with additional deposits known in the surrounding district. ERM considers that the Kudz Ze Kayah Project holds good potential for the discovery of further VHMS deposits and extensions to known mineralisation.

Numerous targets have been identified that are worthy of drill testing as is the case in known VHMS districts. Geochemical and geophysical anomalies have been identified across the project tenements, which are worthy of further exploration work to define drilling targets.

ERM notes the Mineral Assets at a similar stage of development are inherently speculative in nature given the uncertainty in geological interpretations.

BMC has assembled an exploration team which has developed a strong understanding of the VHMS mineralising systems drilled to date and is showing considerable success at applying this knowledge to the discovery of additional mineralisation.

The Company has completed extensive reviews of the Kudz Ze Kayah Project since acquisition of the project. These reviews have been multi-disciplinary and improved the understanding of the geological framework and controls on VHMS mineralisation in the region.

The Kudz Ze Kayah Project comprises a wide range of base metal targets for exploration from near grassroots geochemical anomalies, conceptual geological and geophysical targets to drill ready targets (Fuego, Wolverine extensions, Kona stacked lens, Krakatoa extensions) and advanced stage deposits consisting of Ore Reserves (ABM), Mineral Resources (Kona) and formally defined JORC Code Exploration Targets (GP4F, Wolf and Kona).

In addition to this, large sections of ground within the Kudz Ze Kayah Project remain under-explored. BMC's ABM Deposit remains open beyond the existing Ore Reserves and additional drilling is required to fully define the extents of the mineralisation.

BMC proposes the following actions to further the exploration and evaluation of extensions to the ABM, Kona, GP4F and Wolf deposits.

- Diamond drilling (infill and extensional) into the three defined Exploration Targets (GP4F, Kona, and Wolf).
- Diamond drilling to test defined targets down plunge, down dip, along strike, and fault-offset of the known deposit extents (ABM, Kona), which are defined by interpretation of current geophysical, geochemical, and geological datasets.
- Implement geophysical surveys (electromagnetic (EM), induced polarisation (IP) and magnetics) over potential extensions to the known deposits. Test geophysically-defined targets with diamond drilling and down-hole EM.
- Testwork and studies on "Modifying Factors", such as metallurgy, to determine whether additional mineralisation may have potential feasibility.

BMC proposes the following actions to further the exploration of the KZK, Kona, Wolf, and Pelly properties:

- Diamond drilling to follow-up previous significant intersections at existing prospects, including ABM extensions, Kuril, Fuego, GP4F extensions, Rhyolite Peak, Krakatoa, Kona extensions and Wolverine extensions.

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- Implement geophysical surveys (EM, IP, and magnetics) over prospective formations with coincident geochemical anomalies and/or geological attributes. Follow with diamond drill testing of geophysically-defined targets.
- Detailed structural and geochemical analysis to understand the timing of mineralisation, stratigraphy, and geological controls. Improved understanding of the deposit controls will aid in more regional exploration efforts across the Kudz Ze Kayah Project.
- Implement broad-based geological mapping, geochemical sampling, and geophysical surveys over the remainder on the Kudz Ze Kayah Project tenure to assess for subtle signs of VHMS mineralisation (refer above point).

ERM notes the Mineral Assets at a similar stage of development are inherently speculative in nature given the uncertainty in geological interpretations.

19.1 Reasonable Basis Discussion

A considerable volume of work on the ABM Mine Project has been completed, including a comprehensive range of studies, and updates to those studies (for aspects that are subject to changes over time, such as costs and commodity prices), have been completed.

The technical studies completed by the Company demonstrate that it is reasonable to expect that the project will be economically viable and that the forecasts are achievable. The technical work has been completed by senior and experienced individuals across the full range of the inputs.

The Feasibility Study-level investigations presented in this Report support a Production Target and forecast financial information for the ABM Mine Project and are based on updated Feasibility Study-level investigations for the ABM Mine Project.

The Ore Reserve and Mineral Resources underpinning the production target and forecast financial metrics have been prepared by Competent Persons in accordance with the requirements of the JORC Code. Modifying Factors informing the Ore Reserve estimate are based on extensive and detailed studies.

All material inputs to the production schedule forecasts and forecast financial metrics summarised in this Report are at the level of confidence expected for a Feasibility Study and provide a reasonable basis for the disclosed information.

The Life of Mine Plan (LOM Plan) and subsequent production target and forecast financial metrics are based on Probable Ore Reserves derived from Indicated Mineral Resources; no Inferred Resources have been included in the LOM Plan.

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20. ACRONYMS, ABBREVIATIONS, UNITS OF MEASUREMENT

Item	Description
°	degrees
2D	two-dimensional
3D	three-dimensional
A x b	impact breakage parameters
A$ or AUD	Australian Dollars
AA	atomic absorption
AAS	atomic absorption spectrophotometry
Acme	Acme Analytical Laboratories
AEG	Ensero Solutions (formerly AEG/Alexco Environmental Group)
Ag	silver
AIG	Australian Institute of Geoscientists
AISC	all-in sustaining costs
Al	aluminium
Allnorth	Allnorth Consultants Ltd
ALS	ALS Global includes ALS Perth, ALS Adelaide, ALS Kamloops laboratories
Amax	Amax Potash Ltd
AMC	AMC Consultants Pty Ltd
APS	azimuth positioning system
ARD	acid rock drainage
As	arsenic
ASIC	Australian Securities and Investments Commission
ASL	Above sea level
ASX	Australian Securities Exchange
Atlas	Atlas Copper Ltd
Atna	Atna Resources Ltd
Au	gold
AusIMM	Australasian Institute of Mining and Metallurgy
Ba	barium
BC	British Columbia
Bi	bismuth
BMC	BMC Minerals Ltd (or the Company)
BWI	bond ball mill work index
°C	degrees Celsius
C$ or CAD	Canadian dollars
Cassiar	Cassiar Asbestos Corporation
Cd	cadmium

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Item	Description
CEP	consultation and engagement plan
CERL	Cominco Exploration Research Laboratory
Challenger	Challenger Geomatics Ltd
CIM	Canadian Institute of Mining, Metallurgy, and Petroleum
cm	centimetre(s)
Columbia	Columbia Gold Mines Ltd
CO_2-e	Carbon dioxide equivalent
CRM	certified reference material
CSA Global	CSA Global Pty Ltd, acquired by ERM in 2019
Cu	copper
Cube	Cube Consulting Pty Ltd
CV	coefficient of variation
CY	calendar year
DC	direct current
DCP	double corrosion protected
DEM	digital elevation model
DFO	Canadian (Federal) Department of Fisheries and Oceans
DHEM	down-hole electromagnetic
dmt	dry metric tonne(s)
DWI	drop weight index
EDTA	ethylene diamine tetra acetic acid
EM	electromagnetic
EMR	(Government of Yukon's) Department of Energy, Mines, and Resources
Ensero Solutions	Ensero Solutions (formerly AEG/Alexco Environmental Group)
EPC	engineering, procurement, and construction
EPCM	engineering, procurement and construction management
Equity	Equity Exploration Consultants Ltd
ERM	ERM Consultants Australia Pty Ltd, previously CSA Global
ESG	environmental, social, and governance
Expatriate	Expatriate Resources Ltd
FA	fire assay
FCCOG	fully costed cut-off grade
Fe	iron
FS	Feasibility Study
FEL	front-end loader
FLC	Finlayson Copper Ltd
FLTEM	fixed loop transient electromagnetic
FOB	free on board

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Item	Description
FRS	fibre-reinforced shotcrete
g	gram(s)
G&A	general and administration
g/cm^3	grams per cubic centimetre
g/t	grams per tonne (equivalent to parts per million)
GPS	global positioning system
ha	hectare(s)
HDPE	high-density polyethylene
HDS	high-density sludge
Hg	mercury
HLEM	horizontal loop electromagnetic
HPM	high precious metals (concentrate)
HSE	health, safety, and environmental
HV	high voltage
HVAC	heating, ventilation, and air conditioning
ICOG	incremental cut-off grade
ICP-AES	inductively coupled plasma-atomic emission spectroscopy
ICP-MS	inductively coupled plasma mass spectrometry
ID2	inverse distance squared
ID3	inverse distance cubed
IFRS	International Financial Reporting Standards[17]
IP	induced polarisation
IRA	inter-ramp slope angle
IRR	internal rate of return
ISC	Integrated Sustainability Consultants Inc.
km, km^2	kilometre(s), square kilometre(s)
KNA	kriging neighbourhood analysis
koz	kilo-ounces (or thousands of ounces)
kPa	kilopascal(s)
kt	kilo-tonnes (or thousand tonnes)
ktpa	kilo-tonnes (or thousand tonnes) per annum
kV	kilovolt(s)

[17] Important Note: The financial forecasts in this Report are Non-IFRS Financial Measures. ERM considers these measures provide useful information about the financial outcomes derived from the Feasibility Study, however, they should not be considered in isolation or as a substitute for measures of performance or cash flow prepared in accordance with IFRS.

Since the financial forecasts and economic discussion in this Report are not based on IFRS, they do not have standardised definitions and the way these measures have been derived may not be comparable to similarly titled measures used by other companies. Investors should therefore not place undue reliance on these Non-IFRS Financial Measures.

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Item	Description
kW	kilowatt(s)
L/s	litres per second
LA-ICP-MS	laser ablation inductively coupled plasma mass spectrometry
lb	pound(s)
LBMA	London Bullion Market Association
LFN	Liard First Nation
LiDAR	light detection and ranging (survey)
LNG	liquified natural gas
LOM	life-of-mine
LWMP	Lower water management pond
m	metre(s)
M	million(s)
MAMA	month after month of arrival
MBps	megabytes per second
MD	mechanical dynamic
Merah	Merah Resources Ltd
mg/L	milligrams per litre
Minnovo	Minnovo Pty Ltd
MinQuest	MinQuest Limited
Mlb	million pounds
MLU	Mining Land Use Approval
mm	millimetre(s)
Mm^3	million cubic metres
Moz	million ounces
MRE	Mineral Resource estimate
mRL	metres Relative Level
MSO	mineable shape optimiser
Mt	million tonnes
Mtpa	million tonnes per annum
MW	megawatts
NAD83	North American Datum of 1983
NI 43-101	National Instrument 43-101
NPV	net present value
NSR	net smelter return
NTS	National Topographic System
OK	ordinary kriging
OSA	overall slope angle
oz	troy ounce

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Item	Description
PAG	potentially acid generating
Pb	lead
PDC	process design criteria
PDT	project delivery team
PFS	Preliminary Feasibility Study
pH	acidity or alkalinity of a solution
Pioneer	Pioneer Laboratories Inc.
Placer Dome	Placer Dome Inc.
PLC	programmable logic controller
PMPA	Precious Metals Purchase Agreement
PMVB	Pelly Mountains Volcanic Belt
ppm	parts per million
QA	quality assurance
QAQC	quality assurance and quality control
QC	quality control
QGIS	Open-source Geographical Information System
Q-Q	quantile-quantile
R^2	coefficient of determination
RCP	Reclamation and Closure Plan
Re-stated Feasibility Study	Re-stated Feasibility Study
RFQ	request for quotation
RL	reduced level
ROM	run-of-mine
RPEEE	reasonable prospects for eventual economic extraction
RQD	rock quality designation
RRDC	Ross River Dena Council
RTK	real-time kinematic
RWI	bond rod mill work index
S	sulfur
SAG	semi-autogenous grinding
Sb	antimony
SCADA	supervisory control and data acquisition
Se	selenium
SEDAR	System for Electronic Document Analysis and Retrieval
SEPA	Socio-Economic Participation Agreement
SG	specific gravity
SGS	SGS Canada Inc.

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Item	Description
SLL	safe lifting limit
SMC	semi-autogenous grinding mill comminution
SQUID	superconducting quantum interference device.
t	metric tonne(s)
t/m^3	tonnes per cubic metre
Tl	thallium
tpd	tonnes per day
tph	tonnes per hour
UG	underground
U-Pb	Uranium-lead
US$ or USD	United States dollars
UTEM™	University of Toronto Electro-Magnetometer
UTM	Universal Transverse Mercator
V	volt
VALMIN	The Australasian Code for Public Reporting of Technical Assessments and Valuations of Mineral Assets, 2015 Edition.
VHF	very high frequency
VHMS	volcanic-hosted massive sulfide
VMS	volcanogenic massive sulfide
VSHMS	volcanic and sediment-hosted massive sulfide
VTEM™	versatile time domain electromagnetic
WA	Western Australia
Welcome North	Welcome North Mines Ltd
Wheaton	Wheaton Precious Metals Corp
wmt	wet metric tonne(s)
WSF	waste storage facility(s)
WTP	water treatment plant
XRF	x-ray fluorescence
YESAA	Yukon Environmental and Socio-economic Assessment Act
YESAB	Yukon Environmental and Socio-economic Assessment Board
YG	Yukon Government
Zn	zinc

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21. GLOSSARY

1st BASE Property	The collective Mineral Claims comprising the 1st BASE Claim Block as set out in Schedule A of the Solicitor's Tenement Report.
2019 Feasibility Study	Informal term used by the Company to describe the Feasibility Study reported in 2019, see Feasibility Study below.
2020 Re-stated Feasibility Study	Informal term used by the Company to describe the Feasibility Study reported in November 2020, using long-term consensus C$:US$ exchange metal prices and rate as of 30 October 2020 and all capital, operating, and realisation costs as outlined in the 2019 Feasibility Study.
2023 Economic Update	Informal term used by the Company to describe its updated project costs and economic outcomes for the proposed ABM Mine Project based upon physicals derived from the 2020 Re-stated Feasibility Study and taking into consideration updated estimates of operating and capital costs, the PMPA, conditions in the Decision Document (2022), concentrate offtake agreements, changes to the carbon pricing mechanism, updated commodity prices and foreign exchange rates.
AIG	Australian Institute of Geoscientists
All-in Sustaining Costs (AISC)	Includes C1 cash costs, plus exploration costs at the ABM Mine Project and sustaining capital expenditures (including progressive expansion of WSF, permitting, and customary improvements to the operations over the life of the ABM Mine Project). AISC is divided by the number of payable pounds of zinc or ounces of silver, estimated to be produced for the period to arrive at AISC per zinc pound or silver ounce produced *(Note: a non-IFRS Financial Measure)*
Average Annual Steady-State Rate of Production	The average annual production over the life of the ABM Mine Project, excluding production from the first and final years of the ABM Mine Project (as they are periods of lower production due to project ramp-up and end of operations).
ARD	Acid Rock Drainage
AusIMM	Australasian Institute of Mining and Metallurgy
Base Case	Estimated forecast base case economic results as contemplated in the 2019 Feasibility Study and subsequent updates.
C1 Cash Cost	Net Direct Cash Cost (C1) represents the cash cost incurred at each processing stage, from mining through to recoverable metal delivered to market, less net by-product credits (if any), divided by the number of payable pounds of zinc or ounces of silver, estimated to be produced for the period to arrive at C1 Cash Cost per zinc pound or silver ounce produced. *(Note: a non-IFRS Financial Measure)*
Claim Block	A group of Mineral Claims
Crown Land	Land vested in His Majesty in right of Canada, whether the administration, and control thereof is appropriated to the Commissioner of Yukon or not but does not include settlement land.
CT-bolt	Combination rock bolt used for ground support
Cut-off grade	The lowest grade, or quality, of mineralised material that qualifies as economically mineable and available in a given deposit.
DEM	Digital Elevation Model
Decision Body (Bodies)	A federal, territorial or First Nation government, or agency, which regulates, and permits the proposed activity. For the ABM Mine Project proposal, the designated bodies comprise the Government of Yukon, Fisheries and Oceans Canada, and Natural Resources Canada.
Decision Document	A document that the Decision Body(s) will issue, in writing, that accepts, varies or rejects the recommendation provided at the end of the environmental and socio-economic assessment undertaken by YESAB of the ABM Mine Project proposal. Once the Decision Document has been issued, an agency can issue authorisations or permits in accordance with their process.
Density (bulk density)	Measure of quantity of mass per unit volume.
Dilution	Waste which is unavoidably mined with ore.
Direct Cash Cost	Direct Cash Cost covers: Mining, ore freight, and milling costs Ore purchases and freight costs from third parties in the case of custom smelters or mills Mine site administration and general expenses Concentrate freight, smelting, and smelter general and administrative costs Materials freight, refining, and refinery general and administrative costs Marketing costs (freight and selling) (Note: a non-IFRS Financial Measure)
Discount Rate	A discount rate is the rate of return used to discount future cash flows back to their present value. This rate is often a company's weighted Average Cost of Capital (WACC), required rate of return, or the hurdle rate investors expect to earn relative to the risk of the investment. The discount rate used by the Company is 7%. as the project is anticipated to derive similar levels of revenue from both precious metals and base metals. (Note: a non-IFRS Financial Measure)

Exploration Target or ET	Has the meaning given to the term "Exploration Target" in the JORC Code, being a statement or estimate of the exploration potential of a mineral deposit in a defined geological setting where the statement or estimate, quoted as a range of tonnes and a range of grade (or quality), relates to mineralisation for which there has been insufficient exploration to estimate a Mineral Resource.
Feasibility Study	Has the meaning given to that term in the JORC Code, being a comprehensive technical and economic study of the selected development option for a mineral project that includes appropriately detailed assessments of applicable Modifying Factors together with any other relevant operational factors and detailed financial analysis that are necessary to demonstrate at the time of reporting that extraction is reasonably justified (economically mineable).
Fibrecrete	Fibre-reinforced concrete
Final Investment Decision, FID	A formal decision by the Board to proceed with construction and operation of the ABM Mine Project.
Final Screening Report	The report and recommendation issued by the YESAB executive committee under section 58 of the YESAA at the conclusion of screening of the proposed project by the executive committee.
Free Cash Flow	The cash a company generates after accounting for cash outflows to support operations and maintain its capital assets.
Freshet	The flood of a drainage, it is most commonly used to describe a snowmelt, an annual high-water event on rivers resulting from snow and river ice melting.
Fully costed cut-off grade	The lowest grade of Measured and Indicated mineralisation that covers all operating costs associated with mining.
Fyre Lake Claim Block	Those Mineral Claims that comprise the Claim Blocks set out in Appendix B and owned by Finlayson Copper Ltd.
Geotechnical investigation	A study which investigates the soil and rock structure of a particular site, as well as the passing of water above and beneath the surface.
Geotechnical IRA slope	Geotechnical inter-ramp slope angle.
Geotechnical OSA slope	Geotechnical overall slope angle.
GP4F or GP4F Prospect	An exploration prospect located east-southeast of the ABM Deposit and including the GP4F ET.
Gross Revenue	Revenue from sale of mineral concentrates, being the sum of the quantity of each payable metal multiplied by the sale price for each metal, prior to any deductions related to the sale of the concentrates. (Note: a non-IFRS Financial Measure)
HPM	High precious metals, and in the case of a HPM concentrate means a sulfide concentrate in which the value of contained precious metals (gold and silver) exceeds 50% of the value of all economic metals contained in the concentrate.
Hydrology, Hydrological	Pertaining to water either above or below the surface.
Incremental cut-off grade	The lowest grade of Measured and Indicated mineralisation that covers underground production mining, load, and haul, direct processing, and general, and administration costs.
Internal Rate of Return (IRR)	Is the discount rate that makes the NPV of a project zero. In other words, it is the expected compound annual rate of return that will be earned on a project or investment. The IRR formula is as follows: $0 = CF_0 + \frac{CF_1}{(1+IRR)} + \frac{CF_2}{(1+IRR)^2} + \frac{CF_3}{(1+IRR)^3} + \ldots + \frac{CF_n}{(1+IRR)^n}$ Where: CF0 = the initial Investment / Outlay, CF1, CF2, CF3…CFn = Cash Flows, n = Period Number, IRR = Internal Rate of Return (Note: this is a non-IFRS Financial Measure)
JORC Code	Means the Australasian Code for Reporting of Exploration Results, Mineral Resources, and Ore Reserves (2012 edition).
KE Property or KE Claim Block	The collective Mineral Claims comprising the KE Claim Block as set out in Schedule A of the Solicitor's Tenement Report.
Kona Property or Kona Claim Block	The collective Mineral Claims comprising the Tsa Da Glisza Claim Block and the Fyre Lake Claim Block as set out in Schedules A and B respectively of the Solicitor's Tenement Report (which includes the Kona Deposit and the Kona ET).
MER Property or MER Claim Block	The collective Mineral Claims comprising the MER Claim Block as set out in Schedule A of the Solicitor's Tenement Report.
Mineral claim	A plot of ground staked out and acquired under the Quartz Mining Act (Yukon), Quartz Mining Act (Canada) or regulations or orders in council in force prior to 19 July 1924 providing the holder thereof a chattel interest, equivalent to a lease of the minerals in or under the land for one year, and thence from year-to-year, and the right to enter, prospect and mine for minerals thereon subject to the reservations and exceptions under the Quartz Mining Act (Yukon).
Mineral Resource	Has the meaning given to that term in the JORC Code, being a concentration or occurrence of solid material of economic interest in or on the Earth's crust in such form, grade (or quality), and quantity that there are reasonable prospects for eventual economic extraction.
Modifying Factors	Has the meaning given to that term in the JORC Code, being considerations used to convert Mineral Resources to Ore Reserves. These include, but are not restricted to, mining, processing, metallurgical, infrastructure, economic, marketing, legal, environmental, social, and governmental factors.

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Net Present Value (NPV)	Is the value of all future cash flows (positive and negative) over the entire life of an investment discounted to the present. NPV analysis is a form of intrinsic valuation analysis used extensively across finance and accounting for determining the value of a business, investment security, capital project, new venture, cost reduction programme, and anything that involves a cash flow. The cash flows are "real" cash numbers (not nominal), taking inflation into account. The NPV formula is as follows: $NPV = \sum_{t=1}^{n} \frac{R_t}{(1+i)^t}$ Where: R = net cash inflow-outflows during a single period t, i = discount rate or return that could be earned in alternative investments, t = time of cash flow, n = number of time periods. (Note: a non-IFRS Financial Measure)
Net Revenue	Gross Revenue less the costs and charges incurred in selling and delivering the concentrate to market once concentrate departs the mine site. It includes deductions for road and sea freight, freight insurance, concentrate treatment, and refining charges and concentrate penalty costs. (Note: a non-IFRS Financial Measure)
NSR	Net Smelter Return (Free on Board, FOB) Mine Gate and Royalties by unit of metal in ROM feed. (Note: a non-IFRS Financial Measure)
Operating Cash Flow Margin	A cash flow ratio which measures cash from operating activities as a percentage of sales revenue in each period. It has been calculated by net income + non-cash expenses (depreciation and amortisation) + change in working capital. (Note: a non-IFRS Financial Measure)
Operating Margin	A ratio that measures how much profit a company makes on a dollar of sales after paying for variable costs of production such as wages and raw materials, but before paying interest, or tax. It is calculated by dividing a company's operating income by its sales revenue. (Note: a non-IFRS Financial Measure)
Ore Reserve or Reserves	Has the meaning given to that term in the JORC Code, being the economically mineable part of a Measured and/or Indicated (as those terms are defined in the JORC Code) Mineral Resource.
Payback Period	The payback period shows how long it takes a business to recoup its investment. This type of analysis allows firms to compare alternative investment opportunities and decide on a project that returns its investment in the shortest time, if that criterion is important to them. (Note: a non-IFRS Financial Measure)
Pelly Property or Pelly Claim Block	The collective Mineral Claims comprising the Pelly Claim Block as set out in Schedule A of the Solicitor's Tenement Report.
Pre-Feasibility Study	Has the meaning given to that term in the JORC Code, being a comprehensive study of a range of options for the technical and economic viability of a mineral project that has advanced to a stage where a preferred mining method, in the case of underground mining, or the pit configuration, in the case of an open pit, is established, and an effective method of mineral processing is determined. It includes a financial analysis based on reasonable assumptions on the Modifying Factors and the evaluation of any other relevant factors which are sufficient for a Competent Person, acting reasonably, to determine if all or part of the Mineral Resources may be converted to an Ore Reserve at the time of reporting. A PFS is at a lower confidence level than a Feasibility Study.
Pre-production Capital	Capital expenditures including capitalised development costs incurred to build the ABM Mine Project prior to commencement of production. (Note: a non-IFRS Financial Measure)
Quartz Mining Licence	Mining licence issued under section 135 of the Quartz Mining Act (Yukon).
RB Property or RB Claim Block	The collective Mineral Claims comprising the RB Claim Block as set out in Schedule A of the Solicitor's Tenement Report.
Rivier Property or Rivier Claim Block	The collective Mineral Claims comprising the Rivier Claim Block as set out in Schedule A of the Solicitor's Tenement Report.
Run-of-mine	Raw mined mineralised material above economic cut-off grade, as it is delivered to the processing plant, prior to treatment of any sort.
SMC Test	A laboratory comminution test which provides a range of information on the breakage characteristics of rock samples for use in the mining/minerals processing industry.
Specific gravity	A ratio which for all practical purposes is equivalent to density expressed in t/m^3.
Sustaining Capital	The continuous and ongoing investment of capital necessary to maintain steady-state operations at the ABM Mine Project after it has reached nameplate production. (Note: a non-IFRS Financial Measure)
Total Capital	Pre-production capital plus Sustaining Capital. (Note: a non-IFRS Financial Measure)

Tote Road	Existing Road from the Robert Campbell Highway to the ABM Mine Project
Tsa Da Glisza Claim Block	Those Mineral Claims that comprise a subset of the Kona Property as set out in Schedule A of the Solicitor's Tenement Report.
VMS	Volcanogenic Massive Sulfides
Waste rock	Rock with an insufficient metal content to justify processing.
Water Licence	Class A or B water licence issued pursuant to the Waters Act (Yukon).
Wolf Property or Wolf Claim	The collective Mineral Claims comprising the Wolf Claim Block as set out in Schedule A of the Solicitor's Tenement Report (which includes the Wolf ET).

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APPENDIX A: JORC CODE TABLE 1 – KZK PROPERTY

Covering the ABM Deposit Ore Reserve and Mineral Resource estimate, GP4F Exploration Target, KZK Property Exploration Results, and Pelly Property Exploration Results.

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Section 1: Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections)

Criteria	Commentary
Sampling techniques	The ABM Zone was sampled using core drill holes at nominal 50 m spacing on 25 m north-south oriented sections extending out to 100 m on the peripheries of the deposit. The Krakatoa Zone was sampled targeting pierce points of 25 m to 60 m in the central portion of the deposit to 100 m on the peripheries. The GP4F Exploration Target (ET) was sampled using core drill holes at 50–75 m spacings on 50 m north-south oriented sections extending out to greater than 100 m on the periphery of the deposit. A number of targets have been tested with scattered core drill holes. Exploration holes testing regional targets were sampled using core drill holes at variable spacing. Drilling at the Project was completed by Cominco from 1994 through 1998 (199 holes). Since 2015, BMC Minerals Ltd completed a further 165 holes for 31,036 m at the ABM Deposit. A total of 335 diamond core drill holes were used to define the ABM Deposit and for resource estimation for 55,782 m of drilling. 241 assayed drill holes intersect the interpreted mineralisation zones. ABM holes were generally angled (–30° to –90°) towards grid south with dip angles set to optimally intersect the mineralised horizon. Approximately 20% of the holes have been drilled vertically. Krakatoa holes mostly drilled grid southwest and angled at –30° to –90° to avoid bounding faults. Only one hole was drilled vertically. GP4F drill holes were generally angled (–45° to –90°) towards grid south with dip angles set to optimally intersect the mineralised horizon. Of the 27 holes drilled, two were drilled vertically. Exploration holes testing regional targets were angled (generally between –45° to –90°) with the hole azimuth based on interpreted geology or access. From 1994 to 1998 a total of 29 exploration drillholes were completed by Cominco for 3,970.9m of drilling. BMC has, since 2015, completed a total of 79 exploration drillholes for 22,767.2m of drilling. Significant geochemical surveys have been undertaken away from the known deposits by BMC and Cominco. Surface exploration on the Properties has included the use of silt sampling from streams, soil sampling, rock chip sampling and trenching. BMC soil samples were analysed using an aqua regia digest with an ICP-MS finish. as well as fire assay with an AAS finish for gold. BMC samples were analysed at SGS Vancouver. Quality assurance and quality control (QAQC) was monitored by inserting blanks (silica powder) and field duplicates into the sample stream, at rates of approximately one for every 40 samples.
	Diamond core drilling was used across the KZK Property for all resource definition and exploration drilling. Core was used to obtain high-quality samples that were logged for lithological, structural, density, and other attributes. Cominco: Drill hole locations were originally picked up by survey contractors. Majority of the holes have used “single-shot”, acid-etch style down-hole surveys taken approximately every 30 m down-hole. In 2015, BMC resurveyed a total of 66 Cominco collar locations using a real-time kinematic global positioning system (RTK-GPS), the results of which confirmed the accuracy and location of the historical surveys. BMC drilling indicates no significant issue with Cominco drill hole survey data. Limited quality assurance procedures and quality control results have been documented in various internal reports. A selection of drill holes from three sections were sampled and re-assayed at SGS Laboratory in Burnaby, BC (Vancouver) using the same assaying methodology as the 2015 programme. BMC: Proposed drill hole locations were surveyed and marked by survey contractors prior to drilling. After drilling was completed a total of 161 holes were surveyed by survey contractors and the remaining five were located via an azimuth positioning system (APS) for X and Y coordinates and RL from a DEM derived from a LiDAR survey. Holes were surveyed using a Reflex EZ-Shot on advancement of the hole. Readings were captured below the collar and at 25 m intervals thereafter. In 2016, 30 holes were surveyed using a Reflex Gyro Non-magnetic instrument upon completion of the holes. The use of the Gyro orientation tool continued for all inclined holes in bedrock for the 2017 and 2018 exploration seasons. All 2024 season holes were downhole surveyed using a Devico Devigyro tool supplied by IMDEX Limited.

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Criteria	Commentary
	No documented QAQC procedures have been located for the Cominco drilling programmes. The 2015–2016 BMC field QAQC programmes entailed submission of coarse blank material every 20th sample and CRM every 20th sample. CRM was selected in several grade ranges and manufactured from sulfide ore similar to the target mineralisation. Approximately 3% of samples analysed were submitted to an alternate laboratory for umpire analyses. Additional quartz wash was inserted in the pulverizing stage between major changes in intensity of mineralisation. Quartz wash residues were retained for possible later analyses. Wet screen analyses were completed every 50th sample. Based on an assessment of the past reports, historical drilling results, and review of the current procedures, ERM considers the entire dataset to be acceptable for use in Mineral Resource estimation.
	Cominco: In 1994, all sulfide intersections were sawn with an open circulation rock saw and in 1995, all samples were split by hydraulic splitter, typically into 1.5 m long samples. Samples were sent to Cominco Exploration Research Laboratory (CERL) in Vancouver. Samples were subjected to a three-stage crushing procedure, pulverised, and screened to -150 mesh prior to aqua regia digestion (and solvent extraction in the case of gold) and assaying. Details of the post-1995 sampling and preparation procedures have not been located but the Competent Person considers that it is reasonable to assume that similar procedures have been followed to those used previously. BMC: All sulfide intersections were sawn using an open-circulation rock saw, typically into 1.0 m long samples. Samples were sent to SGS Vancouver. Samples were weighed, dried and crushed to 75% passing 2 mm, with a 250 g split pulverised to 85% passing 75 microns. Gold was analysed by 30 g fire assay with an atomic absorption spectrophotometry (AAS) finish and silver analysed by inductively coupled plasma (ICP) with an AAS finish on a 2 g two-acid digest aliquot. Gold and silver over limits were triggered at Au >5 g/t and Ag >150 g/t respectively, resulting in re-analysis using a 30 g fire assay with gravimetric finish. Assay results for copper, lead, zinc, barium, sulfur, and iron were completed using a sodium peroxide fusion and ICP-AES analysis. Select samples were analysed for trace elements including As, Bi, Hg, Sb and Se using aqua regia digest and ICP-MS finish. Sulfide intersections from exploration holes drilled in 2024 were sent to ALS in Vancouver. Analytical techniques for Au were the same as at SGS. A suite of 48 elements including Cu, Pb, Zn and Ag were analysed using a 4-acid digest and ICP-MS finish. Over limits were analysed using in ICP-AES finish.
Drilling techniques	Cominco: All Cominco drilling at the deposit was NQ size diamond core and was not oriented. BMC: BMC drilling was composed of NQ3 and HQ3 size drill core. Larger diameter core was used where wedging from parent holes to retrieve core used for metallurgical studies was required. For ABM, 109 holes were completed using HQ3 and 57 completed using NQ3 tools. For GP4F, 17 drill holes of HQ3, HQ, and NQ3 were completed. Triple tube coring with inner split tubes were used to maximise recovery. All core was oriented from 20 m above the mineralised zone to the end of hole using the Reflex ACTII RD core orientation system.
Drill sample recovery	Diamond core was visually logged for every hole and recorded in the database. The historical drilling database only recorded sample recovery for core holes drilled in 1998. Significant core loss has been recorded over some mineralised intervals, although the weighted average recovery recorded was 93%. The 1995 PFS (not code compliant) document reported: "Preliminary rock quality data interpreted from drill core, indicates that the western and central portions of the deposit yield fair (50–75%) to good (75–90%) rock quality designation (RQD) values while the eastern portion yields poor (25–50%) to fair (50–75%) RQD values". Drilling recovery and RQD was recorded for all BMC holes. Rock quality was good with recovery values averaging greater than 90% and RQD values confirm the same distribution delineated in the historical data. Special attention was paid to recovery through mineralised intervals, and several mineralised intervals were redrilled to achieve better recoveries.
	ERM is not aware of the historical drilling practices employed to maximise recoveries. However, visual inspection of numerous historical holes displayed excellent core recoveries throughout the mineralised zones. Triple tube coring with inner split tubes were used to maximise core recovery for BMC drilling.
	The massive sulfide style of the mineralisation and the consistency of the mineralised intervals are considered to preclude any issue of sample bias due to

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Criteria	Commentary
	material loss or gain.
Logging	Drill core was extensively logged in detail to support historical and current mining feasibility studies. Historical holes drilled by Cominco (KZK) were relogged by BMC to further exploration and ensure consistent geological interpretation for resource definition work.
	Logging of core recorded lithology, mineralogy, mineralisation, structural, weathering, colour, and other relevant features of the samples. Logging is both qualitative (e.g. colour) and quantitative (e.g. mineral percentages). All drill core, including historical core, was photographed.
	All drill holes were logged in full.
Subsampling techniques and sample preparation	All BMC and majority of historical sulfide intersections were sawn with an open-circulation rock saw in half with half core submitted for chemical analysis. It is evident from field observation that some historical core was split with a manual core splitter. The remaining half core was retained for reference and/or further testwork.
	No non-core holes have been drilled.
	In 1994, all sulfide intersections were sawn with an open-circulation rock saw, typically into 1.5 m long samples, and sent to CERL in Vancouver. Samples were subjected to a three-stage crushing procedure, pulverised, and screened to −150 mesh prior to aqua regia digestion (and solvent extraction in the case of gold) and assaying. In 1995, all samples were split by hydraulic splitter, typically to 1.5 m lengths, and subject to the same preparation and analytical procedures as above. Details of the post-1995 sampling and preparation procedures have not been located but it can be assumed that similar procedures to those used previously were adopted. These procedures were considered appropriate “industry standard” techniques at the time. For BMC drilling, all sulfide intersections were sawn using an open-circulation rock saw, typically into 1.0 m long samples. Samples were sent to SGS Laboratory in Burnaby, BC or ALS in Vancouver. Samples were weighed, dried and crushed to 75% passing 2 mm, with a 250 g split pulverised to 85% passing 75 microns. These procedures are considered industry standard techniques and appropriate for the style of mineralisation.
	No documented quality assurance procedures have been located for the Cominco drilling or geochemical programmes. Detailed and systematic quality control programmes do not appear to have been in place during the Cominco drilling; however, it may be that the documentation has not yet been located. Limited umpire assaying was conducted during the 1995 drill programme with good correlation between the results reported. However, this data has not been verified. BMC field QAQC programmes entailed submission of coarse blank material every 20th sample and CRM every 20th sample. CRM was selected in several grade ranges and with a matrix similar to the mineralogy of the ABM Deposit. Overall, the accuracy of the data is considered excellent. Results from the coarse blank material show little evidence of cross contamination. Additional quartz wash was inserted in the pulverizing stage where high-grade mineralisation was suspected. Quartz wash residues were retained for possible later analyses. Wet screen analyses were completed every 50th sample to ensure consistent crush size.
	Although no documentation has been located detailing the result of field duplicates by Cominco, quarter-core resampling by BMC, and visual validation of the logging compared to the assay results supports the representivity of the sampling. In 2015, field duplicates were not collected however remaining half core from 27 historical holes on three sections drilled by Cominco were re-sampled and analysed on the same intervals. Comparison between the Cominco results and the 2015 results delineate the following: Copper – good agreement up to 3% Lead – slight positive bias in SGS data, once samples with>1% Ba were re-assayed

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Criteria	Commentary
	Zinc – positive bias in SGS data >2.6 to 15% Silver – good agreement to 250 ppm Gold – good to fair agreement to 3 ppm Iron – good agreement in the range 8-15%; positive bias in SGS data <8%; negative bias in SGS data between 15% and 20%. Overall agreement between the 2015 and historical data are very good.
	Sample sizes are considered appropriate for the rock type, style of mineralisation (massive sulfides), the thickness, and consistency of the intersections, the sampling methodology, and percent value assay ranges for the primary elements at ABM, GP4F, and exploration prospects.
Quality of assay data and laboratory tests	Following aqua regia digestion (and solvent extraction in the case of gold), all 1994 samples were analysed by AAS for Cu, Pb, Zn, Ag, Au, and Fe. Base metals and iron were then determined using standard wet chemical assay procedures and precious metals were analysed by fire assay. Barium was determined by pressed pellet/x-ray florescence (XRF). All samples were also analysed by multi-element ICP. Similar assaying procedures were used in 1995, although barium, and iron were not assayed. In 1997, a total of 349 core samples were collected. Of these, 320 were analysed for 27 elements by ICP, gold by aqua regia decomposition/AAS and barium by XRF, in addition to whole rock major and minor oxides by XRF and trace elements zirconium and yttrium by pressed pellet AAS at CERL in Vancouver. For drilling conducted in 1998, a total of 197 core samples were collected and analysed for Cu, Pb, Zn, Ag, As, Cd, Co, Ni, Fe, Mo, Cr, Bi, Sb, V, Sn, W, Sr, Y, La, Mn, Mg, Ti, Al, Ca, Na, and K by ICP, Au by aqua regia decomposition/AAS and Ba by XRF at CERL. Intervals with greater than 1% Pb, Zn, or Cu were assayed for Cu, Pb, Zn, Fe (total), Ag (AAS), Au (fire assay with AA and gravimetric finish) and Se by ICP and XRF. For BMC drilling at ABM, a total of 2,906 samples were collected and analysed for Cu, Pb, Zn, Ag, Au, Fe; 2,256 samples for Ba and 2,315 samples analysed for S using a sodium peroxide fusion and ICP-AES finish. The sodium peroxide fusion is a complete digestion. 1,145 samples were analysed for As, Bi, Hg, Sb, and Se using aqua regia digest with ICP-MS finish. Gold was analysed by 30 g fire assay with an AAS finish and silver analysed by ICP with an AAS finish on a 2 g two-acid digest aliquot. Samples that returned >4% Ba were analysed by XRF. Gold and silver over limits were triggered at Au >5 g/t and Ag >150 g/t respectively, resulting in re-analysis using a 30 g fire assay with gravimetric finish. Samples for all exploration holes drilled up to and including 2018, including at GP4F were analysed as above. 2024 exploration samples were sent to ALS in Vancouver where analytical techniques for Au were the same as at SGS. A suite of 48 elements including Cu, Pb, Zn and Ag were analysed using a 4-acid digest and ICP-MS finish. Over limits were analysed using in ICP-AES finish. The 4-acid digest is considered a complete digestion. For surface sampling by BMC post 2015 All samples were submitted to SGS Vancouver in Burnaby, BC, an ISO 9001:2008 certified laboratory (accredited laboratory No. 744). Analysis included: LOG02: Pre-preparation processing, sorting, logging, boxing; PRP89: weigh, dry, crush to 75% passing 2 mm, split 250 g, pulverise to 85% passing 75 µm; GE ICM90A: sodium peroxide fusion/combined ICP-AES and ICP-MS package (56 elements; trace elements); GEICM90AAE: selenium-sodium peroxide fusion; IC-MS GEFAA30V5: 30 g, fire assay, AAS finish for gold; GO-CP90Q: sodium peroxide fusion/ICP-AES package (if required).
	Magnetic susceptibility measurements were recorded for all mineralised intervals in all holes in the 2015 drill programme using an average of three readings per sampled interval from a KT-10 Magnetic Susceptibility Meter. Magnetic susceptibility measurements were collected from a selection of holes at 0.5 m intervals from top to bottom using a MPP Probe M Magnetic Susceptibility Meter. There is no record of Cominco recording magnetic susceptibility in the earlier drilling campaigns.
	No documented quality assurance procedures have been located for the Cominco drilling programmes or surface sampling. The BMC field QAQC programmes entailed submission of coarse blank material every 20th sample and CRM every 20th sample. CRM was selected in several grade ranges and with a matrix similar to the mineralogy of the ABM Deposit. Results from the 2015 CRM analyses indicate a slight positive bias in the lead and zinc data of 2% and 3% respectively while copper, silver, and gold values

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Criteria	Commentary
	indicate a slight negative bias of -1%, -2% and -2.6% respectively. The observed level of bias is acceptable, and the overall quality of data is considered to be good. Vast majority of the CRM analyses from the 2016 drilling lie within one standard deviation of the certified values and average biases are typically less than 2%. Relative standard deviations of the repeat analyses of the CRMs are well less than 5%. Overall, the accuracy of the data based on these results is excellent. Approximately 3% of samples analysed in 2015 were submitted to ALS Minerals for umpire analyses via sodium peroxide fusion and ICP-OES finish. The check assays are in close agreement for copper and zinc while lead shows a slight positive bias relative to SGS and silver a slight negative bias. Gold shows some variability between the two laboratories reflecting the nuggety nature of the gold distribution. Pulps from a total of 38 samples were submitted to ALS in 2016 for check assay using the same analytical methods as those employed at SGS. There is very good agreement between silver values from SGS and ALS. Apart from gold, all the data examined show strong positive correlations between the SGS and ALS data but with a positive bias in the SGS data copper and lead data relative to ALS, and a negative bias for zinc. Overall, there is very good agreement between the SGS and ALS results. Results from the coarse blank material show little evidence of cross contamination. Additional quartz wash was inserted in the pulverizing stage where high-grade mineralisation was suspected. Quartz wash residues were retained for possible later analyses. Wet screen analyses were completed every 50th sample to ensure consistent crush size. There are no significant issues identified in the 2018 or the 2024 QAQC data.
Verification of sampling and assaying	Historical and 2015 drill core has been viewed by the Mineral Resource estimate Competent Person and BMC's Exploration Manager. Visual validation of mineralisation against assay results was undertaken for several holes.
	A total of 10 Cominco holes on three sections were twinned by BMC in 2015. In general, the hole pairs match well in terms of down-hole metal distribution and observable mineralised intersections.
	Cominco: Documentation of data protocols adopted by Cominco have not been located. BMC has validated all historical data against original records to produce a complete database for the KZK Property. BMC: Data are entered in the field into a Geospark database on a Toughbook field laptop. The data was validated in the field and electronically transferred to a Microsoft Access database off site. Further validation was completed via routine queries.
	No adjustments or calibrations were made to any assay data.
Location of data points	Many of the early drill holes appear to have been drilled on a truncated local grid. Following completion, the 1994 Cominco drill hole collars were surveyed by qualified surveyors, McElhanney Consulting Services Limited of Vancouver, BC. The holes were surveyed using static GPS vectors and adjusted by least squares to within two decimal places and are considered accurate. Details of surveying for post-1994 (but pre-2015) drilling have not been identified; however, majority of these holes were located and resurveyed during the 2015 field season. A total of 84 Cominco collars (66 from ABM) were located, verified, and surveyed by Challenger Geomatics in 2015 using Leica Viva (RTK) GNSS resulting in location accuracy of 0.25 m. A total of 158 holes drilled in 2015 and 2016 field seasons by BMC at ABM were surveyed by Challenger Geomatics using Leica Viva (RTK) GNSS resulting in location accuracy of 0.25 m. The remaining six drill holes were located via an APS for X and Y coordinates and RL from a DEM derived from a LiDAR survey. The APS unit is capable of accuracy down to less than 1 m and the vertical precision of the LiDAR survey is 0.1 m. During the 2016 field programme, BMC resurveyed all Cominco collar locations at GP4F, with the exception of K95-167, using a RTK-GPS system the results of which confirmed the accuracy and location of the historical surveys. The single 1995 hole (K95-167) was surveyed at the collar and end-of-hole using a "single shot" survey. The 2018 and 2024 drill collars were pegged with a Garmin GPSmap 62 handheld GPS. After completion of the drill hole, the location was checked again with a

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Criteria	Commentary
	handheld GPS. The 2024 drill collars were surveyed by Challenger with the RTK-GPS after the completion of the drilling programme. The majority of the Cominco holes have used "single-shot" acid-etch style surveys approximately every 30 m down-hole. Exact details of the historical downhole survey methods for the various drilling programmes have not been located. The reliability of the historical down-hole surveying is considered poor. Down-hole surveying for BMC drilling was conducted using a Reflex EZ-Shot "single-shot" during advancement of the hole starting from start of bedrock and on 25 m intervals thereafter. Magnetic north azimuth readings are corrected to grid north azimuths by adding 22.5°. Accuracy of azimuth values were judged based on magnetic readings from the instrument. Only values between 5,600 nT and 6,000 nT were deemed to be accurate. In 2016, 30 holes were surveyed using a Reflex Gyro Non-magnetic instrument upon completion of the holes. The use of the Gyro orientation tool continued for all inclined holes in bedrock for the 2017 and 2018 exploration seasons. All 2024 season holes were surveyed using a Devico Devigyro tool supplied by IMDEX Limited.
	The grid system for the KZK Property is UTM zone 9 NAD83.
	Topographic control with accuracy to 0.1–0.3 m was provided by a LiDAR survey data flown in 2015 by Challenger Geomatics Ltd.
Data spacing and distribution	ABM Zone holes are drilled at nominal 50 m spacings on 25 m north-south oriented sections extending out to 100 m on the peripheries of the deposit. The GP4F Prospect was sampled using core drill holes at nominal 50–75 m spacings on 50 m north-south oriented sections extending out to greater than 100 m on the periphery of the deposit. The Krakatoa Zone is drilled by southwest oriented holes targeting pierce points of 25–60 m in the central portion of the deposit to 100 m on the peripheries. Holes testing exploration targets have been drilled at variable spacing.
	The mineralised domains for the ABM Deposit have demonstrated sufficient continuity in both geological and grade continuity to support the definition of Mineral Resources and the classification applied under the JORC Code (2012). Drill spacing on exploration targets is insufficient to demonstrate geological and grade continuity.
	Sample compositing was not applied.
Orientation of data in relation to geological structure	The ABM Zone was drilled towards grid south at angles ranging from −30° to vertical (−90°) to intersect the mineralised zones close to perpendicular for the bulk of the deposit. GP4F holes were generally angled 45° to 90°) towards grid south with dip angles set to optimally intersect the mineralised horizon. Of the 27 holes drilled at the prospect, two were drilled vertically. The orientation of these holes is broadly perpendicular to the mineralisation. The Krakatoa Zone was drilled towards grid southwest at varying angles to obtain close to true width intersections and to avoid bounding faults. Exploration holes were angled (generally between −45° to −90°) with the hole azimuth based on interpreted geology or access.
	To date, mineralisation orientation has been favourable and sample widths are not considered to have added a sampling bias.
Sample security	No records detailing sample security have been located for the historical Cominco drilling. For BMC drilling, BMC manages sample chain of custody. All samples were bagged in poly sample bags labelled with unique sample numbers and equivalent bar-coded sample tags included in the bag. Samples were then packaged in lots of 5–10 in white poly rice sacks. The rice sacks were sealed using fibre tape and uniquely numbered non-reusable security seals. Sacks were then palletised and shrink wrapped for shipment to the lab. Tracking numbers, bag inventory and security tag information is then provided to the lab with instructions to notify upon receipt and of any compromised bags.
Audits or reviews	A detailed review of the sampling techniques and data was carried out by CSA Global (now ERM) during October 2015. The sampling techniques and data were of sufficient quality to carry out resource estimation.

Section 2: Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section)

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Criteria	Commentary
Mineral tenement and land tenure status	The KZK Property comprises 879 contiguous Mineral Claims, covering 161.3 km^2. A 0.75% NSR royalty is held by Teck over the Minerals Claims ON 21-85, ON 87-101, ON 104-113, ON 116-125 ON 162-173, and ON 197-198. These claims do not cover the Ore Reserves, Mineral Resources, and Exploration Targets of the KZK Property. No other royalties or similar encumbrance exist over KZK and Pelly Properties. A precious metal stream (the PMPA) was acquired by OMF Fund III (Bi) LP over the KZK Property only. The PMPA has subsequently been sold to Wheaton Precious Metals Corporation. The PMPA encompasses the Ore Reserves and Mineral Resources of the ABM Deposit. The PMPA post-dates completion of the 2020 Feasibility Study, and as such it was not included in the 2020 Feasibility Study and the modelled financial outcomes of that study. The PMPA has been included in both the 2023 and 2025 Economic Updates.
	The KZK Property lies within the traditional territory of the Kaska First Nation (comprising Ross River Dena Council, Liard First Nation, Dease River First Nation, and Kwadacha First Nation). Portions of the Project, including the ABM Deposit, and the proposed infrastructure are covered by a Socio-Economic Participation Agreement. All tenure is in good standing with the Yukon Territorial Government. A staking moratorium exists over the area, but this does not prevent operations within the Project tenure.
Exploration done by other parties	Majority of the previous exploration has been conducted by Cominco and is of a high standard. Limited exploration work and an updated Feasibility Study was also completed by Expatriate Resources Ltd in 2000 before the project was handed back to Teck Cominco in 2001.
Geology	The ABM Deposit is a VHMS style of deposit within a thick felsic tuff and sill/flow complex. Massive sulfide of the ABM Zone is up to 39 m true thickness, extending approximately 700 m along strike and approximately 500 m down dip. It dips to the north-northeast at approximately 35° near surface, transitioning to a dip of approximately 15° at around 200 m depth below the valley floor. The up-dip extent of the deposit is truncated by erosion and covered by approximately 2–20 m of glaciofluvial overburden. It remains open along strike to the northwest. Krakatoa Zone mineralisation is broadly concordant with stratigraphic layering of the host rocks, extending over approximately 200 m of strike, at least 500 m down dip, and up-dip to the base of glacial overburden of 20–30 m thickness. It remains open at depth. Mineralisation at GP4F comprises thin lenses of massive and semi-massive sulfide hosted within a much larger, tabular body of disseminated mineralisation and alteration referred to as the “GP4F Zone”. The GP4F Zone is typically 5–10 m thick and is best-developed in a “central area” (the area of most drilling) that measures greater than 500 m in a north-south direction and 300 m from east to west. The same mineralised zone appears to be weakly defined within a drill hole 400 m to the west of the central area. A second mineralised zone recognised during 2015, the “Lower Zone”, occurs structurally below the GP4F Zone. The alteration and mineralisation are texturally and mineralogically similar to the ABM Deposit.
Drill hole information	Appendix E provides a listing of all exploration drill holes with location data and the length and grades of all significant intercepts. As a MRE has been reported for ABM and an ET for GP4F, these drill holes are not included in this table. Some drill holes are shown on selected cross-sections, while collars locations are shown on plans of the deposits in the report.
	The ABM Deposit is the key mineral asset of the Kudz Ze Kayah Project with an Ore Reserve and positive Feasibility Study having been completed. Therefore, the relative significance of exploration results on the many exploration prospects of the Project is lowered. This justifies the somewhat reduced level of detail with which geological/exploration aspects are covered as their materiality is reduced.
Data aggregation methods	As a MRE has been reported for ABM and an ET for GP4F, data aggregation methods within drill holes are accommodated within the methodology of the estimate. Cross-sections display intersections of massive sulfide based on geological boundaries. There is a sharp contact between barren host rock against massive sulfide in most cases. For exploration prospects, drill hole intervals are calculated using a length-weighted average. Assay values were considered significant and composited if Cu >1% or Pb >2% or Zn >2% with a maximum internal waste of 3 m. When assay value is below detection limit half of the detection limit is used. Intervals were split based on the style of mineralisation (massive, stockwork, disseminated).
	No aggregate intercepts incorporating short lengths of high-grade results and longer lengths of low-grade results have been used.

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Criteria	Commentary
	Metal equivalent values have not been reported, only actual metal grades.
Relationship between mineralisation widths and intersection lengths	Drillholes are broadly orthogonal to the strike and dip of the mineralisation such that true width is approximately equal to down-hole lengths for holes drilled at the ABM Deposit and the GP4F Prospect. Elsewhere the relationship between downhole width and true width is unknown.
Diagrams	An appropriate number of diagrams have been illustrated in this report relative to the importance of each deposit/ prospect to the overall Kudz Ze Kayah Project. Diagrams have been professionally drafted and meet the standards outlined in the VALMIN Code.
Balanced reporting	Exploration results outside the MRE are reported in a balanced fashion which is not misleading. An ET has been reported for the GP4F Prospect to appropriately reflect the advanced stage of exploration of this prospect. Appendix E provides a listing of all exploration drill holes with location data and the length and grades of all significant intercepts.
Other substantive exploration data	Bulk density determinations were completed by Cominco using the water immersion method on only the first 40 drill holes completed at ABM. They selected a 10 cm long core sample from each assayed interval and flanking and intervening waste. In contrast BMC measured bulk densities in the field on new core samples over the entire length of the sample interval and on representative 10–15 cm long whole-core samples of various hangingwall and footwall host rock lithologies using the water immersion method. The selective approach used by Cominco could potentially yield unrepresentative data and hence only bulk densities measured by BMC were used for resource modelling. Data that were clearly erroneous were culled. Calibration readings were taken on reference material every 10th reading and as the last measurement for each drillhole. No historical bulk density measurements were taken by Cominco from GP4F drill core. BMC has conducted geological mapping on the KZK Property, with helicopter support where required. Traverses were completed, covering most of the KZK Property. Bedrock exposure within the mapped area is present mainly along ridges and ravines, moderate on the steep slopes, but typically poor along shallower slopes and in valley bottoms. Individual outcrops were mapped and described. Mapping was conducted on ruggedised, GPS-enabled Panasonic Toughbook computers using QGIS software. Geological fact maps were compiled. Since 2105, a total of 6,289 B-horizon soil samples have been collected at a nominal 100 m by 100 m sample spacing over the majority of the Kudz Ze Kayah formation within the KZK Property. Sample spacing was closed to 50 m by 50 m in areas of anomalous geochemical results from the initial programme. Multi-element analysis identified areas of anomalous results for a range of elements, including in areas of known mineralisation. Numerous geophysical surveys have been carried out over the KZK Property which have been undertaken by specialist geophysical contracting firms using high-quality instrumentation and data processing systems. In particular, down-hole electromagnetic (EM) surveys have been undertaken on selected core drill holes to assist in targeting VHMS mineralisation through the detection of off-hole conductors. Other geophysical programmes at KZK include: Majority of BMC's tenure was flown with airborne geophysical surveys in 2015 and 2016. The principal geophysical sensors included a VTEM™ plus system and horizontal magnetic gradiometer with two caesium sensors. Ancillary equipment included a GPS navigation system and a radar altimeter. During the survey, the helicopter was maintained at a mean altitude of 101 m above the ground with an average survey speed of 80 km per hour. This allowed for an actual average Transmitter-receiver loop terrain clearance of 70 m and a magnetic sensor clearance of 80 m. Modelling of the VTEM™ data identified anomalous EM responses coincident with the ABM Deposit and with known massive sulfide at the Fuego Prospect, along with other anomalous EM responses requiring further investigation. Several targets incorporating anomalous VTEM™ responses were subsequently drilled, including two that returned anomalous base and precious metal results in sulfide bearing intervals at the Kuril and the Rhyolite Peak prospects. A single 2D seismic line completed in 2017 using a 50,000 lb IVI HEMI-50 Vibroseis truck, 2017-2018 Ground Fixed Loop Transient EM surveys using a SMART Fluxgate sensor coupled with an EMIT SMARTem24 Receiver using 6 loops. 2023 pole – dipole 3D IP survey using a Dias GS5000 transmitter to provide an output power of up to 5 kW and 2000 V. The receiver parameters consisted of a dipole interval of 100 m with a receiver sampling rate of 150 samples/sec and receiver Line spacing of 100 to 200 m with a base frequency of 0.125 Hz. In 2024 and 2025 UAV magnetic surveys were flown south of the ABM Deposit at a height of 35 m above ground along lines spaced 25 m apart. Tie lines were flown at 250 m spacing. In 2025 a total of 22.3 km of FLTEM surveying was conducted using three transmitter loops, covering the Rhyolite Peak, ABM West, and Fuego prospects.

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Criteria	Commentary
	Equipment used included an IPTX-2500 transmitter. Data was recorded using a Supracon Jessy Deep SQUID receiver. Survey lines were spaced 50-100m apart, with stations recorded every 25-50m along each line. Several anomalous EM responses were modelled that require further investigation
Further work	In addition to the ET, BMC have defined numerous advanced VHMS prospects within the KZK Property which are at various stages, from requiring further surface studies, through drill ready, to having significant initial drill hole intersections worthy of intense follow-up drilling. At Pelly, BMC has defined 10 prospect areas requiring follow-up exploration. BMC proposes the following actions to further the exploration and evaluation of the KZK Property: Additional resource definition drilling (infill and extension) to identify whether it is possible to upgrade the resource classification (and to identify whether the material classified as an ET can be extended and defined as a Mineral Resource, noting it is uncertain if further exploration will result in the estimation of a Mineral Resource) and seek to extend the known deposits, which presently remain open down plunge and along strike in places (e.g. Krakatoa Zone). Assessment of existing geophysical data and implementation of ground EM surveys and IP surveys. Drill core testing of known multi-component geological, geophysical and geochemical anomalies with DHEM implemented to detect off-hole conductive zones. Detailed structural and geochemical analysis to understand the timing of mineralisation, stratigraphy, and geological controls. Improved understanding of the deposit controls will additionally aid in more regional exploration efforts across the Project. Detailed metallurgical testwork using core samples from infill drilling.
	An appropriate number of diagrams have been illustrated in this report relative to the importance of each deposit/prospect to the overall Kudz Ze Kayah Project. Diagrams have been professionally drafted and meet the standards outlined in the VALMIN Code.

Section 3: Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section)

Criteria	Commentary
Database integrity	The drill hole database was managed off site by OMI Pty Ltd (OMI) based on information provided by BMC, Equity Exploration Consultants Ltd (Equity), and the laboratories. Since December 2017, CSA Global (an ERM Group Company) has managed the KZK database. All data for the Kudz Ze Kayah Project has been migrated to an acQuire 4 GIM Suite database. The database is currently managed out of ERM's Vancouver office. Original "hard copy" data was located by BMC and entered by OMI into a Microsoft (MS) Access database. Results from the 2015 and 2016 exploration programmes were managed by OMI and loaded directly into the master MS Access database. CSA Global (now ERM) compared the original "hard copy" data (drill collars, laboratory assay reports, geological logs, down-hole surveys) for approximately 10% of the total drill holes with the database provided by OMI. No significant issues were noted. Since December 2017, CSA Global (now ERM) has managed the KZK database. All data for the KZK Property has been migrated to an acQuire 4 GIM Suite database.
	Throughout the 2015 to 2017 exploration programmes, data was extensively reviewed and validated by BMC and CSA Global. Since 2017 data was comprehensively reviewed and validated by BMC. Validation of the final data import by CSA Global (now ERM) included checks for overlapping intervals, missing survey data, missing assay data, missing lithological data, and missing collars.
Site visits	A three-day site visit to the Kudz Ze Kayah Project was conducted by Aaron Green (Competent Person) from 11 to 13 October 2015, which included the ABM Deposit. The site inspection achieved the following: Inspected operating drill rigs.

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Criteria	Commentary
	Reviewed current drilling and sampling procedures.
	Verified the location of selected drill collars and down-hole surveys.
	Inspected site geological data collection systems (mapping, logging etc.).
	Reviewed site geology.
	Reviewed sample storage facilities including historical core storage farm.
	Discussed quality assurance with geological personnel.
	Discussed data storage and review the drill hole database.
	Site sample storage facilities and the analytical laboratory in Vancouver (SGS) were also inspected by Aaron Green and Dennis Arne on Thursday 22 October 2015.
	A subsequent site visit to the Kudz Ze Kayah Project was conducted by Aaron Green on 26 July 2017. No active drilling was being undertaken at the time of the site visit. Limited geological outcrops around the ABM Deposit, several exploration project areas, and the core farm were visited.
	A four-day site visit to the Kudz Ze Kayah Project was conducted by Karl van Olden (Competent Person from 15 to 18 August 2016. The site visit achieved the following:
	Inspected the proposed mine site.
	Inspected the site layout, access to site, and proposed mining, processing plant, and infrastructure locations and key local features.
	Discussed geological and geotechnical data, and interpretation with the onsite technical personnel.
	Discussed environmental and social elements of the Project.
	Discussed mine planning considerations with the BMC technical staff and consultants.
	Aaron Green undertook a one-day site visit to the Kona, Wolf and Pelly properties on 26 July 2017. The exercise was helicopter supported and involved initial ground verification with associated outcropping geology and mineralisation, a review of historical drill core stored on the sites, and inspection, and confirmation of historical drill hole locations.
	More recently, Aaron Green undertook a one-day, helicopter supported site visit to the Kudz Ze Kayah Project on 5 June 2024. No active drilling was being undertaken at the time. The site visit achieved the following:
	Inspected the new core farm and core logging facilities.
	Inspected the camp facilities including the new site offices and lodgings.
	Inspected the proposed mine site.
	Inspected the site layout, access to site, and proposed mining, processing plant, and infrastructure locations and key local features.
	Overview of the Kona core farm, camp, and deposit location.
	Discussed environmental and social elements of the Project.
	There were no negative outcomes from any of the above inspections, and all samples, and geological data were deemed fit for use in the ABM MRE.
Geological interpretation	Geological interpretation was completed by Equity, BMC, and CSA Global (an ERM Group Company) geologists. The geological interpretations were found to be of a high standard. Continuity of mineralisation is excellent and is intimately associated with massive sulfide horizons.
	The geological interpretation provided a sound foundation for interpretation of boundaries to the polymetallic zinc-copper-lead-gold-silver mineralisation.
	Detailed geological logging, including re-logging of historical Cominco/Teck holes to ensure data consistency, in conjunction with chemical assays has been used to identify individual lithological units during the interpretation process. Zinc, copper, lead, gold, silver, and lithology were plotted on drill hole traces to assist the interpretation.

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Criteria	Commentary
	Geological continuity is very good between drill holes and conforms well to anticipated geological models for VHMS mineralisation. This is supported by the minor changes required to the geological interpretation following the 2015 and 2016 resource infill drilling programmes and Cominco/Teck drill hole re-logging. The data does not lend itself to alternative interpretations.
	Geology has been the primary influence in controlling the Mineral Resource estimation. Wireframes have been constructed for the main mineralised horizons and geological features as determined by the geological logging and chemical assays.
	Continuity of geology and structures can be identified and traced between drill holes by visual and geochemical characteristics. The massive, semi-massive and stockwork sulfide zones hosting the mineralisation have been logged in the drill core and have been modelled.
Dimensions	The ABM Mineral Resource, including both the ABM Zone and Krakatoa Zone, is contained within an area defined by a strike length of 900 m (414,500 m E to 415,400 m E) and across-strike from 6,814,865 m N to 6,814,755 m N (890 m). The reported Mineral Resource lies within 420 m of surface (1,440 m RL to 1,020 m RL).
Estimation and modelling techniques	All modelling was undertaken using Surpac V6.2, V6.5 and V6.6 software. The deposit was divided into two distinct zones, ABM, and Krakatoa, each estimated separately. For ABM, hard boundaries were used for majority of the domains (both stockwork and massive sulfide), consistent with the geological interpretation. Five minor domains, which had very low data support, had semi-soft boundaries applied with adjacent domains that were deemed appropriate based on grade, domain type, and proximity. These soft boundaries were only applied one way – so that the smaller domain used data from a larger domain, but not vice versa. For Krakatoa, only hard boundaries were used, due to the greater separation and uniqueness of the individual domains. For both ABM and Krakatoa, high-grade cuts were applied to the massive sulfide and stockwork domains following statistical analysis. Statistical analysis was completed using GeoAccess software. Block grades were interpolated using ordinary kriging (OK). An oriented "ellipsoid" search was used to select data for interpolation. For ABM, search ellipsoid orientations were based on orientations derived from the variographical analysis. An ellipsoid was produced for each individual element, with bearings varying from 0° to 20°, and plunges between −30° and −35°, all with zero dip (Surpac convention). These orientations honour the orientation of the ABM Deposit. Where the mineralisation approaches a more horizontal habit north of 6,815,550 m N, the ellipses were adjusted to suit – with the plunges adjusted by −25° to between −5° and −10°. For Krakatoa, search ellipse orientations were duplicated from ABM, as the strike, and dip trends of both Deposits are very similar. The Krakatoa Deposit maintains a consistent strike and dip trend along its extent, and so no plunge adjustment was required. A three-pass estimation search was used to complete estimation for Cu, Pb, Zn, Au, Ag, Fe, As, Ba, Bi, Hg, S, Sb, and Se within the domain objects, with separate dimensions for each element, based on the variogram ranges. For ABM, first pass search radii of 55–150 m, and second pass search radii of 80–225 m along strike were used with the minimum number of samples set to six for both passes. The number of samples per hole was limited to three. A third expanded estimation pass with radii of 160–450 m was used to inform remaining un-estimated blocks. For Krakatoa, first pass search radii ranging from 22 m to 187 m, and second pass search radii of 34 m to 283 m along strike were used with the minimum number of samples set to four or six (varying by object) for both passes. The number of samples per hole was limited to two. A third expanded estimation pass with radii of 68–566 m was used to inform remaining un-estimated blocks. The search parameters were based on Kriging Neighbourhood Analysis, undertaken using Supervisor software, with some consideration towards the overall drilling density.
	As a high-level validation technique, the reported MRE was compared with previous estimates for the deposit. No reliance is placed on the previous estimates in relation to the current MRE. The Krakatoa Zone was discovered in October 2015, and this is the first update of the MRE for this zone since the maiden resource reported on 22nd January 2016. The reported Krakatoa Zone MRE represents a decrease in tonnage compared to the previous resource, primarily

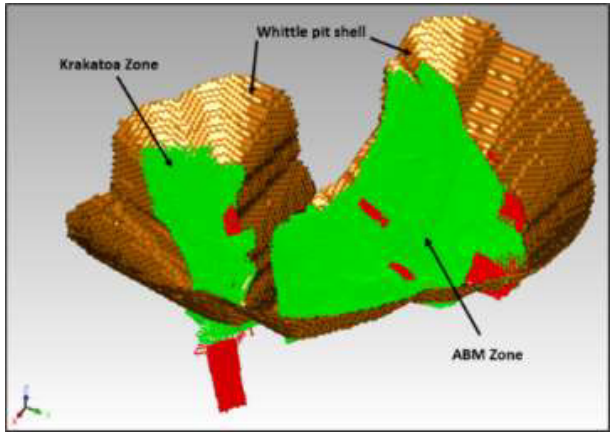
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Criteria	Commentary
	because of drilling to the west (towards the East Fault) failing to intersect significant mineralisation No mining has yet taken place at the ABM Deposit.
	Gold and silver have been estimated as extensive metallurgical testwork undertaken by BMC has demonstrated that they will be recoverable as part of the copper, lead and/or zinc recovery process and/or potentially via gravity separation. This was also confirmed by a review of the Cominco metallurgical testwork and ore petrography undertaken in 1990s.
	Potentially deleterious selenium, mercury, bismuth, barium, sulfur, antimony, and arsenic have been estimated into the block model for use in mining studies.
	A parent cell size of 10 m(E) by 10 m(N) by 5 m(RL) was adopted with standard sub-celling to 5 m(E) by 5 m(N) by 2 5 m(RL) to maintain the resolution of the mineralised lenses while restricting the overall size of the model. The block size is considered appropriate given the dominant drill hole spacing, style of mineralisation, and proposed mining methods.
	No assumptions were made regarding selective mining units.
	No assumptions were made about the correlation between variables.
	The geometry of the massive sulfide horizons, as defined in logging and detailed sectional/plan interpretation, formed the basis for mineralisation interpretations. At the ABM Zone, a footwall mafic intrusive (sill or dyke?) was modelled to control the base of the massive sulfide mineralisation. The main massive sulfide lens is offset down dip by the east-west trending Northwest Fault. The Krakatoa Zone massive sulfide represents a down-thrown block (likely in oblique dextral fashion) to the east of the ABM Zone by the East Fault and appears to be cut-off further to the east by the Fault Creek Fault. It remains open down plunge. Unlike the ABM Zone, the main mineralised lens at Krakatoa occurs within the mafic intrusive unit with smaller, less continuous massive, and stockwork mineralisation in the immediate footwall and hangingwall of the mafic. Additional geological control was provided by modelling of rhyolite intrusives units, hangingwall carbonaceous mudstone units and the overlying Wind Lake formation sediments. Hard boundaries for estimation were used between mineralised lithological domains.
	Following statistical analysis, it was determined that high-grade cuts were required for most elements estimated in the massive sulfide domains for the ABM Zone, while high-grade cuts for copper, lead, zinc, and silver were applied to the stockwork domains. For the Krakatoa Zone, high-grade cuts were applied on an individual domain basis. Varying high-grade cuts were applied for almost all elements estimated other than lead and iron. Statistical analysis was completed using GeoAccess software. The cuts were applied after compositing.
	Validation checks included statistical comparison between drill sample grades and OK block estimate results for each domain. Visual validation of grade trends for each element along the drill sections was also completed in addition to swath plots comparing drill sample grades and model grades for northings, eastings, and elevation. These checks show good correlation between estimated block grades and drill sample grades. No reconciliation data is available as no mining has taken place.
Moisture	Tonnages have been estimated on a dry in situ basis. No moisture values were reviewed.
Cut-off parameters	The mineralisation was modelled using logged semi-massive to massive sulfide horizons on the interpreted geological cross-sections which correlated closely to a nominal 0.5% Cu cut-off grade. To assist in defining reasonable prospects of economic extraction a dollar amount was attributed to each block for the purpose of determining cut-off grade only (i.e. not a project valuation) using estimated factors for: assumed metal prices, metallurgical recoveries, smelter terms (including payable factors, concentrate costs and refining charges) and government royalties. These factors were provided by BMC. No penalties were included. Key factors determining the NSR were:

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Criteria	Commentary
	Metal price assumptions were: US$4.50/lb copper, US$1.65/lb zinc, US$0.90/lb lead, US$1,875/oz gold, and US$22.50/oz silver. An exchange rate of US$0.75 = C$1.00. Three separate concentrates recovered – copper, HPM and zinc with precious metals (gold and silver) reporting to all concentrates at varying recoveries from 15% to 40%. Metal recovery assumptions were: 90% for copper, 90% for zinc, 80% for lead (HPM), 64% for gold (whereby27% is recovered into copper concentrate, 29% is recovered into HPM concentrate and 8% is recovered into zinc concentrate) and 86% for silver (37% into copper concentrate, 38% into HPM concentrate, and 11% into zinc concentrate). Based on these assumptions the formula for the NSR on each block was calculated as: NSR US$/t = (69.17*Cu_cut) + (6.85*Pb_cut) + (19.53*Zn_cut) + (30.13*Au_cut) + (0.49*Ag_cut) To determine the reporting of ABM Deposit Mineral Resources as either open pit or underground, a Whittle™ pit optimisation was undertaken. Parameters used for the optimisation included: Base case metal price assumptions were: US$4.50/lb copper, US$1.65/lb zinc, US$0.90/lb lead, US$1,875/oz gold, and US$22.50/oz silver An exchange rate of US$0.75 = C$1.00 Mining recovery of 97%, dilution 10% Minimum mining width of 25 m Overall slope angle of 50° Total processing costs (fresh) of C$33.02/t Plant throughput of 2 Mtpa. For the ABM Zone, only material reporting inside the selected pit shell (Revenue Factor = 1.00) has been reported above the NSR cut-off of US$40/t. For the Krakatoa Zone, mineralised material inside the pit shell has been reported above the NSR cut-off of US$40/t, while the remainder has been designated as “underground” resource and reported above a cut-off NSR of US$150/t. The NSR calculation is used here to create a composite metal cut-off value for what is a polymetallic Deposit, as a single metal cut-off value is not appropriate. The calculated cut-off value is used primarily for reporting the MRE above the calculated cut-off. Any economic studies are based on the ORE employing the appropriate application of the Economic Modifying Factors.

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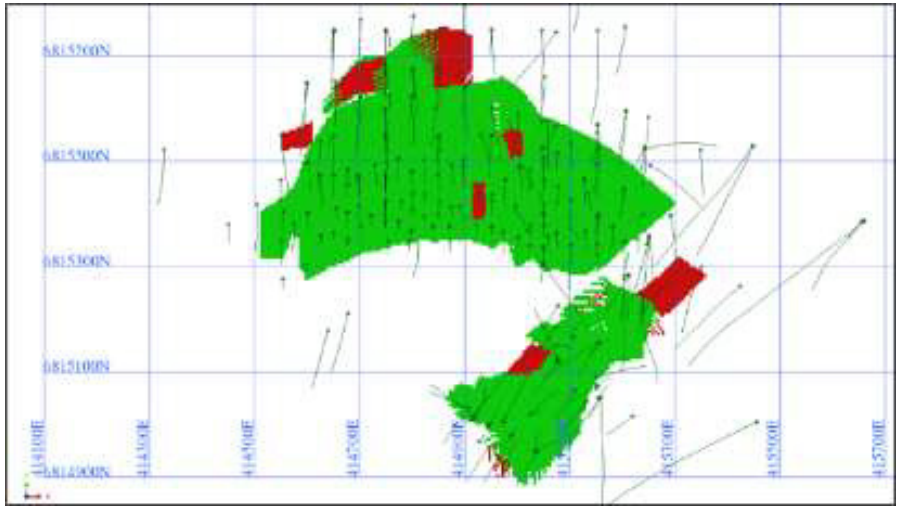
Criteria	Commentary
	 ABM Deposit Mineral Resource by classification inside optimised pit shell looking southwest (red = Inferred, green = Indicated)
Mining factors or assumptions	Previous and current mining studies have shown that the ABM Deposit could be economically exploited by open cut and/or underground mining methods at the reported average model grades. A minimum down-hole composite width of 1.5 m was applied. No other mining assumptions were made. A minimum 3 m "dilution skin" was created for both the ABM and Krakatoa zones to be used for mine planning purposes. The "skin" was created as an independent wireframe enclosing each zone and interpolated as a 'hard boundary' using ID3 interpolation and parameters from the massive sulfide estimation (minimum and maximum samples, search ellipses etc.). ID3 interpolation was used to restricted smoothing and reduce the influence of discontinuous, high-grade mineralisation "outliers".
Metallurgical factors or assumptions	A review of previous metallurgical testwork undertaken on the ABM Deposit by Cominco demonstrated that conventional flotation would produce separate zinc, copper, and HPM concentrates for shipment to a smelter. ALS Metallurgy completed BMC's PFS and Feasibility Study metallurgical testwork in their Perth and Adelaide laboratories in Australia. Five metallurgical domains were defined for the ABM Deposit, based on texture, and mineralogy. The metallurgical testwork programme investigated comminution and flotation performance for all five domains using domain composite samples together with five variability samples for each domain. Variability samples were primarily selected to assess variability in flotation performance over a range of head grades within each metallurgical domain. The LOM recoveries determined for the Feasibility Study are summarised in the table below. Concentrate grades are predicted to be 25.0% Cu, 52.0% Pb and 52.0% Zn for copper, HPM, and zinc concentrates, respectively.

Concentrate	Cu (%)	Pb (%)	Zn (%)	Au (%)	Ag (%)
Copper	73.8	N/A	N/A	27.3	36.8
HPM	N/A	73.5	N/A	29.4	38.2

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Criteria	Commentary
	Zinc N/A N/A 85.9 8.1 11.0
Environmental factors or assumptions	Previous mining studies have highlighted waste production of PAG rock as a key environmental issue. It is assumed that such disposal will not present a significant hurdle to exploitation of the deposit and that any disposal, and potential environmental impacts would be correctly managed as required under the regulatory permitting conditions. For the Feasibility Study, waste rock was classified as Class A, B, or C, based on its potential to produce acid drainage and its metal leaching characteristics and stored accordingly in permanent landforms on surface. In addition, overburden material, comprising glacial till and glaciolacustrine sediments, and topsoil material will both be stockpiled temporarily on surface for later reuse during reclamation of the site. A geological interpretation and wireframes for Acid Rock Drainage (ARD) geodomains was completed by Equity and CSA Global (an ERM Group Company) and incorporated into the block model for analysis as part of the Feasibility Study.
Bulk density	CSA Global (an ERM Group Company) used fixed density values assigned into the block model for each regolith and lithological unit, setting fresh felsic material to 2.76 t/m^3 (based on the median of the normal histogram from the measured bulk density dataset), 2.80 t/ m^3 for the mafic intrusive rock, 2.74 t/ m^3 for the mudstone and Wind Lake formation, 2.68 t/ m^3 for the rhyolite intrusive (RHYi), and 2.00 t/ m^3 for overburden. For the mineralised domains, bulk density was estimated using OK, utilising the variogram parameters that were derived for iron to honour the relationship between density and iron content. To create a reliable bulk density dataset with which to estimate, a regression was derived based on sulfur content (where available) for samples that had no clean bulk density measurement. For samples that had neither a bulk density nor a sulfur value, bulk densities were calculated using the iron-copper-lead-zinc formula -(1.0*Cu%)+(1.81*Pb%)+(0.97*Zn%)+(1.20*Fe%). For Krakatoa data, measured bulk densities were available for all samples within the mineralisation wireframes. Based on the parameters detailed above, calculated bulk densities were derived for 1,027 core samples from 54 holes at ABM for use in the bulk density interpolation. The average bulk densities determined for the ABM stockwork, and massive sulfide mineralisation were 3.44 t/ m^3 and 4.19 t/ m^3 respectively, while the average bulk density values for the Krakatoa Zone were 3.86 t/ m^3 and 4.09 t/ m^3, respectively.
	Density measurements were calculated using the water immersion method from drill core across the deposit and from the various rock types. The entire sample sent for geochemical analysis (i.e. half core) was measured for bulk density in 2015 and 2016.
	Average densities were applied to overburden material as well as the various lithological domains based on measured densities. The bulk density for the mineralised zone was interpolated using a combination of measured and calculated bulk densities for samples within the mineralised wireframes. It is assumed that use of the regression formulas based on correlation between combined metal content and density is an appropriate method of representing the expected variability in bulk density for the grade estimated mineralised blocks. Analysis of the results of application of the regression formulas to the model by individual mineralised domain unit shows that the mean model density compares closely to the mean of the density measurements from within each zone.
Classification	The Mineral Resource was classified as Indicated and Inferred considering the level of geological understanding of the deposit, quality of samples, density data, drill hole spacing, sampling and assaying processes, and the success of the BMC infill drilling programmes in confirming the geological interpretation and continuity of mineralised horizons. ABM Zone: Majority of resource classified as Indicated based on continuity of mineralisation and grade, as well as drill spacing. Minor stockwork zones classified as Inferred. Krakatoa Zone: Majority of resource classified as Indicated based on continuity of mineralisation and grade, as well as drill spacing. Minor footwall stockwork zones classified as Inferred.

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Criteria	Commentary
	 ABM Deposit Mineral Resource classification in plan view (red = Inferred, green = Indicated)
	The classification reflects areas of lower and higher geological confidence in mineralised lithological domain continuity based the intersecting drill sample data numbers, spacing, and orientation. Overall mineralisation trends are reasonably consistent within the various lithology types over numerous drill sections.
	The MRE appropriately reflects the view of the Competent Person.
Audits or reviews	Internal audits were completed by Cube Consulting which verified the technical inputs, methodology, parameters, and results of the estimate.
Discussion of relative accuracy/ confidence	The Mineral Resource accuracy is communicated through the classification assigned to various parts of the deposit. The MRE has been classified in accordance with the JORC Code (2012 Edition) using a qualitative approach. All factors that have been considered have been adequately communicated in Section 1 and Section 3 of this table.

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Section 4: Estimation and Reporting of Ore Reserves

(Criteria listed in section 1, and where relevant in section 2 and 3, also apply to this section)

Criteria	Commentary
Mineral Resource estimate for conversion to Ore Reserves	The MRE for the ABM Deposit at the Kudz Ze Kayah Project ("the Project") was prepared by CSA Global (an ERM Group Company). The MRE is reported inclusive of the ORE.
Site visits	A site visit was conducted by the Competent Person, Karl van Olden, alongside the Chief Mining Engineer for BMC, Jim Newton. The site visit occurred from 15 to 18 August (four days) in 2016. The site visit achieved the following: • The site layout inspection • Inspection of the site access • Inspection of proposed mining, processing plant, and infrastructure locations, and key local features • Discussion of geological and geotechnical data and interpretation with the onsite technical personnel • Discussion of environmental and social elements of the Project • Discussion of the mine planning considerations with the BMC technical staff and consultants. A further site visit to the undeveloped site was considered unnecessary for the purposes of the ORE. The project site was visited by Aaron Green (MRE CP) in June 2024 who provided sufficient information to Karl van Olden to confirm that there is no material change to the Project site since previous visits.
Study status	A Feasibility Study was completed for the Project in June 2019 and updated in 2020 by CSA Global. The 2020 Re-stated Feasibility Study forms the basis of the ORE. The Feasibility Study targets an average process ROM processing throughput rate of 2.0 Mtpa to produce separate copper, HPM, and zinc concentrates. The ORE has been reviewed by AMC in the context of changes since 2020, including 2023 and 2025 updates, with change in effective dates. The work undertaken to date has addressed all the material Modifying Factors required for the conversion of the MRE into an ORE and has shown that the mine plan is technically feasible and economically viable. The project economics were updated in October 2023 to reflect updated revenue and costs estimates. The update confirmed that the project remains economically viable. An updated summary of the Feasibility Study level work on the project was provided in the 2025 Technical Report.
Cut-off parameters	A NSR approach was used to differentiate between ore and waste during mining. Each block classified as at least Indicated Mineral Resource within the block model had an NSR estimated where the total block revenue for each economic metal after the application of processing recoveries, operating costs incurred after the mine gate, government royalties, and First Nations payments. The NSR method was used to determine the economic mineralisation for the Project. The differentiation between ABM open pit ore and waste was not revisited for the 2023 Economic Update. The 2019 ore feed was evaluated against the economic parameters of the 2023 Economic Update that resulted in a substantially positive economic result, demonstrating that the updated commodity prices and exchange rates adequately offset the escalation and changes to the project operating costs. For the Krakatoa underground mine, the original stope shapes from the 2020 Re-stated Feasibility Study (CSA Global, 2020) were assessed against the NSR values applicable to the project parameters used in the 2023 Economic Update. All stopes returned an NSR above the ICOG and the average NSR value for all underground ore production is greater than the FCCOG, demonstrating that the underground mine returns a positive economic outcome. It is understood that there remains an opportunity to optimise cut-off grade decisions at future stages of the mine planning and into operations. The mining operation should take a view to continually assess and adjust cut-off grades throughout the mine life to optimise the Project value across changing project parameters.
Mining factors or assumptions	The ABM Deposit will be mined by open pit mining and underground mining methods. Open pit mining of the ABM Zone will be staged into four separate phases to manage overall waste stripping requirements. The adjoining Krakatoa Zone will be mined as a single phase. Open pit mining will be via conventional drill, blast, load, and haul methods.

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Criteria	Commentary

Underground mining of the Krakatoa Zone beneath the pit will be predominantly via underhand longhole open stoping with cemented paste fill. The method chosen is a top-down mining sequence and respects the geotechnical constraints of the ground conditions.

Prior to open pit development of the ABM Zone, a Class A Water Licence will be required before draining Geona Creek. Several dewatering trenches will be constructed across the valley floor by the mining contractor, at the same time as the ABM pit borrow areas are developed during the construction period. This will allow the creek and overburden to be drained so the ABM pit can be expanded to the eastern embankment early in the operational phase without incurring trafficability issues.

The Feasibility Study describes the input parameters for pit optimisations, stope optimisation, and subsequent financial modelling; mining costs based on mining contractor rates; mineral processing costs and recoveries.

All the Project Modifying Factors and costs are described in the Feasibility Study.

The open pit geotechnical analysis has been undertaken. The proposed open pit slopes are considered likely to be stable for the current pit designs over the mine life.

The underground geotechnical analysis has also been undertaken. Eleven mine-scale geotechnical structural features were identified that impact the planned underground mining zone. The fault structures impacting the underground development and stope designs are of variable thickness and are generally greater than 3 m and up to 30 m in width. All the structures have greater than 300 m strike and dip extents and extend from the base of the overburden through the proposed underground mining zone. The proposed underground development and stopes are considered likely to be stable for the current underground designs and mine plan. The following recommendations have been made for crown pillar mining:

Stope voids, as well as any access development within 20 m of the final pit walls are to be tight filled with cemented paste fill.

Any stope voids or development within 15 m of the pit floor are to be probed drilled from the pit and treated as voids during pit production.

A monitoring programme for the pit walls will be required to monitor and assist the planning and implementation of any mitigation strategies, where large wall movements are detected, or the potential for movement indicated by the monitoring.

Access to the underground will be via a single ramp with portal at the 1,355 mRL bench from the saddle area within Stage 1 of the ABM open pit. A second ramp is proposed for ventilation of the underground workings.

A minimum mining width of 25 m has been adopted for open pit designs.

Open pit mining dilution and mining recovery were estimated by coding mining dilution and ore loss distances into the block model for each area of the deposit, defined by the domains surrounding each individual block. Some blocks are surrounded by both hangingwall and footwall, others by only one or the other, and some blocks are only in contact with other ore blocks. The table below describes the mining dilution and ore loss distances applied:

Deposit area exposed to mining dilution and ore loss	Dilution distance (m)	Ore loss distance (m)
ABM both footwall and hangingwall	1.50	0.50
ABM footwall or hangingwall	0.75	0.25
ABM internal	0.00	0.00
Krakatoa both footwall and hangingwall	2.00	0.80
Krakatoa footwall or hangingwall	1.00	0.40
Krakatoa internal	0.00	0.00

The below table shows the average mining dilution and recovery for each metallurgical domain:

Metallurgical domain	Average mining dilution (%)	Average mining recovery (%)

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Criteria	Commentary

+1,340RL (ABM Domain 1)	6.0	97.6
Met2-4 (ABM Domain 2)	2.0	99.1
Met5-7 (ABM Domain 3)	3.9	98.4
Met8 (ABM Domain 4)	9.9	96.6
Krakatoa (Krakatoa Domain 5)	13.1	94.4

The mining recovery applied to underground stoping is 90%.

Planned dilution for underground stoping is included within the stope wireframing. Unplanned dilution is variable, depending on the geotechnical domain of the rock the stope is within. The below table outlines the stoping dilution by domain:

Stoping dilution					
Domain	D1	D2	D3	D4	D5
Dilution	50%	35%	25%	20%	15%
Mining recovery	90%	90%	90%	90%	90%

All mining dilution for open pit and unplanned dilution for underground stoping has been applied with a zero grade.

No Inferred Mineral Resource has been included in the mine optimisation, LOM schedule, or financial analysis. The Ore Reserves in this statement have been reported exclusive of the Inferred Mineral Resource.

Metallurgical factors or assumptions

The Kudz Ze Kayah Project process plant and associated facilities have been designed to process ROM ore at an average rate of 2.0 Mtpa to produce separate copper, HPM, and zinc concentrates, and tailings; however, the plant will be capable of processing at 270 tph based on average ore comminution properties and average plant feed grades. The process rate will be varied depending on the grade of the ore.

The process flowsheet consists of the following key stages:

Crushing, stockpiling, and grinding of the ore.

Pre-float, rougher and cleaner flotation of copper, including regrind of copper rougher concentrate.

Sequential pre-float, rougher and cleaner flotation of lead, including regrind of lead rougher concentrate.

Sequential pre-float, rougher and cleaner flotation of zinc, including regrind of zinc rougher concentrate.

Thickening, filtration, and stockpiling on site of copper, HPM, and zinc flotation concentrates. Copper and zinc concentrates will be loaded in bulk onto trucks for transport to rail head and port respectively, while HPM concentrate will be loaded into sealable containers before transport by truck to port.

Dewatering of flotation tailings by thickening and pressure filtration.

Transportation of filtered flotation tailings to the Class A Waste Storage Facility for disposal.

Cominco completed a large programme of metallurgical testwork on the ABM Deposit in the 1990s to advance development of the project. This testwork is noted briefly for completeness of the record of testing. BMC commenced metallurgical testwork in 2016 for the PFS (CSA Global, 2017a), initially with SGS in Burnaby, Canada before moving the testwork programme to ALS Metallurgy in Perth, Australia. ALS Metallurgy in Kamloops, Canada also completed confirmatory comminution testwork. Feasibility Study metallurgical testwork continued in 2017 and 2018 with ALS Metallurgy in Adelaide, Australia. The Feasibility Study metallurgical testwork programme was supervised by Minnovo.

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<tr><th>Criteria</th><th>Commentary</th></tr>
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In 2020, BMC undertook additional flotation testwork and mineralogical analysis to investigate chromium deportment following comments received by potential smelter customers, concluding that chromium levels in concentrates are primarily due to wear products of the laboratory stainless steel grinding media. The chromium grades in concentrates have been adjusted from that reported in 2019 to reflect this.
The ABM Deposit comprises the ABM Zone and the adjacent Krakatoa Zone. Three major metallurgical domains were recognised for the ABM Zone in core based on texture and mineralogy:
• MET2-4 – massive sulfide mineralisation with significant magnetite component
• MET5-7 – massive sulfide mineralisation lacking significant magnetite component
• MET8 – vein/stockwork mineralisation with significant silicate gangue component.
A fourth metallurgical domain for the ABM Zone (+1,340RL) was defined by spatially controlled mineralogical zonation above 1,340 m RL, with a higher level of copper-bearing sulfosalt mineralisation (primarily tennantite-tetrahedrite) observed than that of mineralisation below this elevation.
A single metallurgical domain (Krakatoa) was recognised for the Krakatoa Zone, which is like the +1,340RL domain but with silver-rich freibergite as the material sulfosalt component in place of tennantite-tetrahedrite.
Ten composite samples were generated for the PFS testwork and were used for comminution and flotation testing. These samples were reused for the initial Feasibility Study flowsheet optimisation testwork.
Twenty-five composite samples, being five samples for each of the five metallurgical domains, were generated for the Feasibility Study variability testwork.
The SMC Test® was used in the design of the comminution circuit. Eleven composites were submitted for SMC Testing during the PFS. The five Feasibility Study domain composites were also submitted for SMC Testing.
ABM and Krakatoa mineralisation contains gold and silver values that are recovered to the copper, HPM, and zinc concentrates during sequential flotation because of true flotation and as encapsulated particles. Recovery of gold and silver into copper and HPM concentrates is preferable than into zinc concentrate as payability levels are higher than for zinc concentrates.
Bench-scale tests were performed with the aims of:
• Characterising the deportment of gold and silver to the various concentrates
• Increasing the overall recovery of gold and silver to flotation and/or gravity concentrates, as compared to the typical overall recovery to copper and HPM flotation concentrates.
Concentrate grades are predicted to be 25.0% Cu, 52.0% Pb and 52.0% Zn for copper, HPM, and zinc concentrates, respectively.
The table below summarises the processing recoveries applied within the Feasibility Study:
<table>
<tr><th>Concentrate</th><th>Copper (%)</th><th>Lead (%)</th><th>Zinc (%)</th><th>Gold (%)</th><th>Silver (%)</th></tr>
<tr><td>Copper</td><td>73.8</td><td>N/A</td><td>N/A</td><td>27.3</td><td>36.8</td></tr>
<tr><td>HPM</td><td>N/A</td><td>73.5</td><td>N/A</td><td>29.4</td><td>38.2</td></tr>
<tr><td>Zinc</td><td>N/A</td><td>N/A</td><td>85.9</td><td>8.1</td><td>11.0</td></tr>
</table>
</td></tr>
<tr><td>Environmental</td><td>The environmental and socio-economic conditions in and around the project area are well characterised. Baseline environmental and socio-economic studies were initiated in 1994–95 by Cominco to support its Initial Environmental Evaluation. These studies included evaluations of climate and hydrology; surface water and groundwater quality;</td></tr>
</table>

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Criteria	Commentary
	stream sediment quality; aquatic resources (fish, benthic invertebrate and zooplankton characterisation); vegetation and terrain mapping; wildlife; archaeological investigation; and socio-economic data collection. Additional baseline studies were conducted in 1996 to support the Type A Water Licence Application. Baseline studies (water quality and aquatic resources) were conducted every two years between 1998 and 2018, to meet the requirements of the water licence. In 2015, BMC initiated a full suite of environmental baseline studies, to support the environmental assessment of the proposed development at the Kudz Ze Kayah Project. The ninth consecutive year of these studies was completed in 2024. BMC submitted a Project Proposal to YESAB on 17 March 2017, and in October 2020 YESAB issued the Final Screening Report which recommended that the Project be allowed to proceed under s. 58(1)(b) of YESAA. The Final Screening Report affirmed the Final Screening Report in March 2021. In June 2022, a positive Decision Document was received by BMC accepting the YESAB recommendation that the Kudz Ze Kayah Project can proceed to licensing under s. 58(1)(b) of the YESAA. A Judicial Review of the Decision Document was subsequently applied for by Ross River Dena Council and was heard in the Yukon Supreme Court in April 2023. The Decision Document was set aside on 2nd January 2024, and on 8th March 2024 a new Decision Document was issued with several additional terms and conditions and confirmation that the Kudz Ze Kayah Project can proceed to licensing under the YESAA. In February 2024, Kaska appealed the January 2024 judgement on the basis that the government should have specifically included consultation on the financial viability of the ABM Mine Project. In December 2024, the Court of Appeal upheld the application, ordering the Government and Kaska to consult on the matter of financial viability and to issue a new Decision Document. In April 2025, the Yukon government wrote to BMC advising that they were satisfied that the ABM Mine Project was economically feasible, and that they were consulting with Kaska on the matter. BMC has been advised that consultation between the Yukon, Canadian and Kaska governments is ongoing. Once the current government to government consultation is completed BMC will receive a new Decision Document. BMC has submitted applications to the Yukon Water Board for a Water Licence under the Waters Act (Yukon), an application for a Quartz Mining Licence under the Quartz Mining Act (Yukon) and applications for other authorisations required to develop and operate the proposed ABM Mine. While the Decision Document remained in force, regulatory bodies accepted and progressed BMC's applications for licences for project development under terms and conditions contained within the Decision Document. These applications have been reviewed by the Yukon government but are currently on hold until a new Decision Document is issued Since 2015, BMC has extensively engaged, and consulted with government agencies, First Nations, various stakeholder groups, and interested parties. BMC staff meet regularly with Ross River Dena Council and Liard First Nation leadership and officials, as well as holding regular community meetings and BMC provides ongoing financial capacity support to enable First Nation participation in Project assessment, permitting, and development. The engagement with First Nations is consistent with and builds upon the existing SEPA. Waste rock will be stored in separate facilities according to expected acid generation and metal leaching potential, with long-term closure planning considered from the outset. Waste rock will be classified as Class A, B, or C, based on its potential to produce acid drainage and its metal leaching characteristics. Class A waste rock is defined as PAG and metal leaching in the near term (i.e. within the life of the operation). The Class A Waste Storage Facility will store all Class A waste rock from the open pit comingled and compacted with filtered tailings trucked from the process plant. A buttress will be constructed on the downstream slope of the facility using Class C material. The facility will be fully encapsulated with a liner comprising high-density polyethylene (HDPE) geomembrane and associated low permeability material. During reclamation, the facility will be capped with a minimum of 3 m of Class C material for frost and erosion protection. Overburden and topsoil will be spread over the final formation, and the facility will be revegetated. Class B waste rock is defined as PAG with metal leaching potential over the longer term (after cessation of mining activities). The Class B Waste Storage Facility will use the same composite liner and cover system as the Class A facility. In addition to the closure layer, the Class B facility will include 3 m to 8.5 m of Class C waste rock for frost and erosion protection. Overburden and topsoil will be spread over the final formation before being revegetated. Class C waste rock is defined as material that is non-reactive or potentially acid consuming and will have low metal leaching potential; therefore, specific PAG management strategies are not required for this material. Where possible, Class C material will be used for construction purposes around the site as well as capping material for reclamation of the Class A and B facilities. Surplus Class C material will be stored in the Class C Waste Storage Facility. No other encapsulation treatment will be required; however, the facility will be reclaimed by placing a layer of overburden and topsoil material over the final formation surface before being revegetated. Tailings from ore processing will be produced as a filtered tailing product that will be deposited in the Class A Waste Storage Facility together with Class A waste rock. A composite foundation liner system incorporating a geomembrane liner will be constructed at the base of storage facilities that have the potential for acid generation and

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Criteria	Commentary
	metal leaching characteristics. These waste storage facilities also have a composite liner system placed on top of each facility for closure to minimise exposure to oxygen and water as well as promote active revegetation of the facilities. All infrastructure has been designed to be situated within a single watershed to minimise impacts on the broader environment. Water that does not encounter the Project footprint will be diverted around the site for discharge. Contact water not requiring chemical treatment for discharge will be kept separate from water that does to minimise chemical treatment requirements. Reuse of water within the mining and processing facilities will be prioritised to limit the amount of water that will require treatment prior to discharge from the site. A WTP will be constructed to treat water to meet site discharge quality measures.
Infrastructure	A Water Treatment Plant will be constructed adjacent to the process plant to treat influent water streams, a portion of the process water stream, ROM pad runoff, process plant sumps, and mine drainage water. Water quality from each of these sources will be monitored to determine if treatment through the WTP is required, and for the purposes of the Feasibility Study all these streams were treated. Treated water will be discharged into the Lower Water Management Pond. Power will be generated onsite by an LNG/Diesel fired Power Station located adjacent to the process plant. Up to five 5.5 MW main generators in an N+1 configuration and a diesel generator for black start operation will be installed. Remote facilities such as the camp and pumps in water collection ponds and storage facilities will be powered from individual skid-mounted diesel generators. LNG will be sourced from the vendor's offsite liquefaction facility and trucked to site in LNG tankers. Diesel will also be trucked to site in conventional diesel tankers. Mine workshop facilities will be constructed for both the open pit and underground mining operations by respective mining contractors. A vehicle wash bay will also be constructed adjacent to the mine workshop facilities. The main diesel storage facility, comprising four 100,000 L tanks will be constructed adjacent to the mine workshop. Explosives will be stored in secure, fenced facilities well separated from the main activity areas. Bulk explosives will be stored in a bulk explosive compound, together with the explosive services contractor's workshop facilities. Site communications will be established via microwave link to connect KZK directly to the NorthwesTel terrestrial network through the McEvoy Tower approximately 36 km northeast of the Project area. One intermediate repeater site will be required, adjacent to the Tote Road, to relay the signal to the mine site. The existing 24 km Tote Road will be upgraded to an all-weather, single-lane road with sufficient passing bay pull outs to safely facilitate two-way traffic. The Tote Road will be the main access to the site for all traffic including personnel transport, supply trucks, and concentrate transport trucks. In and around the site, approximately 25 km of roads will be either upgraded or constructed new to services the needs of the operation. This will include the construction of both light vehicle access roads and mine haul roads. A permanent accommodation camp will be constructed adjacent to the existing exploration camp. The existing Finlayson airstrip is located approximately 40 km from the site and will be the main facility used to fly all project personnel to and from Whitehorse. It is a gravel strip capable of up to 14-seat capacity aircraft. Personnel will be bussed to site from the airstrip. Should Finlayson airstrip be unable to be used for any reason, contingency options include airstrips at Ross River, Faro, and Watson Lake. Zinc and HPM concentrate will be hauled from KZK to the Port of Stewart along a 905 km southerly route utilising a combination of the gravel site access road, gravelled and sealed secondary highways, and paved primary highways. A portion of the route (Robert Campbell Highway) adopts seasonal payload restrictions of 75% during the spring break-up period. Copper concentrate may be hauled from the ABM Mine south along the Robert Campbell Highway to a rail head in BC for transportation to domestic markets. The concentrate transport operations will be outsourced, with workshop, and support facilities expected to be established at Watson Lake. Zinc and HPM concentrate will be exported from the port at Stewart using upgraded facilities to be provided by Stewart World Port. The port facilities currently comprise a concrete deck and steel pile jetty with one berth suitable for Handysize and Handymax vessels.
Costs	The capital and operating cost estimates are considered within normal limits of accuracy expected for a Feasibility Study. The cost estimates from the Q3 2023 as estimated in the 2023 Economic Update remain valid. The inputs and assumptions of the Feasibility Study-level investigations reported in this Report (and the reports informing it) remain applicable and appropriate for the disclosed information. This update of the Kudz Ze Kayah Project economics was completed to reflect a June 2023 quarter cost base as the Project continues to advance through the regulatory phase of the licensing process, and the Company commences preparations for financing the Project development. A Work Breakdown Structure (WBS) was established for the initial capital cost estimate. Costs have been classified into the various WBS areas to ensure that the full cost of

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Criteria	Commentary

developing the Project has been captured. The capital cost estimate includes contributions from several parties, who are specialists in their field. A bottom-up cost estimate was prepared for the process plant. Quantities were estimated from material take-off of 3D design models (e.g. Navisworks) and 2D design drawings. Project-specific vendor quotes were sourced for all major materials and equipment. Minor equipment costs were sourced from Allnorth. Labor requirements were estimated using typical industry norms for similar style projects. Freight costs were estimated based on factored mark-up of the direct costs.

The open pit mining cost "contractor" model was replaced by an "owner operator" model prepared in-house and using manufacturer supplied operating and maintenance costs. The explosive costs are based on supply under contract by an explosives company. The contract includes the establishment of fixed infrastructure for storage of ammonium nitrate and emulsion explosives and the provision of magazines for packaged explosives and detonators. Diesel consumption was estimated by factoring material movement and explosive consumption and including nominal provisions for owner's equipment and other miscellaneous requirements.

The cost base for the Krakatoa underground project is based on submissions from mining contractors to an RFQ from BMC, where four companies submitted pricing for the construction of the underground mine. The RFQ was based on an earlier mine design than the final design used in the Feasibility Study. For completeness, the final Feasibility Study design was requoted with a Tier 1 contractor.

Processing operating costs include all site related operating costs associated with processing ore. The cost estimate was a bottom-up cost estimate based on typical industry norms. Labor costs were benchmarked against data available for comparable northern mining operations and projects.

Commodity prices and foreign exchange rate used in the 2023 Economic Update model are consensus based, established by taking the average forecast from a range of financial institutions.

No vendor or third-party royalties are applicable to the mine plan presented in the Feasibility Study.

Yukon mining royalties under the Quartz Mining Act are payable to the Yukon Government annually. The Quartz Mining Act royalty is a net profits royalty, based on annual mineral production and sales after deduction of eligible expenses and allowances. The royalty is applied on an incremental cumulative basis until the mine's calculated net profit is accounted for. The royalty rates are summarised in the table below:

Royalty lower band (C$)	Royalty upper band (C$)	Royalty applicable to band
$0	$10,000	0%
$10,000	$1,000,000	3%
$1,000,000	$5,000,000	5%
$5,000,000	$10,000,000	6%
$10,000,000	$15,000,000	7%
$15,000,000	$20,000,000	8%
$20,000,000	$25,000,000	9%
$25,000,000	$30,000,000	10%
$30,000,000	$35,000,000	11%

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<table>
<tr><th>Criteria</th><th>Commentary</th></tr>
<tr><td></td><td>$35,000,000 and above 12%

BMC have entered a streaming arrangement with Wheaton Precious Metals which is discussed in more detail in the Market Assessment section below.</td></tr>
<tr><td>Revenue factors</td><td>Commodity prices used for the Feasibility Study economic model update in October 2023 are consensus prices, established by taking the average price forecasts from a range of financial institutions and are presented in the table below:

<table>
<tr><th>Parameter</th><th>Unit</th><th>2023</th><th>2024</th><th>2025</th><th>2026</th><th>2027/Long-term</th></tr>
<tr><td>Zinc</td><td>US$/lb Zn</td><td>1.21</td><td>1.21</td><td>1.23</td><td>1.24</td><td>1.20</td></tr>
<tr><td>Silver</td><td>US$/lb Ag</td><td>23.55</td><td>23.75</td><td>23.61</td><td>23.36</td><td>22.60</td></tr>
<tr><td>Copper</td><td>US$/lb Cu</td><td>3.90</td><td>3.91</td><td>4.13</td><td>4.27</td><td>3.80</td></tr>
<tr><td>Gold</td><td>US$/oz Au</td><td>1922</td><td>1915</td><td>1853</td><td>1808</td><td>1700</td></tr>
<tr><td>Lead</td><td>US$/lb Pb</td><td>0.95</td><td>0.94</td><td>0.93</td><td>0.94</td><td>0.95</td></tr>
<tr><td>Exchange Rate</td><td>USD:CAD</td><td>1.342</td><td>1.327</td><td>1.320</td><td>1.315</td><td>1.297</td></tr>
</table></td></tr>
<tr><td>Market assessment</td><td>The zinc concentrate produced will be a mid-grade material with payable silver content. There are some elements that may attract penalties, primarily mercury, and cadmium. The cadmium level exceeds the current limit for import into China; however, this market could be accessible through blending the product with other concentrates via trading houses. Other potential markets exist in the Asia region such as Korea and Japan but will be subject to respective concentrate quality criteria. Korea Zinc has indicated that chromium is a critical element as their smelters are limited in the chromium content of the ferrous product from their fuming furnaces. European markets remain a possibility.

There are several advantages of this concentrate. With many of the world's smelters integrated with additional processing facilities, the copper, and lead content of the zinc concentrate represent value added opportunities. The very low silica content of the concentrate (0.1%) will be very attractive, as many of the world's large zinc mines contain silica levels of 4% and higher, and smelters are struggling with the silica load.

The zinc concentrate will be shipped out of the Port of Stewart, BC. Logistics costs will likely be cheapest to Asia which is expected to be the primary destination for the zinc product; however, European ports are also accessible from this location.

The copper concentrate quality for the first 18 months (Quality A concentrate) will be complex, with elevated levels of lead, zinc, antimony, and arsenic. The arsenic and lead levels exceed the current Chinese import limit for copper concentrates, but since the silver, and gold levels are elevated, this concentrate could possibly be sold directly into China as a precious metals concentrate. Alternatively, it could be blended with product from other producers via a trading house.

In December 2021, BMC entered into a streaming agreement with over a portion of the gold and silver produced from the KZK Property only (the PMPA). The PMPA is now held by now held by Wheaton Precious Metals Corp (Wheaton). The proportion of gold and silver covered by the PMPA varies over the life of the project, in accordance with the information in the table below. the holder of the PMPA will pay 20% of the LBMA price for gold and silver delivered into the stream.</td></tr>
</table>

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Criteria	Commentary
	<table><tr><th>Parameter</th><th>Threshold</th><th>Stream</th></tr><tr><td>Gold Tier 1</td><td>First 330,000 oz</td><td>7.125%</td></tr><tr><td>Gold Tier 2</td><td>Next 59,800 oz</td><td>5.875%</td></tr><tr><td>Gold Tier 3</td><td>Next 270,200 oz</td><td>5.250%</td></tr><tr><td>Gold Tail</td><td>Remaining production</td><td>6.500%</td></tr><tr><td>Silver Tier 1</td><td>First 43.300 Moz</td><td>7.125%</td></tr><tr><td>Silver Tier 2</td><td>Next 7.958 Moz</td><td>5.875%</td></tr><tr><td>Silver Tier 3</td><td>Next 35.342 Moz</td><td>5.250%</td></tr><tr><td>Silver Tail</td><td>Remaining production</td><td>6.500%</td></tr></table>
Economic	The economic analysis is based on capital costs originally described in the Feasibility Study and cash flows driven by the production schedule. The revenue parameters, capital, and operating costs have been updated in October 2023 in the KZK 2023 Economic Update. The cash flow projections include initial and sustaining capital estimates; mining, processing, and concentrate logistics costs, revenue estimates based on concentrate pricing adjusted for fees, charges and royalties; and a discount rate of 7%. The economic analysis completed to date demonstrates that the Project is commercially viable. The Base Case LOM metal price assumptions and treatment charges used (which are in real dollar terms), include industry consensus metal prices and concentrate charges derived from long-term forecasts. The sensitivity of project value to key input parameters was assessed by varying each parameter over the range of -10% to +10%. All five metal inputs (zinc, copper, lead, gold, and silver) were varied by the same amount for assessing sensitivities of metal price and head grade. Metal price and head grade inputs demonstrated the greatest sensitivity to project value. The exchange rate was the next most sensitive variable, followed by operating cost, and finally capital cost. The Feasibility Study results remained favourable within these values.
Social	Teck (formerly Cominco) undertook an extensive consultation and engagement programme, which informed Project design, and helped develop the mitigation and management strategies for the Project. BMC's consultation and engagement efforts commenced prior to purchase of the Project, building on the strong and cooperative relationships between the RRDC and Cominco/Teck. This has subsequently been maintained with First Nations Governments, stakeholders and interested parties during the preparation of the exploration permit application, and initiation of the environmental and socio-economic baseline studies. Since 2015, BMC has extensively engaged, and consulted with government agencies, First Nations, various stakeholder groups, and interested parties. BMC staff meet regularly with Ross River Dena Council and Liard First Nation leadership and officials, as well as regular community meetings and BMC provides ongoing financial capacity support to enable First Nation participation in Project assessment, permitting, and development. The engagement with First Nations is consistent with and builds upon the existing SEPA. BMC has also produced a quarterly newsletter to keep the local communities abreast of the Project's developments as well establishing a Project website to engage with a wider public audience. BMC has developed a Consultation and Engagement Plan (CEP) that describes the path forward as the Project transitions from environmental assessment to permitting. The CEP sets out the tools, techniques, and context for consulting with the entire suite of governments, agencies, boards, organisations, and stakeholder groups with whom BMC will continue to engage to support assessment and eventual licensing and operation of the Project. Techniques described in the CEP will ensure that assessment, licensing and operations, and closure of the proposed mine is underpinned by thorough, formal consultation. BMC considers the CEP to be a useful tool in guiding activities and approaches. In many cases, BMC believes it has gone beyond the basic expectations set out in that document. BMC has provided support to First Nations for them to undertake Traditional Knowledge and Traditional Land Use Studies. Any local and traditional knowledge provided by the First Nations will factor into the proposed mine's policies and design of monitoring programmes and this will allow BMC to avoid culturally and/or ecological significant and sensitive areas.
Other	A Risk Assessment Workshop was conducted during the Feasibility Study and a Risk Register developed which identified a number of high-, medium-, and low-level risks after mitigation measures.

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Criteria	Commentary
	Most risks identified could be mitigated to manageable levels; however, of the five remaining high risks, realising full value of the concentrates was predominantly the theme of the remaining elevated risks. This was either through changes in offtake terms, changes to import restrictions, increased sea freight charges, or the ability to meet agreed specifications. While the expected concentrate qualities are considered complex, assessments concluded that they should be able to be produced to the target specification and find a buyer, either as a direct sale to a smelter or through an established trading house. BMC propose to mitigate this risk during the project development phase through securing of sales agreements ahead of production. With regards to sea freight charges, volatility is expected, and provisions within the study are above market long-term median pricing. The fifth remaining high risk was in relation to the Upper and Lower Water Management Pond embankments and reflects the importance of these structures to the operation. It should be noted that these structures are not considered to be an elevated risk; rather, the rating reflects the conservatism and limitations of the assessment criteria, insofar as the "Likelihood" was considered to be at the low end of the "rare" classification (significantly less than 10% chance of occurring threshold for a "rare" classification) and no more appropriate criteria was available to apply. A Type A Water Licence (QZ97-026-1) was granted to Cominco for a period of 20 years on 17 September 1998 and assigned to BMC in January 2015. The Water Licence at the time of grant allowed for construction and operation of the mine as proposed by Cominco and was more recently sufficient for BMC's water use in support of exploration activities. This licence expired on 28 September 2018. Prior to expiry of the Type A Water Licence, BMC was granted a Type B Water Licence (QZ16-085) on 15 June 2017 to allow for continuity of activities after expiry of the Type A licence. This licence expires on 6 June 2027. BMC has submitted applications for Water Licences to the Yukon Water Board and an application for a Quartz Mining Licence to the Yukon Department of Energy, Mines, and Resources. The Company anticipates that the Type A Water Licence and Quartz Mining Licence will be issued in second half of 2026. A Class 3 Exploration Permit (LQ00424), covering the contiguous claims over and adjacent to the ABM Deposit, (the KZK Property) was granted to BMC for a 5-year period from an effective date of 29 June 2015. This permit (MLU LQ00424) was subsequently amended 15 June 2017 to a 10-year period resulting in an expiry of 28 June 2025. It was further extended to 31st December 2025 by an Order in Council. A new Class 3 Mining Land Use permit application has been lodged. A YESAB recommendation to proceed has now been received for this MLU permit application. Next step is to receive a Decision Document from the Decision Body (Yukon Government). Meanwhile, a Yukon Government Order In Council (OIC) has extended current Class 3 MLU permit to end of 2026 as an interim measure. If new class 3 is granted the OIC and current class 3 fall away (refer solicitors report)
Classification	Probable Ore Reserves were estimated from Indicated Mineral Resources as per the JORC (2012) guidelines. 0% of Ore Reserves have been based on Measured Mineral Resources. Mr Karl van Olden, the Competent Person for this Ore Reserve estimation has reviewed the work undertaken to date and considers that it is sufficiently detailed and relevant to the deposit to allow those Ore Reserves derived from Indicated Mineral Resources to be classified as Probable.
Audits or reviews	An internal audit was completed by CSA Global (an ERM Group Company) which verified the technical inputs, methodology, parameters, and results of the ORE. No external audits have been undertaken.
Discussion of relative accuracy/ confidence	This ORE is supported by the 2020 Re-stated Feasibility Study completed in October 2020 and the KZK 2023 Economic Update completed in October 2023. The level of accuracy of the study and the ORE is at a confidence level expected for a Feasibility Study. The Feasibility Study has concluded that the mine plan is both technically achievable and economically viable. The Project has an IRR and NPV which makes it robust in terms of cost variations. There has been no production at the Project to date, so no comprehensive comparison, or reconciliation of data has been made.

APPENDIX B: JORC CODE TABLE 1 – KONA PROPERTY

Covering the Kona Deposit Mineral Resource estimate, Exploration Target, and Exploration Results.

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Section 1: Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections)

Criteria	Commentary
Sampling techniques	The Kona Property has been tested by 126 diamond holes, totalling 23,248.69 m, of NQ2, BQTK and AX core diameter all focused on or about the Kona VHMS Deposit. Drilling in 1996–1997 was completed by Columbia Gold Mines Ltd (now Pacific Ridge Exploration Ltd), who drilled 108 NQ2- and BQTK-core diamond holes, totalling 22,073.25 m. Historical AX core diamond drilling (1966–1967) was completed by Atlas Explorations Ltd and included six drill holes, totalling 593 m. This total does not include the 23 shallow pack-sack drill holes, totalling 224 m, and 12 AX core diamond drill holes, totalling 582 m, completed by Cassiar Asbestos Corporation in 1961 because the drill sites and results are poorly documented. Holes were oriented in various directions due to physical access restrictions (000°, 072°, 162°-177° and 212°-252°) at various dip angles (-45° to -90°). The drill core was geologically and geotechnical logged in detail, exceeding industry standards at the time. This included lithology, mineralogy, RQD, recovery and other attributes. Drill holes were logged and selected intervals were manually split lengthwise. Split samples comprised half-core in 1 m intervals adjusted firstly to lithologic boundaries, and secondly to mineralogy of massive sulfide mineralisation. Core from the 1996-1997 drilling was dispatched to either Min-En or later Chemex Laboratories for prep work (dried, crushed, pulverised) in Smithers, BC and analysis in Vancouver, BC. Approximately 10% of samples were sent for check assay at Acme Analytical Laboratories, no field duplicates were collected during 1996–1997 drill campaigns. Assay analysis was carried out on mineralised subsamples, comprising 0.5 to 2.00 g splits, were analysed for copper, zinc, lead, and silver content using AA. The gold content of the subsample pulp was determined after aqua regia digestion by fire assay and AAS procedures. An additional 2,262 core samples were analysed by 31 elements by ICP techniques. Earlier exploration sampling has been superseded by the extensive drilling which has subsequently taken place, and therefore details of earlier sampling are not discussed.
Drilling techniques	Diamond drilling undertaken by Columbia Gold Mines Ltd used two Super 38 diamond drill rigs with NQ2 (50.6 mm diameter) and BQTK (40.7 mm diameter) core. Drilling equipment and personnel were contracted from J.T. Thomas Diamond Drilling of Smithers, BC. The core was not oriented.
Drill sample recovery	All recovered drill core was thoroughly measured, and the recoveries and RQD were recorded first as handwritten logs and later this data were entered daily into a spreadsheet-style database on site. Drill core recoveries were consistently more than 90%. Reduced core recoveries were only encountered within structurally incompetent zones. Reduced drilling speeds and head pressures plus drilling media additives were used to improve core recoveries in the more structurally incompetent zones. There does not appear to be any bias between drill core recoveries and grade of mineralisation. Core recoveries through weakly mineralised country rocks and, more importantly, the mineralised VHMS horizons, were consistently greater than 90%. This is considered quite adequate to support the MRE.
Logging	The drill core was geologically and geotechnically logged in detail, exceeding industry standards at the time. The level of logging detail was and is appropriate for mineral resource estimation. All geotechnical aspects of the drill core, including recovery and rock quality features, were logged prior to logging its lithology and mineralogy. The geologist then designated sampling intervals based upon its geological features and all the drill core was photographed wet prior to sampling. All 1996 and 1997 diamond drill core comprising 22,073.25 m (in the BMC database) of drilling was thoroughly logged. All relevant intersections were thoroughly logged and sampled by qualified geologists.
Subsampling techniques and sample preparation	The sampled diamond drill core was split in half lengthwise using a manual Longyear core splitter. Any whole sections of drill core collected for metallurgical studies or exhibition were permanently marked in the respective core boxes. No non-core holes have been drilled at the deposit. The samples were manually split, and half-core samples were double bagged and securely stored prior to direct shipping to either Min-En or later Chemex Laboratories in Smithers, BC. There the samples were dried, crushed to minus 1/8 inch and pulverised to 95% minus 150-mesh, rolled and bagged. The subsamples were then direct shipped to Min-En's or later Chemex's assay laboratories in Vancouver, BC for analysis.

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	These procedures are considered industry standard techniques and appropriate for the style of mineralisation. This is considered quite adequate to support MRE. Of the 1,977 mineralised drill core samples collected during the two drilling campaigns, approximately 10% of the mineralised samples (120) were check-assayed at Acme Analytical Laboratories. Check assaying was carried using similar techniques to the original analytical procedures to reduce any bias. No field duplicates were collected during the 1996 and 1997 drilling campaigns. In 2014 Merah Resources (MinQuest) contracted APEX Geosciences to resample existing mineralised core. Half-core was cut with a diamond saw, and 15 quarter-core samples were submitted to ALS in Vancouver, along with standards and blanks. All analytical results returned copper, gold and cobalt values within two standard deviations or less of the 1996–97 half-core assays. The sample size varied according to the sampled drill core lengths. These lengths were determined by the lithology and mineralogy of the drill core based upon geological and geotechnical logging results. Sample lengths were appropriate for the intersected rock type and mineralisation. Subsampling techniques and sample preparation are considered adequate to support MRE.
Quality of assay data and laboratory tests	In 1996–97 mineralised subsamples, 0.5 to 2.0 g splits, were analysed for copper, zinc, lead, and silver using AA technique. The gold content of the subsample pulp was determined with aqua regia digestion followed by fire assay and AA procedures. In addition, 2,262 drill core samples were analysed for 31 elements by ICP techniques. Assaying and analyses were only carried out on selected section of drill core. For the 2014 duplicate analyses; mineralised subsamples, 0.5 to 2.0 g splits were analysed using ALS Chemex ME-ICP61 (four-acid digest) for copper, cobalt, and zinc. Method Au-ICP21 (fire assay – ICP finish) was used to analyse gold. The analytical techniques are total analysis and considered to be appropriate for the style of mineralisation. There is no record of Columbia Gold Mines Ltd recording magnetic susceptibility, taking x-ray fluorescence (XRF) readings, or using other tools. No standards or blanks were inserted with the 1996–97 samples. The 1996-1997 diamond drilling preceded currently accepted QAQC procedures. However, the assay/analytical results from 10% of the mineralised core samples were check-assayed using similar analytical techniques and acceptable levels of accuracy and precision were established. 2014 duplicate sampling confirms the veracity and precision of the 1996–97 analytical results at an acceptable level. Quality of assay data are considered adequate to support MRE.
Verification of sampling and assaying	Selected mineralised intervals have been viewed for verification by BMC. Significant intercepts appear to correlate with the intensity of mineralisation logged in the field. Twin holes have not been completed. All geological and geotechnical features were handwritten as hardcopy logs by a qualified geologist. These logs were photocopied, and data was entered daily into a spreadsheet database. All electronic data was double checked on site, and later visually and statistically verified by Colombia Gold Mines Ltd (Pacific Ridge Exploration Ltd). Assay data was not adjusted or factored.
Location of data points	Proposed drill sites and completed collars for all 1996–97 drill holes were surveyed to an accuracy of 1 cm by a contracted surveyor. Predetermined benchmarks on the property were surveyed in from Federal geodetic points. Down-hole surveys were carried out usually at 30 m intervals using a mechanical down-hole instrument measuring azimuth and inclination deviation. Initial drill hole collar surveying was carried out using the UTM NAD27 coordinate system and was converted to UTM NAD 83 after the airborne photogrammetry survey was completed. Drill hole collars were surveyed with an accuracy of 1 cm, and the aerial photogrammetry gave a topographic control to less than 5 m contours. Location of data points is considered adequate to support MRE.
Data spacing and distribution	The 1996 drilling was done on 25–50 m spaced sections. Once the continuity of the mineralisation had been established, drilling sections were 100–200 m apart to delineate the 1,500 m plunge extent of the buried mineralisation. Surface holes were sited and directed to intersect each of the six horizons of VHMS mineralisation as perpendicular as possible to establish true thicknesses. Drill spacing and distribution is sufficient to establish the geometry and continuity of the stratabound VHMS mineralisation within its drill tested strike length.

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	Sample compositing was not applied. Data spacing and distribution are considered adequate to support MRE.
Orientation of data in relation to geological structure	Drill holes were sited and directed to intersect these lenses as close to perpendicular as possible. Generally, the mineralised lenses strike 130° and plunge 0 to 20° south-easterly. No obvious bias between the sampling and the orientation of drilling along the trend and plunge of the six main lenses is present. Each mineralised lens was pierced and sampled multiple times by several drill holes. No significant sampling bias appears to have been introduced by drill orientation relative to the mineralisation.
Sample security	Samples were collected, labelled, and double bagged in individual 6-mil poly bags with an assay tag, then five to seven bagged samples were placed in woven rice bags that were wired closed. The bagged samples were then securely stored on site until they were flown to Watson Lake, Yukon where they were then trucked directly to the preparation laboratories in Smithers, BC.
Audits or reviews	CSA Global has reviewed the records of BMC and no significant issues were identified in the geological understanding or exploration data integrity.

Section 2: Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section)

Criteria	Commentary
Mineral tenement and land tenure status	The Kona Property comprises the Fire Lake Claim Block, a set of 161 contiguous mineral claims 100% owned by Finlayson Copper Ltd (a wholly owned subsidiary of BMC Minerals Ltd) and the contiguous Tsa Da Glisza Claim Block, a set of 121 contiguous mineral claims 100% owned by BMC Minerals Ltd. No residual royalties reside with the Fire Lake Claim Block. BMC does not hold metals rights over the Tsa Da Glisza Claim Block. There is a 1.0% gross royalty on gemstone production from the Tsa Da Glisza Claim Block. There exists no impediment to obtaining a licence to operate in the area under the existing statutory requirements. A staking moratorium exists over the area, but this does not prevent operations within the project tenure.
Exploration done by other parties	A massive sulfide float boulder was first discovered in 1960 by prospectors of Cassiar Asbestos at the south end of Fire Lake and later discovered massive pyrite mineralisation exposed in Kona Creek. They drilled 23 shallow pack-sack holes (224 m) and 12 AX-size core holes (582 m) testing near surface mineralisation. During 1965–1967, Atlas Copper carried out geological, geochemical, and geophysical (magnetics and electromagnetics (EM)) surveys plus drilled six AX-size core holes. Amax Potash Limited carried out assessment work on the Project prior to Welcome North Mines Ltd (later Welcome Opportunities) acquisition. Welcome North and Placer Dome both undertook ground and airborne geophysical surveys respectively prior to the 1995 optioning by Columbia Gold Mines Ltd. During 1996–1998, Columbia Gold Mines (now Pacific Ridge Exploration) completed detailed geological mapping, surface geochemical sampling, ground-based magnetic and HLEM surveys, and a total 108 diamond drill holes for 22,073.25m of drilling. The ground magnetic and HLEM geophysical surveys delineated an 1,800 m long, northwest-southeast trending response, the southeastern end of which was interpreted to be reflect the up-plunge component of the Kona Deposit. Diamond drilling delineated three horizons of massive to semi-massive sulfide and magnetite mineralisation hosting copper-cobalt-gold (± zinc, silver) mineralisation. Preliminary metallurgical testwork was undertaken on the Kona sulfide mineralisation. In 2014, Merah Resources Ltd undertook core resampling and assaying, and an airborne VTEM™ and magnetic survey.
Geology	The stratiform Kona VHMS Deposit is hosted by the Fire Lake metavolcanic unit (≈365 Ma) that has been thrust emplaced over the Devonian to Mississippian Grass Lakes Group. Two parallel zones of VHMS mineralisation, East Kona and West Kona, comprise the Kona Deposit; separated by an inferred reverse or growth fault. The East Kona zone mineralisation is 100–150 m wide and consists of two massive to banded sulfide-bearing horizons (i.e. Upper and Lower East Kona) separated by 40–70 m of chlorite schist derived from basaltic to andesitic volcanic rocks. The Lower East Kona horizon has been divided into north and south portions separated by an apparent gap in the horizon. The northern portion is 3–16 m thick and the southern portion is 2–11 m thick. The Upper East Kona horizon averages thicknesses of 8–12 m. These horizons consist mainly of pyrite with lesser pyrrhotite and chalcopyrite, local lenses of massive magnetite, and minor sphalerite plus cobalt, gold, and silver values. The West Kona zone is inferred to be 75–125 m wide. The thickness of the mineralised horizon varies across this width from about 44 m in the east to less than 1 m at the western margin; the thickness also varies along strike. It includes mineralisation that changes laterally from magnetite, pyrite and chalcopyrite in a siliceous matrix, through massive pyrite and lesser chalcopyrite, to massive pyrrhotite with minor pyrite and chalcopyrite. This mineralisation occurs close to a stratigraphic contact between chlorite schist derived from basaltic to andesitic volcanic rocks and overlying carbonaceous phyllite derived from sedimentary rocks.

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<table>
<tr><th>Criteria</th><th>Commentary</th></tr>
<tr><td></td><td>The entire host sequence is interpreted to have been fault emplaced over units of the Grass Lake Group.</td></tr>
<tr><td>Drill hole information</td><td>Kona Deposit has been tested by 114 holes totalling 22,666.69 m of diamond drilling in the drill hole database. Most of this drilling was conducted along a 1,500 m plunge extent from near its surface exposure in Kona Creek south-easterly to the ridge between Kona and Outfitter's Creek drainage. The drill tested mineralisation occurs within an area approximately 1,500 m long by 250 m wide, trending at 130°, and plunging at 0° to -20° to the southeast.
No information has been excluded.</td></tr>
<tr><td>Data aggregation methods</td><td>As a Mineral Resource has been estimated and reported, data aggregation methods within drill holes are accommodated within the methodology of the estimate.
Cross-section display intersections of massive sulfide based on geological boundaries. There is a sharp contact between barren host rock against massive sulfide in most cases.
Metal equivalent values have not been reported, only actual metal grades.</td></tr>
<tr><td>Relationship between mineralisation widths and intersection lengths</td><td>The relationship between the geometry of the mineralisation and the drill hole intercepts were individual and variable with each of the six main stratiform VHMS lenses. Generally, the lenses strike 130° and plunge 0 to 20° south-easterly.
Drill holes were sited and directed to intersect these lenses as close to perpendicular as possible.</td></tr>
<tr><td>Diagrams</td><td>Appropriate figures have been provided in body of report to illustrate the exploration results and mineral resource estimation.</td></tr>
<tr><td>Balanced reporting</td><td>Exploration results outside the MRE are reported in a balanced fashion which is not misleading.</td></tr>
<tr><td>Other substantive exploration data</td><td>Historical work which led to the discovery of the Kona Deposit has also resulted in additional targets defined by anomalous geochemistry and geophysics. This work includes geological mapping, geochemical analyses of silt, rock and soil samples and ground geophysical surveys (EM and magnetics).
Preliminary metallurgical studies conducted in 1997 showed recoveries of 90% for copper and 70% for gold are achievable using conventional grinding and flotation circuits. Additional studies on cobalt recoveries indicated 70% and 95% recovery from grinding with flotation and pressure leaching, respectively. The metallurgical studies are considered preliminary in nature and additional work is required to confirm expected metallurgical performance.
In 2014 an airborne VTEM™ and magnetic survey was flown over the property. Results of the survey indicate additional EM, and magnetic high anomalies underlie the property.
BMC has focused on the integration and reinterpretation of existing data sets and three-dimensional modelling of the geology for the purpose of defining a Mineral Resource Estimate and future drill targets. This included remodelling of the 2014 VTEM™ survey data. The Company have relogged existing diamond core and undertaken field mapping and rock chip sampling along strike and down slope of the mineralised iron formation</td></tr>
<tr><td>Further work</td><td>BMC has identified 10 exploration prospects/targets where they intend to undertake further work. These are listed in the following table, with the proposed exploration programmes for each summarised.
<table>
<tr><th>Target</th><th>See Table 16-9</th><th>Exploration programme</th></tr>
<tr><td>Outfitter Creek E-4</td><td rowspan="2">1A-C</td><td>Review existing data; review usefulness of IP for geophysical surveying</td></tr>
<tr><td>Outfitter Creek 2</td><td>Review existing data; ground EM survey</td></tr>
<tr><td>Kona ET Down Plunge</td><td rowspan="4">2A-D</td><td>Diamond drilling, metallurgical testwork, MRE</td></tr>
<tr><td>Kona Stacked Lens</td><td>Re-logging core, down-hole EM existing drill holes, diamond drilling</td></tr>
<tr><td>North Fork 1</td><td>Review historical drilling</td></tr>
<tr><td>Kona Northwest</td><td>Further field work and reinterpretation of data to define drill targets</td></tr>
<tr><td>East Ridge</td><td rowspan="2">3A-B</td><td>Mapping and geochemistry; ground EM or IP</td></tr>
<tr><td>Outfitter Creek 1</td><td>Reprocess geophysical data; diamond drilling</td></tr>
<tr><td>North Ridge</td><td>4</td><td>Ground EM survey; physical property testing of rocks; diamond drilling</td></tr>
<tr><td>GP1</td><td>5</td><td>Further field work</td></tr>
</table></td></tr>
</table>

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Criteria	Commentary
	Appropriate diagrams and inferences on this further work have been provided in the report.

Section 3: Estimation and Reporting of Mineral Resources

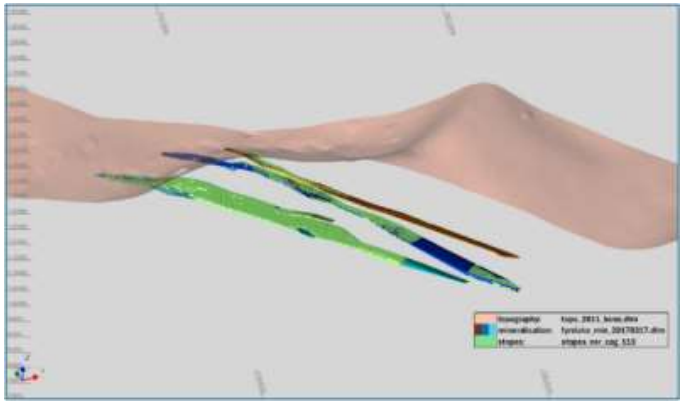
(Criteria listed in section 1, and where relevant in section 2, also apply to this section)

Criteria	Commentary
Database integrity	Data used in the CSA Global MRE was sourced from the database supplied by BMC from original "hard copy" assay files and drill logs. Validation methods included review of drill logs and other hardcopy data and a review in 3 D graphics to highlight any obvious errors. Database scripts were run to check for missing data, abrupt down-hole azimuth changes, sample depths greater than recorded hole depth, overlapping intervals. No errors in data entry or other information were discovered upon review.
Site visits	A site visit was conducted by Aaron Green (Competent Person), Neil Martin (BMC Technical Director) and Robin Black (BMC – VP Exploration) on 26 July 2017. The purpose of the site visit was to: Inspect the principal assets within the Kona Property, and complete initial ground verification with associated outcropping geology and mineralisation Review site layout and access Review the geology Inspect historical drilling locations Review sample storage facilities including historical core storage farm. More recently, Aaron Green undertook a one-day, helicopter supported site visit to the Kudz Ze Kayah Project on 5 June 2024. No active drilling was being undertaken at the time. The site visit included an overview of the Kona core farm, camp and deposit location. There were no negative outcomes from the above site inspection.
Geological interpretation	Geological and mineralisation wireframes were supplied by BMC in Surpac format. CSA Global checked the wireframes to ensure all interpreted strings were 'snapped' to drill holes based on chemical assays and then validated the wireframes for estimation. Continuity of mineralisation is excellent and is intimately associated with massive sulfide horizons. The geological interpretation provided a sound foundation for interpretation of boundaries to the polymetallic copper-zinc-gold-silver mineralisation. Detailed geological logging, in conjunction with mineralogy and chemical assays has been used to identify individual lithological units during the interpretation process. Copper and gold assays, along with the logged geology were plotted on drill hole traces to define the interpretation. No assumptions have been made. Geological continuity is very good between drill holes and conforms well to anticipated geological models for Besshi-style VHMS mineralisation. Wireframes have been constructed for the main mineralised horizons as determined by the geological logging and chemical assays. The data does not lend itself to alternative interpretations. Geology has been the primary influence in controlling the Mineral Resource estimation. Wireframes have been constructed for the main mineralised horizons as determined by the geological logging and chemical assays. Continuity of geology and structures can be identified and traced between drill holes by visual and geochemical characteristics. The massive sulfide and magnetite ± sulfide zones hosting the mineralisation have been logged in the drill core and have been modelled.
Dimensions	Two parallel zones of VHMS mineralisation (East Kona and West Kona) comprise the Kona Deposit; separated by an interpreted reverse or growth fault. The East Kona zone mineralisation is 100–150 m wide and consists of two massive to banded sulfide-bearing horizons (i.e. Upper and Lower East Kona) separated by 40–70 m of chlorite schist. The Lower East Kona horizon has been divided into north and south portions separated by an apparent gap in the horizon. The northern portion is 3–16 m thick

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Criteria	Commentary
	and the southern portion is 2–11 m thick. The Upper East Kona horizon averages thicknesses of 8–12 m. The West Kona zone is interpreted to be 75–125 m wide. The thickness of the mineralised horizon varies across this width from about 44 m in the east to less than 1 m at the western margin; the thickness also varies along strike. The Kona Mineral Resource is contained within an area extending from 418,605 m E to 420,045 m E (1,440 m) and 6,788,330 m N to 6,789,280 m N (950 m). The reported Mineral Resource lies within 530 m of surface (1,540 m RL to 1,010 m RL).
Estimation and modelling techniques	All modelling was undertaken using Surpac V6.6.2 software. Hard boundaries were used for the six massive sulfide domains consistent with the geological interpretation. Following statistical analysis, it was determined that high-grade cuts were required for objects 1, 2 and 3 for silver, gold, copper, and zinc. Statistical analysis was completed using Supervisor™ software. Block grades and density were interpolated using ordinary kriging (OK) techniques. An oriented "ellipsoid" search was used to select data for interpolation. Search ellipsoid orientations were based on lode orientations and drill spacing. An oriented "ellipsoid" search was used to select data for interpolation. Search ellipsoid orientations were based on orientations derived from the variographic analysis. An ellipsoid was produced for each individual element, with bearings varying from 114° to 305°, plunges between 5° and –20°, and dips between 90° and –87°, (Surpac convention). These orientations honour the orientation of the Kona Deposit. A two-pass estimation search was used to complete estimation for copper, zinc, gold, and silver within the domain objects, with separate dimensions for each element, based on the variogram ranges. The first pass search radii of 45–132 m, and second pass search radii of 90–264 m along strike were used with the minimum number of samples set to four and maximum samples per hole set to four for both passes. An average grade was used to inform remaining un-estimated blocks. Greater than 60% of the blocks were estimated in the first pass. As a high-level validation technique, the reported MRE was compared with previous estimates for the deposit. No reliance is placed on the previous estimates in relation to the current MRE. In 2014, IMC was contracted by MinQuest to review and update MRE for the Kona Deposit. No mining has yet taken place at the Kona Deposit. Gold has been estimated as it has been demonstrated that it will be recoverable as part of the copper recovery process. This was demonstrated by metallurgical testwork undertaken in the 1990s. Cobalt was not estimated by CSA Global as it occurs predominantly within pyrite (i.e. gangue) and was not deemed to have a likelihood of economic extraction at this time and is not material to the economic extraction of copper, gold and silver-bearing minerals. Potentially deleterious elements have not been estimated into the block model. A review of multi-element analyses undertaken by Lakefield Research metallurgical testwork indicates no significant deleterious elements. Future work will require additional trace and major element analysis for environmental assessment. A parent cell size of 20 m(E) by 10 m(N) by 5 m(RL) was adopted with standard sub-celling to 5 m(E) by 2.5 m(N) by 1.25 m(RL) to maintain the resolution of the mineralised lenses while restricting the overall size of the model. The block size is considered appropriate given the dominant drill hole spacing, style of mineralisation and possible mining methods. No assumptions were made regarding selective mining units. No assumptions were made about the correlation between variables. The geometry of the massive sulfide and massive magnetite ± sulfide horizons, as defined in logging and sectional/plan interpretation, formed the basis for mineralisation interpretations. An inferred fault was interpreted to separate the west and east Kona domains. The wireframe objects were used as hard boundaries for grade interpolation. Statistical analysis was completed using Supervisor™ software. Following statistical analysis, it was determined that several elements across the mineralised zones required high-grade cuts to reduce the impact of extreme outliers. Validation checks included statistical comparison between drill sample grades and OK block estimate results for each domain. Visual validation of grade trends for each element

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Criteria	Commentary
	along the drill sections was also completed in addition to swath plots comparing drill sample grades and model grades for northings, eastings, and elevation. These checks show good correlation between estimated block grades and drill sample grades. No reconciliation data is available as no mining has taken place.
Moisture	Tonnages were estimated on a dry *in situ* basis. No moisture values were reviewed.
Cut-off parameters	The mineralisation was modelled using logged semi-massive to massive sulfide horizons on the interpreted geological cross-sections which correlated closely to a nominal 0.5% Cu cut-off grade. Based on an assessment of similar deposits and preliminary mining studies, potential Mineral Resources were reported above a C$113/t NSR cut-off. The NSR was calculated as NSR US$/t = (68.31*cu_cut) + (60.26*au_cut), with inputs costs based upon on-site processing and only fresh, unoxidised material being processed. A gold price of US$3000/oz and a copper price of US$4.50/l. The US dollar NSR was converted to Canadian dollars using the exchange rate: NSR C$/t = (NSR US$/t)/0.75.  View Looking NE – Stope Outlines (pale green) over Mineralised Lodes generated for C$113/t cut-off
Mining factors or assumptions	Conceptual mining studies indicate that the Kona Deposit could be (subject to more detailed feasibility studies) exploited by underground mining methods given the scale and continuity of the mineralisation, particularly as a satellite mining operation to a central processing facility at the Kudz Ze Kayah Project. No other mining assumptions were made. Additional drilling is required to determine key deposit characteristics before detailed mining evaluation can take place.
Metallurgical factors or assumptions	Preliminary metallurgical testwork results from studies undertaken in 1997 indicate that recoveries of 90% for the copper values and 70% for the gold values could be achieved from a feed head grade of approximately 2% Cu and 1.2 g/t Au. Additional detailed metallurgical testwork is recommended as part of the next round of drilling for the Kona Deposit.
Environmental factors or assumptions	It has been assumed that the eventual extraction of the deposit can obtain environmental approvals. Waste production of PAG rock is potentially a key environmental issue. It is assumed that such disposal will not present a significant hurdle to exploitation of the deposit and that any disposal and potential environmental impacts would be correctly managed as required under the regulatory permitting conditions.
Bulk density	Fixed density values based on 3,828 "water immersion" measurements were assigned to the block model for each lithological unit, setting overburden to 2.0 t/m^3, oxide to 2.4 t/m^3, mixed volcanic sediments ("Vseds") to 2.79 t/m^3, siltstone to 2.82 t/m^3, and mafic to 2.88 t/m^3. The massive sulfide density was estimated using OK interpolation resulting in an average bulk density of 3.57 t/m^3 across the deposit.

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Criteria	Commentary
	During the 1996–97 programmes 3,828 bulk density measurements were determined on site using the dry vs water immersion method. Competent 5–10 cm long pieces of drill core were measured at 8 m intervals, except in mineralised zones where measurements were recorded at 1 m intervals. A portion of these field measurements were checked later by resin process in the assay laboratory during the drill core assaying. Bulk densities of drill core samples were measured at regular intervals for: both unaltered and altered host rocks in addition that within the various mineralised lenses along and across the entire known deposit. Average densities were applied to the host lithologies based on measured densities from drill core, while densities for the mineralised zones were interpolated. The densities used and estimated are comparable to other nearby VHMS deposits in the region.
Classification	The Mineral Resource classified as Indicated and Inferred taking into account the level of geological understanding of the mineralisation, quality of samples, density data, drill hole spacing, historical nature of the drilling, and sampling and assaying processes. Kona Deposit classification in plan view (Green = Indicated Mineral Resource, Red = Inferred Mineral Resource) – see Figure 16-16 The classification reflects areas of lower and higher geological confidence in mineralised lithological domain continuity based the intersecting drill sample data numbers, spacing and orientation. Overall mineralisation trends are reasonably consistent within the various litho-types over numerous drill sections. The MRE appropriately reflects the view of the Competent Person.
Audits or reviews	Internal audits were completed by CSA Global which verified the technical inputs, methodology, parameters and results of the estimate. No external audits were conducted on the MRE.
Discussion of relative accuracy/ confidence	The Mineral Resource accuracy is communicated through the classification assigned to various parts of the deposit. The MRE has been classified in accordance with the JORC Code (2012 Edition) using a qualitative approach. All factors that have been considered have been adequately communicated in Section 1 and Section 3 of this Table. The Mineral Resource statement relates to a global estimate of *in situ* tonnes and grade. No production data exists for reconciliation as the deposit has not and is not currently being mined.

Appendix C: JORC Code Table 1 – Wolf Property

Covering the Wolf Deposit Exploration Target and Exploration Results.

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Section 1: Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections)

Criteria	Commentary
Sampling techniques	The Wolf Prospect has been sampled using diamond drill holes spaced ≈60 m apart on sections spaced ≈60 m to ≈80 m apart. Historical drilling at the project was completed by Newmont (three holes) and Atna Resources Ltd (Atna) (45 holes). A total of 48 diamond drill holes occur within the supplied dataset for 10,402.3 m of drilling. Holes were generally angled (-45° to -90°) primarily towards ≈020° (Wolf) and 050° (East Slope Zone) with dip angles set to optimally intersect the mineralised horizon where access permitted. Diamond core was used to obtain high-quality samples that were logged for lithological, structural, density and other attributes. All 1997 and 1998 drill collar locations were picked up by survey contractors up to hole WF98-32. The remainder of the 1998 holes were located with reference to adjacent drilling and GPS. The 1997 and 1998 holes were set out with a compass and have used Pajari "single-shot" magnetic down-hole surveys taken at least once in most cases. Exact details of the down-hole survey methods for the earlier drilling programmes have not been located. Limited historical quality assurance procedures and quality control results have been documented in various internal reports. Further investigation is required. Drill holes were logged and selected intervals were cut with a diamond saw. Cut samples comprised half-core from down-hole intervals nominally 1 m in length adjusted to geological boundaries. Core from the 1997 programme was dispatched to Pioneer Laboratories Inc. for analysis, and from the 1998 programme to Acme Analytical Laboratories, both located in British Columbia. Samples were crushed and pulverised, although record of the subsample size which was pulverised no longer exists. For 1997 drilling: 1 g of sample digested with 50 mL of aqua regia, diluted to 100 mL with water and finished by AA to provide copper, lead, zinc analyses to 0.01 wt% detection limit and silver to 0.1 ppm detection limit. 10 g of sample digested with aqua regia, MIBK extracted, finished with graphite furnace AA to provide gold analyses to 1 ppb detection limit. For 1998 drilling: All samples were analysed using 0.5 g sample digesting in 3 mL of equal parts HCl, HNO_3-H_2O Select higher-grade intervals were initial digestion of 1 g and then later 0.25 g of sample with 30 mL of aqua regia, diluted to 100 mL with water and finished by ICP to provide lead, zinc analyses to 0.01 wt% detection limit and silver to 0.01 oz/t detection limit.
Drilling techniques	Diamond drilling undertaken by Atna used a BB2500 hydraulic fly-drill with NQ core size. Core was not oriented.
Drill sample recovery	Core was logged in the field and core recovery was recorded on drill logs. Mineralised zones are typically fresh and coherent and >90% recovery was achieved. There is no record available for methods applied to maximise sample recovery. The massive sulfide style of the mineralisation, consistency of the mineralised intervals and the good core recovery are considered to preclude any issue of sample bias due to material loss or gain.
Logging	Core was logged for geology, alteration, mineralisation and geotechnical aspects to a level suitable for resource estimation (although no Mineral Resource is defined or forecast for the Wolf Property) and preliminary metallurgical and mining studies. Core logging was both qualitative and quantitative in nature. RQD and recovery data for each hole was also recorded. No photographic record of the core exists. The drill core was inspected in the field by BMC personnel on 9 September 2016. Most of the core is intact, minor core has been lost due to consumption of the core boxes by vermin. However, adequate core remains to facilitate a resampling programme to verify results (see below). All drill holes were logged in full.
Subsampling techniques and sample preparation	In 1997, core was split using a manual splitter. In 1998, well mineralised samples were cut with a rock saw, and lesser mineralised intervals were split as per the 1997 programme. Only core drilling has been employed at Wolf. This methodology is considered appropriate for this style of mineralisation. Core recovery was also recorded as part of the logging process.

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Criteria	Commentary
	These procedures were considered appropriate "industry standard" techniques at the time. No documented quality assurance procedures have been located. No field duplicate samples were taken during the previous drilling campaigns. In 2016, a resampling programme collected 45 samples of remaining half-core over intervals identical to the original sample intervals. Results show strong correlation between original and duplicate data for elements of interest. Sample sizes are considered appropriate for the rock type, style of mineralisation (massive sulfides), the thickness and consistency of the intersections, the sampling methodology and percent value assay ranges for the primary elements at Wolf.
Quality of assay data and laboratory tests	Core from the 1997 programme was dispatched to Pioneer Laboratories Inc. for analysis, and from the 1998 programme to Acme Analytical Laboratories, both located in British Columbia. Samples were crushed and pulverised, although record of the subsample size which was pulverised no longer exists. 1997 drilling: 1 g of sample digested with 50 mL of aqua regia, diluted to 100 mL with water and finished by AA to provide copper, lead, zinc analyses to 0.01 wt% detection limit and silver to 0.1 ppm detection limit. 10 g of sample digested with aqua regia, MIBK extracted, finished with graphite furnace AA to provide gold analyses to 1 ppb detection limit. 1998 drilling: All samples were analysed using 0.5 g sample digesting in 3 mL of equal parts HCl, HNO_3-H_2O Select higher-grade intervals were initial digestion of 1 g and then later 0.25 g of sample with 30 mL of aqua regia, diluted to 100 mL with water and finished by ICP to provide lead, zinc analyses to 0.01 wt% detection limit and silver to 0.01 oz/t detection limit. The analytical techniques used are appropriate given the style of mineralisation and mineralogy and is considered to approximate a total extraction technique. No geophysical tools were used to measure drill holes or core. No certified standards or blanks were inserted with the samples; hence laboratory bias could not be assessed. Internal analytical standards and occasional pulp and residue repeats were included by the laboratories for each sample run, with results returning an acceptable level of reproducibility.
Verification of sampling and assaying	The historical drill core was viewed by BMC in 2016. Massive sulfide mineralisation was visually consistent with the original logging and assays. Significant intercepts appear to correlate with the intensity of mineralisation logged in the field. In 2016, a resampling programme collected 45 samples of remaining half-core over intervals identical to the original sample intervals. Results show strong correlation between original and duplicate data for elements of interest. Twin holes have not been completed. Drill data was logged by hand on site using customised logging forms based on a GEOLOG software format. The hand entered logs were then entered into GEOLOG software. BMC has reviewed the hand entered logs and exports from the GEOLOG software and view the consistency between logged and electronic data to be good. BMC assembled a digital drill database from GEOLOG data exports. All collar and down-hole surveys were validated against original survey files. Pre-1998 assays were compiled from digital certificates received from Atna and 1998 assays were compiled from digital certificates received directly from Acme (now Bureau Veritas) laboratory. As a final check assay values in the electronic database were validated by selecting random samples and comparing the values to a scanned copy of the original hard copy certificates. Assay data was not adjusted or factored.
Location of data points	Collars for all 1997 holes and 1998 holes to WF98-32 were surveyed by qualified surveyor to 0.1 m resolution. Remaining collars were laid out using chain and triangulation from established survey points to ≈5 m lateral resolution. Down-hole positions were measured by compass and clinometer at the collar and at (typically) one or (occasionally) more "pajari" single-shot magnetic surveys down-hole for dip and azimuth. The grid system for the Wolf Property is UTM zone 9 NAD83, with holes originally drilled on a local grid. Local topographic data and adjacent surveyed collars were used to provide RL to what appears ≈1 m accuracy.

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Criteria	Commentary
	Verification of some historical drill collar locations by a licenced surveyor as well as more detailed topographic surveys are required for further evaluation of the project.
Data spacing and distribution	Drill holes are spaced ≈60 m apart on sections spaced ≈60 m to ≈80 m apart. The current drill spacing is sufficient to establish the degree of geological and grade continuity for an Inferred Mineral Resource (although no Mineral Resource is defined or forecast for the Wolf Property). Sample compositing was not applied.
Orientation of data in relation to geological structure	Drill orientation is close to orthogonal to the tabular mineralised horizons to the extent which is known. To date, mineralisation orientation has been favourable and sample widths are not considered to have added a sampling bias.
Sample security	No information is available for historical drilling sample security.
Audits or reviews	Internal audits were completed by CSA Global which verified the technical inputs, methodology, parameters, and results of the estimation of the Exploration Target ranges.

Section 2: Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section)

Criteria	Commentary
Mineral tenement and land tenure status	The Wolf Property comprises 18 Mineral Claims (Wolf 1–18) covering 372 ha which is owned 100% by BMC Minerals Ltd. No residual royalties or joint ventures remain on the property. A staking moratorium exists over the area, but this does not prevent operations within the project tenure. There exists no impediment to obtaining a licence to operate in the area under the existing statutory requirements. A Class 1 Notification Q2025_0160 (exploration permit) was granted on 17 July 2025 and is valid for 1 year.
Exploration done by other parties	Newmont identified gossans and base metal mineralisation in the area in 1955, and in 1966 staked the area. Hesca Resources Ltd staked claims in 1974 and drilled two x-ray holes without success. Newmont and Asamera Oil conducted geochemical, electromagnetic and magnetometer surveys, mapping and trenching in 1976. In 1978, Newmont undertook trenching, drilling of three BQ diamond holes for 528 m, intersecting 1.4 m at 5.6% Zn and 27 g/t Ag. In 1982, Amax staked the area and undertook prospecting, geological mapping and geochemical sampling, delineating anomalous lead and silver in soils. In 1990, YGC Ltd staked the area and over the next 2 years optioned the property to Cominco who undertook rock and soil geochemistry surveys, mapping, UTEM™ and ground magnetic surveys which identified coincident soil and geophysical targets. Atna optioned the property from YGC in 1995, and undertook prospecting, mapping and surface sampling which identified high-grade galena-barite samples at Mount Vermilion. The following field season Atna completed four trenches which returned assays to 3.2% Pb and 111 g/t Ag over 5.3 m which was followed up by diamond drilling. Two holes intersected sub-economic mineralisation. A jointly funded heliborne EM survey, magnetic and VLF-EM survey was flown in 1997. The 1997 diamond drilling programme, comprising 12 holes for 2,769 m, was completed by Atna, intersecting 25.2 m (true) of massive sulfide at 6.9% Zn, 2.8% Pb, 139 g/t Ag. In 1998, Atna completed 30 diamond holes targeting the Wolf Deposit and discovering the east Slope Zone. 31 holes defined the Wolf Deposit, and six holes intersected the East Slope Zone. A horizontal loop coplanar EM survey was also completed in 1998. A conceptual mining study undertaken in 2000 indicated that the deposit was amenable to underground and open pit mining but was not economic at that time. No additional work has since been undertaken, and no forecast is made of whether the Wolf Property may become feasible in future.
Geology	The Wolf Prospect is a polymetallic (zinc + lead + silver) volcanogenic massive sulfide deposit. The deposit is bedded and consists of several parallel massive sulfide horizons that are moderately dipping (45° to the southwest), conformable to stratigraphy and are fairly continuous. The mineralised stratigraphic horizon can be traced for several hundred metres, however the strike length of the main body of mineralisation is approximately 300 m. The total down dip extent of the zone is approximately 400 m. A steeply northeast dipping reverse fault has offset mineralisation. The Upper zone extends from 1,330 m RL to 1,560 m RL and from section 5,130 m N to 5,400 m N. The Lower zone extends from 1,160 m RL to 1,350 m RL and from

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Criteria	Commentary
	section 5,160 m N to 5,370 m N. The deposit and host stratigraphy may be overturned.
Drill hole information	A tabulation of the required information for all Material drill holes is provided in the report as Appendix F. No drill hole information has been excluded.
Data aggregation methods	Significant intersections illustrated on cross-sections in the report and in Appendix E were calculated using the following method: Length-weighted average with maximum 3 m internal waste (true thickness) When assay value is below detection limit, half the detection limit is used Assay values composited if Cu >1% or Pb >2% or Zn >2% Azimuth is magnetic and rounded to the nearest degree. True widths have been stated for all significant intersections reported in Appendix F Metal equivalent values have not been reported.
Relationship between mineralisation widths and intersection lengths	Majority of the drilling is close to orthogonal to the mineralisation and is therefore considered representative.
Diagrams	Refer to figures in body of report.
Balanced reporting	The Competent Person has reported the exploration results in a balanced way as an Exploration Target by applying advanced estimation techniques using Surpac software involving validation and statistical analysis of the drill data, 3D block modelling, wireframe interpretation, sample compositing, geostatistical analysis, grade interpolation using inverse distance squared (ID^2) techniques, oriented "ellipsoid" search was used to select data in three search passes, application of density using measurements on drill core, applying a cut-off of 2% Zn, and applying ranges of tonnes and grade based on an exploration prospectivity basis.
Other substantive exploration data	Ground EM identifies the Wolf Prospect, and additional EM responses exist on the Mineral Claims. Metallurgical or geotechnical studies have not as yet been undertaken. Bulk density measurements were undertaken on core samples at the laboratory using an air pycnometer method. In 2016, BMC Minerals conducted a VTEM™ and magnetic survey over the Wolf Property, which has identified targets for further exploration.
Further work	Initial work will comprise data compilation, geological interpretation, and block modelling. As the Wolf Prospect remains open down dip and along strike, it is expected that additional drilling will be undertaken to identify whether a base and precious metal Mineral Resource can be defined. The East Slope Prospect will also be the focus of further diamond drilling, as will the other untested EM targets. All relevant diagrams and inferences have been illustrated in this report.

APPENDIX D: JORC CODE TABLE 1 – PELLY PROPERTY

Covering the Jackman Exploration Target and Exploration Results.

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Section 1: Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections)

Criteria	Commentary
Sampling techniques	The Jackman Prospect has been sampled using diamond drill holes in 4 holes drilled at variable spacings. Historical drilling at the Project was completed by Expatriate (three holes for 1,665 m) and Westmin (1 hole for 513.4 m) for a total of 2178.5 m. Holes were angled between -60° to -90° towards grid north. Diamond core was used to obtain high-quality samples that were logged for lithological, structural, density and other attributes. Historical quality assurance procedures and quality control procedures were not documented. Drill holes were logged and intervals selected for assay based on geology. Core was cut with a core saw with half core sampled and sent to the laboratory and the remaining half core kept on site. Sample intervals ranged between 0.3 m and 6.4 m with a median sample length of ≈1.5 m. Samples were sent to ALS Chemex in Vancouver for preparation and analysis.
Drilling techniques	Diamond with predominantly HQ and some NQ core size. Core was not oriented.
Drill sample recovery	Core recovery was logged by the geologist and varied from excellent in the banded iron formations and semi-massive to massive sulfide mineralisation to poor in some sections of the hangingwall argillite. There is no record available for methods applied to maximise sample recovery. The massive sulfide style of the mineralisation, consistency of the mineralised intervals and the good core recovery are considered to preclude any issue of sample bias due to material loss or gain.
Logging	Core was logged for geology, alteration, mineralisation and fracture intensity to a level suitable for resource estimation (although no Mineral Resource is defined). Core logging was both qualitative and quantitative in nature. Recovery data for each hole was also recorded. No photographic record of the core exists. All drill holes were logged in full. Historical holes drilled by Expatriate were relogged by BMC to further exploration and ensure consistent geological interpretation for resource definition work
Subsampling techniques and sample preparation	Core was cut with a rock saw. This methodology is considered appropriate for this style of mineralisation. Core recovery was also recorded as part of the logging process. These procedures were considered appropriate “industry standard” techniques at the time. No documented quality assurance procedures have been located. No field duplicate samples were taken during the previous drilling campaigns. Sample sizes are considered appropriate for the rock type, style of mineralisation (massive sulfides), the thickness and consistency of the intersections, the sampling methodology and percent value assay ranges.
Quality of assay data and laboratory tests	Analytical methods used by Westmin and Expatriate were the same with samples sent to ALS Chemex in Vancouver for analysis. Samples were crushed to 150 µm and split to a maximum sample size of 3kg. Gold and silver were analysed by a 30 g fire assay with a gravimetric finish. Lower detection limits were 0.07 ppm for gold and 3 ppm for silver, which is appropriate for the range of Au and Ag grades encountered in the mineralisation. Base metals were analysed by AAS after a hydrochloric, nitric, and hydrofluoric acid digest Lower detection limits were 0.01% Cu, Pb and Zn. Quality control was not reported.

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Criteria	Commentary
Verification of sampling and assaying	The historical drill core has been viewed by BMC, but no samples have been reassayed.
Location of data points	Drill collar locations including elevation were picked up by registered survey contractors Underhill Geomatics Ltd from Whitehorse, but the accuracy of the surveys was not provided. In 2005 a second survey company re-surveyed the holes at Wolverine, and no discrepancies were identified. It is not known whether the Pelly holes were included as part of the re-survey programme. Down-hole surveys were measured by a single shot camera. The grid system is UTM zone 9 NAD27 and Wolverine mine grid. Data is reported here in UTM zone 9 NAD83.
Data spacing and distribution	Only four holes have been drilled at the Jackman Exploration Target. There is no consistent drill spacing between the holes. The current drill spacing is not sufficient to establish the degree of geological and grade continuity for an Inferred Mineral Resource. Sample compositing was not applied.
Orientation of data in relation to geological structure	Drill orientation is close to orthogonal to the tabular mineralised horizons to the extent which is known. To date, mineralisation orientation has been favourable and sample widths are not considered to have added a sampling bias.
Sample security	One half of the drill core was placed inside a 6-mil poly sample bag along with the corresponding sample tag from ALS Chemex; which possesses a bar-code. The other half of the drill core is then placed back into the core box for permanent record. The sample bag is then sealed using a zap-strap to prevent tampering and placed sequentially on the layout table in the saw room. Samples are then sequentially placed into pre-labelled rice sacks, which are then sealed by metal tie-straps. Each drill hole was shipped to the laboratory individually with the rice bags colour-coded per individual drill hole. Bag numbers and sample locations within each bag are also tracked. All rice sacks containing assay samples were transported by a charter company from the Wolverine Deposit to Whitehorse, and then to ALS Chemex in North Vancouver, British Columbia.
Audits or reviews	No audits have been completed on the Exploration Target

Section 2: Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section)

Criteria	Commentary
Mineral tenement and land tenure status	The Pelly Property consists of 422 mineral claims that cover 70.6 k m^2 which are owned 100% by BMC. No residual royalties or joint ventures remain on the property. A staking moratorium exists over the area, but this does not prevent operations within the project tenure. There exists no impediment to obtaining a licence to operate in the area under the existing statutory requirements. The Pelly Property comprises three separate claim groups: JACK – located northeast of Wolverine, GO – located southwest of Wolverine, and WOL – located northwest along Wolverine Lake. The JACK and GO claim groups flank the northeast and southwest sides of claims covering the Wolverine Deposit and mine.
Exploration done by other parties	Exploration activities across the general area from 1973 to 1993 included programmes of soil sampling, geological mapping, trenching and diamond drilling. After discovery of the ABM Deposit in 1994, 3,255 line-km of a regional DIGHEM survey covered most of the Pelly Property, returning a series of anomalous electromagnetic responses in the vicinity of the Fetish (Wolverine) surface expression. In 1994 field activity included geological mapping, collection 279 soil samples at 100 m spacing along topographic contours. The latter returned several zones of anomalous lead, zinc, silver, and barium, with the most promising of these responses associated with elevated copper and gold values occurring downslope of favourable stratigraphy. Westmin Resources Ltd (Westmin) discovered the adjacent Wolverine Deposit in 1995, where initial drilling returned up to 8.3 m of Zn-Cu-Pb-Ag-Au-rich massive sulfide mineralisation. In 1994, Cominco staked the WOL claims to cover geophysical targets. From 1995 to 1998, field programmes across the Pelly Property included geological mapping, surface geochemical sampling (16 rock, 2,183 soil and 34 silt samples) that defined several zones of anomalous base metals, and geophysical surveys including 56.8 line-km of HLEM, 53.5 line-km of ground magnetic and 1.5 line-km of gravity surveys. The 1995 HLEM survey identified a good conductor and strong magnetic feature at the northwest

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Criteria	Commentary
	corner of the JACK claim group where the Wolverine mineralised horizon is projected to cross the Pelly Property northwest of the Wolverine Deposit. Elsewhere, the 1996 HLEM surveys returned numerous EM conductors, flanked by strong magnetic features, which were interpreted as reflecting graphitic sedimentary rocks. From 1996 to 2004 a total of 23 drill holes were completed within the Pelly Property for a total of 11,618m. The most significant of these, completed by Expatriate Resource Ltd (Expatriate) in 2000 for 1,664.2 m, were 3 holes drilled on the WOL219 claim, which now forms part of the JACK claim group, to the immediate north of the Wolverine Deposit. Hole WW00-001 intersected 7.4 m of massive sulfide at 0.7% Cu, 1.2% Pb, 13.6% Zn, 152 g/t Ag, 0.6 g/t Au, hole WW00-03 intersected 2.5 m of massive and semi-massive sulfide at 8.33% Zn, 1.32% Pb, 1.55% Cu, 293 g/t Ag and 1.17 g/t Au, which is interpreted as the down-dip extension of the Wolverine Deposit. Drillhole WW-00-02 intersected weak mineralisation. The drilling indicates that sulfide mineralisation extends at least 200 m down-dip from BMC's mineral claim boundary. Additionally, a 1996 drill hole, collared outside of BMC's mineral tenure, intersected 4.2m of massive sulfide mineralisation at 0.8% Cu, 3.9% Pb, 15.6% Zn, 2.0 g/t Au and 558 g/t Ag, approximately 20 m inside the Pelly Property. The remainder of the holes drilled were mainly drilled in the vicinity of the Fisher Prospect, with a drill hole WV95-06 intersecting 2.4 m at 2.8% Zn, 1.4% Pb, 0.12% Cu and 66 g/t Ag in sulfides below iron exhalative units interpreted to be the equivalent of the Wolverine host stratigraphy.
Geology	The Jackman Exploration Target is the interpreted down-dip extension of the Wolverine VHMS deposit. The Wolverine Deposit is a VHMS type deposit with host rocks comprising deformed meta-volcanic, meta-volcaniclastic and metasedimentary rocks of the Wolverine Lake group. The deposit extends approximately 800 m along strike, at least 475 metres down-dip, and is 1-10 metres in true thickness. Sulfide mineralisation is present as a reasonably continuous stratiform sheet that appears to trend parallel to the host rock stratigraphy and is interpreted to extend beyond the limit of Yukon Zinc mineral tenure into mineral tenure that comprises BMC's Pelly Property. The thickest sulfide accumulations occur in the Wolverine and Lynx zones, each of which comprise a series of stacked lenses totalling 5-15 m of massive sulfide separated by layers of argillite up to 8 m thick. Both zones are tabular, approximately 250 m long and separated from each other by 200 m of less mineralised rocks that comprise the Saddle zone.
Drill hole information	A tabulation of the required information for all Material drill holes is provided in the report as Appendix E. No drill hole information has been excluded.
Data aggregation methods	Significant intersections illustrated on cross-sections in the report and in Appendix E were calculated using the following method: Length-weighted average with maximum 3 m internal waste (true thickness) When assay value is below detection limit, half the detection limit is used Assay values composited if Cu >1% or Pb >2% or Zn >2% Azimuth is magnetic and rounded to the nearest degree. Downhole widths have been stated for all significant intersections reported in Appendix E. True width is interpreted to be approximately 80% to 95% of the down-hole width. Metal equivalent values have not been reported.
Relationship between mineralisation widths and intersection lengths	Majority of the drilling is close to orthogonal to the mineralisation and is therefore considered representative.
Diagrams	Refer to figures in body of report.
Balanced reporting	The Competent Person has reported the exploration results in a balanced way as an Exploration Target by applying advanced estimation techniques using Surpac software involving validation and statistical analysis of the drill data, 3D block modelling, wireframe interpretation, sample compositing, geostatistical analysis, grade interpolation using inverse distance squared (ID2) techniques, oriented "ellipsoid" search was used to select data in three search passes, application of density using measurements on drill core, applying a cut-off of 2% Zn, and applying ranges of tonnes and grade based on an exploration prospectivity basis.
Other substantive exploration data	Metallurgical or geotechnical studies have not as yet been undertaken, however metallurgical test results for the adjacent Wolverine Deposit are available in the public

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Criteria	Commentary
	domain. Bulk density measurements were undertaken on core samples at the laboratory using an air pycnometer method. Hyperspectral measurements were collected from selected field samples at Pelly (473 measurements from 129 surface rock samples) and at every 1 m interval in the Cominco drill hole WO96-2 (344 measurements). Field samples required cutting, then samples were washed, marked with grease pencil, described, and photographed prior to measurement with a field portable TerraSpec® VIS-NIR Spectrometer ("TerraSpec"). The system uses visible and near infrared (VNIR; 350–1,000 nm) and short-wave infrared (SWIR; 1,000–2,500 nm) wavelengths to determine mineral speciation based on bond reflectance Air photography was undertaken by BMC using a Piper Navajo and a large format camera to cover the Pelly Property at 20 cm resolution. BMC has conducted geological mapping on the KZK and Pelly Properties, with helicopter support where required. Traverses were completed, covering a total area of ≈70 k m2 at Pelly and most of the KZK Property. Bedrock exposure within the mapped area is present mainly along ridges and ravines, moderate on the steep slopes, but typically poor along shallower slopes and in valley bottoms. Individual outcrops were mapped and described. Mapping was conducted on ruggedised, GPS-enabled Panasonic Toughbook computers using QGIS software. Geological fact maps were compiled. Numerous geophysical surveys have been carried out over the Pelly Property which have been undertaken by specialist geophysical contracting firms using high-quality instrumentation and data processing systems. In 2014 an airborne VTEM™ and magnetic survey was flown over the property. Results of the survey indicate additional EM, and magnetic high anomalies underlie the property.
Further work	Additional diamond drilling and down-hole EM are planned once the required Exploration Land Use Permit has been approved.

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APPENDIX E: SIGNIFICANT INTERSECTIONS

Significant intersections are defined as samples returning assay results greater than 1% Cu, or 2% Pb, or 2% Zn.

All mineral exploration drill holes drilled within the respective properties are presented in the following tables, both drill holes with significant intercepts and drill holes with barren or weakly anomalous analytical results below the thresholds.

Drill holes which contributed to Mineral Resources are not listed in these table; their significance has been measured and reported in the MREs for the ABM and Kona Deposits.

Intersection calculation method:

- Length-weighted average with maximum 3 m internal waste (true thickness)
- When assay value is below detection limit, half the detection limit is used
- Assay values composited if Cu >1% or Pb >2% or Zn >2%

Azimuth is magnetic and rounded to the nearest degree

NSI = No significant Interval.

True Widths

Reported intersections:

- For Kuril & Fuego reported intersections are downhole widths (true width not known).
- For Pelly, Krakatoa, Rhyolite Peak & GP4F downhole intersections approximate true widths.

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KZK Property – Exploration Drill holes

Prospect	Hole ID	Easting	Northing	Elevation	Total depth (m)	Dip	Az	Depth from (m)	Depth to (m)	Interval (m)	Cu (%)	Pb (%)	Zn (%)	Ag (g/t)	Au (g/t)	Comment
ABM	K18-482	414354	6815675	1515	401.0	-60	180									NSI
ABM Northwest	K18-482	414354	6815675	1515	401.0	-60	180									NSI
Class A Facility	K18-470	414217	6817993	1464	24.0	-90	360									NSI
Class A Facility	K18-471	414005	6818143	1477	27.0	-90	360									NSI
Class A Facility	K18-472	414120	6818196	1458	31.0	-90	360									NSI
Fuego	K94-051	414747	6814656	1422	136.6	-60	181									NSI
Fuego	K97-181	414748	6814605	1430	130.1	-60	180	12.9	19.3	6.4	5.2	1	5.6	142	2.4	Stringer/Massive
Fuego	K97-181	incl.						17.7	19.3	1.6	10.4	0.5	3.2	201	6.0	Massive
Fuego	K97-182	414747	6814399	1451	135.9	-60	180	15.6	18.0	2.4	0.6			19		Disseminated
Fuego	K97-182	and						38.9	47.5	8.4	0.3		0.5	8		Disseminated
Fuego	K97-182	and						65.2	70.4	5.2	0.4		0.2	7		Disseminated
Fuego	K97-183	414746	6814558	1432	84.1	-90	180	6.1	8.2	2.1	3.4	0.9	11.5	99	0.7	Massive
Fuego	K97-183A	414750	6814560	1434	10.0	-30	180									NSI
Fuego	K97-184	414708	6814585	1436	29.6	-90	180									NSI
Fuego	K97-185	414800	6814630	1423	55.2	-90	180									NSI
Fuego	K97-186	414843	6814825	1408	49.1	-60	180									NSI
Fuego	K97-187	414850	6814661	1415	65.8	-90	180									NSI
Fuego	K15-329	414801	6814638	1422	200.0	-55	180									NSI
Fuego	K15-332	414797	6814638	1422	182.0	-83	180									NSI
Fuego	K24-501	414750	6814315	1460	239.0	-62	3	32.0	34.4	2.4	0.8	0.1	0.3	18	0.1	Stringer
	and							79.0	82.0	3.0	0.3	0.1	0.1	8	0.1	Stringer
Fuego	K24-502	414753	6814433	1445	201.0	-65	183	60.0	62.8	2.8	0.3	<0.1	0.2	10	0.1	Stringer
Fuego	K24-503	414679	6814510	1447	251.0	-51	183									NSI
Fuego	K24-505	414896	6814482	1414	270.0	-66	180									NSI
Fuego	K24-527	414816	6814803	1406	321.0	-55	137	37.5	53.5	16.0	3.5	0.5	3.2	88	0.8	Massive
	and							56.0	57.0	1.0	2.9	0.3	2.2	72	0.5	Semi-massive
Fuego	K24-528	415114	6814358	1444	294.0	-72	360									NSI
Fuego	K24-529	414816	6814803	1412	141.0	-75	138									NSI
Fuego	K24-546	414641	6814695	1452	303.0	-54	134									NSI

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Prospect	Hole ID	Easting	Northing	Elevation	Total depth (m)	Dip	Az	Depth from (m)	Depth to (m)	Interval (m)	Cu (%)	Pb (%)	Zn (%)	Ag (g/t)	Au (g/t)	Comment
Fuego	K24-551	414816	6814803	1412	285.0	-60	183	33.7	37.6	3.9	3.5	0.1	0.3	74	0.8	Massive
	and							106.0	108.6	2.6	0.3	1.8	6.4	63	0.3	Massive
Fuego	K24-553	414410	6814619	1496	525.0	-53	128									NSI
Fuego	K24-554	415045	6814605	1399	237.0	-65	182									NSI
Fuego	K24-555	414876	6814809	1407	99.0	-60	135	57.4	61.2	3.8	<0.1	3.9	6.4	168	0.6	Massive
	and							78.2	80.6	2.4	0.4	0.8	9.9	67	0.1	Massive
Fuego	K24-556	414876	6814809	1407	114.0	-55	180	24.5	26.8	2.3	0.2	1.4	8.2	125	1.8	Massive
Fuego?	K18-485	413249	6813442	1770	201.0	-70	151									NSI
Fuego?	K18-480	413374	6813450	1732	215.4	-69.5	147.7	20.3	33.0	12.6	0.1	0.8	2.0	24	0.05	Semi-massive
Fuego?	K18-485	413249	6813442	1770	201.0	-70	151.1									NSI
Fuego/Krakatoa	K16-368	425219	6815016	1418	145	-65	233	100.7	105.4	4.7	1.0	2.5	6.2	87	0.9	Semi-massive
GP4F	K95-167	419466	6813328	1342	108.2	-70	180									NSI
GP4F	K98-188	419466	6813229	1340	182.0	-62	180	71.6	80.5	8.9	0.2	4.0	7.8	117	1.8	semi-massive
GP4F	K98-189	419465	6813228	1340	124.7	-90	0	76.9	92.7	15.8	0.1	2.4	3.1	76	0.9	semi-massive
							incl.	83.6	92.7	9.1	0.2	4.0	5.2	128	1.5	semi-massive
GP4F	K98-190	419566	6813209	1326	109.1	-53	180	77.0	82.9	5.9	0.1	3.4	4.8	105	19.7	disseminated
							incl.	79.2	80.6	1.4	0.1	1.4	0.7	111	77.4	disseminated
GP4F	K98-191	419566	6813208	1326	112.5	-90	0	89.5	91.8	2.3	<0.1	1.1	2.4	17	0.2	disseminated
							and	94.3	95.0	0.7	0.1	9.2	14.8	247	0.8	semi-massive
GP4F	K98-192	419357	6813228	1357	93.6	-74	180	63.5	65.3	1.8	0.2	0.5	3.8	14	0.2	disseminated
GP4F	K98-193	419461	6813401	1358	199.9	-59	175	173.2	179.5	6.3	0.1	3.6	9.1	94	0.8	semi-massive
GP4F	K98-196	419457	6813517	1363	316.1	-61	180	233.5	241.6	8.1	0.2	1.1	5.6	51	0.4	semi-massive
							and	262.5	286.2	23.7	0.1	0.6	2.3	10	0.1	disseminated
GP4F	K98-197	419357	6813370	1373	172.8	-62	180	133.7	136.7	3.0	0.1	0.8	3.5	10	<0.1	disseminated
GP4F	K98-198	419356	6813495	1382	249.0	-64	180	204.5	206.4	1.9	0.1	1.3	4.1	14	0.1	disseminated
GP4F	K15-247	418953	6813685	1477	414.0	-85	180									NSI
GP4F	K15-261	419651	6813231	1311	302.0	-60	180	177.2	183.4	6.2	0.1	1.1	3.7	8	0.0	Disseminated
GP4F	K15-261	and						214.5	215.0	0.5	0.3	2.6	3.9	117	0.0	Massive
GP4F	K15-268	418753	6814107	1493	355.0	-70	180									NSI
GP4F	K15-280	419662	6813562	1325	408.0	-70	180	277.8	279.3	1.5	0.0	0.5	3.1	6	0.0	Disseminated
GP4F	K15-280	and						283.0	283.8	0.8	0.0	2.4	2.5	24	0.0	Disseminated
GP4F	K15-280	and						364.3	365.8	1.5	0.3	3.5	6.8	492	0.8	Semi-massive

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Prospect	Hole ID	Easting	Northing	Elevation	Total depth (m)	Dip	Az	Depth from (m)	Depth to (m)	Interval (m)	Cu (%)	Pb (%)	Zn (%)	Ag (g/t)	Au (g/t)	Comment
GP4F	K15-285	419650	6813355	1138	306.0	-70	179	225.5	233.1	7.6	0.0	0.7	1.6	28	0.2	Disseminated
GP4F	K15-285	and						235.0	236.0	1.0	0.2	0.6	3.3	12	0.0	Disseminated
GP4F	K15-285	and						241.2	242.3	1.1	0.1	0.3	2.1	7	0.0	Disseminated
GP4F	K15-294	419406	6813500	1377	306.0	-85	180	227.8	237.0	9.2	0.1	0.5	2.4	8	0.0	Disseminated
GP4F	K15-302	419500	6813355	1340	210.0	-60	180	137.9	139.4	1.5	0.2	0.4	2.0	11	0.0	Disseminated
GP4F	K15-302	and						145.6	155.1	9.5	0.1	2.0	2.9	34	0.3	Disseminated
GP4F	K15-306	419500	6813555	1340	246.0	-85	180	159.9	168.6	8.7	0.1	1.7	4.7	70	0.6	Massive
GP4F	K15-306	and						170.5	171.0	0.5	0.4	4.7	7.3	417	0.4	Massive
GP4F	K15-306	and						205.0	225.3	20.3	0.1	0.5	3.5	11	0.0	Disseminated
GP4F	K16-380	419400	6813386	1366	323.7	-80.1	180.3	153.3	159.7	6.4	0.1	0.8	2.6	8	0.1	Stringer
GP4F	K16-388	419401	6813385	1366	236.8	-55.2	169.7	159.5	166.9	7.4	0.2	3.2	5.4	107	1.2	Stringer
GP4F	K16-388	and						220.7	226.3	5.6	0.1	1.3	3.3	27	0.0	Stringer
GP4F	K16-393	419505	6813219	1334	156.0	-44.8	180.3	77.1	80.1	3.0	0.2	6.9	11.5	200	4.4	Disseminated
GP4F	K16-396	419505	6813219	1334	210.0	-88	180.3	83.7	86.5	2.8	0.2	2.3	3.0	49	0.7	Stringer
GP4F	K16-396	and						86.5	90.5	4.0	0.4	5.1	8.1	138	2.2	Massive
GP4F	K16-396	and						160.6	164.8	4.2	0.1	0.2	3.1	6	0.0	Stringer
GP4F	K16-400	419401	6813207	1349	98.5	-60	179.9	46.1	50.4	4.3	0.2	0.5	5.4	14	0.0	Stringer
GP4F	K16-400	and						52.2	57.9	5.7	0.1	1.2	2.3	22	0.3	Stringer
GP4F	K16-403	419513	6813450	1353	343.7	-81	169.3	217.8	222.8	5.0	0.1	1.7	3.0	101	1.9	Semi-massive
GP4F	K16-403	and						233.5	238.0	4.5	0.1	1.00	2.4	203	1.0	Disseminated
GP4F	K16-407	419400	6813390	1366	185.0	-54.5	170.4									NSI
Kermadec	K18-467	413413	6820445	1332	590.0	-61	161									NSI
Kermadec	K18-468	413670	6820318	1341	56.0	-70	177									NSI
Kermadec	K18-469	413672	6820318	1341	692.0	-70	172									NSI
Krakatoa	K16-384	415661	6815386	1563	400.0	-65	224.9									NSI
Krakatoa	K16-391	415655	6815385	1568	101.0	-64.9	224.8									NSI
Krakatoa	K16-394	415655	6815385	1568	231.6	-65	233	797.4	797.9	0.5	0.50	0.2	9.3	8	0.0	Massive
Krakatoa	K16-408	415424	6815263	1548	491.0	-67	228									NSI
Krakatoa	K16-416	415440	6815276	1550	854.5	-68	183									NSI
Kuril	K15-327	414639	6815178	1,442	221	-60	195	65.3	67.9	2.6	0.6	1.5	3.3	30	0.04	Semi-massive
Kuril	K15-328	414678	6815205	1429	236.0	-60	195									NSI
Kuril	K18-481	414060	6814770	1642	300.0	-51	169									NSI

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Prospect	Hole ID	Easting	Northing	Elevation	Total depth (m)	Dip	Az	Depth from (m)	Depth to (m)	Interval (m)	Cu (%)	Pb (%)	Zn (%)	Ag (g/t)	Au (g/t)	Comment
Kuril	K18-486	414184	6814844	1560	251	-51	169									NSI
Kuril	K18-487	414511	6815092	1485	359.0	-50	168.8	47.0	52.0	5.0	0.4	0.0	0.2	8	0.02	Disseminated
Kuril	K18-488	414509	6815092	1485	225.0	-89	252.2	68.9	71.2	2.3	1.1	0.2	1.3	35	0.03	Disseminated
Kuril	K24-531	414244	6814638	1544	360.5	-60	333									NSI
Kuril	K24-533	414258	6814952	1538	411.0	-70	153	45.8	47.3	1.5	0.8	0.1	1.2	24	0.1	Stringer
	and							79.2	80.2	1.0	1.4	0.0	0.3	26	0.0	Stringer
Kuril	K24-534	414259	6814951	1530	261.0	-85	153									NSI
Kuril	K24-541	413967	6814748	1671	522.0	-75	153									NSI
Rhyolite Peak	K16-415	413575	6815210	1712	854.5	-60	195	46.5	47.0	0.5	0.8	0.3	9.0	26	0.1	Massive
							and	81.9	84.1	2.2	0.3	0.1	3.2	29	0.0	Semi-massive
							and	142.7	143.1	0.4	0.3	1.0	4.8	51	0.1	Semi-massive
Rhyolite Peak	K18-483	413609	6815315	1715	297.0	-60	195.8									NSI
Rhyolite Peak	K18-484	413310	6814850	1737	135.0	-61	196	7.5	11.3	3.8	0.4	1.3	5.1	128	0.8	Massive
Rhyolite Peak	K24-544	413319	6814890	1720	78.0	-50	198	20.1	24.6	4.5	0.3	2.5	8.7	291	1.7	Massive
Rhyolite Peak	K24-545	413294	6814886	1734	111.0	-50	198	18.3	20.7	2.4	0.5	2.4	6.7	595	3.2	Semi-massive
Rhyolite Peak	K24-547	413334	6814951	1726	81.0	-80	183	43.4	47.1	3.7	0.3	2.3	6.1	226	1.1	Massive
Rhyolite Peak	K24-548	413375	6815149	1714	192.0	-60	183									NSI
Rhyolite Peak	K24-549	413421	6814982	1714	102.0	-60	183									NSI
Rhyolite Peak	K24-550	412758	6815002	1731	141.0	-60	183									NSI
TD	K95-162	414900	6818925	1340	75.3	-90	180									NSI
TD	K95-163	414900	6818675	1324	45.1	-90	180									NSI
TD	K95-164	414900	6818375	1335	90.5	-90	180									NSI
-	K95-170	417105	6815120	1619	442.0	-90	150									NSI
-	K97-179	416150	6814900	1685	505.4	-86	180									NSI
-	K98-194	420337	6814627	1314	95.7	-60	180									NSI
-	K98-195	420542	6814411	1348	98.1	-60	180									NSI
-	K16-372	415124	6814798	1388	597.0	-60	240									NSI
-	K16-374	415450	6814995	1513	801.0	-60	245									NSI
-	K16-413	415800	6815170	1595	147.0	-65	240									NSI
-	K16-414	415800	6815170	1595	339.0	-65	245									NSI

NSI = No significant interval. Excludes drill holes which are within the Mineral Resource for the ABM Deposit (which are covered by the MRE).

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Kona Property – Exploration Drill holes – Significant Drill hole Intersections

Hole ID	Easting	Northing	Elevation	Total depth (m)	Dip	Azimuth	Depth from (m)	Depth to (m)	Interval (m)	True width (m)	Cu (%)	Pb (%)	Zn (%)	Ag (g/t)	Au (g/t)	Comment
97-080	418520	6789433	1457	79.3	-60	72	-		-		-				-	NSI
97-083	418450	6789408	1448	82.3	-60	72	-		-		-				-	NSI
97-085	418457	6789522	1482	109.7	-85	72	-		-		-				-	NSI
97-086	418329	6789587	1498	103.6	-60	72	-		-		-				-	NSI
97-087	418313	6789690	1530	67.1	-50	72	-		-		-				-	NSI
97-107	419883	6788460	1811	805.3	-85	252	687.9	688.3	0.4	0.38	1.3				0.4	
97-108	419892	6788667	1800	694.9	-85	252	-		-		-				-	NSI
97-111	419762	6788735	1701	520.3	-82	252	421.5	422.2	0.7	0.67	2.0				0.3	
97-111		and					482.4	495.6	13.2	12.67	1.3				1.0	
97-112	418152	6788984	1438	189.0	-45	252	-		-		-				-	NSI
97-113	418064	6788536	1613	197.5	-45	252	-		-		-				-	NSI
97-114	420096	6788473	1770	831.2	-85	252	614.2	616.8	2.6	2.48	2.2				0.2	
97-114		and					716.7	717.8	1.1	1.05	2.1				0.2	
97-115	420095	6788472	1770	825.1	-80	252	703.6	705.6	2.0	1.92	1.8				1.3	
97-115		and					711.6	719.9	8.3	7.98	1.6				0.5	
97-115		and					792.5	794.5	2.0	1.92	1.2				0.3	

NSI = No significant interval. Excludes drill holes which are within the Mineral Resource for the Kona Deposit (which are covered by the MRE).

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Wolf Property – Significant Drill hole Intersections

Hole ID	Easting	Northing	Elevation	Total depth (m)	Dip	Azimuth	Depth from (m)	Depth to (m)	Interval (m)	True width (m)	Pb (%)	Zn (%)	Ag (g/t)	Comment
DDHJ78-01	366672	6802187	1559	181.7	-45	42	47.5	48.9	1.4	1.2	N/A	5.6	27	
DDHJ78-02	365890	6802765	1864	250.3	-46	22								NSI
DDHJ78-03	366823	6801696	1454	93.6	-50	42								NSI
DDHWF96-01	365570	6803423	1560	190.7	-90	0								NSI
DDHWF96-02	365570	6803423	1560	152.4	-60	100								NSI
DDHWF96-03	365570	6803423	1560	137.2	-65	280								NSI
DDHWF97-04	365592	6803055	1614	388.6	-60	18	320.0	323.0	3.0	2.8	0.0	2.6	7	
DDHWF97-05	365592	6803055	1614	392.6	-50	70								NSI
DDHWF97-06	367714	6801203	1639	54.9	-45	70								NSI
DDHWF97-07	366884	6801981	1527	300.8	-45	20	77.8	105.2	27.4	26.6	2.7	6.2	114	
DDHWF97-07	366884	6801981	1527	300.8	-45	20	113.4	115.9	2.5	2.4	0.9	3.0	28	
DDHWF97-07	366884	6801981	1527	300.8	-45	20	185.3	187.7	2.4	2.3	0.4	2.0	12	
DDHWF97-08	366884	6801981	1527	160.3	-80	20	119.6	135.2	15.6	15.1	1.1	5.1	56	
DDHWF97-09	367001	6801952	1531	354.2	-50	23	118.9	124.0	5.1	4.9	1.3	3.8	33	
DDHWF97-10	367001	6801952	1531	192.0	-80	23	132.7	135.0	2.3	1.9	0.8	2.1	39	
DDHWF97-11	367180	6801935	1580	149.7	-45	20								NSI
DDHWF97-12	366816	6802049	1556	137.2	-45	20	95.2	97.3	2.1	1.0	0.2	5.2	21	
DDHWF97-12	366816	6802049	1556	137.2	-45	20	124.1	125.7	1.6	1.0	0.0	2.8	3	
DDHWF97-13	366816	6802049	1556	191.1	-80	20	101.5	103.0	1.5	1.2	0.2	2.9	52	
DDHWF97-13	366816	6802049	1556	191.1	-80	20	106.6	108.1	1.5	1.2	0.1	2.6	13	
DDHWF97-13	366816	6802049	1556	191.1	-80	20	136.2	137.2	1.0	0.8	0.6	2.1	6	
DDHWF97-14	366798	6801861	1487	249.9	-45	20	182.0	186.0	4.0	3.9	1.8	7.8	63	
DDHWF97-15	366700	6802088	1546	198.1	-45	30	87.5	88.5	1.0	0.9	0.0	3.0	23	
DDHWF97-15	366700	6802088	1546	198.1	-45	30	91.5	95.9	4.4	4.1	0.1	3.8	12	
DDHWF98-16	366700	6802088	1546	176.8	-85	30	101.5	102.5	1.0	0.8	0.5	5.2	36	
DDHWF98-17	366798	6801860	1487	265.2	-69	20								NSI
DDHWF98-18	366828	6801930	1516	179.8	-49	24	148.7	158.5	9.8	9.4	0.6	6.1	84	
DDHWF98-19	366652	6802019	1544	201.2	-76	20	104.1	109.7	5.6	4.7	0.5	4.3	45	
DDHWF98-20	366754	6802003	1522	301.8	-45	24	127.0	130.6	3.6	3.4	0.3	3.5	72	
DDHWF98-21	366754	6802003	1522	176.8	-80	20								NSI
DDHWF98-22	367033	6802108	1554	62.8	-90	18								NSI
DDHWF98-23	367033	6802108	1554	225.6	-45	18								NSI
DDHWF98-24	366932	6801874	1512	298.7	-46	20	143.3	145.5	2.2	2.1	0.3	2.6	54	
DDHWF98-24	366932	6801874	1512	298.7	-46	20	152.2	158.5	6.3	6.1	0.5	3.4	77	
DDHWF98-25	366932	6801874	1512	292.7	-65	20	196.9	215.9	19.0	17.5	0.3	4.9	82	

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Hole ID	Easting	Northing	Elevation	Total depth (m)	Dip	Azimuth	Depth from (m)	Depth to (m)	Interval (m)	True width (m)	Pb (%)	Zn (%)	Ag (g/t)	Comment
DDHWF98-25	366932	6801874	1512	292.7	-65	20	232.0	233.4	1.4	1.3	0.4	2.4	4	
DDHWF98-26	366932	6801874	1512	323.1	-84	24	227.8	234.3	6.5	5.0	0.4	4.2	71	
DDHWF98-27	366805	6802158	1607	170.7	-45	14	72.7	76.1	3.4	3.3	0.3	2.2	8	
DDHWF98-27	366805	6802158	1607	170.7	-45	14	128.0	130.4	2.4	2.4	0.8	3.3	27	
DDHWF98-28	366805	6802158	1607	143.3	-86	14	96.3	104.7	8.4	6.3	0.5	2.4	10	
DDHWF98-29	367770	6801090	1632	43.6	-50	48								NSI
DDHWF98-30	366958	6801792	1495	274.3	-45	24	239.1	241.9	2.8	2.7	0.4	1.8	94	
DDHWF98-31	366958	6801792	1495	274.3	-64	24	243.8	246.4	2.6	2.4	0.9	4.0	163	
DDHWF98-32	366958	6801792	1495	313.6	-80	24	288.5	290.2	1.7	1.4	0.8	3.0	31	
DDHWF98-33	367985	6801133	1730	256.9	-50	50	51.8	55.4	3.6	3.0	0.4	1.7	2	
DDHWF98-33	367985	6801133	1730	256.9	-50	50	70.1	71.6	1.5	1.3	0.5	2.3	0	
DDHWF98-33	367985	6801133	1730	256.9	-50	50	92.4	95.0	2.6	2.2	0.2	1.8	3	
DDHWF98-33	367985	6801133	1730	256.9	-50	50	123.2	127.2	4.0	3.3	1.1	4.6	111	
DDHWF98-34	367946	6801118	1717	271.3	-80	50	70.4	73.2	2.8	2.2	0.4	2.8	0	
DDHWF98-35	367045	6801878	1537	210.3	-45	14	168.4	170.7	2.3	2.3	1.3	5.4	78	
DDHWF98-35	367045	6801878	1537	210.3	-45	14	191.2	192.2	1.0	1.0	1.1	2.7	11	
DDHWF98-36	366925	6802105	1568	173.7	-44	24	40.5	45.7	5.2	5.0	0.8	2.8	33	
DDHWF98-37	366925	6802105	1568	100.6	-90	0	63.8	65.1	1.3	0.9	0.2	2.1	11	
DDHWF98-37	366925	6802105	1568	100.6	-90	0	75.6	76.6	1.0	0.7	0.7	3.3	28	
DDHWF98-38	366852	6801828	1480	268.2	-50	22	225.8	230.6	4.8	4.6	0.1	7.4	18	
DDHWF98-39	366852	6801828	1480	326.1	-72	22	257.0	268.4	11.4	10.0	0.9	8.2	45	
DDHWF98-39	366852	6801828	1480	326.1	-72	22	275.2	279.3	4.1	3.6	1.2	2.0	27	
DDHWF98-40	366852	6801828	1480	362.7	-87	22	299.6	304.3	4.7	3.5	0.3	7.1	29	
DDHWF98-41	366650	6802139	1560	152.4	-61	24	91.6	95.1	3.5	3.3	0.3	2.9	14	
DDHWF98-42	367920	6801184	1724	176.8	-45	50								NSI
DDHWF98-43	367920	6801184	1724	164.6	-80	50	65.5	70.8	5.3	4.1	0.3	2.4	18	
DDHWF98-43	367920	6801184	1724	164.6	-80	50	97.0	99.3	2.3	1.8	0.4	2.6	22	
DDHWF98-44	368008	6801078	1732	219.5	-51	45	92.0	94.5	2.5	2.2	0.9	2.3	18	
DDHWF98-44	368008	6801078	1732	219.5	-51	45	104.9	106.9	2.0	1.7	0.7	2.8	27	
DDHWF98-45	368008	6801078	1732	219.6	-86	45	143.4	148.3	4.9	3.6	0.9	4.6	44	

NSI = No significant interval.

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Pelly Property – Significant Drill hole Intersections

Hole ID	Easting	Northing	Elevation	Total depth (m)	Dip	Azimuth	Depth from (m)	Depth to (m)	Interval (m)	Cu (%)	Pb (%)	Zn (%)	Ag (g/t)	Au (g/t)	Comment
W096-1	432131	6817677	1169	124.4	-60	212									NSI
W096-2	433628	6818258	1662	346.9	-70	235									NSI
WV95-06	433890	6817491.929	1300	233.5	-81.3	214	194.3	196.7	2.4	0.1	1.4	2.8	66	0.1	Stringer
WV95-07	434563	6816857.938	1300	465.7	-70	216.5									NSI
WV95-15	433819.5711	6817726.931	1300	207.9	-77.5	215									NSI
WV96-35	440000.6	6811258.1	1503	513.4	-60	33.4	505.2	509.1	4.2	0.8	3.9	15.6	558	2.0	Massive
WV96-37	433999.273	6817599.13	1670	380.7	-80	212									NSI
WV96-38	433887.172	6817792.626	1670	508.7	-80	212									NSI
WV96-41	434363.075	6817060.439	1711.7	539.5	-80	212									NSI
WV96-42	434166.37	6817489.229	1670	392.9	-80	212									NSI
WV96-45	434338.767	6817387.628	1680	405.1	-80	212									NSI
WV96-51	434499.565	6817269.328	1700	481.3	-80	212									NSI
WV96-55	435282.971	6816275.547	1680	546.8	-80	212									NSI
WV97-87	435546.5642	6816344.933	1626	617.8	-70	212									NSI
WV97-91	435222.5685	6816592.942	1659	610.79	-70	212									NSI
WV97-96	434868.5662	6816751.94	1715	572.39	-70	212									NSI
WV97-101	435834.5668	6816053.942	1611	602.86	-70	212									NSI
WV97-103	435531.2517	6816652.03	1575	549.86	-70	212									NSI
WV97-103A	435531.2517	6816652.03	1575	701.3	-70	212									NSI
WV04-130	435115	6816663	1715	514.6	-75	220									NSI
WV04-131	435096.6	6816684.9	1695	487.8	-74	200									NSI
WW00-01	439743	6811672	1513	463.3	-90	213.4	426.01	434.16	8.15	0.7	1.2	13.6	155	0.6	Massive
WW00-02	439743	6811672	1513	684.58	-65	33.4	668.87	669.81	0.94			0.8	28		NSI
WW00-03	439771	6811630	1515	516.94	-78	33.36	499.87	505.04	5.17	0.8	0.8	4.9	160	0.6	Massive

NSI = No significant interval.

APPENDIX F: TENEMENT SUMMARY

The following table provides a summary of the tenements which comprise the Kudz Ze Kayah Project held by BMC and its wholly owned subsidiary Finlayson Copper Ltd.

A full discussion of the Company's tenements and related matters is provided in the Solicitor's Report elsewhere in this prospectus.

All Claims are in the Watson Lake District, except the KE Property claims which are in the Mayo District.

Claims with consecutive Claim Numbers are grouped together to reduce the length of the table.

Claims with consecutive Claim Numbers have identical properties.

The total number of claims within each claim block (or Property) is provided at the end of each claim block series in bold font.

Abbreviations

BMC = BMC Minerals Ltd – 100%.

FLC = Finlayson Copper Ltd.

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Schedule A: Yukon Mineral Claim Searches – Watson Lake and Mayo Mining Districts

Watson Lake Claims

CLAIM NAME	CLAIM BLOCK	ACTIVE	LEASE / RENEWAL NUMBER	GRANT NUMBER	LAPSE DATE	REGISTERED OWNER
Watson Lake Mining District						
1st BASE 1 – 1st BASE 4	1st BASE	YES	N/A	YB51866 – YB51869	30/11/2032	BMC
1st BASE 13 – 1st BASE 20		YES	N/A	YB51878 – YB51885	30/11/2032	BMC
1st BASE 29 – 1st BASE 44		YES	N/A	YB51894 – YB51909	30/11/2032	BMC
Total Claims				**28**		
RB 1 – 12	RB	YES	N/A	YB93186 – YB93197	30/08/2032	BMC
RB 23 – 38		YES	N/A	YB93208 – YB93223	30/08/2032	BMC
RB 45 – 52		YES	N/A	YB93230 – YB93237	30/08/2032	BMC
Total Claims				**36**		
MER 1 – 66	MER	YES	N/A	YD00001 – YD00066	19/10/2030	BMC
MER 67 – 80		YES	N/A	YD00067 – YD00080	19/10/2029	BMC
MER 81 – 86		YES	N/A	YD00081 – YD00086	19/10/2030	BMC
MER 87 – 92		YES	N/A	YD00087 – YD00092	19/10/2031	BMC
MER 93 – 98		YES	N/A	YD00093 – YD00098	19/10/2030	BMC
MER 99 – 104		YES	N/A	YD00099 – YD00104	19/10/2029	BMC
MER 123 – 124		YES	N/A	YD00123 – YD00124	19/10/2030	BMC
MER 125 – 129		YES	N/A	YD00125 – YD00129	19/10/2031	BMC
MER 130 – 132		YES	N/A	YD00130 – YD00132	19/10/2030	BMC
MER 133		YES	N/A	YD00133	19/10/2029	BMC
MER 134 – 150		YES	N/A	YD00134 – YD00150	19/10/2030	BMC
MER 151 – 158		YES	N/A	YD00151 – YD00158	19/10/2031	BMC
MER 159 – 162		YES	N/A	YD00159 – YD00162	19/10/2030	BMC
MER 163 – 170		YES	N/A	YD00163 – YD00170	19/10/2029	BMC
MER 189 – 190		YES	N/A	YD00189 – YD00190	19/10/2030	BMC
MER 191 – 196		YES	N/A	YD00191 – YD00196	19/10/2031	BMC
MER 197 – 198		YES	N/A	YD00197 – YD00198	19/10/2030	BMC
MER 199 – 208		YES	N/A	YD00199 – YD00208	19/10/2029	BMC
MER 209 – 236		YES	N/A	YD00209 – YD00236	19/10/2030	BMC
MER 251 – 276		YES	N/A	YD00251 – YD00276	19/10/2029	BMC
MER 277 – 282		YES	N/A	YD00277 – YD00282	11/02/2030	BMC
Total Claims				**232**		
BOOT 1 – 7	Pelly	YES	N/A	YB47794 – YB47800	2/04/2035	BMC
BOOT 8 – 18		YES	N/A	YB48402 – YB48412	2/04/2035	BMC
BOOT 19 – 22		YES	N/A	YB84457– YB84460	2/04/2035	BMC
Total Claims				**22**		
GO 1 – 28	Pelly	YES	N/A	YB47402 – YB47429	2/04/2035	BMC
GO 29 – 62		YES	N/A	YB47760 – YB47793	2/04/2035	BMC
GO 77 – 81		YES	N/A	YB55781– YB55783	2/04/2035	BMC
GO 82 – 106		YES	N/A	YB52227 – YB52251	2/04/2035	BMC
GO 108 – 109		YES	N/A	YB55779 – YB55780	2/04/2035	BMC
GO 110 – 124		YES	N/A	YB52252 – YB52266	2/04/2035	BMC
GO 125 – 127		YES	N/A	YB89634 – YB89636	2/04/2035	BMC
Total Claims				**110**		
JACK 1 – 18	Pelly	YES	N/A	YB84461 – YB84478	2/04/2035	BMC
JACK 19		YES	N/A	YB85305	2/04/2035	BMC
JACK 20 – 26		YES	N/A	YB85328 – YB85334	2/04/2035	BMC
JACK 28		YES	N/A	YB85336	2/04/2035	BMC
JACK 30		YES	N/A	YB87487	2/04/2035	BMC
JACK 31 – 33		YES	N/A	YB88805 – YB88807	2/04/2035	BMC
Total Claims				**31**		
LOW 1 – 14	Pelly	YES	N/A	YB85382 – YB85395	2/04/2034	BMC
Total Claims				**14**		
WOL 1 – 28	Pelly	YES	N/A	YB47712 – YB47739	2/04/2035	BMC
WOL 29 – 40		YES	N/A	YB47434 – YB47445	2/04/2035	BMC
WOL 41 – 156		YES	N/A	YB48801 – YB48916	2/04/2035	BMC
WOL 164 – 180		YES	N/A	YB55784 – YB55800	2/04/2035	BMC
WOL 181 – 239		YES	N/A	YB55378 – YB55436	2/04/2035	BMC
WOL 240 – 244		YES	N/A	YB70142 – YB70146	2/04/2035	BMC
WOL 246		YES	N/A	YB70148	2/04/2035	BMC
WOL 249		YES	N/A	YB70151	2/04/2035	BMC
Total Claims				**239**		
TAG 1388	Pelly	YES	N/A	YB55308	2/04/2035	BMC
TAG 1412 – TAG 1415		YES	N/A	YB55862 – YB55865	2/04/2035	BMC
TAG 1430		YES	N/A	YB55880	2/04/2035	BMC
Total Claims				**6**		

CLAIM NAME	CLAIM BLOCK	ACTIVE	LEASE / RENEWAL NUMBER	GRANT NUMBER	LAPSE DATE	REGISTERED OWNER
Total Pelly Claims				**422**		
GOAL 204	KONA	YES	N/A	YB70474	17/03/2043	BMC
GOAL 213 – 230	(TSA DA GLISZA)	YES	N/A	YB76789 – YB76806	17/03/2043	BMC
GOAL 233 – 250		YES	N/A	YB76809 – YB76826	17/03/2043	BMC
GOAL 252 – 270		YES	N/A	YB76828 – YB76846	17/03/2043	BMC
GOAL 283 – 303		YES	N/A	YB77164 – YB77184	17/03/2043	BMC
GOAL 304 – 319		YES	N/A	YB76860 – YB76875	17/03/2043	BMC
Total Claims				**93**		
MEG 101 – 122	KONA (TSA DA GLISZA)	YES	N/A	YB93485 – YB93506	12/03/2032	BMC
Total Claims				**22**		
YIR 2 – 7	KONA (TSA DA GLISZA)	YES	N/A	YB93280 – YB93285	18/07/2031	BMC
Total Claims				**6**		
Total Kona Claims				**121**		
TAG 1 – 30	KZK	YES	N/A	YB46227 –YB46256	2/04/2044	BMC
TAG 31 – 113		YES	N/A	YB47461 – YB47543	2/04/2042	BMC
TAG 114 – 157		YES	N/A	YB47668 – YB47711	2/04/2042	BMC
TAG 158 – 202		YES	N/A	YB47544 – YB47588	2/04/2042	BMC
TAG 204		YES	N/A	YB47590	2/04/2042	BMC
TAG 206 – 263		YES	N/A	YB47592 – YB47649	2/04/2042	BMC
TAG 264 – 265		YES	N/A	YB48413 – YB48414	2/04/2042	BMC
TAG 266 – 269		YES	N/A	YB48415 – YB48418	2/04/2044	BMC
TAG 270 – 303		YES	N/A	YB48419 – YB48452	2/04/2042	BMC
TAG 306 – 312		YES	N/A	YB48455 – YB48461	2/04/2042	BMC
TAG 315 – 319		YES	N/A	YB48464 – YB48468	2/04/2042	BMC
TAG 328 – 337		YES	N/A	YB48477 – YB48486	2/04/2042	BMC
TAG 358 – 377		YES	N/A	YB48507 – YB48526	2/04/2042	BMC
TAG 383		YES	N/A	YB48532	2/04/2042	BMC
TAG 385 – 387		YES	N/A	YB48534– YB48536	2/04/2042	BMC
TAG 398 – 461		YES	N/A	YB48940 – YB49003	2/04/2042	BMC
TAG 489 – 516		YES	N/A	YB49565 – YB49592	2/04/2042	BMC
TAG 559 – 562		YES	N/A	YB50436 – YB50439	2/04/2042	BMC
TAG 633 – 642		YES	N/A	YB50510 – YB50519	2/04/2042	BMC
TAG 644		YES	N/A	YB50521	2/04/2042	BMC
TAG 712 – 719		YES	N/A	YB50589 – YB50596	2/04/2042	BMC
TAG 723		YES	N/A	YB50600	2/04/2042	BMC
TAG 725		YES	N/A	YB50602	2/04/2042	BMC
TAG 727		YES	N/A	YB50604	2/04/2042	BMC
TAG 729 – 732		YES	N/A	YB50606 – YB50609	2/04/2042	BMC
TAG 734		YES	N/A	YB50611	2/04/2042	BMC
TAG 736		YES	N/A	YB50613	2/04/2042	BMC
TAG 738		YES	N/A	YB50615	2/04/2042	BMC
TAG 740		YES	N/A	YB50617	2/04/2042	BMC
TAG 746		YES	N/A	YB50623	2/04/2038	BMC
TAG 748		YES	N/A	YB50625	2/04/2038	BMC
TAG 750		YES	N/A	YB50627	2/04/2038	BMC
TAG 752		YES	N/A	YB50629	2/04/2038	BMC
TAG 754		YES	N/A	YB50631	2/04/2038	BMC
TAG 756		YES	N/A	YB50633	2/04/2038	BMC
TAG 758		YES	N/A	YB50635	2/04/2038	BMC
TAG 760		YES	N/A	YB50637	2/04/2038	BMC
TAG 762		YES	N/A	YB50639	2/04/2038	BMC
TAG 764		YES	N/A	YB50641	2/04/2038	BMC
TAG 766		YES	N/A	YB50643	2/04/2038	BMC
TAG 787 – 790		YES	N/A	YB50664 – YB50667	2/04/2042	BMC
TAG 793 – 794		YES	N/A	YB50670 – YB50671	2/04/2042	BMC
TAG 815		YES	N/A	YB50692	2/04/2042	BMC
TAG 839		YES	N/A	YB50716	2/04/2038	BMC
TAG 841		YES	N/A	YB50718	2/04/2038	BMC
TAG 843		YES	N/A	YB50720	2/04/2038	BMC
TAG 845 – 846		YES	N/A	YB50722 – YB50723	2/04/2038	BMC
TAG 848		YES	N/A	YB50725	2/04/2038	BMC
TAG 857 – 860		YES	N/A	YB50734 – YB50737	2/04/2042	BMC
TAG 863 – 864		YES	N/A	YB50740 – YB50741	2/04/2042	BMC
TAG 921		YES	N/A	YB50798	2/04/2038	BMC

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CLAIM NAME	CLAIM BLOCK	ACTIVE	LEASE / RENEWAL NUMBER	GRANT NUMBER	LAPSE DATE	REGISTERED OWNER
TAG 923 – 925		YES	N/A	YB50800 – YB50802	2/04/2038	BMC
TAG 928 – 931		YES	N/A	YB50805 – YB50808	2/04/2042	BMC
TAG 1057 – 1095		YES	N/A	YB51214 – YB51252	2/04/2042	BMC
TAG 1096, 1098, 1100, 1102		YES	N/A	YB51253, YB1255, YB1257, YB1259	2/04/2044	BMC
TAG 1097, 1099, 1101, 1103-1104		Yes	N/A	YB51254, YB1256, YB1258, YB1260 – YB51261	2/04/2042	BMC
TAG 1105-1112		YES	N/A	YB1262 – YB51269	2/04/2044	BMC
TAG 1113-1114		YES	N/A	YB1270 – YB51271	2/04/2042	BMC
TAG 1449 – 1468		YES	N/A	YB55325 –YB55344	2/04/2042	BMC
TAG 1469 – 1501		YES	N/A	YB55899 – YB55931	2/04/2042	BMC
TAG 1505		YES	N/A	YB55346	2/04/2042	BMC
TAG 1507		YES	N/A	YB55348	2/04/2042	BMC
TAG 1509		YES	N/A	YB55350	2/04/2042	BMC
TAG 1536 – 1537		YES	N/A	YB55934 – YB55935	2/04/2042	BMC
TAG 1538		YES	N/A	YB55377	2/04/2042	BMC
TAG 1539 – 1541		YES	N/A	YB55936 – YB55938	2/04/2042	BMC
TAG 1544 – 1553		YES	N/A	YB56713 – YB56722	2/04/2042	BMC
TAG 1560 – 1569		YES	N/A	YB56729 – YB56738	2/04/2042	BMC
Total Claims				**651**		
ON 21 – 101	KZK	YES	N/A	YB62677–YB62757	2/04/2042	BMC
ON 104 – 113		YES	N/A	YB62760–YB62769	2/04/2042	BMC
ON 116 – 125		YES	N/A	YB62772–YB62781	2/04/2042	BMC
ON 162 – 174		YES	N/A	YB62816– YB62828	2/04/2042	BMC
ON 176		YES	N/A	YB62830	2/04/2042	BMC
ON 178		YES	N/A	YB62832	2/04/2042	BMC
ON 180		YES	N/A	YB62834	2/04/2042	BMC
ON 197 – 203		YES	N/A	YB62851– YB62857	2/04/2042	BMC
ON 205		YES	N/A	YB62859	2/04/2042	BMC
Total Claims				**125**		
PLATE 1 – 25	KZK	YES	N/A	YB46325 – YB46328	2/04/2044	BMC
Total Claims				**25**		
EL 1 – 8	KZK	YES	N/A	YB48917 – YB48924	2/04/2034	BMC
Total Claims				**8**		
HOME 1 – 17	KZK	YES	N/A	YB46350 – YB46355	2/04/2044	BMC
Total Claims				**17**		
KZK 1 – 29	KZK	YES	N/A	YB85276 – YB85279	2/04/2042	BMC
Total Claims				**29**		
LIMY 1 – 9	KZK	YES	N/A	YB49654 – YB49662	2/04/2038	BMC
Total Claims				**9**		
LY 1 – 15	KZK	YES	N/A	YB48925 – YB48939	2/04/2042	BMC
Total Claims				**15**		
Total KZK Claims				**879**		
WOLF 1 – 18	WOLF	YES	N/A	YB16894 – YB16911	30/03/2034	BMC
Total Claims				**18**		
Rivier 1-18	Rivier	YES	N/A	YD58798 - YD58815	20/01/2031	BMC
Rivier 23 - 40		YES	N/A	YD58820 - YD58837	20/01/2031	BMC
Rivier 45 - 62		YES	N/A	YD58842 - YD58859	20/01/2031	BMC
Rivier 67 - 112		YES	N/A	YD58864 - YD58909	20/01/2031	BMC
Rivier 19 - 22		YES	N/A	YD61450 – YD61453	20/01/2031	BMC
Rivier 41 - 44		YES	N/A	YD61454 – YD61457	20/01/2031	BMC
Rivier 63 - 66		YES	N/A	YD61458 – YD61461	20/01/2031	BMC
Rivier 113 - 116		YES	N/A	YD61462 – YD61465	20/01/2031	BMC
Total Claims				**116**		
Total Claims				**1852**		

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Schedule B: Yukon Mineral Claim Searches – Watson Lake Mining District

CLAIM NAME	CLAIM BLOCK	ACTIVE	LEASE / RENEWAL NUMBER	GRANT NUMBER	LAPSE DATE	REGISTERED OWNER
KONA 43 – 46	KONA	YES	N/A	YA56602 – YA56605	9/09/2035	FLC
Total Claims			**4**			
FIRE 2	KONA	YES	N/A	YB33749	31/12/2036	FLC
FIRE 4		YES	N/A	YB33751	31/12/2036	FLC
FIRE 6		YES	N/A	YB33753	31/12/2036	FLC
FIRE 12		YES	N/A	YB33759	31/12/2036	FLC
FIRE 14		YES	N/A	YB33761	31/12/2036	FLC
FIRE 19 – 21		YES	N/A	YB33766 – YB33768	31/12/2036	FLC
FIRE 23		YES	N/A	YB33770	31/12/2036	FLC
FIRE 26		YES	N/A	YB33773	31/12/2036	FLC
FIRE 28 – 29		YES	N/A	YB33775 – YB33776	31/12/2036	FLC
FIRE 31		YES	N/A	YB33778	31/12/2036	FLC
FIRE 48 – 60		YES	N/A	YB33795 – YB33807	31/12/2036	FLC
FIRE 73 – 77		YES	N/A	YB33820 – YB33824	31/12/2036	FLC
FIRE 79		YES	N/A	YB33826	31/12/2036	FLC
FIRE 81		YES	N/A	YB33828	31/12/2036	FLC
FIRE 131 – 133		YES	N/A	YB33878 – YB33880	31/12/2036	FLC
FIRE 185		YES	N/A	YC31894	25/08/2036	FLC
FIRE 193		YES	N/A	YC31895	25/08/2036	FLC
FIRE 195		YES	N/A	YB86834	14/08/2036	FLC
FIRE 301 – 306		YES	N/A	YB94275 – YB94280	12/11/2036	FLC
FIRE 307 – 311		YES	N/A	YC22651 – YC22655	9/12/2036	FLC
FIRE 312 – 328		YES	N/A	YB94281 – YB94297	12/11/2036	FLC
Total Claims			**67**			
EMBER 62 – 98	KONA	YES	N/A	YB88869 – YB88905	3/12/2036	FLC
EMBER 99		YES	N/A	YB88906	3/12/2029	FLC
Total Claims			**38**			
STRAW 1 –37	KONA	YES	N/A	YB93671 – YB93707	8/01/2037	FLC
STRAW 38 – 40		YES	N/A	YB93708 – YB93710	8/01/2035	FLC
STRAW 38 – 41		YES	N/A	YB93711 – YB93713	8/01/2037	FLC
Total Claims			**43**			
SPARK 1 – 9	KONA	YES	N/A	YC91767 – YC91775	14/12/2036	FLC
Total Claims			**9**			
Total Claims in Claim Block			**161**			

Mayo Claims

CLAIMNAME	CLAIMBLOCK	ACTIVE	LEASE / RENEWAL NUMBER	GRANT NUMBER	LAPSE DATE	REGISTERED OWNER
KE 1 – 40	KE	YES	N/A	YD121663 – YD121702	03/02/29	BMC
KE 41 – 56	KE	YES	N/A	YD122177 – YD122192	03/02/29	BMC
KE 57 – 88	KE	YES	N/A	YE36956 – YE36987	22/07/29	BMC
Total Claims				88		

APPENDIX G: Potential Permits, Licences and Other Authorisations Required for the ABM Mine

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Agency	Authorisation and Legislation	Activity Authorised	Submission Date
Dept. of Energy Mines and Resources Mineral Resources Branch	Quartz Mining Licence *Quartz Mining Act*	All activities undertaken on quartz claims in support of mine development, construction, operation, and closure.	August 2022
Yukon Water Board	Type A Water Licence *Waters Act – Waters Regulation*	Use of water and deposit of waste related to quartz mining undertakings.	November 2020
	Type B Water Licence *Waters Act – Waters Regulation*	Use of water and deposit of waste related to municipal undertakings, including potable water supply and municipal wastewater treatment and disposal.	August 2022
Dept. of Energy Mines and Resources Land Management Branch	Lease *Territorial Lands Act – Land Use Regulation*	Long-term use of land with exclusive use for borrow quarry areas along the access road.	September 2020
	Lease *Territorial Lands Act – Land Use Regulation*	Long-term use of land with exclusive use for the portion of the Class C Storage Facility that is not located on quartz claims.	September 2020
	Lease *Territorial Lands Act – Land Use Regulation*	Long-term use of land with exclusive use for the access road.	September 2020
	Resource Road Permit *Territorial Lands Act – Resource Regulation*	Access to the existing tote road.	not yet submitted
Dept. of Energy Mines and Resources Geothermal and Petroleum Resources Branch	Liquefied Natural Gas Facility Licence *Oil and Gas Act – Gas Processing Plant Regulation, Oil and Gas Licence Administration Regulations*	LNG facility construction and operation.	September 2025
Dept. of Environment Environmental Protection and Assessment Branch	Consolidated Solid Waste Management Permit *Environment Act – Air Emissions Regulations, Solid Waste Regulations, Special Waste Regulations*	Operation of a solid waste incinerator; disposal of solid waste; handling, disposal, generation or storage of special (hazardous) wastes; transportation of dangerous goods / waste; and operation of a land treatment facility.	April 2025
	Air Emissions Permit *Environment Act – Air Emissions Regulations*	Obtaining gravel/sand from a quarry; and operation of equipment capable of generating, burning or using heat energy.	April 2025

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Agency	Authorisation and Legislation	Activity Authorised	Submission Date
Dept. of Highways and Public Works Transportation Engineering Branch	Performance of Work within Highway Right-of-Way Permit *Highways Act – Highways Regulations*	Performing work within Robert Campbell Highway right-of-way.	not yet submitted
	Sign Permit *Highways Act – Highways Regulations*	Erecting signs within Robert Campbell Highway right-of-way.	not yet submitted
	Quarry Permit for Designated Public Pit *Territorial Lands Act – Quarry Regulations*	Use of existing quarry at Km230.7 of the Robert Campbell Highway.	February 2025
Dept. of Highways and Public Works Transport Services Branch	Freight Vehicle Permit *Highways Act – Highways Regulations*	Overweight and/or over-dimensional freight, including dangerous goods and non-dangerous goods.	As needed
	Bulk Commodity Haul Agreement *Highways Act – Bulk Commodity Haul Regulations*	Bulk commodity haulage.	not yet submitted
Dept. of Community Services Building Safety and Standards Branch	Building Permit *Building Standards Act*	Construction of buildings; installation of fuel appliances and storage tanks.	not yet submitted
	Plumbing Permit *Building Standards Act*	Plumbing.	not yet submitted
	Electrical Permit *Electrical Protection Act – Canadian Electrical Code*	Electrical work.	not yet submitted
	Gas Installation Permit *Gas Burning Devices Act*	Gas installation or modification; use of propane gas.	not yet submitted
Dept. of Community Services Fire Marshall's Office	Storage Tank Systems Permit *Environment Act – Storage Tank Regulations*	Storage and handling of petroleum products.	not yet submitted
Dept. of Community Services Wildland Fire Management Branch	Burning Permit *Forest Protection Act – Forest Protection Regulations*	Burning of refuse wood and brush.	As needed
	Permit to Operate a Large Public Drinking Water System *Public Health and Safety Act – Drinking Water Regulation*	Construction, installation, modification and operation of drinking water systems, including the water source and associated infrastructure.	not yet submitted

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Agency	Authorisation and Legislation	Activity Authorised	Submission Date
Dept. of Health and Social Services Environmental Health Services	Permit to Operate a Food Premises *Public Health and Safety Act – Regulations Governing the Sanitation of Eating or Drinking Places*	Providing food services.	not yet submitted
Dept. of Tourism and Culture Cultural Services Branch	Class 2 Archaeology Permit *Historic Resources Act – Archaeological Site Regulations*	Survey, documentation, excavation, or alteration of heritage sites and the collection of artifacts, if encountered.	As needed
Worker's Compensation Health and Safety Board Occupational Health and Safety and/or Natural Resources Canada Minerals and Metals Sector	ANFO Permit *Explosives Act – Occupational Health and Safety Regulations*	Manufacture of ANFO, if required.	not yet submitted
	Factory Permit *Explosives Act – Occupational Health and Safety Regulations*	Manufacture of explosives other than ANFO, if required.	not yet submitted
	Explosives Magazine Permit *Explosives Act – Occupational Health and Safety Regulations* *Workers Safety and Compensation Act - Workplace Health and Safety Regulations*	Explosives storage, if required.	not yet submitted
	Underground and Surface Authorisation to Conduct Blasting in Yukon *Workers Safety and Compensation Act - Workplace Health and Safety Regulations*	Underground or surface blasting.	not yet submitted
	Temporary Blasters Permit *Workers Safety and Compensation Act - Workplace Health and Safety Regulations*	Temporary blasting (maximum of 90 days).	As needed
Worker's Compensation Health and Safety Board Occupational Health and Safety	Notice of construction project *Workers Safety and Compensation Act - Workplace Health and Safety Regulations*	Commencement of construction.	not yet submitted
	Notice of mining project *Workers Safety and Compensation Act - Workplace Health and Safety Regulations*	Commencement of mining.	not yet submitted
Dept. of Environment	Wildlife Research Permit *Wildlife Act*	Wildlife research.	As needed

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Agency	Authorisation and Legislation	Activity Authorised	Submission Date
Conservation Officer Services			
Dept. of Environment Fish and Wildlife Branch	Fisheries Permit *Fisheries Act*	Fish research and surveys.	As needed
Fisheries and Oceans Canada	Fisheries Act Authorisation *Fisheries Act*	Affecting fish and fish habitat.	November 2024

Notes:

- 1. Based on discussion with the Dept. of Energy Mines and Resources – Forest Management Branch, no authorisations are needed under the Forest Resources Act or associated regulations for the proposed Kudz Ze Kayah Project activities.
- 2. Based on discussion with the Dept. of Highways and Public Works – Aviation Branch, no authorisations are needed under the Public Airports Act or associated regulations for the proposed Kudz Ze Kayah Project activities.

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ERM is one of the world's leading environmental, health, safety, and social consulting services providers.

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We have a high-level of technical expertise across mineral commodities gained from 35 years of experience within the global exploration and mining industry. Our team possess experience in all stages of the mining cycle, from project generation to production and the challenge of finding, developing, and mining orebodies.

ERM has multiple points of entry throughout the mining lifecycle, and our global network of expertise, together with ERM, enables us to provide innovative solutions to improve operational performance and support efficient mine operations.

Our team has specific experience working in the mining sector with junior, mid–tier, and major exploration, and mining companies, as well as advising pension funds, private equity firms, and international development finance institutions on investment risks and opportunities.

We offer an integrated and comprehensive set of services covering the entire mineral asset lifecycle. Our services include corporate advisory, operational support, mining, and feasibility studies, resource estimation, geometallurgical modelling, exploration, data and water management, and technology expertise.

Our highly experienced teams provide insight and innovative solutions to produce optimal outcomes for our clients. Our team can take your project from a concept through discovery and resource definition to a profitable and sustainable operating mine, with a robust closure plan and positive stakeholder engagement.

ERM's capabilities align seamlessly with this mission and vision, from the new country entry risk assessment, global operational strategy, geoscience, and advanced technological solutions, data capture, and management, hydrogeology, nature, and beyond, through all stages of exploration, acquisition, mine planning, and development, operations, and closure. ERM plays a pivotal role in addressing the strategic, operational, and tactical challenges encountered by major, mid–tier, and junior mining companies worldwide.

Our specialists are supported by a huge team of scientists, engineers, social, environmental, health, safety, and sustainability consultants from our parent company ERM. ERM's Technical Mining Services Team offers substantial depth of expertise and breadth of service to the mining community.

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Snapshot of Our Services

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- Mineral systems targeting & project generation
- Remote sensing, geophysics, & geochemistry
- Mapping & drill programme planning & supervision
- Exploration strategy & project management
- Project review & due diligence
- Geometallurgical optimisation & orebody characterisation

Resource Estimation & Mine Geology

- Mineral Resource estimation, validation, classification, & reporting
- Resource audits & risk analysis
- Geological & geometallurgical modelling
- Geostatistical analysis & variography
- Grade control & reconciliation
- Drill hole spacing analysis
- *In situ* recovery/*in situ* leaching
    - Resources & reserves
    - Suitability & optimisation
    - operations

Data & Mapping

- Data management (capture, data validation, & quality assurance/quality control)
- Geological Database administration
- Data visualisation, analytics, & cartography
- Geographic Information systems (GIS), plans, sections, & 3D plots
- Machine learning

Mining Engineering

- Mining & engineering studies (concept to feasibility)
- Mine optimisation, scheduling, design, & Ore Reserve estimation
- Productivity improvement & project management

Hydrogeology & Hydrology

- Water management & groundwater supply
- Project approvals
- Dewatering & depressurisation
- Ground/Surface water modelling
- Formulating water stewardship strategies & advanced technical solutions.

Mining Transactions & Corporate Advice

- Project reviews & independent reports
- Due diligence & mineral asset valuations
- Geo–corporate advice
- Conducting independent evaluations to guide decisions on mergers, acquisitions, due diligence, & compliance assessments
- Advice on reporting to public codes such as the JORC, VALMIN, SAMREC, NI 43–101, CIM codes, S–K 1300
- Expert witness

Environmental, Social, & Governance

- Efficiently bringing new mines to fruition in adherence to ESG best practices
- Advancing strategic & practical decarbonisation throughout the value chain, from mining equipment to processing & transportation
- Expert knowledge of ‘licence to operate’ issues, their prevention, & solutions.

Planning & Approvals

- Environmental risk identification, management, & compliance
- Climate change, biodiversity, natural resources
- Indigenous & historical heritage management
- Social strategy & policy development
- Community consultation programmes
- Environmental & social impact assessments (ESIAs)
- Operational management & compliance.

Health & Safety

- Enhancing health & safety strategies & practical incident prevention through managing operational risks & controls, certifications, & compliance with safety regulations, policies, standards, & procedures
- Risk assessment & management systems
- Risk management & incident investigation
- Hazard identification, inspections, risk assessments & prevention control
- Occupational health & safety systems & compliance auditing

Rehabilitation & Mine Closure

- Planning for repurposing or transitioning sites
- Rehabilitation appraisals, planning, & progress monitoring, closure plans
- Community development & economic transition
- Earthworks, cover, landform designs, & modelling, erosion & sediment management
- Waste characterisation & final void assessment
- Water management & reduction strategies
- Land use capability assessment
- Estimated rehabilitation costs
- Site closure costs/financial provisioning

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